SUMMARY OF EPA-MANDATED PERFORMANCE ASSESSMENT VERIFICATION TEST (REPLICATE 1) AND COMPARISON WITH THE COMPLIANCE CERTIFICATION APPLICATION CALCULATIONS

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1.0 INTRODUCTION

This report summarizes the results obtained from replicate 1 of the U.S. Environmental Protection Agency (EPA) Mandated Performance Assessment Verification Test of the U.S. Department of Energy's Performance Assessment (PA) Analyses supporting the Waste Isolation Pilot Plant (WIPP) Compliance Certification Application (CCA). Results from replicates 2 and 3 will be presented in a subsequent document. The EPA-Mandated Performance Assessment Verification Test (replicate 1) will be referred to as the PAVT in the remainder of this report.

The report is divided into seven sections: An Introduction and Summary of the Differences Between the PAVT and CCA (Section 1); Salado Flow Calculations (Section 2); Salado Transport Calculations (Section 3); Culebra Flow and Transport Calculations (Section 4); Cuttings, Cavings, and Spallings Calculations (Section 5); Direct Brine Release Calculations (Section 6); and Complimentary Cumulative Distribution Function (CCDF) Calculations (Section 7). In each section, the following information is provided:

- A description of changes in PA input parameters requested by EPA.
- A description of changes in model implementation and computer codes.
- Results of the PAVT calculations and their comparison with the CCA results.

Because of the importance of understanding the results of the Salado Flow calculations, a detailed analysis of gas and brine migration modeling results is presented in Appendices A and B. Additional information supporting the other calculations is also provided in Appendices C (Salado Transport), D (Culebra Transport), E (Cuttings, Cavings, and Spallings), and F (Direct Brine Release). In the final section, CCDFs representing futures of the repository and calculation of cumulative releases for the PAVT are presented and compared to the CCA CCDFs. Supporting information is provided in Appendix G. A listing of code versions and associated Software Problem Report (SPR) numbers is included in Appendix H. Detailed discussions of CCA results may be found in the Analysis Packages listed in the References (Section 8).

It is important to note that a different set of seed numbers, which determine the random LHS combinations of uncertain input parameters for BRAGFLO and other codes, was used in the PAVT than in the CCA. Therefore, specific vectors from PAVT replicate 1 do not map directly to vectors from CCA replicate 1.

1.1 Summary of Differences Between the PAVT and CCA

In both the PAVT and the CCA, total releases to the accessible environment were dominated by cuttings and spallings releases, with a smaller contribution from direct brine release. Culebra, Salado interbed, and Dewey Lake releases across the LWB were negligible. The PAVT mean CCDF for total normalized releases to the accessible environment does not exceed or come within

an order of magnitude of the EPA Limit. The following discussion summarizes the major differences in the PAVT results relative to the CCA. Factors affecting indirect releases through the Salado and Culebra are discussed first, followed by a discussion of direct releases (cuttings, spallings, and direct brine release) and CCDFs. Factors responsible for differences include parameter changes and model implementation changes. Impact analyses (see Appendix H for a table of associated Software Problem Reports (SPRs)) performed on CCA results suggest that computational model (code) changes had an insignificant impact on results.

Salado Flow

Undisturbed Scenario

In terms of repository pressures, brine saturations, and gas generation, undisturbed repository performance was not significantly impacted by changes in parameters. However, one vector (#38) produced increased flow (3326 m³) across the land withdrawal boundary (LWB). This flow was caused by a combination of factors: the highest interbed permeability, the 8th highest DRZ permeability, low far-field pressure, and a high repository pressure at 1000 years. The maximum flow across the LWB in the CCA was 216 m³.

Disturbed Scenarios S2 and S3 (E1 intrusion at 350 and 1000 years)

Parameter changes that had the most impact on repository performance in the E1 intrusion scenarios were the brine reservoir volume (approximately two orders of magnitude larger), borehole permeability (lower minimum permeabilities), and corrosion rates (higher). These changes resulted in higher repository pressures and larger upward borehole brine flows to the Culebra, with the maximum flow about two times larger than the maximum amount predicted in the CCA (102,340 m³ versus 67,000 m³). As in the undisturbed scenario, one vector (#38) produced increased flow (2630 m³) across the LWB. In the CCA, flows across the LWB in all disturbed scenarios were negligible.

Disturbed Scenarios S4 and S5 (E2 intrusion at 350 and 1000 years)

Parameter changes that had the most impact on repository performance in the E2 intrusion scenarios were corrosion rates (higher), borehole permeabilities (lower minimum permeabilities), and DRZ permeability (sampled over a range of higher and lower permeabilities). These changes resulted in higher repository pressures and smaller upward borehole brine flows to the Culebra, with the maximum flow about ten times smaller than the maximum amount predicted in the CCA (4,474 m³ versus 40,000 m³). As in E1 intrusion scenario, cumulative brine flow across the LWB was significant in vector #38 (2735 m³) only.

Disturbed Scenario S6 (E2 intrusion at 1000 years and an E1 intrusion at 2000 years) Parameter changes that had the most impact on repository performance in the E2E1 intrusion scenarios were the brine reservoir volume (approximately two orders of magnitude larger), borehole permeability (lower minimum permeabilities), and corrosion rates (higher). As in scenarios S2 and S3, these changes resulted in higher repository pressures and larger upward borehole brine flows to the Culebra, with the maximum flow about two times larger than the

maximum amount predicted in the CCA (108,960 m³ versus 62,000 m³). Again, cumulative brine flow across the LWB was significant in vector #38 (3203 m³) only.

Salado Transport

Parameter changes that had the most impact on radionuclide releases to the Culebra via the borehole were the changes in actinide solubilities. In particular, these changes substantially reduced the solubilities of 241 Am in the Salado and Castile brines and reduced the solubility of ²³⁹Pu in the Salado brine. The solubility of ²³⁹Pu in the Castile brine was similar to the CCA. ²⁴¹Am was the dominant radionuclide for transport at early time (<2000 years after closure) while ²³⁹Pu was the dominant radionuclide at later times. Castile solubilities were used for E1 intrusion scenarios (S2, S3, S6) and Salado solubilities were used for the other scenarios. For the E1 scenarios with early time intrusions, larger upward borehole flows (relative to the CCA), were offset by the reduced ²⁴¹Am solubility. As a consequence, radionuclide releases to the Culebra from early time E1 intrusions were only slightly larger, on average, than those in the CCA. For later E1 intrusion times, PAVT releases tended to be moderately larger than those in the CCA. The larger flows were not offset as much at later times because the ²³⁹Pu solubilities were similar to the CCA. For E2 intrusions at all times, radionuclide releases to the Culebra tended to be less than in the CCA due to both lower upward borehole flows and reduced solubilities. There were no radionuclide releases upward in the borehole beyond the top of the Rustler in any scenario. Integrated releases across the LWB via the interbeds were very small (< 5.0E-10 EPA units) even for vector #38. These releases were likely artificial and due to numerical dispersion.

Culebra Transport

The most significant factors impacting Culebra transport were the matrix distribution coefficients (k_d) . The k_d s were represented by loguniform probability distributions rather than the uniform probability distributions used in the CCA. As a result, sampled k_d values tended to be lower in the PAVT and several more realizations discharged ²³⁴U across the LWB in the PAVT than in the CCA. However, as in the CCA, these discharges were very small and were not significant contributors to total mean CCDF.

Cuttings, Cavings, and Spallings

The most significant factors that impacted total cuttings, cavings, and spallings volume releases were the waste shear strength and the parameters influencing repository pressure (corrosion rate, brine reservoir volume, and borehole permeability). The change in the waste shear strength distribution produced more cuttings and cavings volume releases in the PAVT. Repository pressures in the PAVT disturbed scenarios tended to be higher than in the CCA (more vectors had pressures above 8 MPa). As a result, more vectors produced spallings volume releases.

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Direct Brine Release

The most significant factors impacting direct brine release volumes were the parameters influencing repository pressure (corrosion rate, brine reservoir volume, waste permeability, and borehole permeability). In the disturbed scenarios, repository pressures and direct brine volume releases tended to be higher in the PAVT as compared to the CCA, with nearly as many replicate one realizations releasing brine as in all three replicates of the CCA combined. However, due to reduced actinide solubilities (as described previously in the Salado Transport summary), direct brine radionuclide releases in the PAVT were only slightly larger than in the CCA.

CCDFs

The PAVT mean CCDF for total normalized releases is a factor of 2 to 3 larger than the CCA mean CCDF for all probabilities of exceedance. This increase is primarily due to the increase in cuttings releases. Total releases to the accessible environment were dominated by cuttings and spallings releases, with a smaller contribution from direct brine release. Culebra, Salado interbed, and Dewey Lake releases across the LWB were negligible. The PAVT mean CCDF for total normalized releases to the accessible environment does not exceed or come within an order of magnitude of the EPA Limit.

2.0 SALADO FLOW CALCULATIONS

This section summarizes differences between the PAVT and CCA Salado two-phase flow calculations. These calculations were performed using BRAGFLO. Six different repository scenarios were considered:

- S1. Undisturbed
- S2. E1 Intrusion at 350 Years
- S3. E1 Intrusion at 1000 Years
- S4. E2 Intrusion at 350 Years
- S5. E2 Intrusion at 1000 Years
- S6. E2E1 Intrusion

This summary focuses on values of key BRAGFLO performance measures for each scenario. Key performance measures for the S1 scenario include pressure and brine saturation in the panel at times of 350 and 1000 years and cumulative brine flow across the LWB via the interbeds. Brine flow up the shaft was found to be insignificant and is therefore not presented. Panel pressure and brine saturation values are useful for assessing the potential impact of the PAVT input changes on direct releases up the borehole (spallings and direct brine release). Cumulative brine flow across the LWB is useful since the interbeds are the primary pathway for radionuclide release in the undisturbed scenario. In the disturbed scenarios, S2, S3, S4, S5, and S6, the borehole is the primary pathway for radionuclide release. Thus, in addition to the S1 performance measures, a key performance measure is the cumulative brine flow up the borehole to the Culebra. Figures and Tables with performance measure values are provided. A detailed discussion of two-phase flow behavior (gas and brine migration) in each of the repository scenarios is provided in Appendix A. Differences between the PAVT and CCA results are summarized in Appendix B.

2.1 Changes to Parameters

Changes to input parameters were implemented in BRAGFLO as follows:

- (1) DRZ log permeability (m²) was changed from a constant value of -15.0 to a uniform distribution ranging from -19.4 to -12.5 with a mean and median of -15.95.
- (2) Inundated corrosion rate (m/s) distribution (without CO₂) was changed from a uniform range of 0 to 1.58 x 10⁻¹⁴ to a uniform range of 0 to 3.17 x 10⁻¹⁴.
- (3) Waste permeability (m²) was changed from a constant value of 1.7×10^{-13} to a constant value of 2.4×10^{-13} .
- (4) Castile brine reservoir rock compressibility (Pa⁻¹) was changed from a log triangular distribution ranging from -11.3 to -8.0 to a triangular distribution ranging from 2.0 x 10⁻¹¹ to 1.0 x 10⁻¹⁰ (log: -10.7 to -10.0).

- Castile brine reservoir porosity was calculated from the condition that the product of Castile brine reservoir rock compressibility (Pa⁻¹) and porosity was constant and equal to 1.848 x 10⁻¹¹ Pa⁻¹. Based on the new range for rock compressibility (see (4) above) the calculated porosity ranges from 0.1848 to 0.924. The bulk volume of the brine reservoir is fixed by the grid geometry at 1.84 x 10⁷ m³. The sampled porosities resulted in one hundred initial brine reservoir volumes (m³) ranging from 3.6 x 10⁶ to 1.4 x 10⁷. In the CCA, the volume of brine in the Castile brine reservoir was sampled between a minimum of 32,000 m³ and a maximum of 160,000 m³ resulting in five possible volumes of 32,000, 64,000, 96,000, 128,000, and 160,000 m³, which were controlled by the parameter GRIDFLO (see Section 2.2).
- (6) Sand-filled borehole log permeability (m²) was changed from a uniform distribution ranging from -14.0 to -11.0 to a uniform distribution ranging from -16.3 to -11.0.
- (7) Concrete plug permeability (m²) was changed from a constant value of 5.0×10^{-17} to a uniform distribution ranging from 1.0×10^{-19} to 1.0×10^{-17} .

2.2 Changes to Model

To avoid calculating unrealistic repository pressures (far above lithostatic), the DRZ was allowed to fracture under the same conceptual model and parameters as Marker Beds 138 and 139.

One computational model change was implemented via input parameters. For vector #78 of the S2 scenario, the solution tolerances were changed to prevent excessive time step reductions. This change was not required for any other vectors or any other scenarios. These tolerance changes are described in Appendix B (Section B.5).

As described in Section 2.1, parameter change (5), Castile brine reservoir volumes were determined in the CCA using the sampled parameter GRIDFLO. In the PAVT, brine reservoir volumes were calculated as described above in parameter change (5), and GRIDFLO was not used.

Subsequent to the CCA, several minor code changes were implemented in BRAGFLO. These changes were shown to have no impact on the CCA Salado flow calculations (SPR Numbers 97-002, 97-003, 97-007, 97-008, 97-009, 97-010, which are all described in the Change Control Form for BRAGFLO, WPO #45223).

2.3 Impact of Changes on Model Results

2.3.1 Undisturbed Scenario S1

Parameter changes that had the most impact on repository performance in the undisturbed scenario were corrosion rates (higher) and DRZ permeability (sampled over a range with both



higher and lower permeabilities and a lower median). Values for important performance measures are provided in Table 2.1. The higher corrosion rates produced marginally higher pressures through 1000 years in the PAVT relative to the CCA. The range in DRZ permeability resulted in a wider range in brine inflow volumes. However, 64 realizations had initial DRZ permeabilities less than the CCA value of 1x10⁻¹⁵ m² which resulted in lower mean and median cumulative brine flows into the repository than in the CCA. Higher brine consumption rates (associated with the higher corrosion rates), slightly higher pressures, and lower inflow rates resulted in lower brine saturations in the repository. At times greater than 1000 years, these conditions resulted in slightly lower gas generation rates and less overall total gas generation.

DRZ fracturing appears to have had only a small effect on brine flows within the repository and DRZ and no apparent impact on flow up the shaft or across the LWB. Cumulative brine flows across the LWB were slightly less than in the CCA (see Table 2.1), except for one vector (#38) which produced significant flow (3326 m³) across the LWB (the majority of this flow occurs in Marker Bed 139). The maximum flow across the LWB in the CCA was 275 m³. This significant flow in vector #38 was caused by a combination of factors: the highest interbed permeability, the 8th highest DRZ permeability, low far-field pressure, and a high repository pressure at 1000 years.

2.3.2 Disturbed Scenarios S2 and S3 (E1 intrusion at 350 and 1000 years)

Parameter changes that had the most impact on repository performance in the E1 intrusion scenarios were the brine reservoir volume (approximately two orders of magnitude larger), borehole permeability (lower minimum permeabilities), and corrosion rates (higher). Values for important performance measures are provided in Tables 2.2 and 2.3. Panel pressures and brine saturations prior to intrusion were the same as shown in Table 2.1 (prior to intrusion, the E1 intrusion scenarios were identical to the undisturbed scenario). The higher corrosion rates produced marginally higher repository pressures prior to intrusion in the PAVT relative to the CCA. Following intrusion, lower borehole permeabilities and higher corrosion rates in combination with increased flow from the brine reservoir (brine reservoir pressures remain high after intrusion) resulted in substantially higher pressures in the repository. Brine flows upward in the borehole to the Culebra were substantially higher, with the maximum flow about two times larger than that predicted in the CCA. As in the CCA, there were also very small amounts of brine flow upward in the borehole beyond the top of the Rustler (< 1.2 m³). Salado transport results (see Section 3.3.2) show that these small volumes of brine were uncontaminated. As in the undisturbed scenario, one vector (#38) produced significant flow across the LWB. In the CCA, flows across the LWB in all disturbed scenarios were negligible. In addition to having high interbed and DRZ permeability, vector #38 also had the 17th lowest borehole permeability. As a consequence, flow across the LWB is decreased only slightly from the S1 value.

2.3.3 Disturbed Scenarios S4 and S5 (E2 intrusion at 350 and 1000 years)

Parameter changes that had the most impact on repository performance in the E2 intrusion

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scenarios were corrosion rates (higher), borehole permeabilities (lower minimum permeabilities), and DRZ permeability (sampled over a range of higher and lower permeabilities). Values for important performance measures are provided in Tables 2.4 and 2.5. Panel pressures and brine saturations prior to intrusion were the same as shown in Table 2.1 (prior to intrusion, the E2 intrusion scenarios were identical to the undisturbed scenario). Higher corrosion rates produced marginally higher pressures prior to intrusion in the PAVT relative to the CCA. The range in DRZ permeability resulted in a wider range in brine inflow volumes. However, 64 realizations had initial DRZ permeabilities less than the CCA value of $1x10^{-15}$ m² which resulted in lower mean and median cumulative brine flows into the repository than in the CCA. The net result of the higher brine consumption, higher pressures, and decreased brine inflow was lower brine saturations in the repository. Following the borehole intrusion, panel pressures stayed higher in the PAVT than in the CCA due primarily to the lower borehole permeabilities.

Although the upper end of the borehole permeability range was not changed, brine flows up the borehole were substantially less than those predicted in the CCA. This behavior was due to a combination of factors: lower brine saturations in the repository; lower borehole permeabilities at the lower end of the range; and the range of DRZ permeabilities. In the CCA, the DRZ added brine directly to the borehole in the highest flow cases. In the PAVT, the highest flow cases have a high borehole permeability and a low DRZ permeability. As a result there was no additional contribution from the low permeability DRZ to flow up the borehole (which is already lower than in the CCA because of the lower brine saturations). As in the E1 intrusion scenarios, cumulative brine flow across the LWB was significant in vector #38 (2735 m³) only.

2.3.4 Disturbed Scenario S6 (E2 intrusion at 1000 years and an E1 intrusion at 2000 years)

Parameter changes that had the most impact on repository performance in the E2E1 intrusion scenarios were the brine reservoir volume (approximately two orders of magnitude larger), borehole permeability (lower minimum permeabilities), and corrosion rates (higher). Results for S6 are provided in Table 2.6. As in scenarios S2 and S3, S6 was dominated by the E1 intrusion because of the large brine reservoir. Panel pressures and brine saturations prior to the E2 intrusion were the same as shown in Table 2.1 (prior to first intrusion, the E2E1 intrusion scenarios is identical to the undisturbed scenario). The higher corrosion rates produced marginally higher repository pressures prior to the E2 intrusion in the PAVT relative to the CCA. Following intrusion, lower borehole permeabilities and higher corrosion rates in combination with increased flow from the brine reservoir (brine reservoir pressures remain high after intrusion) resulted in substantially higher pressures in the repository. Brine flows upward in the borehole to the Culebra were substantially higher, with the maximum flow about two times larger than that predicted in the CCA. Flows up the borehole were slightly larger than those in S2 and S3 due to a larger head gradient between the Castile brine reservoir and panel at the time of the E1 intrusion. The larger head gradient between the Castile and panel was due to the E2 intrusion at 1000 years and the subsequent venting of panel gas up the borehole. As in E1 and E2 intrusion scenarios, cumulative brine flow across the LWB was significant in vector #38 (3203 m³) only.

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Table 2.1. 10th Percentile, Median, Mean, 90th Percentile, and Maximum Output Variable Values from the PAVT and CCA Simulations for Scenario S1 (Undisturbed).

Output Variable	Time		PAVT	Simulati	on (R1)			CCA S	imulation (l	R1, R2, R3)	
Description	(yrs)	10th	Median	Mean	90th	Max.	10th	Median	Mean	90th	Max
Average Pressure in Waste Panel (MPa)	350	1.6	4.0	4.4	9.0	10.5	1.0 1.0 1.2	3.2 3.2 3.2	4.0 4.0 4.0	9.2 9.2 9.2	10.4 10.2 10.0
	1000	3.7	7.1	7.7	12.9	14.0	2.1 2.0 2.7	6.1 6.1 6.0	6.7 6.7 6.7	12.2 12.4 12.4	13.5 14.0 14.5
	10000	6.9	10.2	10.5	13.6	16.8	7.0 7.1 6.8	10.8 11.0 10.7	10.8 10.8 10.7	14.2 14.1 14.0	15.5 16.3 16.2
Average Brine Saturation in Waste Panel	350	0.04	0.16	0.23	0.52	0.98	0.12 0.09 0.09	0.22 0.23 0.23	0.27 0.27 0.27	0.50 0.42 0.55	0.80 0.75 0.88
	1000	0.00	0.17	0.26	0.70	0.98	0.10 0.07 0.08	0.26 0.27 0.28	0.33 0.34 0.34	0.77 0.67 0.85	0.98 0.91 0.98
Cumulative Brine Flow out of MBs Across LWB (m³)	10000	0.0	0.0	35	0.0	3326	0.0 0.0 0.0	0.1 0.1 0.1	5.0 4.2 4.5	0.3 0.4 0.3	216 275 168
Total Volume of Gas Generated (10 ⁶ m ³)	10000	5.2	11.2	11.9	18.8	34.0	5.0 5.0 4.8	11.8 12.5 11.8	12.2 12.4 12.1	21.5 20.0 18.8	28.1 30.7 26.0
Cumulative Brine Flow into Repository (m³)	10000	1000	7500	13000	35000	72000	3200 3200 3000	11200 12400 12200	16000 16000 16000	33000 32000 33500	85000 57000 55500

Table 2.2. 10th Percentile, Median, Mean, 90th Percentile, and Maximum Output Variable Values from the PAVT and CCA Simulations for Scenario S2 (E1 Intrusion at 350 Years).

Output Variable	Time		PAVT	'Simulati	on (R1)			CCA Simu	ılation (R)	, R2, R3)	
Description	(yrs)	10th	Median	Mean	90th	Max.	10th	Median	Mean	90th	Max
Average Pressure in Waste Panel (MPa)	10000	4.7	7.9	8.9	14.2	16.6	1.6 1.5 1.5	4.7 5.0 4.7	4.5 4.5 4.5	7.3 7.0 7.3	9.7 10.1 11.0
Average Brine Saturation in Waste Panel	350	0.04	0.16	0.23	0.52	0.98	0.12 0.09 0.09	0.22 0.23 0.23	0.27 0.27 0.27	0.50 0.42 0.55	0.80 0.75 0.88
Cum. Brine Flow up Borehole at Rustler/Cul. (m³)	10000	0.0	27	6381	18100	105040	0.0 0.0 0.0	0 0 0	1030 1230 350	1330 700 670	39000 62000 12500
Cumulative Brine Flow out of MBs Across LWB (m³)	10000	0.0	0.0	26	0.0	2487	0.02 0.02 0.02	0.08 0.08 0.08	0.11 0.11 0.10	0.25 0.26 0.22	0.79 0.43 0.43

Table 2.3. 10th Percentile, Median, Mean, 90th Percentile, and Maximum Output Variable Values from the PAVT and CCA Simulations for Scenario S3 (E1 Intrusion at 1000 Years).

Output Variable	Time		PAVT	Simulati	on (R1)			CCA Sim	ılation (R	, R2, R3)	<u> </u>
Description	(yrs)	10th	Median	Mean	90th	Max.	10th	Median	Mean	90th	Max
Average Pressure in Waste Panel (MPa)	10000	3.2	7.4	8.1	12.7	15.4	1.7 1.5 1.5	4.7 5.0 4.7	4.5 4.5 4.5	7.3 7.0 7.2	9.2 10.2 10.1
Average Brine Saturation in Waste Panel	1000	0.00	0.17	0.26	0.70	0.98	0.10 0.07 0.08	0.26 0.27 0.28	0.33 0.34 0.34	0.77 0.67 0.85	0.98 0.91 0.98
Cum. Brine Flow up Borehole at Rustler/Cul. (m³)	10000	0.0	16	5935	18300	102340	0.0 0.0 0.0	0.0 0.0 0.0	1050 1150 450	1300 425 900	35200 67000 15600
Cumulative Brine Flow out of MBs Across LWB (m³)	10000	0.0	0.0	26	0.0	2630	0.02 0.02 0.02	0.08 0.08 0.08	0.12 0.12 0.11	0.25 0.26 0.24	1.28 0.66 0.41

Table 2.4. 10th Percentile, Median, Mean, 90th Percentile, and Maximum Output Variable Values from the PAVT and CCA Simulations for Scenario S4 (E2 Intrusion at 350 Years).

Output Variable	Time		PA	VT Simul	ation			CC	A Simulat	ion	
Description	(yrs)	10th	Median	Mean	90th	Max.	10th	Median	Mean	90th	Max
Average Pressure in Waste Panel (MPa)	10000	1.7	6.4	6.5	12.5	13.9	1.4 1.4 1.4	3.3 3.4 3.4	3.9 3.9 3.9	6.7 6.4 6.4	9.0 10.0 9.3
Average Brine Saturation in Waste Panel	350	0.04	0.16	0.23	0.52	0.98	0.12 0.09 0.09	0.22 0.23 0.23	0.27 0.27 0.27	0.50 0.42 0.55	0.80 0.75 0.88
Cum. Brine Flow up Borehole at Rustler/Cul. (m³)	10000	0.0	2.3	151	238	4774	0.0 0.0 0.0	0.0 0.0 0.0	638 330 250	110 93 70	40000 17800 13700
Cumulative Brine Flow out of MBs Across LWB (m³)	10000	0.0	0.0	26	0.0	2640	0.02 0.02 0.02	0.08 0.08 0.08	0.11 0.11 0.10	0.25 0.23 0.22	0.73 0.42 0.35

Table 2.5. 10th Percentile, Median, Mean, 90th Percentile, and Maximum Output Variable Values from the PAVT and CCA Simulations for Scenario S5 (E2 Intrusion at 1000 Years).

Output Variable	Time		PA	VT Simul	ation			CC	A Simulat	ion	
Description	(yrs)	10th	Median	Mean	90th	Max.	10th	Median	Mean	90th	Max
Average Pressure in Waste Panel (MPa)	10000	1.6	6.4	6.5	12.5	14.1	1.4 1.4 1.4	3.3 3.4 3.2	3.9 3.9 3.9	6.8 6.4 6.4	9.0 10.2 9.3
Average Brine Saturation in Waste Panel	1000	0.00	0.17	0.26	0.70	0.98	0.10 0.07 0.08	0.26 0.27 0.28	0.33 0.34 0.34	0.77 0.67 0.85	0.98 0.91 0.98
Cum. Brine Flow up Borehole at Rustler/Cul. (m³)	10000	0.0	1,8	133	160	4472	0.0 0.0 0.0	0.0 0.0 0.0	563 270 210	100 75 70	36100 13000 13000
Cumulative Brine Flow out of MBs Across LWB (m³)	10000	0.0	0.0	27	0.0	2735	0.02 0.02 0.02	0.08 0.08 0.08	0.12 0.11 0.11	0.25 0.25 0.23	1.28 0.71 0.38

Table 2.6. 10th Percentile, Median, Mean, 90th Percentile, and Maximum Output Variable Values from the PAVT and CCA Simulations for Scenario S6 (E2E1 Intrusion).

Output Variable	Time		PA	VT Simul	ation			CC	A Simulat	ion	
Description	(yrs)	10th	Median	Mean	90th	Max.	10th	Median	Mean	90th	Max
Average Pressure in Waste Panel (MPa)	10000	4.8	7.5	8.4	12.9	14.5	1.5 1.5 1.5	4.8 5.1 5.2	4.5 4.5 4.6	7.2 6.9 7.3	9.1 10.2 9.5
Average Brine Saturation in Waste Panel	1000	0.00	0.17	0.26	0.70	0.98	0.10 0.07 0.08	0.26 0.27 0.28	0.33 0.34 0.34	0.77 0.67 0.85	0.98 0.91 0.98
Cum. Brine Flow up Borehole at Rustler/Cul. (m³)	10000	0.0	66	7108	22000	108960	0.0 0.0 0.0	20 20 20	950 1280 620	780 340 1700	37100 62000 14000
Cumulative Brine Flow out of MBs Across LWB (m³)	10000	0.0	0.0	32	0.0	3203	0.02 0.02 0.02	0.08 0.08 0.09	0.12 0.11 0.11	0.25 0.25 0.23	1.65 0.56 0.39

3.0 SALADO TRANSPORT CALCULATIONS

This section summarizes differences between the PAVT and CCA Salado transport calculations. These calculations were performed using NUTS and PANEL. NUTS was used to calculate the transport of radionuclides throughout the repository, shaft system, Salado formation, and possible human-intrusion boreholes in scenarios S1, S2, S3, S4, and S5. PANEL was used to calculate the movement of radionuclides through the repository and boreholes in the multiple intrusion scenario S6 only. The key performance measure for comparing PAVT and CCA Salado transport results is cumulative radionuclide release to the Culebra via the intruding borehole. Transport of radionuclides to the accessible environment via the shaft and interbeds was found to be insignificant in both the PAVT and the CCA. Detailed Salado transport results are presented in Appendix C.

3.1 Changes to Parameters

The EPA requested that the solubilities of actinides in oxidation states +III, +IV, and +V be changed as shown in Table 3.1.

Table 3.1. PAVT and CCA Solubilities (moles/liter) of Actinide Oxidation States in Salado and Castile Brines Controlled by the MgO/MgCO₃ Buffer

	+III		+III +IV		+	V	+VI		
	PAVT	CCA	PAVT	CCA	PAVT	CCA	PAVT	CCA	
Salado	1.2E-7	5.8E-7	1.3E-8	4.4E-6	2.4E-7	2.3E-6	8.7E-6	8.7E-6	
Castile	1.3E-8	6.5E-8	4.1E-8	6.0E-9	4.8E-7	2.2E-6	8.8E-6	8.8E-6	

3.2 Changes to Model

The NUTS PAVT calculations were performed using an implicit dissolution/precipitation algorithm whereas the CCA NUTS calculations were performed using an explicit dissolution/precipitation algorithm. This algorithm change resulted from a previous investigation of the NUTS CCA calculations (SPR No. 97-004). This investigation indicated that radionuclide releases to the Culebra via the borehole and across the LWB via the interbeds may have been underestimated because of the explicit implementation of the precipitation/dissolution algorithm in NUTS version 2.03. To determine if CCA results were underestimated, a fully implicit dissolution/precipitation algorithm was incorporated in NUTS version 2.04 (Change Control Form, WPO #45998) and several CCA calculations were repeated. The conclusion of this investigation was that the impact of the explicit precipitation/dissolution algorithm on the CCA results was not important and that releases were not significantly underestimated. Based on this investigation it is concluded that differences in results between the CCA and PAVT are not

attributable to the change in the dissolution/precipitation algorithm change. However, because the implicit dissolution/precipitation algorithm is more robust and stable, it was implemented in the PAVT calculations.

In the CCA, ²³⁸Pu and ²³⁹Pu shared the same elemental solubility. To simplify the implementation of the implicit dissolution/precipitation algorithm in the PAVT calculations, these two isotopes were treated as separate elements and did not share the same elemental solubility. This treatment was implemented by assigning the solubility of ²³⁹Pu equal to the Pu solubility times the mole fraction of ²³⁹Pu at time zero (Stockman, 1997). This simplification is conservative in the sense that it overestimates ²³⁸Pu and ²³⁹Pu solubilities during the early part of the 10,000 year regulatory period. However, the impact of this overestimation of solubilities should not be significant.

3.3 Impact of Changes on Model Results

A screening analysis using a hypothetical inert tracer was conducted to reduce the large number of potential Salado transport simulations to a tractable number. An identical screening analysis was conducted previously for the CCA. For the screening analysis, a source concentration of 1 kg/m³ was applied to the source region. All realizations that transported a cumulative mass of inert tracer greater than or equal to 10^{-7} kg to the accessible environment over 10,000 years were considered significant and retained for complete transport analysis. The number of realizations screened in for scenarios S1, S2, S3, S4, and S5 are summarized in Table 3.2. A total of 151 runs were screened in for further analysis in PAVT replicate 1 compared to 57, 53, and 64 runs in replicates 1,2, and 3 of the CCA. Note that in scenario S6, all 100 realizations are analyzed using PANEL.

	PAVT		CCA	
Scenario	R1	R1	R2	R3
S1	4	1	5	3
S2	68	23	17	22
S3	50	21	21	25
S4	15	6	5	7
S5	14	6	5	7

Table 3.2. Summary of Realizations Screened In

As noted in Section 3.1, the solubilities of actinides in oxidation states +III, +IV, and +V were changed in the PAVT (Table 3.1). These changes reduce the effective solubilities of contaminants with the exception of actinides in the +IV state in the Castile brine. Note that the actinide oxidation states of +VI were unchanged. The net effect of the solubility changes is illustrated in

Figures 3.1 to 3.4. These Figures¹ show representative contaminant concentrations in EPA units/m³ within the repository as a function of time. S1 concentrations, which assume that Salado brine is present in the repository, are shown for the PAVT (Figure 3.1) and the CCA (Figure 3.2). S2 concentrations, which assume that Castile brine is present in the repository, are also shown for the PAVT (Figure 3.3.) and CCA (Figure 3.4). Two major regions are evident in each of these figures. In the first several thousand years, constant concentrations are seen for the period in which ²⁴¹Am (oxidation state +III) controls the total EPA unit concentration and is solubility limited. This region is shorter for realizations that sampled a higher ²⁴¹Am solubility. The transition to the second region occurs as the ²⁴¹Am changes from solubility to inventory limited and the EPA unit concentrations decrease. In the second region, ²³⁹Pu solubility (oxidation state +III or +IV) controls the EPA unit concentration. Note that higher concentrations are constant but the lower concentrations show a slow decrease with time. This behavior occurs because the sampled ²³⁹Pu solubility is low enough that other isotopes, which are inventory limited and have intermediate half-lives, contribute to the total EPA unit concentrations.

In the first region (241 Am-controlled), the lower 241 Am solubilities in the PAVT are seen by comparing Figures 3.1 (PAVT) and 3.2 (CCA) for the Salado brine and Figures 3.3 (PAVT) and 3.4 (CCA) for the Castile brine. For the Salado brine, the PAVT 241 Am concentrations are clustered around 1 x $^{10^{-3}}$ EPA units whereas in the CCA they are clustered around the higher value of 6 x $^{10^{-3}}$ EPA units. For the Castile brine, the PAVT 241 Am concentrations are clustered around 2 x $^{10^{-4}}$ EPA units whereas in the CCA they are clustered around 8 x $^{10^{-4}}$ EPA units.

These same four Figures can also be used to compare solubilities in the second region (²³⁹Pu-controlled). For the Salado brine, the PAVT ²³⁹Pu concentrations (Figure 3.1) are lower and are clustered around 2 x 10⁻⁵ EPA units whereas in the CCA (Figure 3.2) there are two distinct clusters of solubilities, one around the solubility of ²³⁹Pu(+III) and another around the solubility of ²³⁹Pu(+IV). In the PAVT, two distinct clusters are not seen because both actinide solubilities are very low. For the Castile brine, the PAVT ²³⁹Pu concentrations (Figure 3.3) show a slightly larger spread than the CCA values (Figure 3.4), but with an increased number of lower concentrations near 1 x 10⁻⁵ EPA units. The larger spread is due to the increase in ²³⁹Pu(+IV) solubility for Castile brine.

Based on the above discussion, both the Salado and Castile solubilities of ²⁴¹Am tended to be significantly lower in the PAVT than in the CCA. Salado ²³⁹Pu solubilities in the PAVT also tended to be much lower than in the CCA. In Castile brine, ²³⁹Pu solubilities were higher or lower than in the CCA depending on the sampled oxidation state, and on average were similar to the CCA.

¹These Figures were constructed for illustrative purposes only using the computer code PANEL. Concentrations are based on a typical waste panel brine volume of 4,000 m³. Since PANEL requires a flow rate as input, a low flow rate of 10⁻⁵ m³/yr was assigned to prevent inventory depletion during PANEL calculations.

3.3.1 Undisturbed Performance

The Salado flow analysis showed that only one undisturbed scenario (S1) vector (#38) produced significant flow (3326 m³) outward across the LWB. This vector was the only realization that released contaminants across the LWB (see Appendix C). These releases occurred at the LWB to the south of the repository in Marker Bed 139, with a total integrated discharge of 4.84E-10 EPA units out of all interbeds (see Figures C.1 - C.7 in Appendix C). The majority of this activity was due to ²³⁹Pu (3.4E-10 EPA units) and ²⁴¹Am (8.67E-11 EPA units). These results are similar to the CCA results where a total activity of 3.33E-10 EPA units was released. Further, as in the CCA, these releases were likely due to numerical dispersion that was caused by the coarse lateral gridding between the repository and lateral LWB, and large time steps at later times in the calculation. This conclusion is also supported by the fact that the pore volume of Marker Bed 139 (which provides most of the flow in vector #38) between the repository and LWB is greater than 155,000 m³.

3.3.2 Disturbed Performance (E1, E2, and E2E1 Intrusions)

In both the PAVT and the CCA, the only pathway for significant release in the disturbed scenarios was the intrusion borehole. This behavior, described below, justifies the use of PANEL, which ignores all pathways other than the borehole, for S6 calculations. For Salado transport calculations under disturbed conditions, brine may enter the repository from the Castile, Salado, or Culebra. For E1 intrusion scenarios where a borehole penetrates the Castile brine reservoir (S2, S3, S6), actinide solubilities in Castile brine were used. For E2 intrusions (S4, S5), solubilities in Salado brine were used.

The brine flow fields required for NUTS transport calculations are provided by the two-phase flow model BRAGFLO. BRAGFLO was used to model two intrusion times of 350 and 1000 years. The flow fields corresponding to these two intrusion times were used to approximate flow fields for the additional intrusion times of 100, 3000, 5000, 7000, and 9000 years. For example, for the 100-year intrusion, flow fields from the 350-year intrusion were applied beginning at 100 years. For the period from time zero to 100 years, flow fields from the undisturbed scenario were used. Similarly, for each of the intrusions at 3000, 5000, 7000, and 9000 years, BRAGFLO flow fields from the 1,000-year intrusion were applied beginning at 3000, 5000, 7000, and 9000 years, respectively. In each of these intrusion cases, from time zero until the intrusion time, flow fields from the undisturbed scenario were used.

In the E2E1 intrusion scenario, one borehole penetrates the waste-filled panel at 1000 years and a second borehole, drilled at the same location, penetrates the panel and underlying Castile brine reservoir at 2000 years. The additional brine flow fields required for the PANEL calculations (at times 100, 350, 1000, 4000, 6000, and 9,000) were simulated by shifting the BRAGFLO E2E1 flow conditions at the time of the E1 intrusion (2000 years) to the nominal intrusion time of concern. For example, a 100 year intrusion was simulated by shifting the BRAGFLO time steps backwards in time by 1900 years. Thus, at the start of the 100 year PANEL run, the repository

had already had an E2 intrusion for 900 years and at 100 years, the E1 intrusion occurred. The releases during the final 1900 years were obtained by using the panel brine volume and borehole flow rate from the final time step in the BRAGFLO E2E1 simulation. For a nominal intrusion time after 2000 years, the BRAGFLO initial conditions were maintained until the first BRAGFLO time shifted time step. This method of time shifting resulted in artificially high repository saturations at very early times in the 100, 350, and 1000 year time shifted runs, which can be seen in the large volumes of brine that were released at early times in these calculations.

The integrated discharges (in EPA units) up the borehole and into the Culebra from the NUTS and PANEL calculations for all screened-in realizations are listed in tabular form in Appendix C. The realizations in each of the Tables were sorted by the total EPA units discharged to the Culebra summed over all 5 transported isotopes. Figures C.8 through C.91 show the discharge to the Culebra for all intrusion times for scenarios 2 through 5. For all scenarios, releases decreased with later intrusion times because of ²⁴¹Am decay. Releases also decreased with later intrusion time because of less time for long-term flow after the intrusion. Figures C.92 through C.133 show the discharge to the Culebra for the multiple intrusion E2E1. Like the E1 intrusions, the E2E1 intrusion was ²⁴¹Am dominated for the first 3000 to 4000 years, after which radioactive decay of ²⁴¹Am results in ²³⁹Pu dominance. In the S2 and S3 scenarios, a small amount of brine (<1.2 m³) flowed upward in the borehole beyond the top of Rustler (see Appendix A, Sections A.2.1.1.1.3 and A.2.1.2). NUTS transport results show that this brine was uncontaminated.

A summary of PAVT replicate 1 statistical measures (10th percentile, median, mean, 90th percentile, and maximum) for total releases to the Culebra (in EPA units) for each scenario and intrusion time is shown in Table 3.3. Equivalent information for the three CCA replicates combined is shown in Table 3.4

For the E1 scenarios (S2, S3, S6) with early time (<2000 years after closure) intrusions, larger upward borehole flows in the PAVT relative to the CCA, were offset by the reduced ²⁴¹Am solubility. As a consequence, radionuclide releases to the Culebra from early time E1 intrusions were only slightly larger, on average, in the PAVT (Table 3.3) than in the CCA (Table 3.4). For later E1 intrusion times, PAVT releases tended to be moderately larger than those in the CCA. The larger PAVT flows were not offset as much at later times because the ²³⁹Pu solubilities were similar to the CCA. Releases to the Culebra from later E1 intrusion times were much less than from early intrusions.

The top realizations in terms of maximum 10,000 year integrated release (in EPA units) to the Culebra for specified intrusion times for scenarios S2 through S6 are summarized for the PAVT (maximum from replicate 1) in Table 3.5 and for the CCA (maximum from all 3 replicates) in Table 3.6. As was predicted in the CCA, high releases were controlled either by ²⁴¹Am or ²³⁹Pu. Contrary to the larger mean and 90th percentile releases in the PAVT, maximum releases to the Culebra from early time E1 intrusions were smaller in the PAVT. For example, in PAVT replicate 1, the maximum release to the Culebra is 28.9 total EPA units (vector #28, S6 at 100 yrs) as compared to 95.0 total EPA units (vector #111, S6 at 100 yrs) in the CCA (replicate 2). It should

be noted that in the CCA the maximum releases to the Culebra in replicates 1 and 3 were 9.2 and 26.3 total EPA units, respectively. Both of these maximum releases are less than the maximum PAVT replicate 1 release. The reduced maximum early time E1 release in the PAVT was likely caused by the significant reduction in the Castile solubilities of ²⁴¹Am. The ²⁴¹Am solubility in PAVT vector #28 was 1.62E-7 moles/liter versus 2.63E-6 moles/liter in CCA vector #111. In the PAVT, vector #28 had the largest brine discharge to the Culebra (108,960 m³ in S6, 102,340 m³ in S3, and 105,040 m³ in S2); in the CCA, vector #111 had the highest brine discharge to the Culebra (62,000 m³ in S6, 67,000 m³ in S3, and 62,000 m³ in S2). The lower ²⁴¹Am solubility in the PAVT offset the higher upward borehole flow, resulting in a lower release to the Culebra.

For E2 intrusions (S4, S5) at all times, radionuclide releases to the Culebra tended to be much less than in the CCA due to both lower upward borehole flows and reduced solubilities of both ²⁴¹Am and ²³⁹Pu in Salado brine. For E2 intrusions, maximum releases were also significantly lower in the PAVT.

Note that other factors such as volume of repository swept by incoming brine and the flow path brine takes once it is contaminated, also influence the quantity of radionuclides that enter the borehole and flow upward to the Culebra. These factors were responsible for the large differences in releases between scenarios S3 and S6 in both the PAVT and the CCA. For example, in S3 a large fraction of the brine flow that flowed upward from the Castile continued to flow up the borehole without mixing with the waste. This behavior occurred for two reasons: (i) the waste inventory in the region near the borehole became depleted; and (ii) outward flow into the repository from the borehole decreased as the repository became saturated with brine. In S6, radionuclide releases computed with PANEL were based on the assumption that all of the brine that flowed upward beyond the top of the DRZ had contacted all of the waste within the intruded panel and was then instantly injected into the Culebra.

In the single intrusion scenarios, the highest release to the Culebra in the PAVT was from scenario S2 (vector#28), an E1 intrusion at 100 years. In the CCA, the highest single intrusion release occurred in scenario S4 (vector#24), an E2 intrusion at 100 years. CCA vector #24 discharged 40,000 m³ to the Culebra following the E2 intrusion. In the PAVT, the E2 intrusions (S4 and S5 scenarios) produced only small brine discharges to the Culebra (< 5000 m³) as discussed in Section 2 and, coupled with the reduced ²⁴¹Am solubility, produced much lower releases than in the CCA. For further comparison, the maximum releases to the Culebra in the PAVT from ²⁴¹Am, ²³⁹Pu, ²³⁸Pu, ²³⁴U, and ²³⁰Th were 27.5, 2.99, 0.202, 0.014, and 0.029 EPA units, respectively. In the CCA, the corresponding maximum releases to the Culebra were 94.6, 20.8, 0.005, 0.013, and 0.177 EPA units. Again, as was predicted in the CCA, high releases to the Culebra are controlled either by ²⁴¹Am or ²³⁹Pu.

Table 3.3. Statistical Summary of PAVT Total 10,000 Year Integrated Release (EPA units) up the Borehole to the Culebra* For Each Scenario (Replicate 1).

Scenario	Intrusion Time (yrs)	10th Percentile	Median	Mean	90th Percentile	Maximum
S1	none*	0.00	0.00	4.8E-12	0.00	4.8E-10
S2	100	0.00	8.00E-06	0.164	0.621	2.90
	350	0.00	7.97E-06	0.146	0.597	2.51
						<u> </u>
	1000	0.00	0.00	6.65E-02	0.270	1.11
Ĺ	3000	0.00	0.00	4.13E-02	0.174	0.65
S3 [5000	0.00	0.00	3.15E-02	0.128	0.52
Ĺ	7000	0.00	0.00	2.20E-02	0.0771	0.29
	9000	0.00	0.00	1.27E-02	0.0401	0.23
	ė					
S4 -	100	0.00	0.00	3.77E-03	1.28E-03	0.20
	350	0.00	0.00	3.43E-03	1.09E-03	0.19
						
	1000	0.00	0.00	1.52E-03	6.37E-04	0.06
	3000	0.00	0.00	5.22E-04	0.00	0.01
S5	5000	0.00	0.00	2.24E-04	0.00	0.01
L	7000	0.00	0.00	1.14E-04	0.00	0.01
	9000	0.00	0.00	0.00	0.00	0.0
			***		<u> </u>	<u> </u>
	100	1.51E-12	3.31E-03	1.38	4.26	28.9
	350	1.51E-12	3.25E-03	1.30	4.07	27.1
	1000	1.51E-12	3.23E-03	1.03	3.64	18.2
S6	2000	1.44E-12	3.04E-03	0.567	2.40	7.11
	4000	0.00	6.03E-04	0.150	0.408	2.46
	6000	0.00	1.25E-04	0.0974	0.207	1.82
	9000	0.00	7.60E-05	0.0496	0.0951	1.01

^{*} S1 releases are through the Salado interbeds to the LWB. S2 through S6 releases are up the borehole to the Culebra

Table 3.4. Statistical Summary of CCA Total 10,000 Year Integrated Release (EPA units) up the Borehole to the Culebra* For Each Scenario (Replicates 1,2, and 3).

Scenario	Intrusion Time (yrs)	10th Percentile	Median	Mean	90th Percentile	Maximum
S1	none*	0.00	0.00	1.5E-12	0.00	3.3E-10
S 2	100	0.00	0.00	0.0750	0.0395	6.62
	350	0.00	0.00	0.0650	0.0323	6.04
	1000	0.00	0.00	2.66E-02	2.53E-02	2.19
	3000	0.00	0.00	4.69E-03	5.10E-03	0.36
S3	5000	0.00	0.00	1.76E-03	1.98E-03	0.24
	7000	0.00	0.00	9.63E-04	7.50E-04	0.14
	9000	0.00	0.00	3.00E-04	1.04E-04	0.035
S4 -	100	0.00	0.00	9.25E-02	0.00	21.1
	350	0.00	0.00	8.83E-02	0.00	20.4
					<u> </u>	
1	1000	0.00	0.00	7.68E-02	0.00	18.4
Į	3000	0.00	0.00	4.76E-02	0.00	11.6
S5	5000	0.00	0.00	2.14E-02	0.00	5.62
	7000	0.00	0.00	5.48E-03	0.00	1.10
	9000	0.00	0.00	1.43E-04	0.00	0.027
1	100	0.00	2.06E-03	0.728	0.629	95.0
L	350	0.00	2.05E-03	0.603	0.555	68.7
	1000	0.00	2.05E-03	0.368	0.479	26.0
S6	2000	0.00	1.76E-03	0.165	0.384	5.57
	4000	0.00	2.68E-04	0.0162	0.0408	0.792
	6000	0.00	4.63E-05	6.52E-03	8.85E-03	0.491
	9000	0.00	2.75E-05	3.16E-03	4.98E-03	0.195

^{* \$1} releases are through the Salado interbeds to the LWB. \$2 through \$6 releases are up the borehole to the Culebra

Table 3.5. Maximum PAVT Total 10,000 Year Integrated Release (EPA units) up the Borehole to the Culebra For Each Disturbed Scenario at Specified Intrusion Times (Replicate 1).

Scenario	Intrusion Time (yrs)	Vector	²⁴¹ Am	²³⁹ Pu	²³⁸ Pu	²³⁴ U	²³⁰ Th	Total
S2	100	28	2.33E+00	5.36E-01	3.15E-02	3.06E-04	3.15E-03	2.90
52	350	28	1.96E+00	5.32E-01	1.79E-02	3.02E-04	3.15E-03	2.51
								<u> </u>
	1000	28	5.83E-01	5.20E-01	2.95E-06	2.84E-04	2.82E-04	1.11
	3000	83	3.03E-02	6.15E-01	2.03E-08	4.20E-03	5.69E-04	0.65
S 3	5000	83	6.60E-03	5.10E-01	1.53E-10	3.48E-03	5.64E-04	0.52
	7000	28	1.34E-04	2.90E-01	8.41E-15	1.67E-04	1.51E-03	0.29
	9000	28	6.01E-06	2.29E-01	5.98E-17	9.71E-05	1.25E-03	0.23
S4	100	28	1.90E-01	1.34E-02	4.66E-05	9.52E-07	1.95E-05	0.20
	350	28	1.79E-01	1.34E-02	1.84E-06	9.50E-07	1.95E-05	0.19
								
	1000	28	4.91E-02	1.13E-02	2.02E-08	8.06E-07	1.70E-05	0.06
	3000	5	4.90E-06	1.43E-02	1.17E-16	3.90E-05	9.56E-06	0.01
S5	5000	28	7.66E-05	1.13E-02	1.52E-14	8.06E-07	1.66E-05	0.01
	7000	28	6.29E-06	1.13E-02	3.27E-17	8.06E-07	1.66E-05	0.01
	9000		0.0	0.0	0.0	0.0	0.0	0.0
1	100	28	2.75E+01	1.29E+00	1.05E-01	5.64E-04	1.77E-02	28.9
<u> </u>	350	28	2.58E+01	1.28E+00	1.47E-02	5.61E-04	1.86E-02	27.1
\$6	1000	28	1.70E+01	1.23E+00	8.85E-05	5.43E-04	2.08E-02	18.2
	2000	54	4.48E+00	2.60E+00	6.54E-08	9.75E-03	1.82E-02	7.11
Į	4000	54	2.44E-01	2.19E+00	9.59E-15	8.25E-03	1.92E-02	2.46
	6000	54	3.17E-02	1.76E+00	1.40E-21	6.66E-03	1.82E-02	1.82
	9000	54	1.80E-02	9.73E-01	7.81E-32	3.70E-03	1.23E-02	1.01

Maximum Release

28.9

Table 3.6. Maximum CCA Total 10,000 Year Integrated Release (EPA units) up the Borehole to the Culebra For Each Disturbed Scenario at Specified Intrusion Times (Replicates 1,2, and 3).

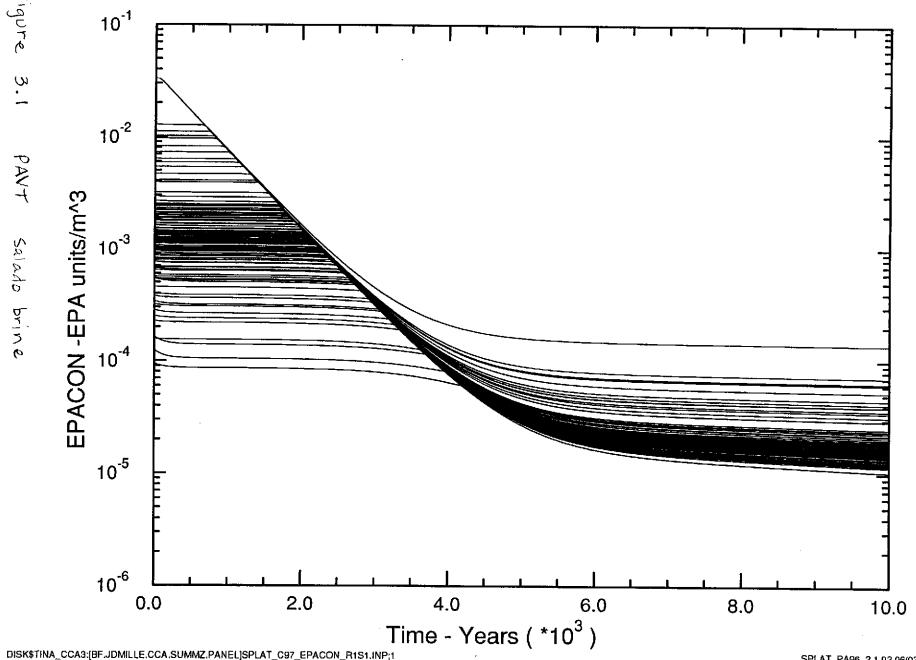
Scenario	Intrusion Time (yrs)	Vector	²⁴¹ Am	²³⁹ Pu	²³⁸ Pu	²³⁴ U	²³⁰ Th	Total		
S2	100	111	6.57E+00	4.51E-02	1.73E-03	5.23E-05	9.40E-04	6.62		
32	350	111	6.00E+00	4.44E-02	8.07E-05	2.21E-05	9.28E-04	6.04		
	1000	111	2.15E+00	4.40E-02	1.23E-06	7.48E-06	1.01E-03	2.19		
	3000	128	4.32E-02	3.16E-01	2.69E-08	9.86E-06	3.21E-04	0.36		
S3	5000	128	3.76E-03	2.36E-01	1.76E-10	7.20E-06	2.41E-04	0.24		
	7000	128	2.06E-04	1.42E-01	2.67E-13	4.26E-06	1.49E-04	0.14		
	9000	128	1.36E-05	3.53E-02	2.59E-15	1.05E-06	4.94E-05	0.04		
ļ,								<u> </u>		
S4	100	23	1.41E-01	2.08E+01	1.55E-06	1.31E-02	1.77E-01	21.1		
	350	23	5.87E-02	2.01E+01	2.39E-07	9.43E-03	1.72E-01	20.4		
<u></u>										
 	1000	23	1.34E-02	1.82E+01	6.12E-09	1.16E-02	1.55E-01	18.4		
	3000	23	2.82E-04	1.15E+01	6.59E-14	5.47E-03	9.85E-02	11.6		
S5 .	5000	23	1.65E-05	5.57E+00	1.39E-16	2.72E-03	4.76E-02	5.62		
	7000	23	6.81E-08	1.09E+00	1.68E-18	5.14E-04	9.24E-03	1.10		
	9000	124	8.75E-08	2.67E-02	1.86E-18	3.54E-06	2.64E-04	0.03		
	100	111	9.46E+01	4.29E-01	3.83E-02	6.88E-05	2.03E-03	95.0		
ļ	350	111	6.82E+01	4.24E-01	5.36E-03	6.85E-05	2.13E-03	68.7		
\$6	1000	111	2.56E+01	4.09E-01	3.23E-05	6.63E-05	2.37E-03	26.0		
	2000	111	5.18E+00	3.87E-01	1.24E-08	6.29E-05	2.69E-03	5.57		
	4000	128	1.34E-01	6.57E-01	6.83E-14	2.05E-05	1.28E-03	0.79		
	6000	128	2.30E-02	4.67E-01	1.00E-20	1.46E-05	1.03E-03	0.49		
	9000	128	9.80E-03	1.84E-01	5.60E-31	5.78E-06	4.73E-04	0.20		

Maximum Release

95.0





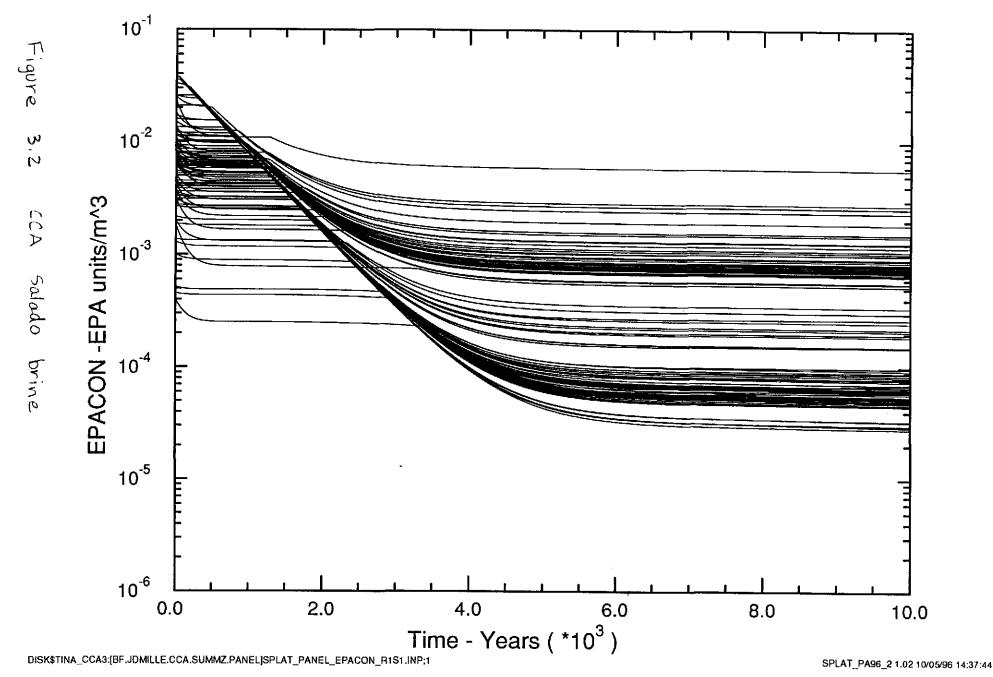


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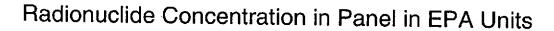
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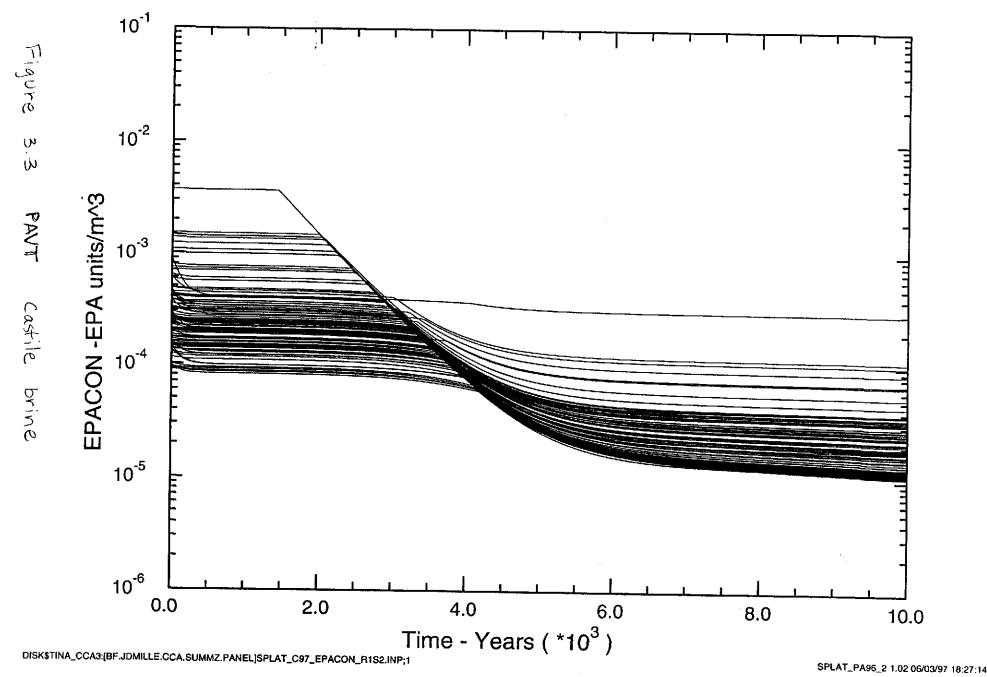
SNL WIPP PA96: PANEL SIMULTIONS (CCA R1 S1)

Radionuclide Concentration in Panel in EPA Units



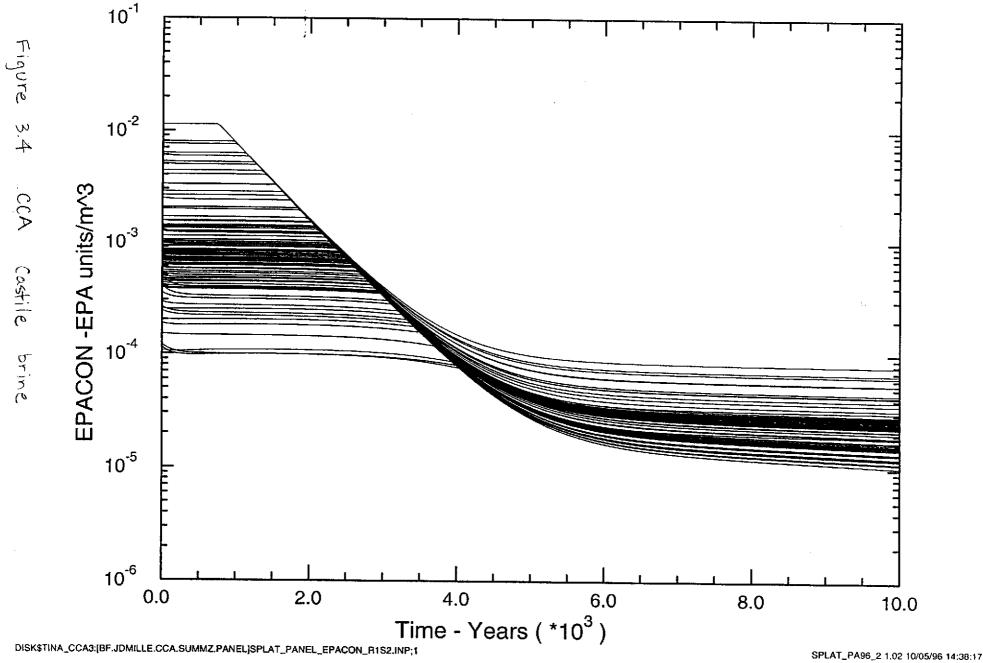
SNL WIPP PA: PANEL SIMULA NS (C97 R1 S2)





SNL WIPP PA96: PANEL SIMU TIONS (CCA R1 S2)

Radionuclide Concentration in Panel in EPA Units



4.0 CULEBRA TRANSPORT CALCULATIONS

This section summarizes differences between the PAVT and CCA Culebra transport calculations. These calculations were performed using SECOFL2D and SECOTP2D. SECOFL2D was used to calculate ground-water flow assuming single porosity, steady-state conditions. SECOTP2D was used to calculate transport and cumulative release of radionuclides to the accessible environment assuming dual-porosity transport behavior with linear equilibrium sorption. Sorption is assumed to occur in the matrix only. Important future events such as potash mining and climate change were included.

The key performance measure for comparing PAVT and CCA Culebra transport results is the cumulative discharge of radionuclides across the LWB.

4.1 Changes to Parameters

The Culebra matrix distribution coefficients were represented by loguniform probability distributions rather than the uniform probability distributions used in the CCA. The ranges of $k_{\rm d}$ values used in the CCA for each probability distribution were unchanged.

4.2 Changes to Model

Seven significant code changes were made to SECOTP2D subsequent to the CCA calculations (Change Control Form, WPO #45730):

- (1) mass balance reporting was implemented to enable monitoring of the total mass of each contaminant in the system during the 10,000 year regulatory period (WPO #45730);
- the source-term algorithm was corrected to ensure that the correct amount of mass (1 kg) was injected into the system (SPR No. 97-006);
- the discharge calculation at the model domain (grid) boundary was corrected to ensure that the mass of each contaminant leaving the system was accurately tracked (SPR No. 97-012);
- (4) the total variation diminishing (TVD) limiters at the boundaries of the model domain were restricted to have values equal to zero (equivalent to upwinding) to reduce the potential for numerical instabilities near boundaries (SPR No. 97-013);
- (5) logic was modified to avoid redundant coefficient generation and LU decomposition calculations in the solution of the matrix diffusion equation when a constant time step was used (WPO #45730);
- (6) the van Leer TVD limiter was changed so that it is consistent with published references (WPO #45730);
- (7) logic was introduced to limit the application of TVD to computational cells in which the Courant number was less than or equal to one (WPO #45730).

These modifications have improved the robustness, computational efficiency, and accuracy of

SECOTP2D.

Three important model implementation changes were made for the PAVT. Numerical studies of SECOTP2D have shown that substantially improved mass balance characteristics are obtained in the Culebra transport calculations if the operator splitting factors (SECOTP2D User's Manual, Version 1.30, WPO #36695) are set to a_x=0 and a_y=1. In the CCA, these parameters were both set to 0.5. The second implementation change was to set Dirichlet boundary conditions equal to zero (specified concentrations equal to zero) at the transport grid boundaries. In the CCA, the automatic boundary condition scheme was implemented; this scheme enforced a zero Neumann condition (zero flux) at the boundary if flow was out of the model domain and zero Dirichlet (zero concentration) if flow was into the domain. In the PAVT, a zero Dirichlet condition (zero concentrations) was enforced at all grid boundaries during the simulation to avoid instabilities caused by alternating flow directions in adjacent computational cells along the model domain boundaries. Note that this choice of boundary condition does not influence the predicted contaminant discharges across the LWB since the model domain boundaries were positioned far from the LWB. The third important model implementation change was to use a variable time step in the transport calculations to avoid solution oscillations at early times. The variable time step was prescribed as follows: the initial time step was 0.01 years for the 50 years, a variable time step that gradually increased to one year by a factor of 1.001 each year up to the time of approximately 1000 years, and a constant time step of one year thereafter.

Two additional changes were implemented in the PAVT. First, in the CCA, the matrix was discretized with 20 nodes; in the PAVT, 21 nodes were used. Second, in the CCA, the northeastern corner of the regional domain was modeled using no-flow boundary conditions. In the PAVT, these boundary conditions were changed to a specified head boundary condition to be more consistent with the specified head boundary conditions that are applied in this region during the transmissivity field generation process (Analysis Package for the Culebra Flow and Transport Calculations, WPO #40516). This change should not influence the flow field at the local (transport) scale and therefore should not influence the PAVT Culebra transport results.

4.3 Impact of Changes on Model Results

The following steps in the analysis were implemented identically in the PAVT and CCA. The first step in the transport analysis was to generate the Culebra transmissivity field (T-field). Uncertainty in the T-field was quantified by generating 100 equally likely representations of the T-fields through geostatistical analysis. Potash mining was incorporated into the analysis according to the guidelines and recommendation given in 40 CFR Part 194. Mining impacts were considered by uniformly scaling the transmissivity in regions considered to contain economically-extractable resources by a factor (MINP_FAC) of 1 to 1000. Mining effects were treated differently depending on the location of the resources with respect to the LWB. Outside the LWB, it was assumed mining will occur prior to sealing the disposal facility. Inside the LWB, mining occurred with a probability of 1 in 100 each century. The probabilistic aspects of mining associated with the time of occurrence within the LWB are accounted for in the construction of

the CCDF. The analysis was therefore essentially based on two sets of transmissivity fields; one with mining outside the LWB (partial mining scenario), and one with all regions mined (full mining scenario). These two sets of transmissivity fields were used to produce two sets of steady-state groundwater flow fields, one for the partial mining scenario and one for the full mining scenario. The impact of potential climate variations on these steady-state flow fields was addressed by uniformly scaling the x and y components of the Darcy flow velocity by a single value ranging from 1.0 to 2.25, known as the climate index (CLIMTIDX). The PAVT results are summarized as follows.

In the CCA, only two realizations resulted in conditional releases² across the LWB. In these two realizations, only two radionuclides were released, 234 U and negligible amounts of 230 Th (less than 3.0E-7 kg). Because a loguniform distribution for k_d was used in the PAVT, sampled k_d values tended to be much smaller than those used in the CCA. As a consequence, several realizations resulted in the conditional releases of 234 U and insignificant amounts of 230 Th (less than 4.0E-6 kg) at the LWB.

The realizations were ranked according to the conditional release of ²³⁴U. Results are provided in Appendix D for both the partial mining and full mining scenarios. Also provided are corresponding values of the following parameters; MINP FAC (mining impact factor), CLIMTIDX (climate index), APOROS (fracture porosity), DPOROS (matrix porosity), HMBLKT (half block length of the matrix), OXSTAT (actinide oxidation state parameter), and MKD_U (k_d value for matrix sorption). The tabulated results show that 22 partial mining and 20 full mining scenarios produced a conditional ²³⁴U release greater than 1.0E-10 kg. Only 7 partial mining and 8 full mining scenarios produced a conditional release greater than 0.1 kg. The maximum possible release of the entire source of 1 kg occurred in realization #79 with full mining and almost occurred (> 0.9 kg) in realization #74 with full mining and realization #79 with partial mining. These results are shown graphically in Figures 4.1 (partial mining) and 4.2 (full mining). Note that all conditional releases greater than 1.E-10 kg had a value of OXSTAT greater than 0.5 corresponding to an oxidation state of released ²³⁴U of +VI. This isotope had the lowest range of matrix distribution coefficients as shown in Table 4.1. Other factors such half-block length of the matrix, mining impact factor, climate index, and transmissivity field also influence, in a complex way, the conditional release across the LWB. This combination of factors is why vector #79 had the highest discharge yet didn't have the lowest k_d.

Statistical summaries of PAVT and CCA Culebra conditional ²³⁴U releases are shown in Tables 4.2 and 4.3, respectively. Mean, 90th percentile, and maximum discharges are all higher in the PAVT. However, even with the maximum PAVT SECOTP2D conditional discharge (full mining vector #79) of 1 kg, the maximum release of ²³⁴U to the Culebra predicted by the Salado transport

4 - 3

²The computational strategy used in the Culebra transport analysis takes advantage of the linearity of the system of partial differential equations that underlies SECOTP2D. Transport calculations were performed for unit kg releases to the Culebra. These calculations identify conditional releases. Using the linearity of the system, the conditional releases are then used to construct transport results for arbitrary time-dependent releases into the Culebra using NUTS and PANEL calculated radionuclide sources.

analysis is only 0.0136 EPA units (Appendix C, scenario S6, 100 year intrusion time, vector #83). If these two maximum values were combined, the 1 kg conditional release would produce a ²³⁴U release of only 0.0136 EPA units across the LWB (assuming 1 intrusion in 10,000 years).

Table 4.1 Matrix Distribution Coefficients

Isotope Low/High Oxidation State	Low Oxidation State k _d range (m³/kg)	High Oxidation State k _d range (m³/kg)	
²³⁴ U (IV)/(VI)	0.9 to 20	0.00003 to 0.03	
²³⁹ Pu (III)/(IV)	0.02 to 0.5	0.9 to 20	
²⁴¹ Am (III)/(III)	0.02 to 0.5	0.02 to 0.5	
²³⁰ Th (IV)/(IV)	0.9 to 20	0.9 to 20	

Table 4.2. Statistical Summary of PAVT Conditional ²³⁴U Release (kg) Through the Culebra to the LWB from a 1 kg Source (Replicate 1)

Mining	10th Percentile	Median	Mean	90th Percentile	Maximum
Full	0.0	0.0	0.057	0.027	1.00
Partial	0.0	0.0	0.035	0.047	0.92

Table 4.3. Statistical Summary of CCA Conditional ²³⁴U Release (kg) Through the Culebra to the LWB from a 1 kg Source (All 3 Replicates)

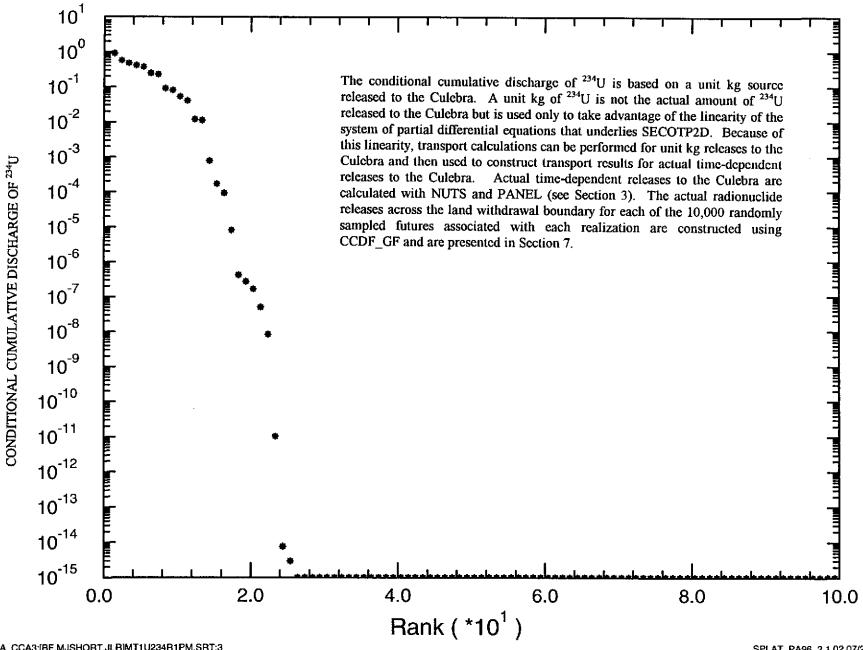
Mining	10th Percentile	Median	Mean	90th Percentile	Maximum
Full	0.0	0.0	0.003	0.0	0.91
Partial	0.0	0.0	0.0004	0.0	0.11

The hydraulic conductivity fields (K-fields), hydraulic head contours, and contaminant concentrations for vector #79, in both the partial and full mining scenarios, are presented in Figures 4.3 through 4.8. The locations of the high-K zones are identified in both scenarios (Figures 4.3 and 4.4), as are the locations of the LWB and waste repository area. The groundwater flow solutions at 10,000 years, in the form of hydraulic heads, for both scenarios (Figures 4.5 and 4.6) show that flow within the region defined by the LWB was predominately southward through the higher K-zones, with some flow in the southwesterly direction, particularly with full mining. Conditional ²³⁴U concentrations (based on a unit source) at 10,000 years (Figures 4.7 and 4.8) show that the contaminant plumes also moved predominately southward with the flow field.

Finally, conditional mass balance errors³ for each radionuclide were monitored in the PAVT Culebra transport simulations and are presented in Appendix D (Figures D.1 through D.5 for partial mining and Figures D.6 through D.10 for full mining). These Figures show that conditional mass balance errors for all radionuclides and simulations were very small, with the maximum error being 0.014 kg for ²³⁴U in full mining vector #57 (Figure D.6).

³These mass balance errors are based on a unit 1 kg source in the Culebra.

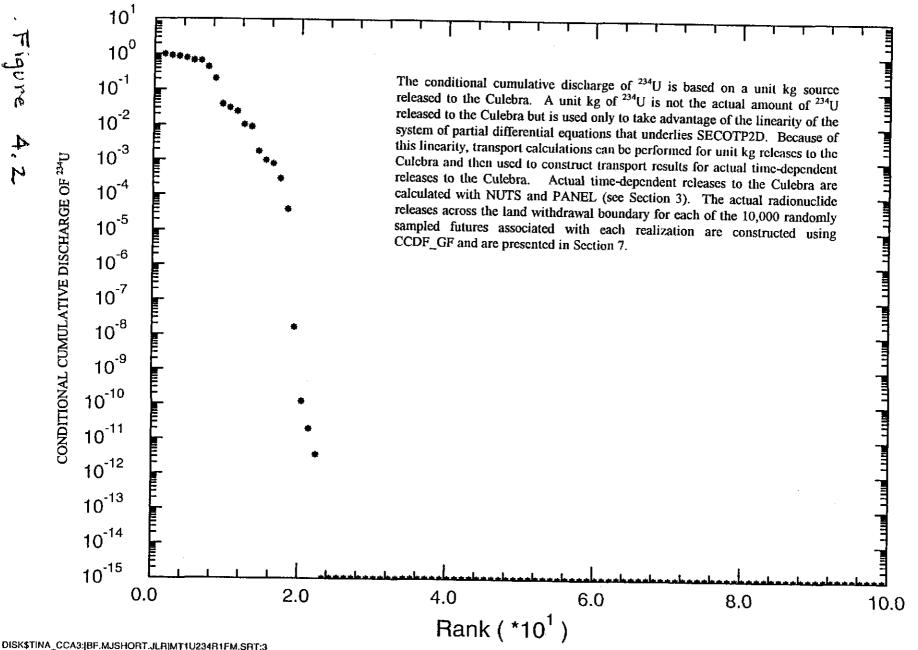
Cumulative Discharge @ 1E4 yrs (MT1U234)



DISK\$TINA_CCA3:[BF.MJSHORT.JLR]MT1U234R1PM.SRT;3

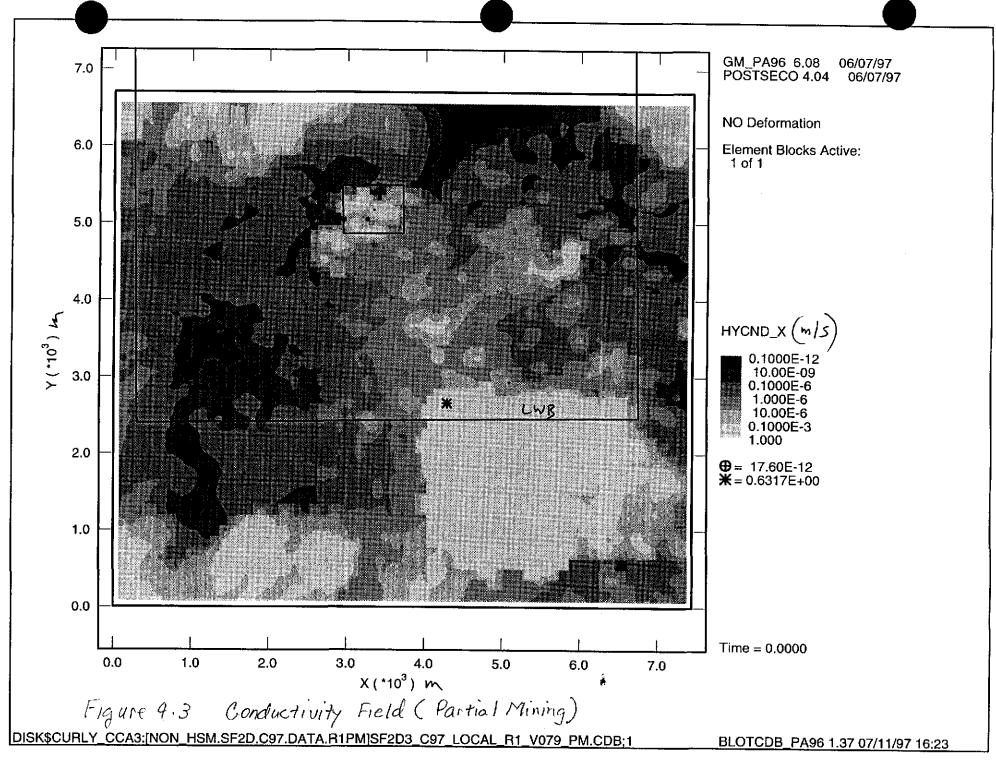
SPLAT_PA96_2 1.02 07/21/97 14:04:01

Cumulative Discharge @ 1E4 yrs (MT1U234)

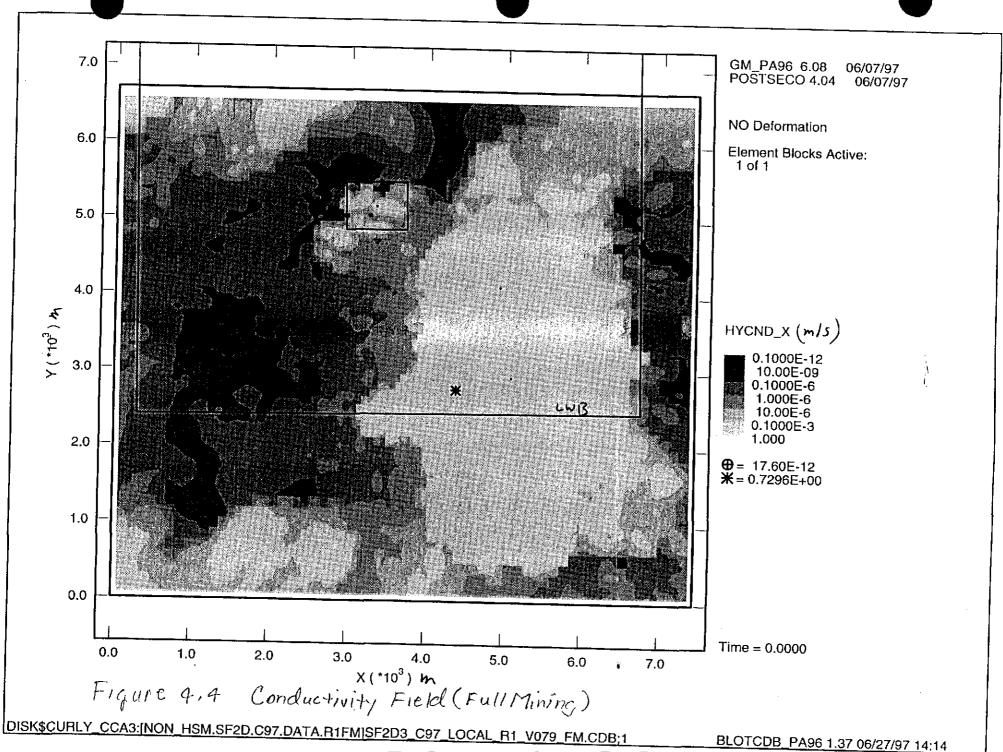


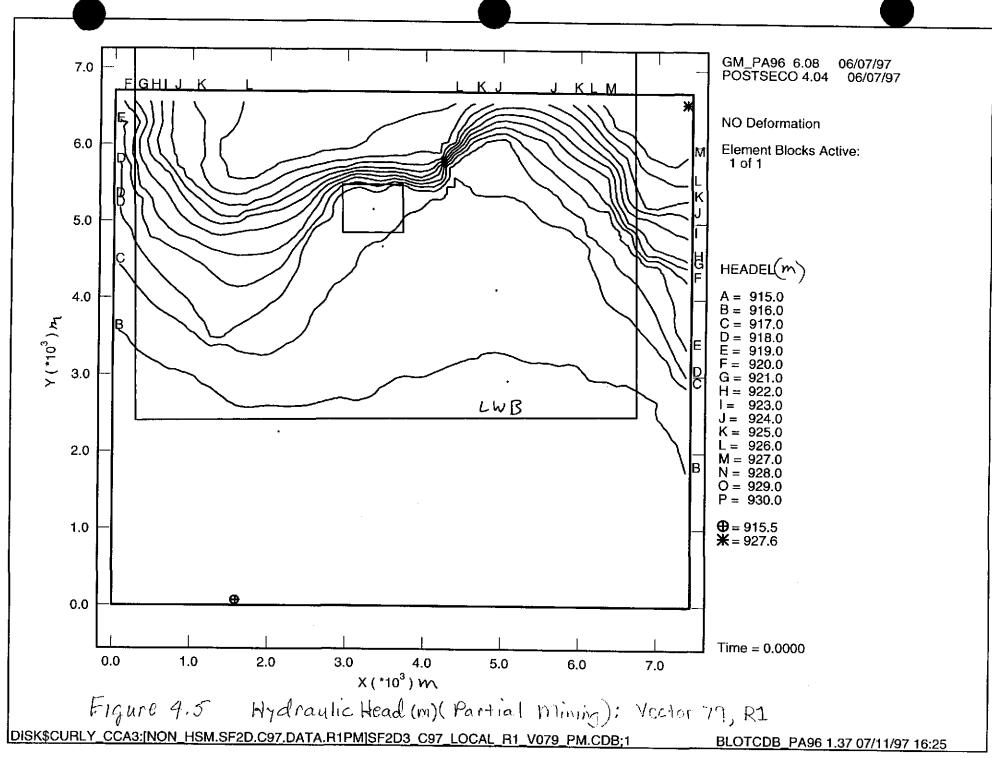
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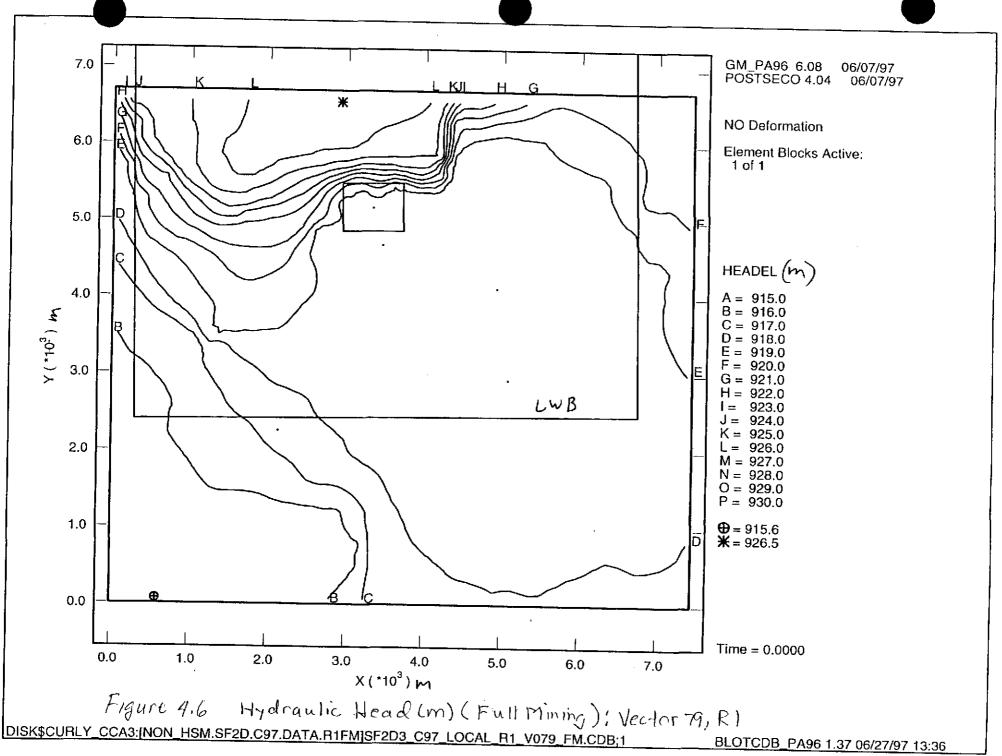


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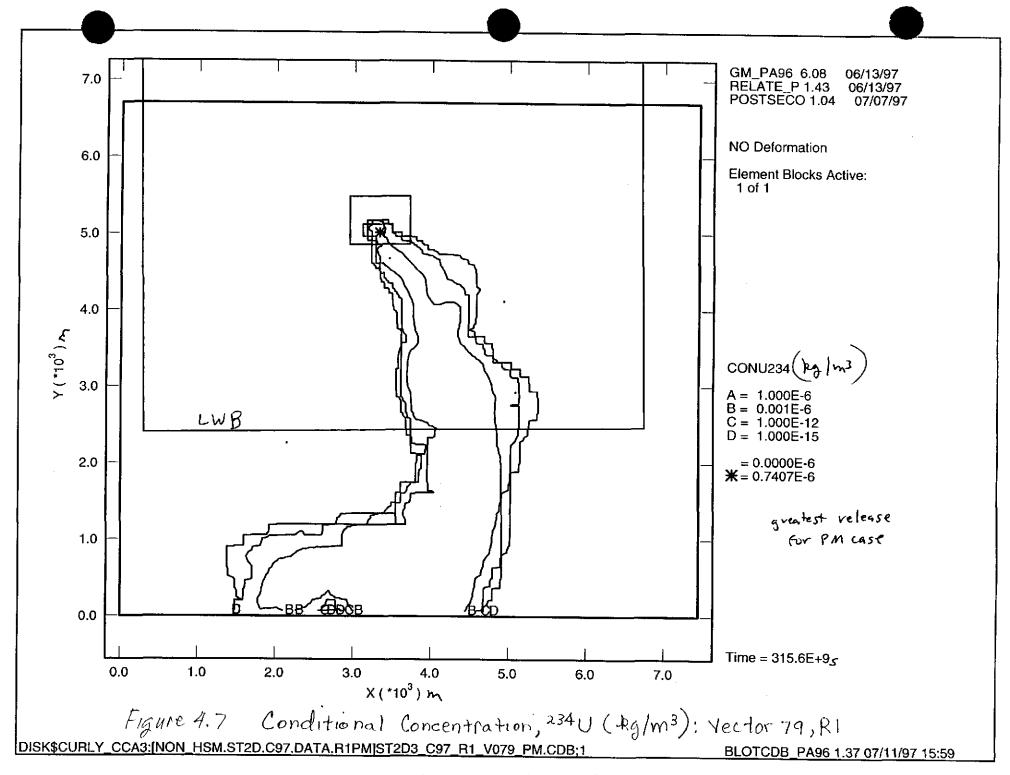




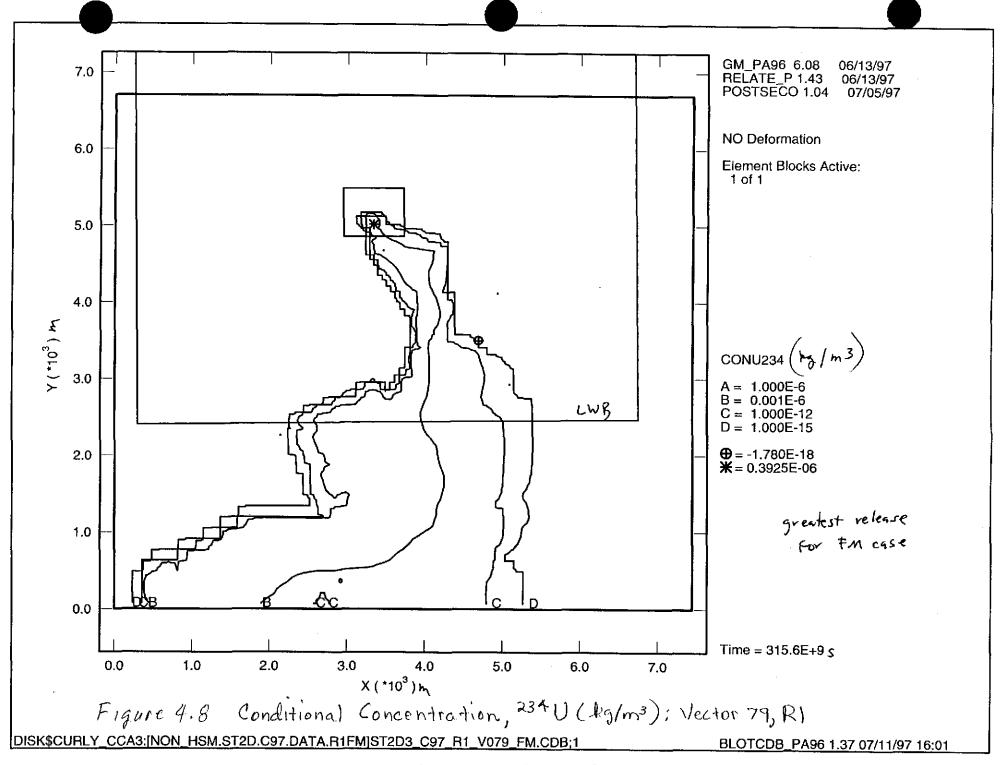
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5.0 CUTTINGS, CAVINGS, AND SPALLINGS CALCULATIONS

This section summarizes differences between the PAVT and CCA direct releases due to cuttings, cavings, and spallings. The cuttings, cavings, and spallings calculations were performed using CUTTINGS_S. Note that in the PAVT, releases due to spallings were calculated using a different approach than the one used in the CCA. The new approach is described below in Section 5.2

The key performance measure for comparing PAVT and CCA direct releases due to cuttings, cavings, and spallings is the volume of waste released at the ground surface. Volume of waste released is passed on to CCDF_GF where this information is combined with activity data and scenario probabilities to compute direct radionuclide releases due to cuttings, cavings, and spallings.

5.1 Changes to Parameters

Changes to input parameters were implemented in CUTTINGS_S as follows:

- (1) The waste shear strength (Pa) was changed from a uniform distribution ranging from 0.05 to 10 to a loguniform distribution ranging from 0.05 to 77 based on expert elicitation (Wang and Larson, 1997).
- (2) The drill string angular velocity (rad/s) was changed from a constant value of 7.8 to cumulative distribution ranging from 4.2 to 23.0 with a mean value of 7.77.
- (3) The new approach used to calculate spallings volumes did not require values for diameter of solid particles and gravitational effectiveness factor. In the CCA, particle diameter was sampled from a loguniform distribution ranging from 4.0E-5 to 0.2 m and gravitational effectiveness factor was sampled from a uniform distribution ranging from 1.0 to 18.1.

5.2 Changes to Model

The following approach was used for calculating releases due to spallings in the PAVT (Change Control Form, WPO #45969). Volumes of waste released due to spallings were calculated by sampling a probability distribution for spallings volume. If the repository pressure exceeded 8 MPa at the time of intrusion, the sampled spallings volume was used as a spallings release. Spallings volume was represented by a uniform distribution ranging from 0.5 to 4.0 m³.

5.3 Impact of Changes on Model Results

Volumes of material released due to cuttings, cavings, and spallings were determined for the following conditions:

- (1) An initial intrusion at 100, 350, 1000, 3000, 5000, or 10000 years after closure for undisturbed conditions (designated scenario S1);
- (2) An initial E1 intrusion at 350 years followed by a second intrusion at 550, 750, 2000, 4000, or 10000 (designated scenario S2);
- (3) An initial E1 intrusion at 1000 years followed by a second intrusion at 1200, 1400, 3000, 5000, or 10000 years (designated scenario S3);
- (4) An initial E2 intrusion at 350 years followed by a second intrusion at 550, 750, 2000, 4000, or 10000 years (designated scenario S4);
- (5) An initial E2 intrusion at 1000 years followed by a second intrusion at 1200, 1400, 3000, 5000, or 10000 years (designated scenario S5).

For the S1 scenario, spallings calculations were performed for intrusions into both upper and lower waste panels. For scenarios S2 through S5, releases were calculated for two cases for each of the second intrusion times: (i) intrusion into the same waste panel as the first intrusion; and (ii) intrusion into a different waste panel than the first intrusion. Intrusion times 200 and 400 years after the initial time (i.e., 550 and 750 years for an initial intrusion at 350 years, and 1200 and 1400 years for an initial intrusion at 1000 years) were selected to give results just before and after the borehole plugs are assumed to fail. Wider time intervals were used at later times because gas pressure tends to change rather slowly at later times. The distinction between intrusion into same and different panels was made because of the possible effects of the resistance to flow between waste panels.

Representative release volumes to the accessible environment from cuttings, cavings, and spallings are shown for the PAVT and CCA in Figures 5.1 through 5.10. Results are only presented for an S1 scenario with an intrusion into the lower repository region at 10,000 years and an S2 scenario with the second intrusion at 10,000 years. Tabulated results for scenarios S1 (lower) and S2 through S5, all with an intrusion at 10,000 years are provided in Appendix E. In addition, box plots showing volume removed and normalized release (EPA units) for all conditions are provided in Appendix E in Figures E.1 through E.12 (for the PAVT) and Figures E.13 through E.24 (for the CCA).

Cuttings and cavings releases for the scenario S1 (replicate 1) 10,000-year intrusion are shown in Figure 5.1 (for the PAVT) and 5.2 (for the CCA). Cuttings and cavings results for other scenarios and intrusion times were the same because cuttings and cavings volumes are not influenced by repository conditions at the time of intrusion and are therefore scenario independent. Cuttings and cavings volumes depend only on sampled parameters such as waste shear strength and drill string angular velocity. Statistical measures of PAVT and CCA cuttings and cavings release volume are shown in Table 5.1. Releases for the PAVT range from approximately 0.3 to 3.9 m³. Releases for the CCA range from approximately 0.4 to 2.9 m³. The PAVT results show a much larger number of releases greater than 1.0 m³ (36 versus 7) and greater than 2.0 m³ (16 versus 1). The uncertainty in the volume of waste removed by cuttings and cavings was determined by the waste shear strength parameter TAUFAIL (Figures 5.3 and 5.4). In the PAVT, the range of TAUFAIL values was increased and the distribution was

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changed from a uniform to loguniform distribution. The impact of the higher maximum TAUFAIL value resulted in more small releases while the impact of converting the distribution to loguniform resulted in more large releases (more TAUFAIL values near zero were sampled). Also note that the PAVT curve is less smooth than the CCA curve; this behavior is likely due to the fact that the drill string angular velocity was sampled in the PAVT whereas it was a fixed value in the CCA.

Representative spallings release volumes are shown in Figures 5.5 and 5.6. Spallings releases occur only if the repository pressure exceeds 8 MPa at the time of intrusion. Spallings releases in both the PAVT and the CCA range from 0.0 m to 4.0 m³. In the CCA, there were two distinct groupings of releases with no releases in the region from 2.4 to 3.2 m³. In the PAVT, releases were spread uniformly over the range of releases because the volumes were sampled from a uniform distribution (see Section 5.2). For scenario S1, repository pressures were similar in the PAVT and CCA, therefore, spallings volumes removed were also similar (see Figures 5.5 and 5.6 and Table 5.1). For the disturbed scenarios (S2 and others), there were more repository pressures greater than 8 MPa in the PAVT than in the CCA resulting in many more vectors which produced spallings volume releases. The increased spallings releases (volume removed and normalized release) in the PAVT are evident in the statistical comparison in Table 5.2 which shows that the mean and 90th percentile values were much higher in the PAVT than in the CCA.

The combined impact of cuttings, cavings, and spallings for scenarios S1 and S2 are shown in Figures 5.7 through 5.10. In scenario S1, total release volumes in the PAVT range from 0.3 to 6.6 m³ (Figure 5.7) compared to values in the CCA that range from 0.4 to 4.6 m³ (Figure 5.8). In the disturbed scenario S2 (as well as in the other disturbed scenarios), the PAVT release volumes (Figure 5.9) were also larger than the CCA volumes (Figure 5.10) due to the larger cuttings and cavings releases. In addition, there were more PAVT vectors with releases, corresponding to vectors with repository pressures greater than 8 MPa.

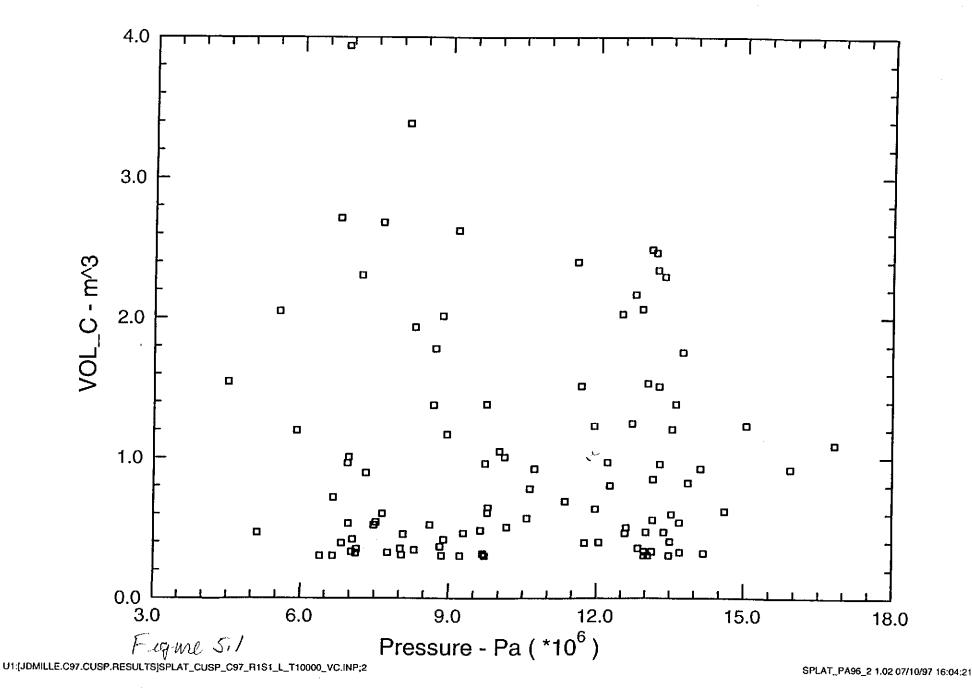
Table 5.1. 10th Percentile, Median, Mean, 90th Percentile, and Maximum Output Variable Values from the PAVT and CCA Simulations for Scenario S1 (initial E2 intrusion at 10,000 years)

Output Variable Description	Time	PAVT Simulation (R1)					CCA Simulation (R1,R2, R3 combined)					
	(yrs)	10th	Median	Mean	90th	Max.	10th	Median	Mean	90th	Max	
Cuttings and Cavings Volume (m³)	10000	0.32	0.67	1.0	2.3	3.9	0.43	0.51	0.60	0.87	2.9	
Spallings Volume (m³)	10000	0.0	1.6	1.7	3.5	4.0	0.0	2.1	2.1	3.7	3.9	
Spallings Release (EPA units)	10000	0.0	0.0072	0.0074	0.015	0.018	0.0	0.0093	0.0091	0.016	0.017	

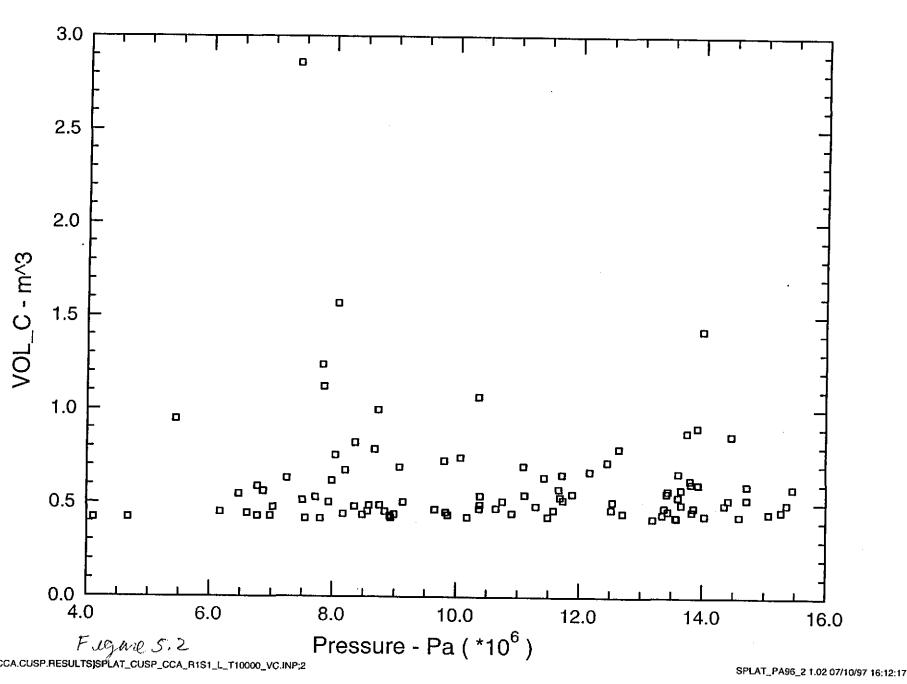
Table 5.2. 10th Percentile, Median, Mean, 90th Percentile, and Maximum Output Variable Values from the PAVT and CCA Simulations for Scenario S2 (E1 intrusion at 350 yrs, E2 intrusion at 10,000 years, same panel)

Output Variable Description	Time	PAVT Simulation (R1)					CCA Simulation (R1, R2, R3 combined)					
	(yrs)	10th	Median	Mean	90th	Max.	10th	Median	Mean	90th	Max.	
Cuttings and Cavings Volume (m³)	10000	0.32	0.67	1.0	2.3	3.9	0.43	0.51	0.60	0.87	2.9	
Spallings Volume (m³)	10000	0.0	0.0	1.2	3.3	4.0	0.0	0.0	0.19	0.0	3.7	
Spallings Release (EPA) units	10000	0.0	0.0	0.0051	0.015	0.018	0.0	0.0	0.0009	0.0	0.016	

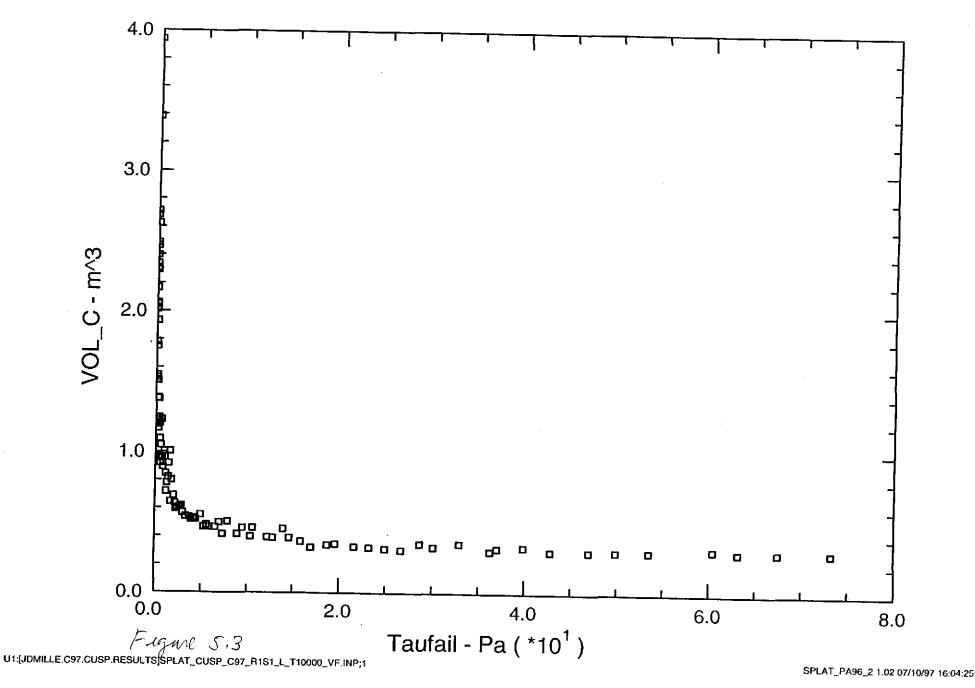




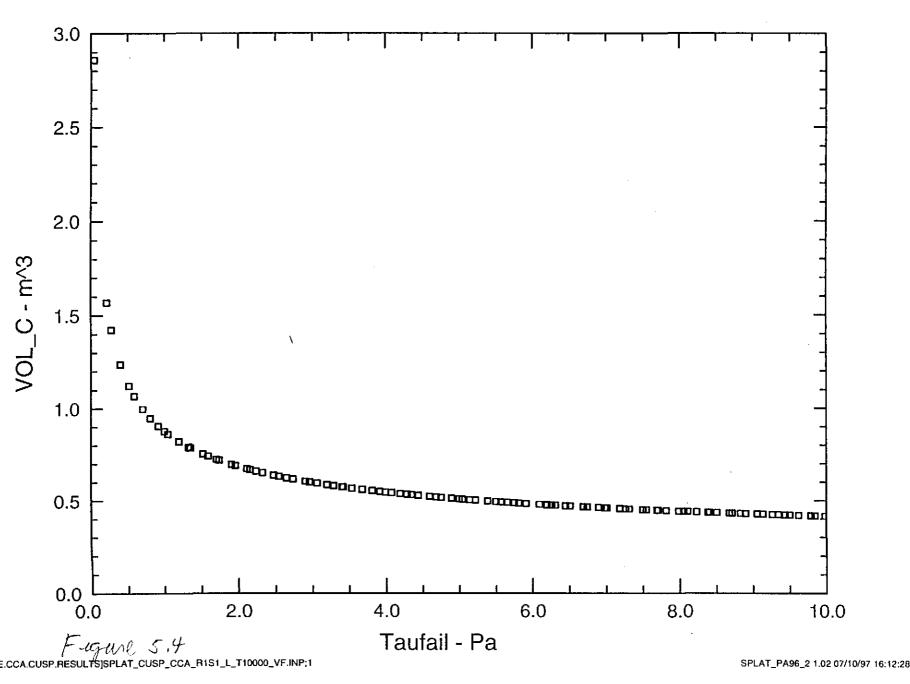
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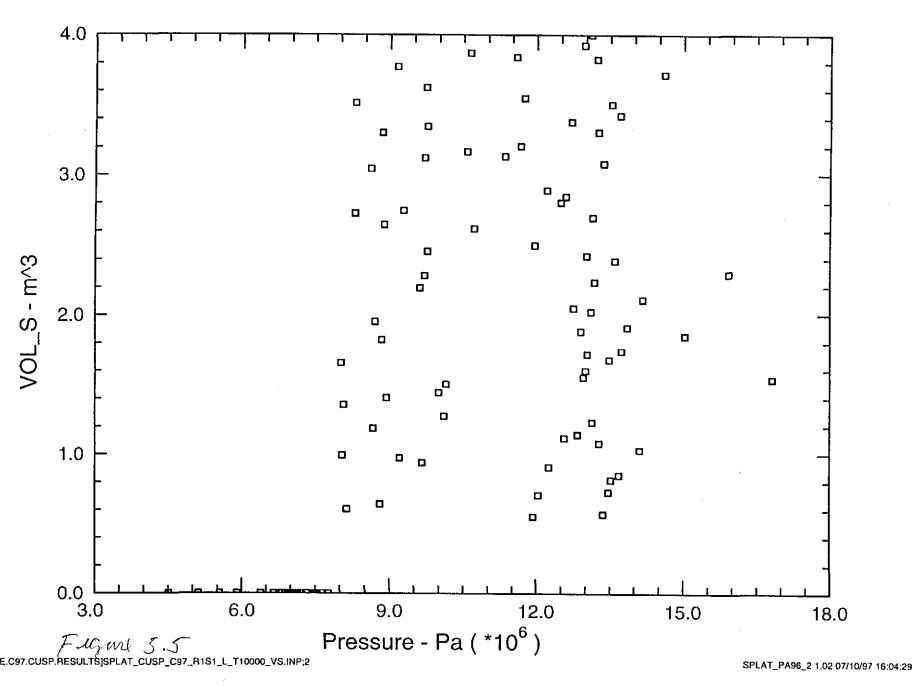




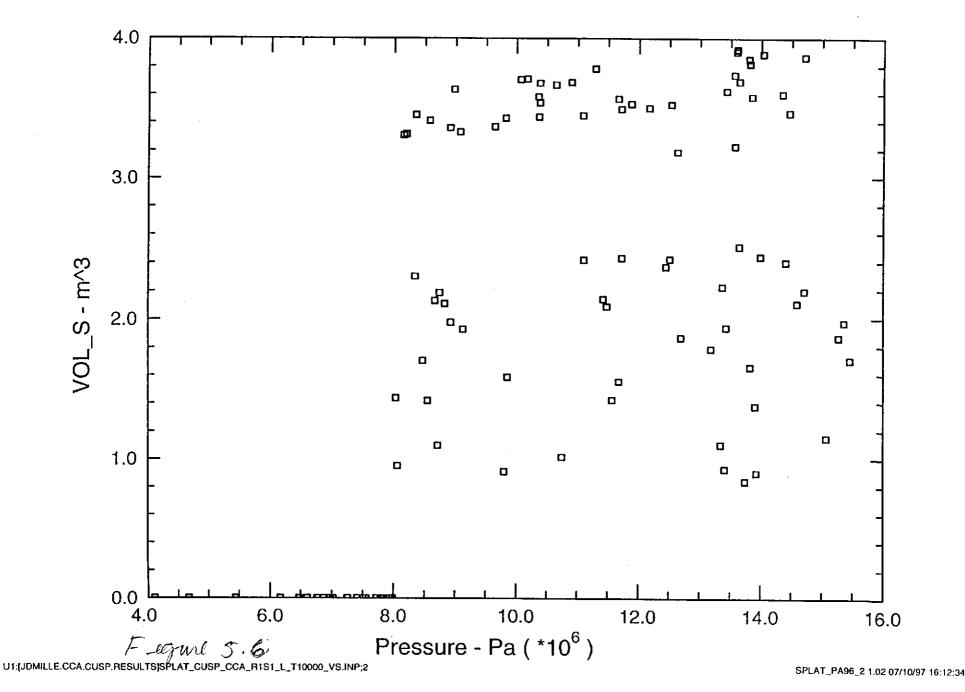
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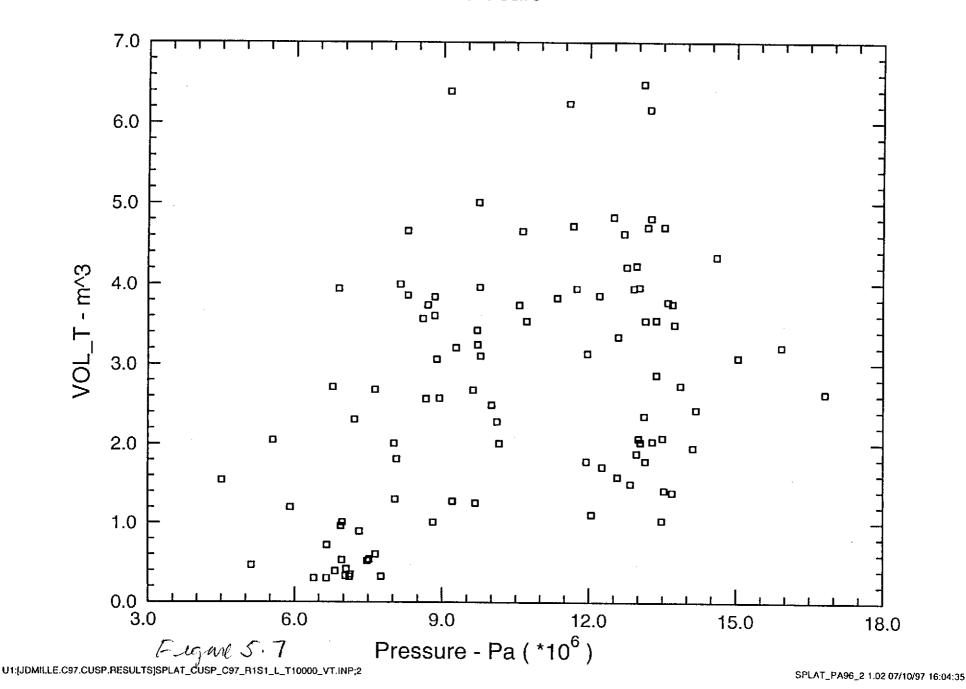




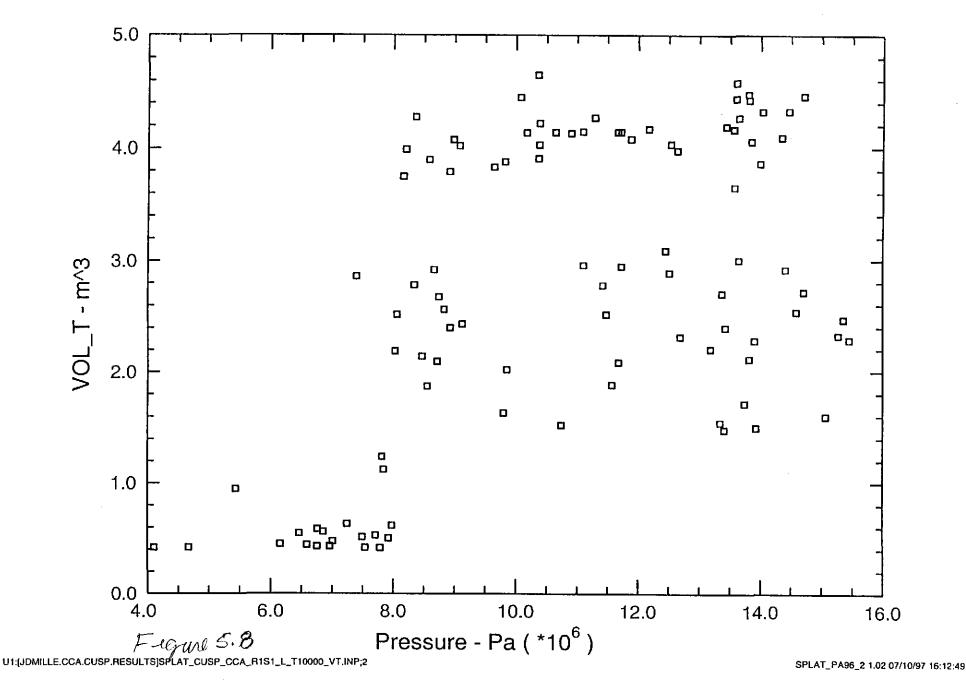
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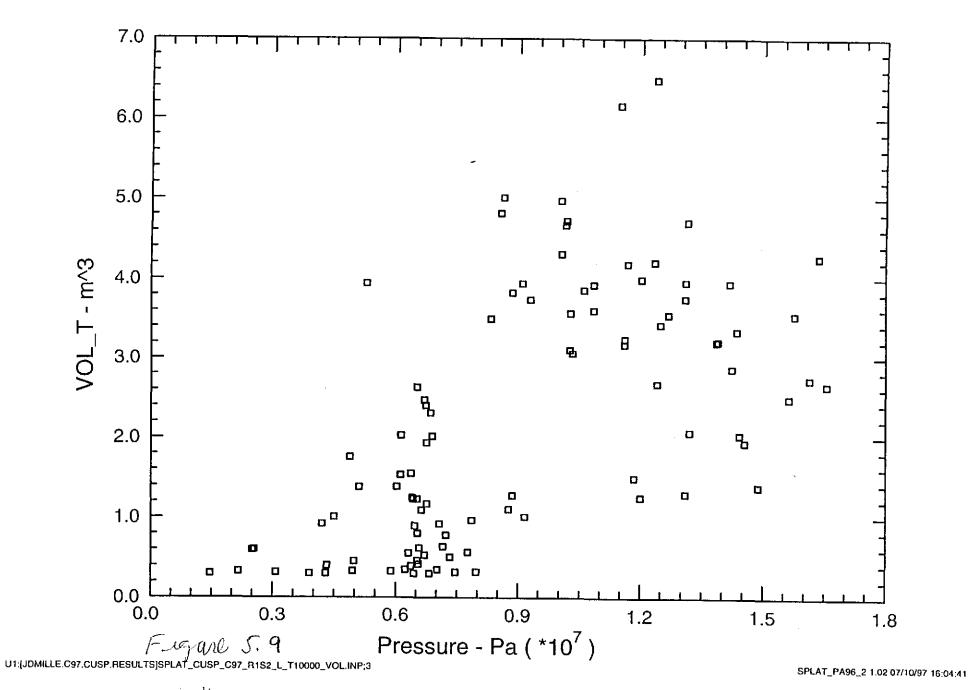
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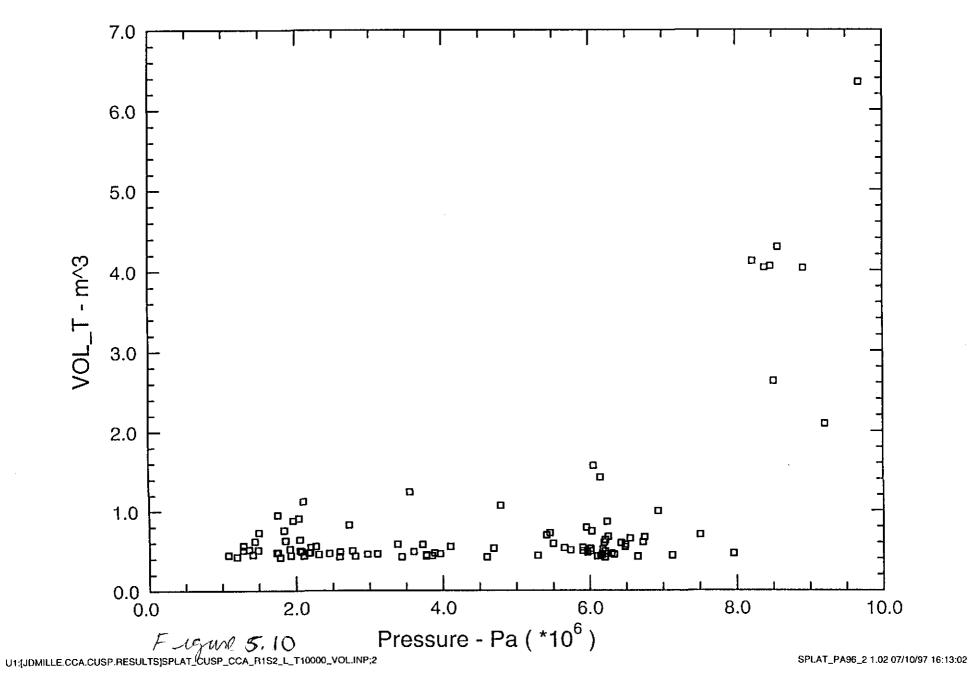
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SNL WIPP PA: CUSP (C97 R1 L)



SNL WIPP PA: CUSP (CCA R1 L)



6.0 DIRECT BRINE RELEASE CALCULATIONS

This section summarizes differences between the PAVT and CCA direct brine release (DBR) calculations. Note that in the CCA, DBR was sometimes referred to as blowout. In these calculations, the release of brine to the surface via an intruding borehole was predicted by using BRAGFLO to model short-term flow in the repository. Repository features such as panel closures and pillars were considered in the analysis. The key performance measure for comparing PAVT and CCA direct brine release results is the volume of brine released at the surface within a time period of up to eleven days.

6.1 Changes to Parameters

The following changes to input parameters were implemented in the BRAGFLO DBR analysis:

- Waste permeability was increased from a constant value of $1.7 \times 10^{-13} \text{ m}^2$ to a constant value of $2.4 \times 10^{-13} \text{ m}^2$.
- (2) DRZ log permeability (m²) was changed from a constant value of -15.0 to a uniform distribution ranging from -19.4 to -12.5 with a mean and median of -15.95.

Note that these parameter changes were specified in Section 2.1.

6.2 Changes to Model

In the CCA, the DBR conceptual model represented the DRZ permeability and porosity using a constant DRZ permeability value of 10^{-15} m² and a porosity value slightly enhanced over the intact halite value, $\phi_{DRZ} = \phi_{halite} + 0.0029$. The intact halite porosity was sampled from a cumulative distribution ranging from 0.001 to 0.03 with a median value of 0.01. These values were assigned to both the DRZ region surrounding the repository and the pillars in the repository. Because the DRZ grid volumes in the DBR and Salado grids were different, the porosity value for the DBR grid was adjusted so that pore volume of the DRZ was conserved. In the PAVT, the pillars in the repository were assigned the initial sampled value of DRZ permeability. Further, the permeability and porosity of the DRZ surrounding the repository were assigned volume-averaged permeability and porosity values of the DRZ at the time of intrusion. As in the CCA, the DRZ porosity was adjusted to account for the different grid volumes. Note that the DRZ permeability and porosity were time dependent because the DRZ was allowed to fracture under the same conceptual model as Marker Beds 138 and 139 (for further discussion see Section 2 and Appendix A).

For the PAVT, a code change was implemented in BRAGFLO, Version 4.10, to allow it to be used for DBR calculations in addition to Salado flow calculations (Change Control Form #45223). In the CCA, a separate code, BRAGFLO_DBR was used for DBR calculations.

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6.3 Impact of Changes on Model Results

Direct brine releases may occur when a future driller penetrates the WIPP and contaminated brine is unknowingly brought to surface during the drilling process. These releases are not specifically accounted for in the CUTTINGS_S code, as that code only calculates the solids removed during the drilling process. Certain conditions must exist within the waste in order for contaminated brine to flow directly to the surface during a drilling intrusion:

- Pressure in the waste must be greater than that exerted by the column of drilling mud that penetrates a waste panel. Drillers in the Delaware Basin currently use a salt saturated mud while drilling through the Salado, with a specific gravity of 1.23 (WP#40520). This corresponds to 7.7 MPa (which is the conversion of specific gravity of the brine to an equivalent pressure at the depth of the repository horizon), which is the minimum pressure needed to overcome a static column of drilling mud. Additional pressure is created in the wellbore due to frictional forces associated with the fluid flow up the annular space between the drill string and open hole (the assumed flow regime for direct releases). Therefore, a pressure of ~8 MPa is needed in the waste panel for fluids to flow into the intrusion borehole under dynamic flow conditions.
- There must be mobile brine present in the waste panels to flow to the surface. Corrosion and biodegradation processes consume brine and produce gas, and it is possible for the brine volume in the waste to drop below its "mobile" (residual) saturation. It is possible for gasonly flows to occur up a drill hole, but these flows are only of concern for the solids releases (spallings).

Direct brine releases were calculated for the same repository conditions (scenarios and intrusion times) that were used in the cuttings, cavings, and spallings calculations (Section 5.3), resulting in a total of 5200 DBR calculations (2600 up dip and 2600 down dip) for PAVT replicate 1. The pressure and saturation time-histories from the 10,000 year BRAGFLO PAVT realizations provided the basic input needed for the direct brine release calculations. The pressure and saturation at specified times for each consequence furnished the initial and boundary conditions needed to run the separate repository scale BRAGFLO model to determine the volumes of direct brine releases to the surface. The model assumed no-flow boundary conditions beyond the footprint of the waste region for the (several day) flow period of direct releases (i.e., there is no connection to the surrounding geology). All relevant flow parameters (permeability, porosity, characteristic curves, etc.), both sampled and unsampled, were the same as those used for the 10,000 year BRAGFLO models.

In the PAVT replicate 1, nearly as many calculations resulted in brine release as in all three CCA replicates combined (821 vs. 907). The number of calculations that released brine in the PAVT (from the total of 5200) are tabulated by scenario in Table 6.1. This increase in the number of releases was primarily due to the increased repository pressures in the disturbed scenarios and to a lesser extent the increased waste permeability.

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Table 6.1 Summary of PAVT Calculations by Scenario that Produced Direct Brine Releases

Scenario	Dow	vn-Dip	Up-Dip			
	Number of Calculations with Releases	Total Number of Calculations	Number of Calculations with Releases	Total Number of Calculations		
S1	96	600	12	600		
S2	272	500	85	500		
S3	202	500	48	500		
S4	37	500	7	500		
S5	53	500	9	500		
Total	660	2600	161	2600		

Figures 6.1 and 6.2 show how brine releases vary with initial panel pressure for all down-dip intrusion DBR calculations in the PAVT and CCA. Brine release volumes in the PAVT were, in general, larger than release volumes in the CCA. These larger release volumes were due in part to the increased waste permeability. As in the CCA, the PAVT data shows a tendency for releases to increase with increasing pressure. Pressures ranged up to 17 MPa in the PAVT with a maximum release of about 180 m³; in the CCA the maximum release was approximately 55 m³ at a pressure of 15 MPa. In addition, there were many more calculations that released brine in volumes greater than 10 m³ in PAVT replicate 1 than in all three replicates in the CCA.

Statistical measures for direct brine releases (brine volumes and radionuclides) are given in Tables 6.2 and 6.3. Results are presented for a single intrusion into the lower panel of an undisturbed repository (S1) at 5000 and 10000 years (Table 6.2) and for an E1 intrusion at 1000 years (S3) followed by a second intrusion at 1200, 5000, and 10000 years (Table 6.3). Results for all scenarios are given in Appendix F along with box plots of releases (brine volume and EPA units) for the PAVT (Figures F.1 through F.10) and CCA (Figures F.11 through F.20).

Results show that, for the S1 scenario, released brine volumes tended to be slightly larger in the PAVT (Figure F.1) than in the CCA (Figure F.11), but radionuclide releases tended to be smaller in the PAVT (Figure F.6) than in the CCA (Figure F.16). These differences are summarized with a statistical comparison in Table 6.2. The reduced radionuclide releases in the PAVT were due to the reduced solubilities of ²⁴¹Am and ²³⁹Pu in Salado brine.

In the E1 intrusion scenarios (S2 and S3), released brine volumes were much higher (about an order of magnitude on average) in the PAVT (Figures F.2 and F.3) than in the CCA (Figures F.12 and F.13). Corresponding radionuclide releases were slightly larger, on average, in the PAVT at

early intrusion times (Figures F.7, F.8, F.17, and F.18) and moderately larger at later intrusion times. At early time, the higher brine volumes released in the PAVT were counteracted by the lower ²⁴¹Am solubilities in Castile brine. The later time PAVT radionuclide releases were influenced by ²³⁹Pu solubilities in Castile brine; these solubilities were comparable (sometimes larger, sometimes smaller, depending on oxidation state) in the PAVT and CCA. These differences are summarized with a statistical comparison in Table 6.3.

In the E2 intrusion scenarios (S4 and S5), released brine volumes were also about an order of magnitude larger on average in the PAVT (Figures F.4 and F.5) than in the CCA (Figures F.14 and F.15). Corresponding PAVT radionuclide releases were generally slightly larger, and at later times were actually smaller than CCA releases (Figures F.9, F.10, F.19, and F.20). In these scenarios, the larger brine volumes were counteracted by the reduced Salado brine solubilities.

Figures 6.3 and 6.4 show how brine releases vary with initial brine saturation ($Sw_{initial}$) for all down-dip direct brine release calculations. In both the PAVT and CCA, the scatter in the data suggests that generally higher initial brine saturations result in higher brine volume releases with the majority of the larger releases occurring at saturations between 0.7 and 0.8.

Figures 6.5 and 6.6 show how brine releases vary with initial panel pressure for all up-dip direct brine release calculations. Several more calculations release brine in PAVT replicate 1 than in the three replicates of the CCA. Again, as in the down-dip calculations, the releases were much larger in the PAVT with the maximum value of about 150 m³ near 16 MPa, whereas the maximum release in the CCA results was 32 m³ at 11 MPa.

Figures 6.7 and 6.8 show how brine releases vary with initial brine saturation (Sw_{initial}) for all updip direct brine release calculations. As with the down-dip calculations, higher initial brine saturations generally resulted in higher brine volume releases.

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Table 6.2. 10th Percentile, Median, Mean, 90th Percentile, and Maximum Output Variable Values from the PAVT and CCA Simulations for Scenario S1 (initial intrusion at time specified in lower panel)

Output Variable	Intrusion Time		CCA Simulation (R1, R2, R3 combined)								
Description	(yrs)	10th	Median	Mean	90th	Max.	10th	Median	Mean	90th	Max.
Brine Volume (m³)	5000	0.0	0.0	3.8	12	93	0.0	0.0	1.0	1.2	28
Release (EPA units)		0.0	0.0	2.1E-4	3.9E-4	1.0E-2	0.0	0.0	7.4E-4	2.9E-4	5.1E-2
Brine Volume (m³)	10000	0.0	0.0	4.0	15	51	0.0	0.0	1.9	5.5	37
Release (EPA units)		0.0	0.0	1.1E-4	3.4E-4	3.5E-3	0.0	0.0	1.0E-3	9.2E-4	5.2E-2

Table 6.3. 10th Percentile, Median, Mean, 90th Percentile, and Maximum Output Variable Values from the PAVT and CCA Simulations for Scenario S3 (E1 intrusion at 1000 yrs followed by a second intrusion at time specified in same panel)

Output Variable	Intrusion Time		PAVI	Simulation	n (R1)		CCA Simulation (R1, R2, R3 combined)					
Description	(yrs)	10th	Median	Mean	90th	Max.	10th	Median	Mean	90th	Max.	
Brine Volume (m³)	1200	0.0	2.5	5.5	15	76	0.0	0.0	0.62	.43	15	
Release (EPA units)		0.0	5.1E-4	1.6E-3	3.5E-3	1.9E-2	0.0	0.0	8.1E-4	3.3E-4	5.8E-2	
Brine Volume (m³)	5000	0.0	0.0	3.7	13	64	0.0	0.0	0.25	0.0	13	
Release (EPA units)		0.0	0.0	1.3E-4	6.2E-4	1.9E-3	0.0	0.0	9.9E-6	0.0	5.6E-4	
Brine Volume (m³)	10000	0.0	0.0	4.0	8.6	100	0.0	0.0	0.18	0.0	11	
Release (EPA units)		0.0	0.0	6.3E-5	1.6E-4	1.9E-3	0.0	0.0	3.7E-6	0.0	2.3E-4	



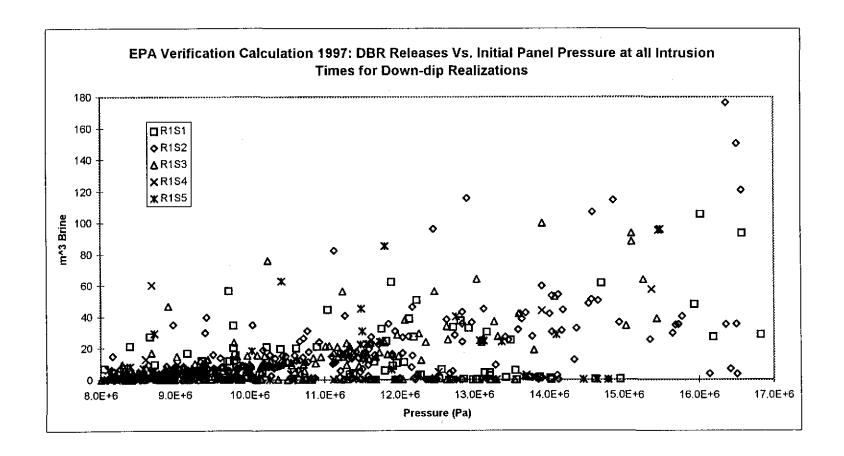
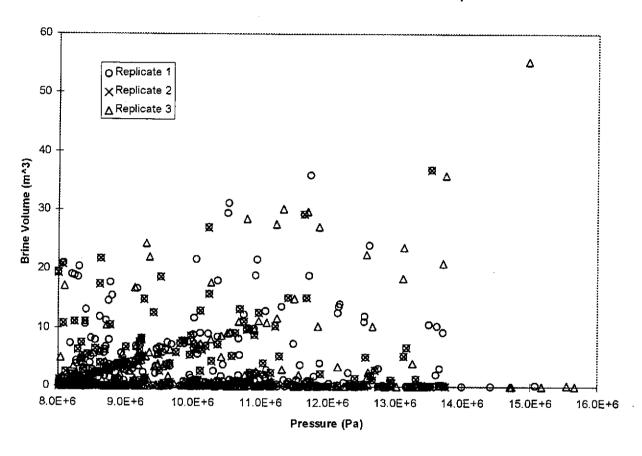


Figure 6.1

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Figure 6.2: Brine Releases vs. Initial Panel Pressure: All Down-dip Realizations (CCA)

Brine Releases vs Initial Panel Pressure: All Down-dip Vectors





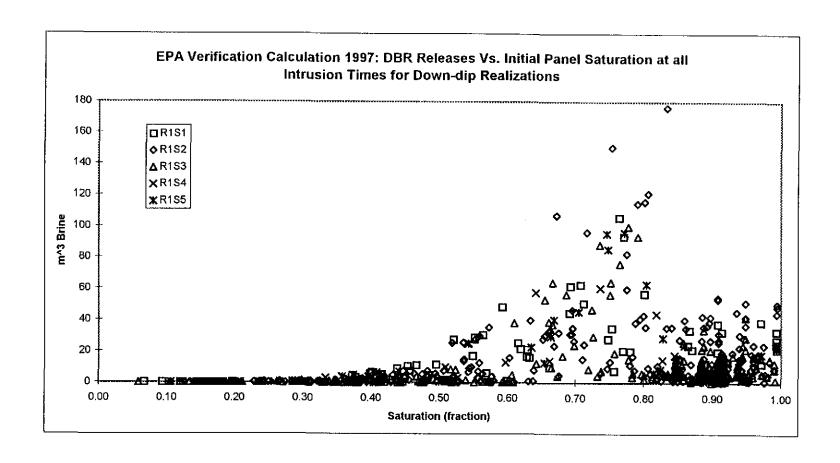
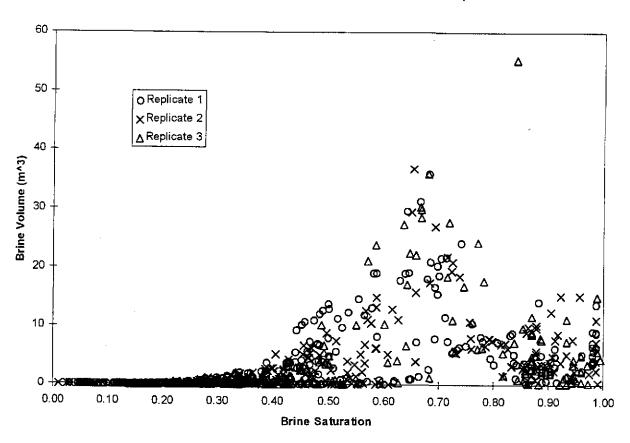


Figure 6.3

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Figure 6.4: Brine Releases vs Initial Panel Saturation: All Down-dip Realizations (CCA)







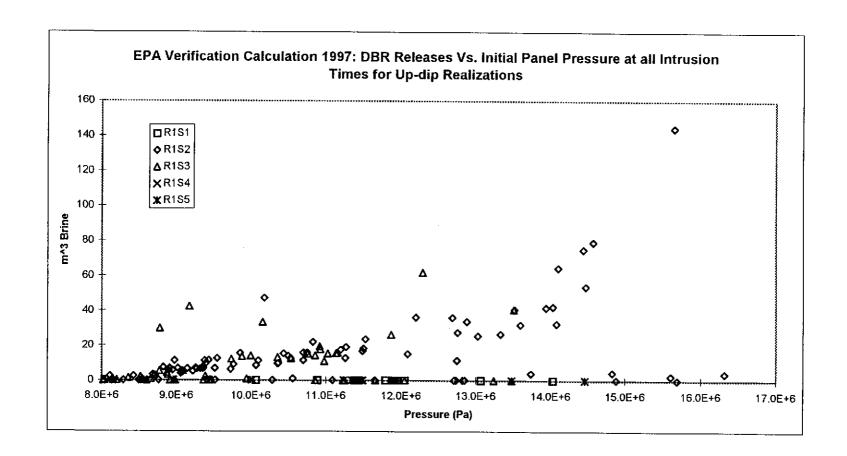


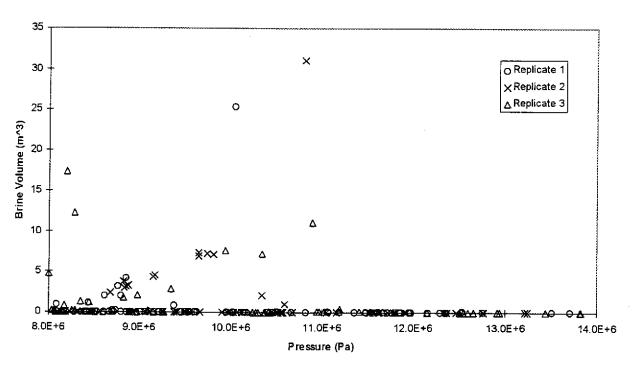
Figure 6.5

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Figure 6.6: Brine Releases vs Initial Panel Pressure: All Up-dip Realizations (CCA)

Brine Releases vs Initial Panel Pressure: All Up-dip Vectors





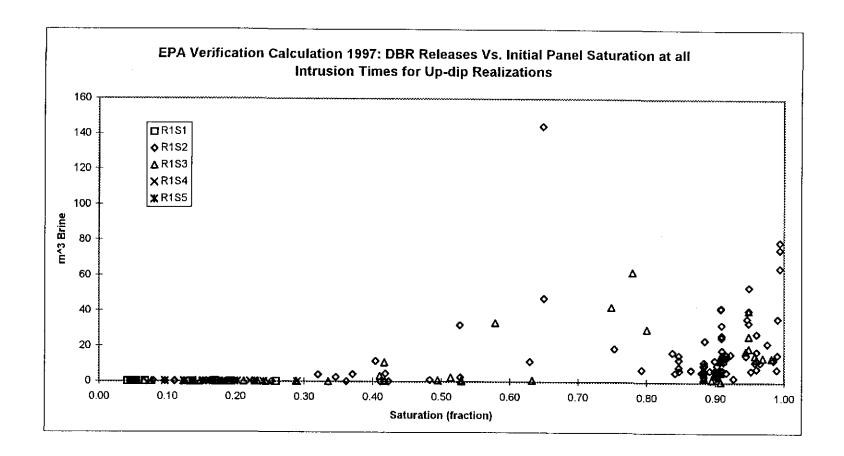


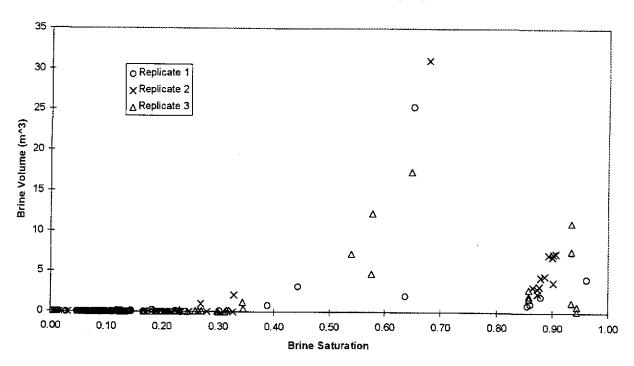
Figure 6.7

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Figure 6.8: Brine Releases vs Panel Saturation: All Up-dip Realizations (CCA)





Figur 6.8

7.0 CCDF CALCULATIONS

This section summarizes differences between the CCDFs resulting from the PAVT and CCA simulations. The CCDFs were calculated using a three step process: (1) determine futures (random sequences of events that may occur over the next 10,000 years); (2) estimate the radionuclide releases resulting from these futures; and (3) construct a CCDF for each future. The computer code CCDF_GF was used to perform these three steps. CCDF_GF uses the results of calculations performed in Sections 2 through 6 to produce the CCDFs.

The key performance measure for comparing PAVT and CCA results is summed normalized releases in EPA units as compared with EPA limits.

7.1 Changes to Parameters

The CCDF calculations were affected by all of the parameter changes made to the other codes (see Sections 2 through 6) which impacted radionuclide releases to the accessible environment. Only one CCDF_GF parameter was changed for the PAVT calculations. Parameter PBRINE was changed from a constant value of 0.08 to a uniform distribution ranging from 0.01 to 0.60. PBRINE is the probability that an intrusion borehole will intersect a brine reservoir.

7.2 Changes to Model

The model implementation was enhanced to include releases from the Culebra and Salado interbeds at the LWB. For the PAVT calculations, these releases were not significant but they were non-zero. The CCA only included direct releases from the intrusion borehole because the other releases were zero. A second change to the model implementation involved the number of intrusions required to deplete a brine reservoir. In the CCA, the number of intrusions was correlated with sampled reservoir volume and varied from 2 to 10 intrusions. For the PAVT, brine reservoirs were assumed not to deplete because of the larger sampled brine reservoir volumes (see Section 2.1). A third change to the model implementation was related to Passive Institutional Controls (PICs). The PAVT does not take credit for PICs whereas for the CCA, the impact of PICs was included.

There were no changes to the computational model which had any significant impact on the results.

7.3 Impact of Changes on Model Results

Differences between the CCDFs from the PAVT and CCA calculations are due to a combination of the following factors:

 Cuttings and cavings releases were higher for all scenarios due to a change in the waste shear strength distribution.

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- Spallings releases were slightly higher and more frequent for all scenarios due to higher repository pressures at the time of intrusion.
- Direct brine releases were higher due to higher repository pressures.
- The change in PBRINE resulted in a higher probability of futures containing an E1 intrusion than in the CCA.
- Culebra releases across the LWB were higher due to more small sampled k_d's but were still small relative to direct releases.
- For E1 intrusion scenarios at early intrusion times, radionuclide releases up the borehole to the Culebra were slightly larger, on average, than in the CCA. At later E1 intrusion times, releases were moderately larger than in the CCA. These results were due to greater flow up the borehole combined with similar and/or lower solubilities.
- For E2 intrusion scenarios, releases up the borehole to the Culebra were less by a factor of about 100 due to lower flow up the borehole and lower solubilities.
- Salado interbed releases to the LWB were still insignificant.

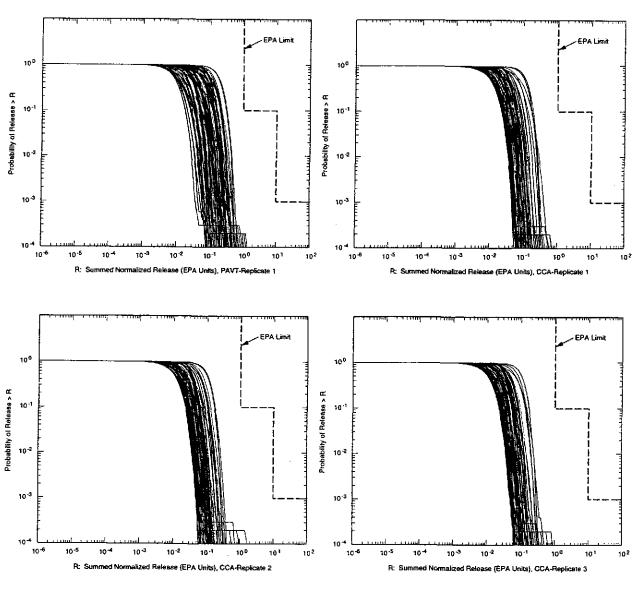
A summary of CCDF results is presented in this section. Additional CCDF plots providing more detail about releases are provided in Appendix G. Figure 7.1 compares the family of CCDFs for summed (combined total contributions from all release mechanisms) normalized releases from PAVT replicate 1 with those from each of the three CCA replicates. All of the CCDFs have a similar lower bound, with the PAVT family of CCDFs containing several curves with total releases a factor of 2 or 3 higher than in the CCA.

Figures 7.2 through 7.6 show mean normalized releases for the PAVT and the CCA. Means for PAVT replicate 1 and each of the three CCA replicates as well as an overall CCA mean are shown. The summed releases for the PAVT mean CCDF are a factor of 2 to 3 larger than the CCA values for all probabilities of exceedance (Figure 7.2). For a specific release, the probability of exceedance has increased by as much as a factor of 10. These increases were primarily due to the increase in cuttings releases (Figure 7.3). Other contributors to total summed releases include spallings (Figure 7.4), direct brine release (Figure 7.5), and Culebra (Figure 7.6) releases. Note that mean CCDFs for all of these components of the summed normalized releases are greater (to the right) of the CCA mean CCDFs. The absence of PICs and the change in PBRINE were also minor contributors to the change in releases. Even with the slightly higher releases, the PAVT mean CCDF does not exceed or come within an order of magnitude of the EPA Limit.

Figure 7.7 shows the relative contributions of each release mechanism to the summed release for both the PAVT and the CCA. Releases from each of the CCA replicates are similar and only

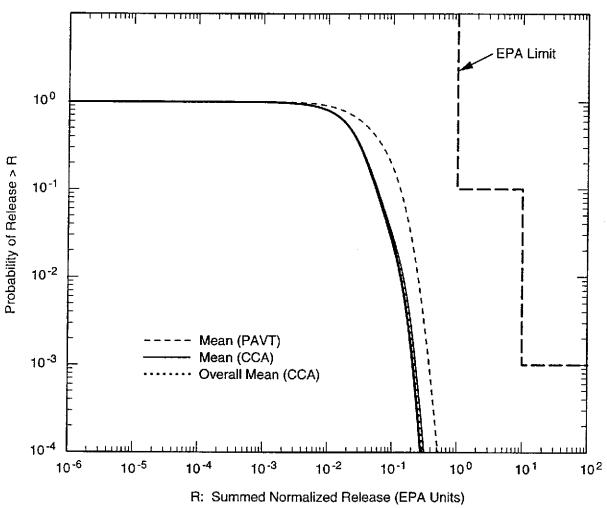
were the most important contributors to the total mean CCDF. Spallings also made an important contribution to the total CCDF, particularly in the CCA. Direct brine releases were slightly more important in the PAVT than in the CCA, but have only a minor effect on the total CCDF. Subsurface releases due to Culebra groundwater transport were not significant. Salado interbed and Dewey Lake releases were also negligible and are not shown.

Figure 7.8 shows additional statistical information about total summed CCDFs for PAVT replicate 1 and the three CCA replicates. This Figure shows CCDFs representing the mean, median, 10th, and 90th percentiles for each replicate.



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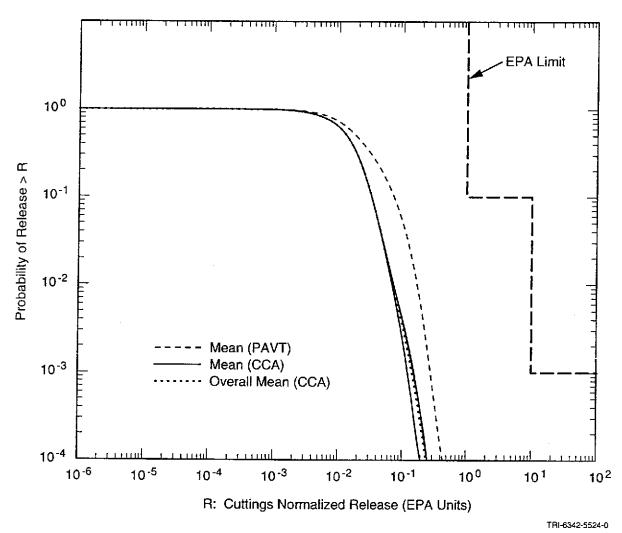
Figure 7.1 Distribution of CCDFs for Normalized Radionuclide Releases to the Accessible Environment from the WIPP



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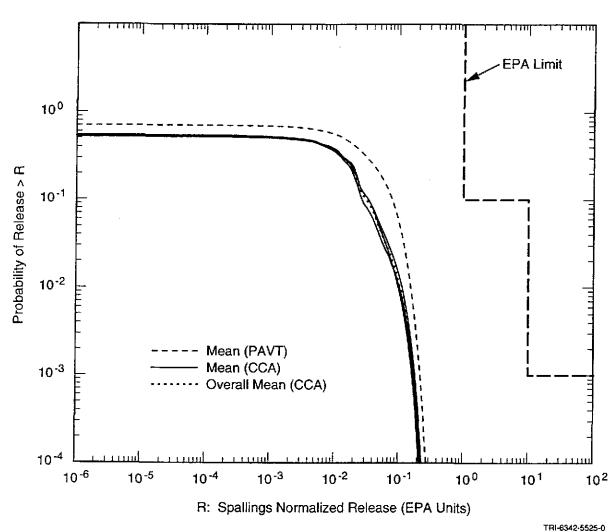
Note: Four CCA CCDFs are shown, including three individual mean CCDFs calculated for each of the three distributions of CCDFs calculated for the three replicates and an overall mean CCDF that is the arithmetic mean of the three individual mean CCDFs.

Figure 7.2 Mean CCDFs for Summed Normalized Radionuclide Releases to the Accessible Environment



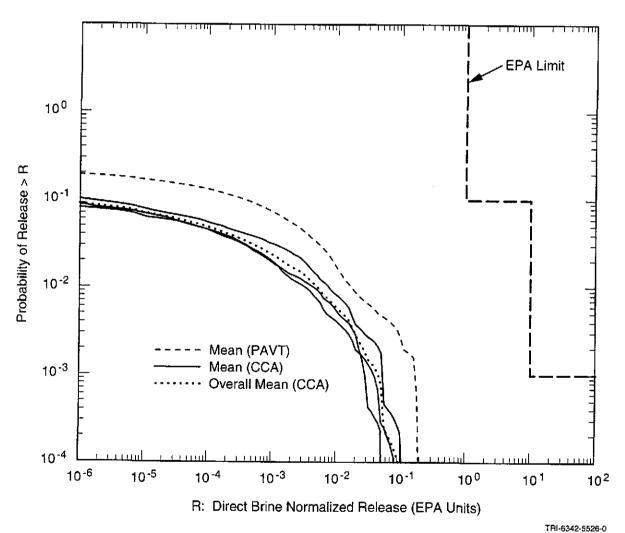
Note: Four CCA CCDFs are shown, including three individual mean CCDFs calculated for each of the three distributions of CCDFs calculated for the three replicates and an overall mean CCDF that is the arithmetic mean of the three individual mean CCDFs.

Figure 7.3 Mean CCDFs for Cuttings Normalized Radionuclide Releases to the Accessible Environment



Note: Four CCA CCDFs are shown, including three individual mean CCDFs calculated for each of the three distributions of CCDFs calculated for the three replicates and an overall mean CCDF that is the arithmetic mean of the three individual mean CCDFs.

Figure 7.4 Mean CCDFs for Spallings Normalized Radionuclide Releases to the Accessible Environment



Note: Four CCA CCDFs are shown, including three individual mean CCDFs calculated for each of the three distributions of CCDFs calculated for the three replicates and an overall mean CCDF that is the arithmetic mean of the three individual mean CCDFs.

Figure 7.5 Mean CCDFs for Direct Brine Release Normalized Radionuclide Releases to the Accessible Environment

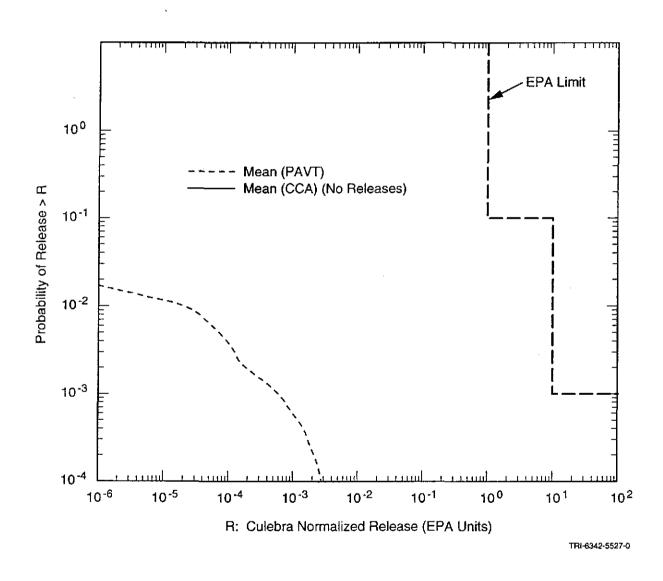


Figure 7.6 Mean CCDFs for Culebra Normalized Radionuclide Releases to the Accessible Environment

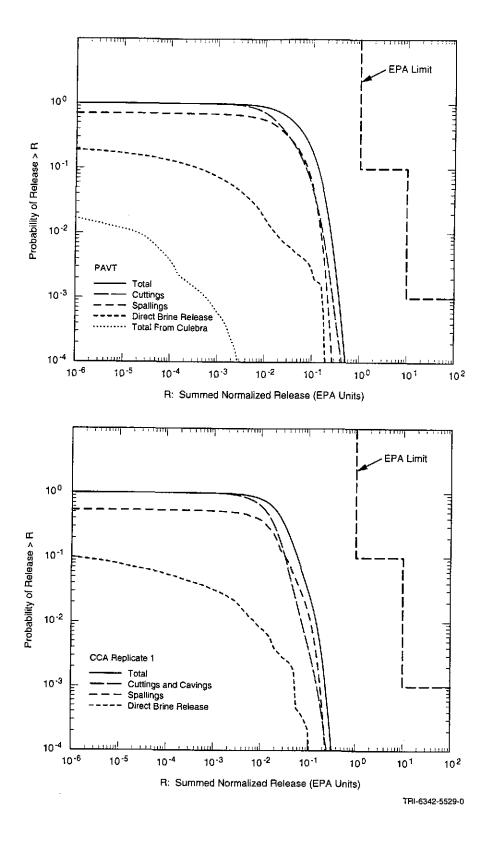
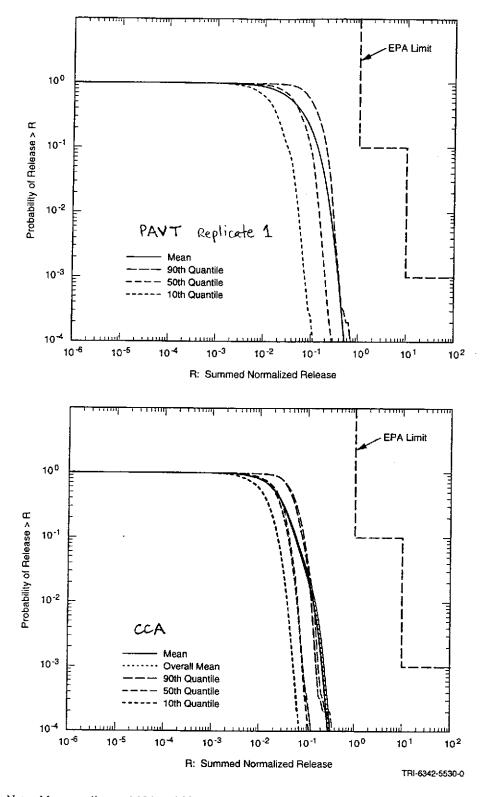


Figure 7.7 Mean CCDFs for Specific Release Modes



Note: Mean, median, and 10th and 90th percentile CCDFs are shown together with the overall mean.

Figure 7.8 Summary CCDFs

8.0 REFERENCES

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APPENDIX A

GAS AND BRINE MIGRATION IN UNDISTURBED AND DISTURBED REPOSITORY SYSTEMS FOR THE PAVT CALCULATIONS

In this Appendix, gas and brine migration modeling results are presented and discussed for undisturbed and disturbed repository performance. For disturbed performance, three representative borehole intrusion scenarios are considered. In the first scenario, the E1 scenario, a borehole penetrates a waste-filled panel and a hypothetical pressurized brine reservoir in the underlying Castile Formation. In the second scenario, the E2 scenario, a borehole penetrates the waste-filled panel only. To examine the impact of different intrusion times, the E1 and E2 scenarios are subdivided into computational scenarios on the basis of two different intrusion times of 350 and 1000 years. In the third scenario, the E2E1 scenario, a borehole penetrates the repository at 1000 years (an E2 intrusion) and a second borehole, drilled at the same location, penetrates the repository and the hypothetical brine reservoir at 2000 years (an E1 intrusion).

In the following sections, results are presented in terms of volume-averaged quantities such as volume-averaged pressure. Volume-averaged pressure is given by forming the product of grid block pressure and grid block volume for each grid block in the region of concern, summing this product up over all grid blocks in the region, and dividing by the bulk volume of the region. All other volume-averaged quantities are computed in the same manner. Cumulative and net flow volumes are also presented. Cumulative flow into a region is defined as the time-dependent flow into a region integrated over time. Cumulative flow out of a region is defined as the time-dependent flow out of a region integrated over time. Net flow into a region is defined as cumulative flow into a region minus cumulative flow out of a region. Similarly, net flow out of a region is cumulative flow out of a region minus cumulative flow into a region.

The following sections describe PAVT replicate 1 results. Corresponding results from CCA replicate 1 are shown in parentheses.

A.1 UNDISTURBED PERFORMANCE

This section examines repository behavior and the flow of brine and gas along two potential pathways for migration of radionuclides in dissolved brine (Figure A.1-1). In the first pathway, brine may migrate through the panel seals or through the disturbed rock zone (DRZ) surrounding the repository to the shaft and then upward toward the Culebra Dolomite Member of the Rustler Formation. The quantity of brine reaching the Culebra is important because transport may then occur laterally in the Culebra toward the subsurface land withdrawal boundary. In the second pathway, brine may migrate from the repository through the DRZ and laterally toward the subsurface land withdrawal boundary within the anhydrite interbeds in the Salado Formation.

Note that of the seven changes to input parameters for the PAVT simulations listed in Section 2.1, only the first three are relevant to undisturbed performance. The final four changes relate to the Castile brine pocket and to intrusion borehole properties. Two additional differences from the CCA simulations of the S1 scenario should be noted: (1) H2 viscosity was changed slightly; and (2) the grid was the same as for disturbed (human intrusion) scenarios. Both of these changes had little or no effect on the results.

A.1.1 Replicate 1 Results and Discussion

A.1.1.1 Repository Behavior

Repository behavior is characterized by interactions between creep closure, fluid flow, and gas generation. Creep closure of excavated regions begins immediately because of excavation induced loading. In the waste disposal region, waste consolidation will continue until backstresses imposed by the compressed waste resist further closure or until fluid pressures become sufficiently high. Pressure in the disposal region is governed by the quantities of brine present in the disposal region, the rates of gas generation, and the ease at which fluids can escape the repository. Depending on material properties and pressure conditions, brine may flow into the disposal region by moving down shafts and through the DRZ and anhydrite layers. Brine contained in the Salado also flows into the waste disposal region because of pressure gradients created by the excavation. As a consequence, significant quantities of gas may be generated by the availability of brine, causing pressures to increase. Brine flow into the repository will be reduced as repository pressure increases, and brine may be expelled from the repository if pressure exceeds brine pressure in the immediately surrounding formation. Brine saturation has to exceed the residual brine saturation in order for brine to be expelled from the repository. Similarly, gas may flow away from the waste into lower pressure areas, which may include disturbed areas surrounding the repository, the interbeds, and the shafts. Gas flow into intact halite rock is not significant because of the high threshold pressure of halite.

Pressures in the waste panel and rest of repository (Figures A.1-2 [GVAR 023] and A.1-3 [GVAR 024]) increase from their initial value of 1 atmosphere. Pressure responses in the experimental and operation regions are nearly equal to those in the waste panel and rest of repository because the permeability of excavated regions, drift and panel seals, and DRZ are high, on the order of 10⁻¹⁵ m². This allows relatively free movement of gas throughout the excavated regions, and equalizes pressures there quickly (relative to the 10,000-year regulatory period). In a few realizations where the DRZ or lower shaft permeability is low, on the order of 10⁻¹⁸ m², the experimental area shows a slower pressure response, however, this behavior does not influence the rest of the repository or the surrounding formations. In many realizations, pressures increase rapidly during the first 500 years. These rapid increases in pressure are caused by a high gas generation rate coupled with creep closure. In these realizations, plastics and rubbers are included in the inventory of biodegradables; this results in a higher net rate of gas generation during the first 1000 years. In some realizations, the pressure reaches a maximum even though gas generation may continue long after the peak pressure is reached. In these realizations, gas is vented out of the waste through the interbeds, shaft, and DRZ fractures since the far-field pressure is lower than the peak pressure in the waste. Also, creep closure is essentially complete by 1000 years, so there are no pressure changes due to repository pore volume changes. In some realizations, the pressure after 10,000 years is higher than the far-field pressure because gas continues to be generated faster than brine and gas can flow out of the waste. In contrast to this behavior, some realizations (#13, #45, #1, #6, #83, #100, #57, near the bottom of the plots) exhibit slowly increasing pressures. In these realizations, pressure increases

during the first 300 - 500 years results primarily from creep closure since there is very little gas generation from corrosion (sampled corrosion rates are among the lowest) and none from biodegradation. The different rates of pressure increase in these cases are largely a result of different anhydrite permeabilities and corresponding inflow rates of brine. The third type of behavior exhibited in Figures A.1-2 [GVAR_023] and A.1-3 [GVAR_024] is a moderately rapid initial rise in pressure. This behavior is a result of creep closure in combination with moderate gas generation rates. At later times, pressures level off in some realizations, indicating that gas generation by microbial degradation has ceased after the cellulose inventory has been exhausted. For most realizations, the cellulose inventory is generally exhausted within 1500 years (Figure A.1-4 [GVAR 002]). Simultaneously, corrosion consumes most of the brine present in the waste, and it also slows down depending on the rate of inflow of brine from the surrounding formations. In several realizations, pressures continue to increase over the full 10,000-year regulatory period. In some of these cases, pressures in excess of the far-field pressure are reached. This behavior is expected when the gas generation rate is relatively low and enough brine is present in the waste or flows in from outside the repository to sustain the corrosion reactions.

A.1.1.1.1 Gas Generation

The rate and amount of gas generation varies significantly, as shown in Figure A.1-5 [GVAR 022]. Among the 100 realizations, the volume of gas generated varies over more than an order of magnitude, from $2.2 \times 10^6 \,\mathrm{m}^3$ to $3.4 \times 10^7 \,\mathrm{m}^3$ (1.5 × 10⁶ m³ to $2.8 \times 10^7 \,\mathrm{m}^3$) of hydrogen, at reference conditions (30 °C, 1.01325 × 10⁵ Pa). Of the total volume of gas generated (Figures A.1-6 [GVAR_017] and A.1-7 [GVAR_020]), corrosion accounts for volumes ranging between 4×10^5 m³ to 2.3×10^7 m³ (5×10^5 m³ to 1.89×10^7 m³) and biodegradation accounts for volumes ranging between 3.3×10^6 m³ to 1.15×10^7 m³ (3 × 10⁶ m³ to 1.15×10^7 m³). As shown in Figure A.1-7 [GVAR_020], the amount of gas generated by biodegradation is grouped into two distinct branches. The lower and higher branches correspond to the inclusion and exclusion, respectively, of plastics and rubbers in the cellulosics inventory. Also, biodegradation ceases in most realizations within 1500 years, whereas corrosion generally continues for 10,000 years or as long as brine is present. Although the rate of microbial gas generation is constant in any computational cell for a given realization, when the inventory of cellulose or brine is depleted in some cells, the rate of gas generation in the repository as a whole drops. This is manifested in Figure A.1-7 [GVAR 020] by the decrease in the slopes of the curves, reflecting the reduction in the overall rate of microbial gas generation.

The fraction of gas generated by corrosion for all realizations is shown in Figure A.1-10 [GVAR_175]. In those realizations where gas generation from corrosion ceases, the cause is a lack of brine in the waste. In contrast, biodegradation, which also requires brine to be present, completely consumes the inventory of cellulosics (Figure A.1-4 [GVAR_002]) in all but nine (one) realizations. In these realizations, corrosion consumes all the available brine before the entire inventory of cellulosics is consumed. (Recall that 50 realizations have no biodegradation at all, these are indicated by the horizontal line showing no change in cellulose content from the

initial inventory of 9.1×10^6 kg.) As shown in Figure A.1-11 [GVAR_001], iron is present in the waste in all 100 realizations after 10,000 years, yet the rate of gas generation by corrosion has decreased greatly in most (all but about 15%) of the realizations. Higher rates of corrosion are maintained in a few realizations because brine saturations remain relatively high (greater than 10%), as shown in Figure A.1-12 [GVAR_046]. The amount of iron remaining after 10,000 years ranges from 28% to 98% (40% to about 98%) of the initial inventory (Figure A.1-13 [GVAR_003]). This behavior primarily represents that of the rest of the repository, which accounts for about 90% of the waste volume. In the panel, iron is generally consumed at a faster rate than in the rest of the repository due to the larger number of realizations with elevated brine saturations (Figures A.1-14 [GVAR_042] and A.1-15 [GVAR_043]). In three (one) realizations, 100% of the initial iron inventory is consumed; among the other 97 (99) realizations, the amount of initial iron inventory remaining after 10,000 years ranges from 0% to 98% (17% to 98%) (Figure A.1-16 [GVAR_144]) in the single waste panel. In two realizations (#58 and #28) there are large increases in brine saturation in the panel at times beyond the initial 1000 years (Figure A.1-14 [GVAR 144]). These increases are due to increases in brine inflow to the repository.

The volume of brine consumed in the waste panel ranges from 100 m³ to 5800 m³ (100 m³ to 5650 m³) (Figure A.1-17 [GVAR_157]). For comparison, the initial pore volume of a panel is 40,670 m³, and the minimum pore volume after creep closure ranges from about 2800 m³ to 8500 m³, corresponding to a range of minimum porosity of 0.07 to 0.21 (Figure A.1-18 [GVAR_048]). Thus, the amount of brine consumed is generally just a fraction of the total pore volume of the waste. The amount of brine consumed in the rest of the repository ranges from 700 m³ to 32,500 m³ (1000 m³ to 30,000 m³) (Figure A.1-19 [GVAR_158]).

A.1.1.1.2 Halite Creep

Halite creep causes the pore volume of the repository to decrease over time. As shown in Figure A.1-20 [GVAR_052], the porosity of the waste drops from its initial porosity of 84.8% during the first few hundred years, as the repository creeps shut. The porosity reaches a minimum between 7% and 22% of the initial excavated volume, depending on the rate at which the pressure in the repository increases, primarily as a result of gas generation. In approximately 10 realizations, the gas generation rate is very low, which causes the waste pressure to remain low, allowing creep closure to reduce the waste porosity very rapidly. The porosity continues to decrease until 1000 - 2000 years in some cases. Eventually closure ceases and porosities reverse slightly due pressure buildup in the waste. This pressure buildup is the net effect of gas generation, equilibration with far-field pressure, and compression of the waste and fluids. After bottoming out at 7% - 8%, the porosity slowly increases to 8% - 15% in these realizations. In the intermediate group of realizations, the porosity again decreases rapidly for the first 300 years, but gas generation inhibits creep closure to the point that closure ceases in about 1000 years.

Subsequently, the waste repository inflates slightly and minimum porosities ranging from 10% - 17% increase to final porosities of approximately 20% at 10,000 years. In some realizations, the

porosity continues to drop very slowly over the full 10,000 years, reaching lows of 11% - 12% at 10,000 years. In these cases pressures in the repository remain so low that no inflation occurs.

A.1.1.1.3 Fluid Flow

Fluid flow behavior in the repository and surrounding strata are largely determined by the gas generation rate. If the gas generation rate is relatively low, primarily as a result of low reaction rates or the absence of biodegradation, the pressure in the repository rises relatively slowly as brine from the far field flows in to equilibrate repository pressure with the far field. Under these conditions, the direction of flow is mostly inward toward the repository. A less common response is for gas to be generated sufficiently rapidly so that the pressure in the repository becomes high enough to drive significant quantities of brine and gas away from the repository out the most permeable pathways: the three anhydrite layers and the sealed shaft.

Although the brine saturation in the waste panel and rest of the repository (Figures A.1-21 [GVAR_042] and A.1-15 [GVAR_043], respectively) vary greatly from realization to realization, the variations with time show similar trends in all but a few realizations. There is an initial period when the brine saturation increases rapidly during the first 100-300 years, with most realizations peaking within 1500 years. This rise in brine saturation is caused primarily by the rapid and large reduction in porosity due to creep closure (Figure A.1-20 [GVAR_052]) and, to a lesser degree, brine inflow (Figure A.1-22 [GVAR_064]) from the surrounding DRZ. Both of these processes occur initially at a rate faster than corrosion consumes brine. As shown in Figure A.1-23 [GVAR_032], brine volume (mass) in the repository begins to decrease immediately after this initial period in all but a few realizations. This decrease in brine volume is largely caused by consumption of brine due to corrosion (Figure A.1-24 [GVAR 053]) since only a few realizations exhibit decreases in net brine flow into the repository with time (Figure A.1-22 [GVAR_064]). It should also be pointed out that brine saturations tend to be higher in the panel because the panel is located down-dip of the rest of the repository. In two realizations there is a significant increase in brine inflow after the initial 1000 years, one occurs at 1500 years (#58) and the other at 3500 years (#28). These increases correspond to fracturing and significant permeability increases in the DRZ.

Figures A.1-25 [GVAR_181] and A.1-26 [GVAR_184] show that there is more flow out of the panel seal and into the waste panel than there is out of the rest of the repository and into the panel seal. The mean flow into the panel is about 160 m³ (700 m³), whereas the mean flow out of the repository is only about 38 m³ (200 m³). Also, the number of realizations in which there is flow into the panel is much greater than the number in which there is flow out of the rest of the repository. In only a few (four) realizations is there any substantial brine flow (greater than 100 m³) in the northerly direction out of the panel and into the seal (Figure A.1-27 [GVAR_183]) and out of the seal and into the rest of the repository (Figure A.1-28 [GVAR_182]).

For contaminated brine to flow up the shaft, it must first flow either through the panel seals and into the shaft, or through the DRZ above and below the waste region. As Figure A.1-29

[GVAR_069] shows, there are several realizations in which brine flows upward in the shaft, and the maximum flow is 112 m³ (150 m³). All of the brine that flows up the shaft flows into the Culebra; none of it flows beyond the Rustler Formation (Figure A.1-30 [GVAR_070]). There is some downward flow in the shaft as well, although Figures A.1-29 [GVAR_069] and A.1-30 [GVAR_070] do not reflect this because only upward flows are integrated to generate these plots.

A.1.1.2 Behavior in Formations Surrounding the Repository

A.1.1.2.1 Two-Phase Flow

The bulk of the gas generated in the repository flows up-dip into the anhydrite layers north of the repository (Figures A.1-31 [GVAR_106] to A.1-37 [GVAR_112]). However, substantial gas flow out the marker beds (more than $100,000 \text{ m}^3$ in 10,000 years) occurs in only 16 (17) realizations. The maximum cumulative gas flow out any marker bed is $2.1 \times 10^6 \text{ m}^3$ ($3.8 \times 10^6 \text{ m}^3$) out Marker Bed 139 (Anhydrite a and b) (Figure A.1-33 [GVAR_108]). Gas flow out the marker beds to the south of the repository are much less than to the north, the maximum being $4.7 \times 10^5 \text{ m}^3$ ($8.2 \times 10^5 \text{ m}^3$) out Anhydrite a and b (Marker Bed 139) (Figure A.1-35 [GVAR_110]). The maximum total gas flow out all marker beds over 10,000 years is $3.3 \times 10^6 \text{ m}^3$ ($6.8 \times 10^6 \text{ m}^3$) (Figure A.1-37 [GVAR_112]), with a mean gas flow volume of $1.5 \times 10^5 \text{ m}^3$ ($3.8 \times 10^6 \text{ m}^3$). Comparing this quantity with a maximum of $3.4 \times 10^7 \text{ m}^3$ ($2.8 \times 10^7 \text{ m}^3$) total gas generated (Figure A.1-38 [GVAR_022]), it can be determined that, as an approximate upper bound, 10% (26%) of the gas generated in the repository flows out into the marker beds. The mean total gas volume generated is $1.19 \times 10^7 \text{ m}^3$ ($1.24 \times 10^7 \text{ m}^3$), so the mean percentage of gas generated that flowed out the marker beds is 1.3% (3.1%).

Cumulative brine flows out of the repository are shown in Figure A.1-39 [GVAR_059]. Three vectors (#24,#44,#22) have rapid (within 200 years) outflow. These vectors have high DRZ permeability, high brine saturation, and low residual brine saturation. This potentially contaminated brine cannot migrate significant distances in halite because of the low permeability of halite. To get to the land withdrawal boundary, brine from the repository must first flow through the DRZ into one of the permeable anhydrite layers (Marker Beds 138 or 139 or the combined Anhydrite a and b), or up the sealed shaft. Cumulative net brine flow into the DRZ region surrounding the repository from all anhydrite layers is shown in Figure A.1-40 [GVAR_099]. In this figure positive values indicate flow inward, toward the repository from the marker beds, and negative values indicate net flow outward, from the repository into the marker beds. Cumulative net outward flow (from the DRZ into the marker beds) occurs in approximately 10% of the realizations, with the maximum after 10,000 years being about 7800 m³ (3700 m³) in any single realization with the contribution from all marker beds combined. This is summarized in Table A.1-1. The two realizations with the highest outward flow showed increased flow at 2000 years (#58) and 4000 years (#51).

The contributions to the net brine flow from individual marker beds to the north of the repository are shown in Figures A.1-41 [GVAR_093] to A.1-43 [GVAR_095] and to the south of the

repository in Figures A.1-44 [GVAR_096] to A.1-46 [GVAR_098]. In these six figures, positive flows are to the north and negative flows are to the south. These figures again show that net flow is inward in approximately 90% of the realizations. The maximum outward flows occur in MB139 [to the north ~1800 m³ (1800 m³) and to the south ~7200 m³ (1800 m³)]. The cumulative net flows out each of the anhydrite layers are summarized in Table A.1-1.

Table A.1-1. Cumulative Net Interbed Brine Flows for Undisturbed Conditions (S1 Scenario).

Marker Bed	Max. Net Brine Flow from MB into DRZ, m ³	Max. Net Brine Flow from DRZ into MB, m ³		
MB138 North	90 (330)			
MB138 South	1,650 (4,000)	550 (600)		
Anhydrite a & b North	2,700 (9,500)	0.0 (0.0)		
Anhydrite a & b South	2,150 (10,700)	0.0 (0.0)		
MB139 North	7,000 (21,800)	1,800 (1,800)		
MB139 South	5,600 (23,000)	7,200 (1,800)		
All Marker Beds*	15,500 (69,000)	7,800 (3,700)		

^{*}Because the maximum flows in individual marker beds may occur in different realizations, the sum of maximum flows in each marker bed may not add up to the maximum flow when the contribution from all marker beds is combined in each realization.

The cumulative flows across the land withdrawal boundary in the marker beds are summarized in Figure A.1-47 [GVAR_174] and in Table A.1-2. Flows in individual layers are presented in Figures A.1-48 [GVAR_168] to A.1-53 [GVAR_173]. (In these seven plots, only flows away from the repository are integrated.) As shown, only five (eight) realizations produce brine flow outward beyond the land withdrawal boundary. Brine volumes crossing the land withdrawal boundary during the 10,000 regulatory period range up to 3300 m³ (#38) (216 m³). The other four realizations (#61, #93, #26, #58) had volumes crossing the land withdrawal boundary of less than 100 m³. Important factors producing brine flow at the land withdrawal boundary include: high pressure at 1000 years (which may build due to high gas generation, tight DRZ and or marker beds which subsequently fracture, or high residual brine saturation which prevents early time brine and pressure release); high marker bed permeability; high DRZ permeability; low DRZ porosity (low brine storage so more brine is available to flow into marker beds); and low far-field pressure. The high flow across the land withdrawal boundary in vector #38 is due to a high pressure at 1000 years, the combination of very high DRZ and marker bed permeabilities, a very low DRZ porosity, and a low far-field pressure.

The brine that flows across the land withdrawal boundary does not originate in the repository; rather, it is brine that is initially present in the marker beds, as is demonstrated in Section 3.0 describing the Salado transport analysis. This result is not surprising since the pore volume of

Marker Bed 139 (which provides most of the flow in vector #38) between the repository and the land withdrawal boundary is greater than 155,000 m³.

Table A.1-2. Cumulative Interbed Brine Flows Outward Across Land Withdrawal Boundary for Undisturbed Conditions (S1 Scenario)

Marker Bed	Maximum Brine Outflow across Land Withdrawal Boundary, m ³				
MB138 North	150 (14.3)				
MB138 South	155 (10.6)				
Anhydrite a & b North	620 (39)				
Anhydrite a & b South	160 (47)				
MB139 North	1,550 (78)				
MB139 South	700 (50)				
All Marker Beds	3,300 (216)				

A.1.1.2.2 Mechanical Response

Fracturing in the interbeds occurs in approximately 18 (19) realizations (Figures A.1-54 [GVAR_113] to A.1-59 [GVAR_118]), although in most marker beds, a significant amount of fracturing occurs in only four (five or six) realizations. The most extensive fracturing occurs in realizations #58 and #61. In these realizations, all three anhydrite layers fracture. In realization #58, fracture lengths exceed 1000 m to the north in Marker Bed 138 and Anhydrite a and b and to the south in Marker Bed 138 and Marker Bed 139. In the CCA, maximum fracture lengths to the north in Marker Bed 138 and Anhydrite a and b were 1900 m and 1000 m, respectively, and to the south 1000 m. In realization #61, fracture lengths exceed 1000 m to the north in Anhydrite a and b and to the south in Marker Bed 138 and Marker Bed 139. Other realizations (#51, #28) also display significant fracturing. In addition to realizations #61 and #58, the other realizations in which brine flowed across the land withdrawal boundary (#38, #93, #26) showed moderate fracturing. In most other realizations, gas is not generated at sufficiently high rates to reach interbed fracture pressures and/or pressure is dissipated through DRZ fracturing. Note that in some cases fractures close up some time after opening.

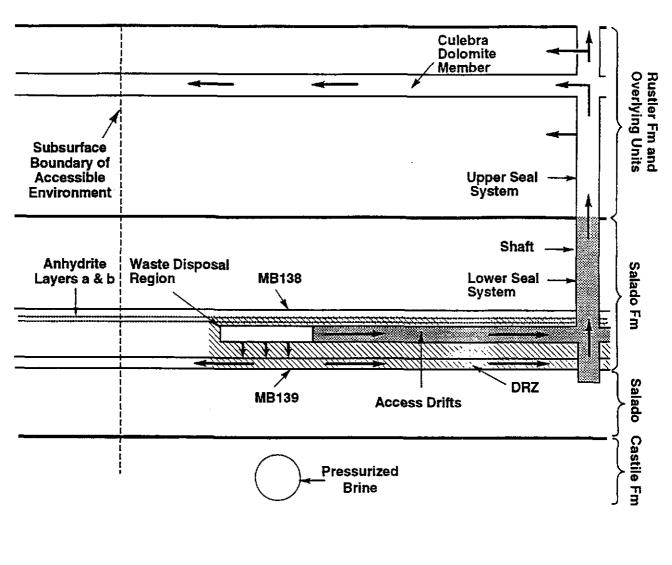
Significant fracturing in the DRZ occurs in about 20 realizations, as indicated by increasing DRZ permeability (Figure A.1-60 [EX_H033]). In all of these realizations, gas is generated by corrosion and biodegradation of cellulosics and plastics and rubbers. Three realizations (#51, #58, #28) result in DRZ permeabilities greater than 1x10⁻¹¹ m² and porosities greater than 0.03. These realizations had high initial DRZ porosities, medium to high DRZ permeabilities, and medium to low Marker Bed permeabilities. DRZ porosity increases, indicative of DRZ

fracturing, are also evident in many of the realizations (Figure A.1-61 [EX_H022]) with realizations #51, #58, and #28 showing the largest porosity increases. Mean, median, and maximum values for DRZ permeability and porosity are shown in Table A.1-3.

Table A.1-3. Volume-Averaged DRZ Permeability and Porosity from PAVT Replicate 1.

Scenario	Time (yrs)	Average DRZ Permeability			Average DRZ Porosity		
		mean	median	max	mean	med	max
S1	0	2.01E-14	1.14E-16	2.82E-13	9.22E-3	6.16E-3	2.52E-2
	10000	4.30E-12	2.98E-16	3.48E-10	1.52E-2	1.31E-2	4.65E-2
S2	0	2.01E-14	1.14E-16	2.82E-13	9.22E-3	6.16E-3	2.52E-2
	350	2.01E-14	1.14E-16	2.82E-13	1.10E-2	8.52E-3	3.03E-2
	10000	6.60E-12	3.55E-16	5.83E-10	1.45E-2	1.11E-2	4.74E-2
S3	0	2.01E-14	1.14E-16	2.82E-13	9.22E-3	6.16E-3	2.52E-2
	1000	3.06E-14	6.69E-16	4.87E-13	1.30E-2	1.16E-2	3.44E-2
	10000	3.77E-13	1.82E-16	3.53E-11	1.33E-2	1.08E-2	3.72E-2
S4	0	2.01E-14	1.14E-16	2.82E-13	9.22E-3	6.16E-3	2.52E-2
	350	2.01E-14	1.14E-16	2.82E-13	1.10E-2	8.52E-3	3.03E-2
	10000	2.12E-14	1.76E-16	3.18E-13	1.22E-2	1.01E-2	3.40E-2
S5	0	2.01E-14	1. 14E-1 6	2.82E-13	9.22E-3	6.16E-3	2.52E-2
	1000	3.01E-14	1.48E-16	4.87E-13	1.30E-2	1.16E-2	3.44E-2
	10000	2.11E-14	1.58E-16	3.08E-13	1.22E-2	1.01E-2	3.45E-2
\$6	0	2.01E-14	1.14E-16	2.82E-13	9.22E-3	6.16E-3	2.52E-2
	1000	3.01E-14	1.48E-16	4.87E-13	1.30E-2	1.16E-2	3.44E-2
	2000	2.94E-14	1.50E-16	4.11E-13	1.22E-2	1.03E-2	4.00E-2
	10000	4.17E-14	1.55E-16	2.02E-12	1.33E-2	1.08E-2	3.19E-2

Undisturbed Performance



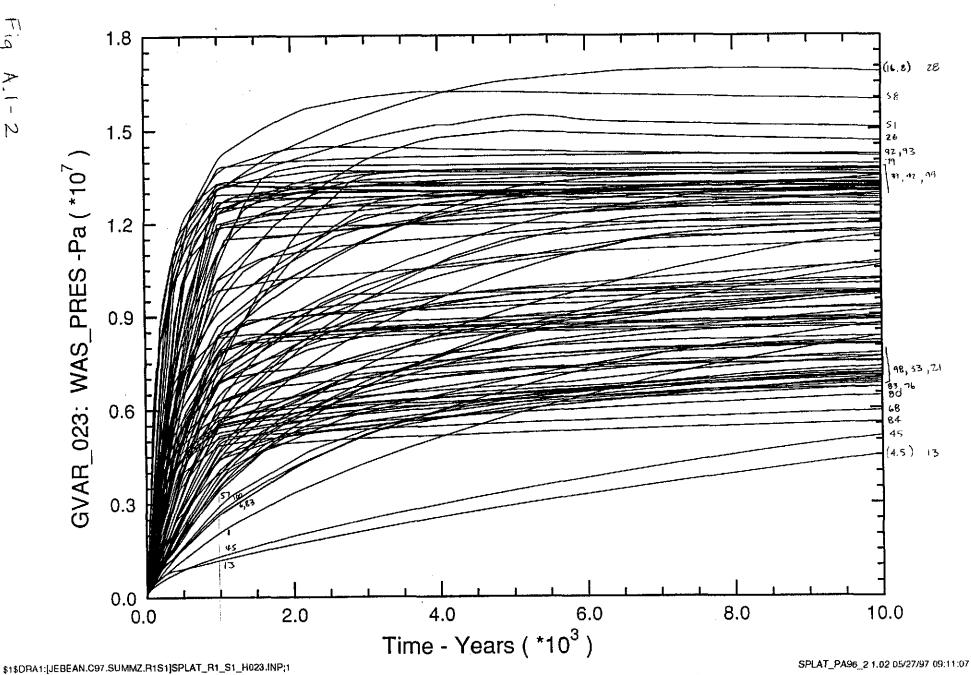
(Not to Scale)

A.1-\

Figure 7:1-1. Conceptual model used in simulating undisturbed performance.

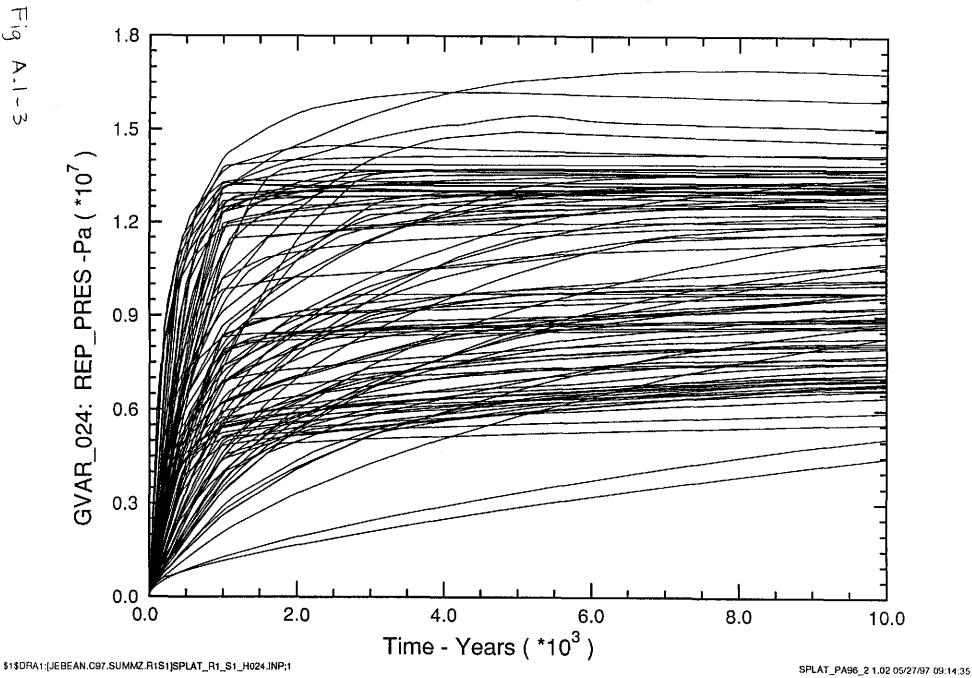
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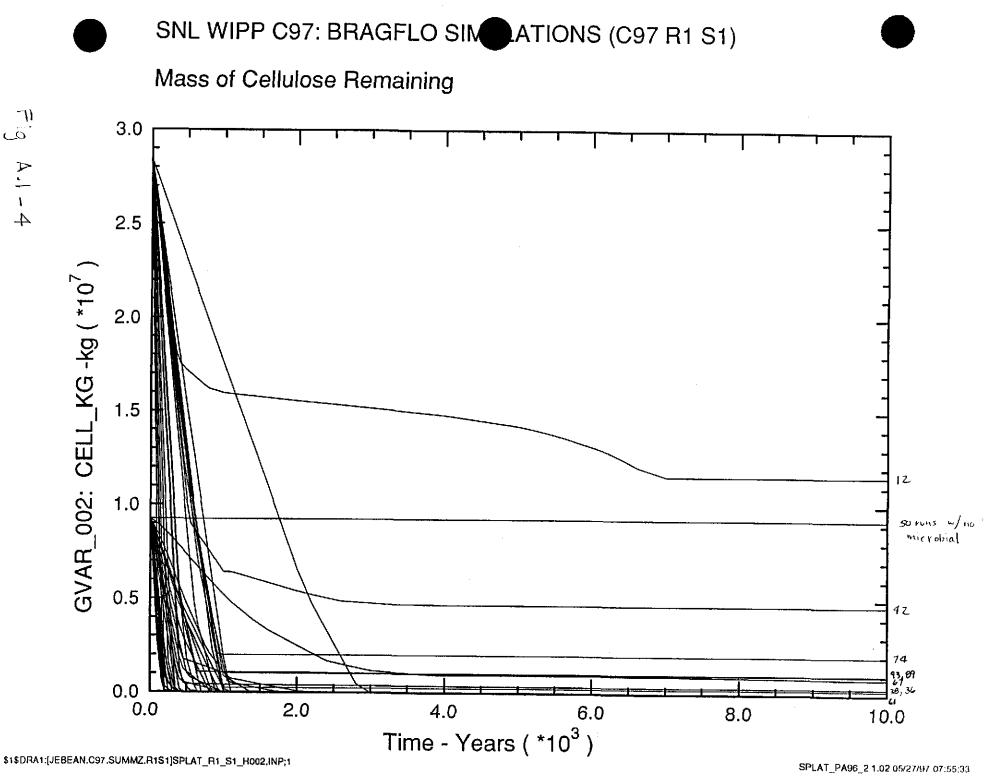
Volume-Averaged Pressure in Waste Panel

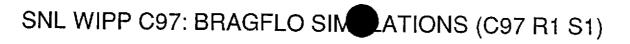




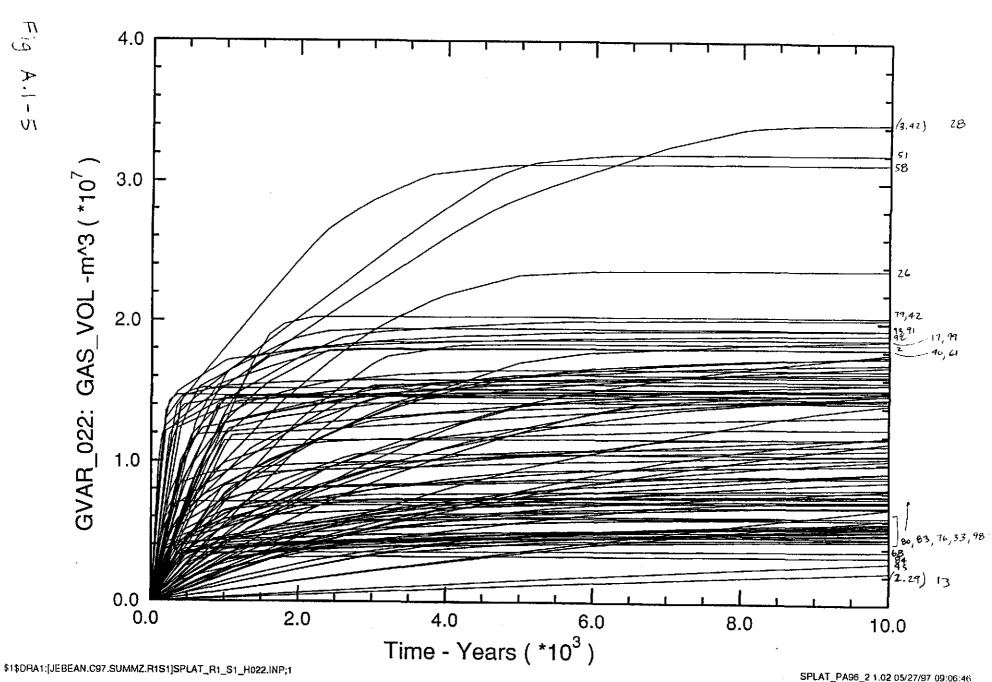
Volume-Averaged Pressure in Rest of Repository

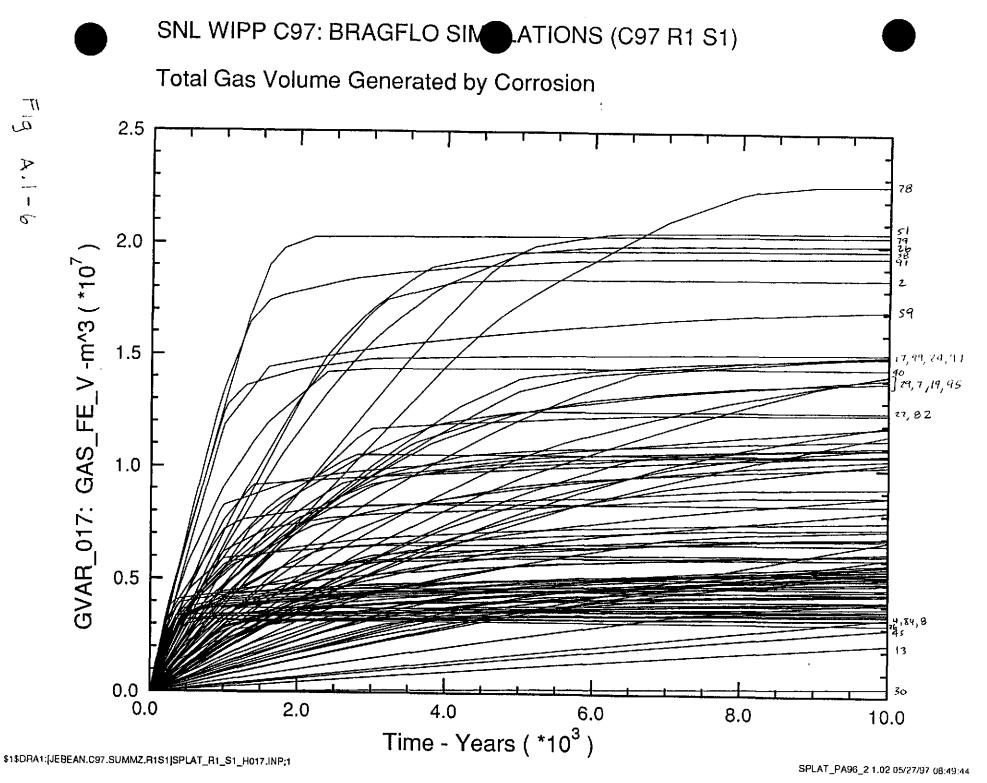






Total Gas Volume Generated





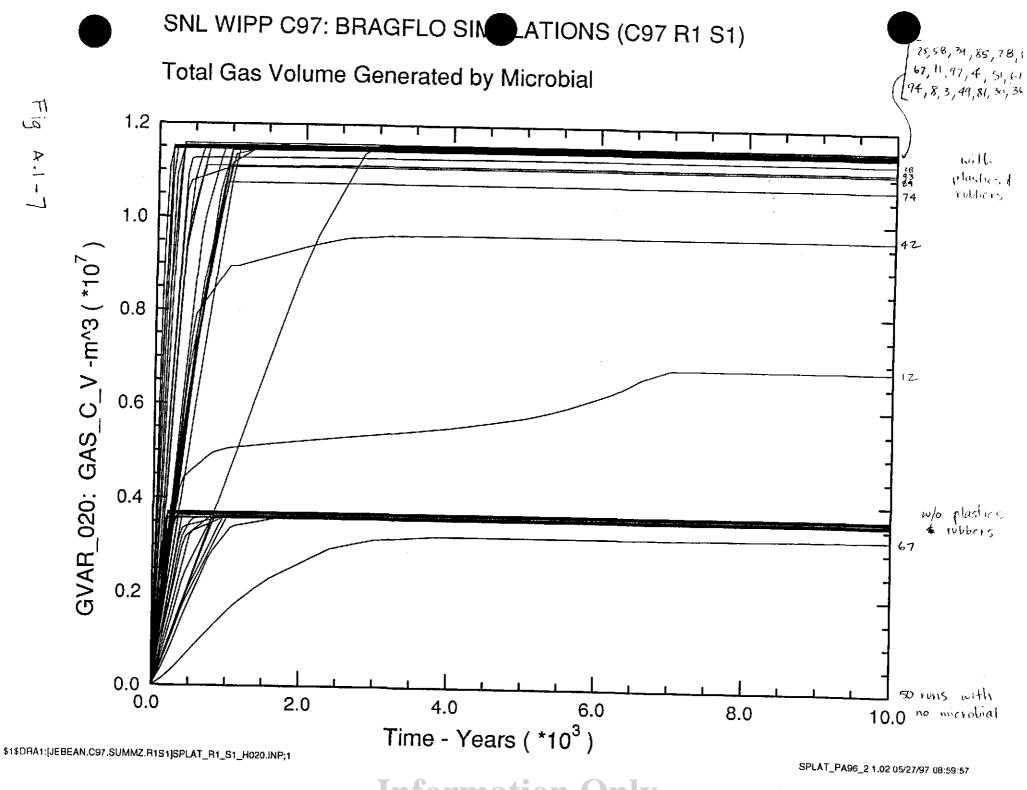


Figure corresponding to CCA Fig. 7.1-8 not used.

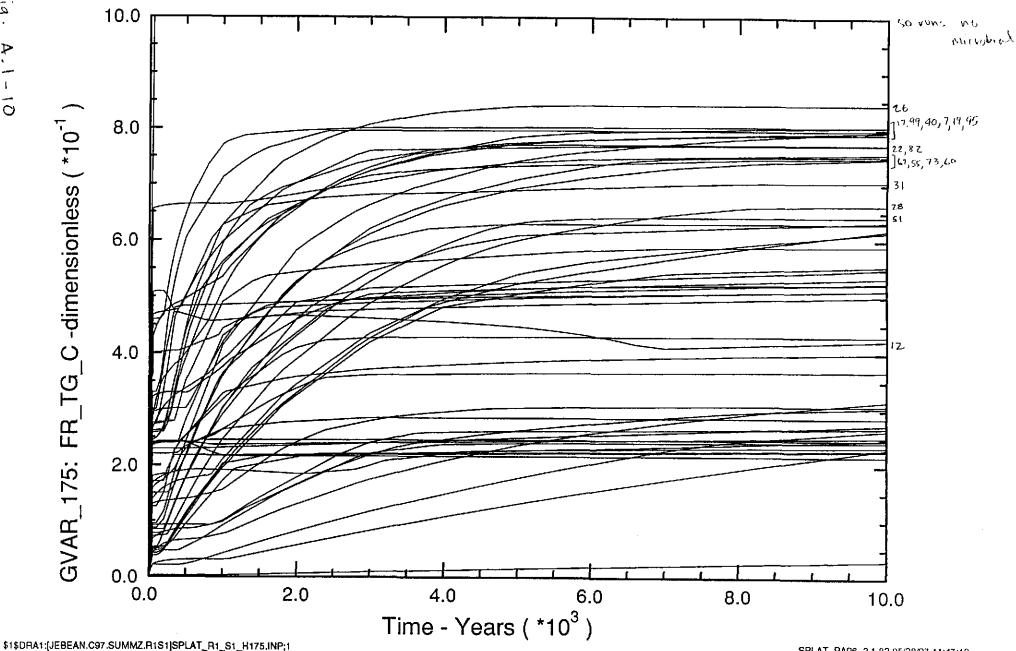
Fig A.1-8

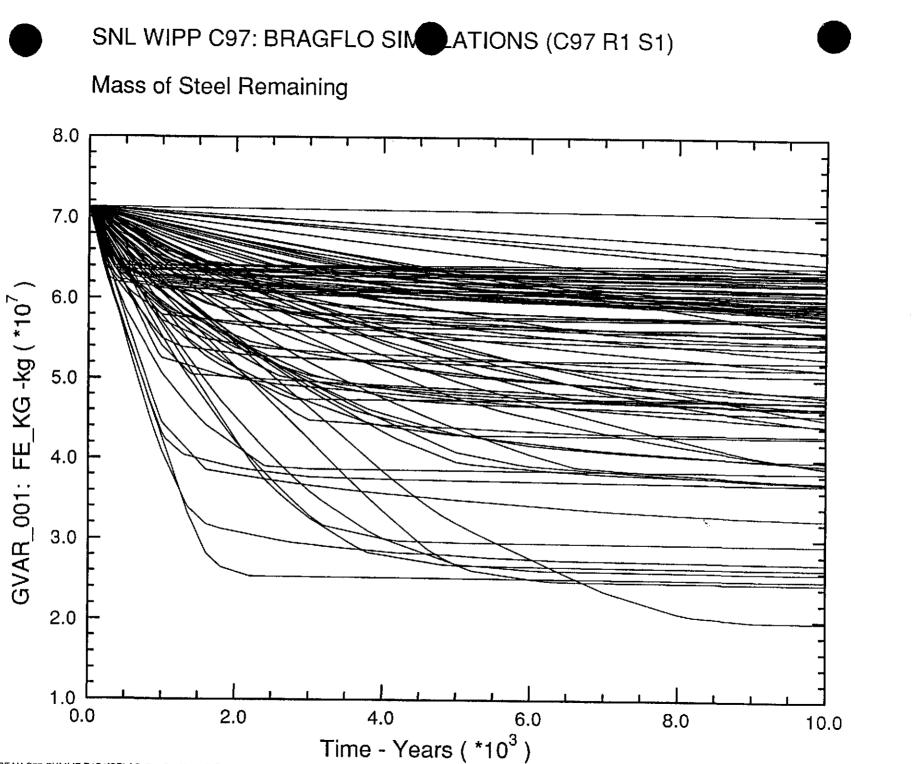
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Fig. A.1-9



Fraction of Gas due to Steel Corrosion





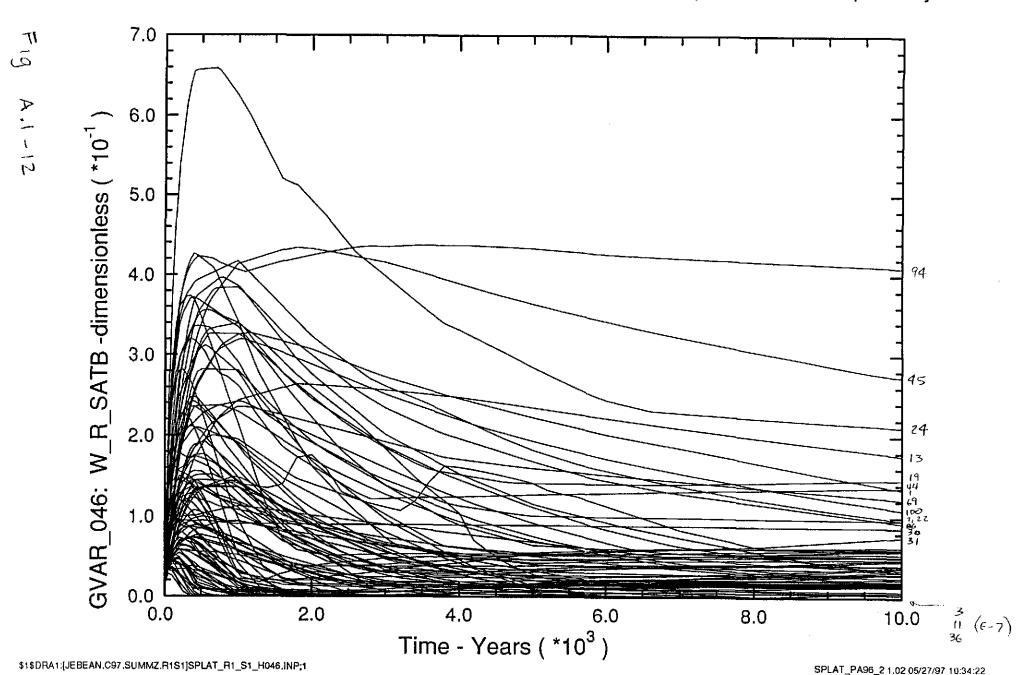
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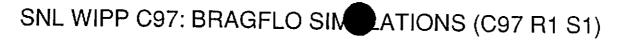
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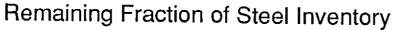
SNL WIPP C97: BRAGFLO SIMPLATIONS (C97 R1 S1)

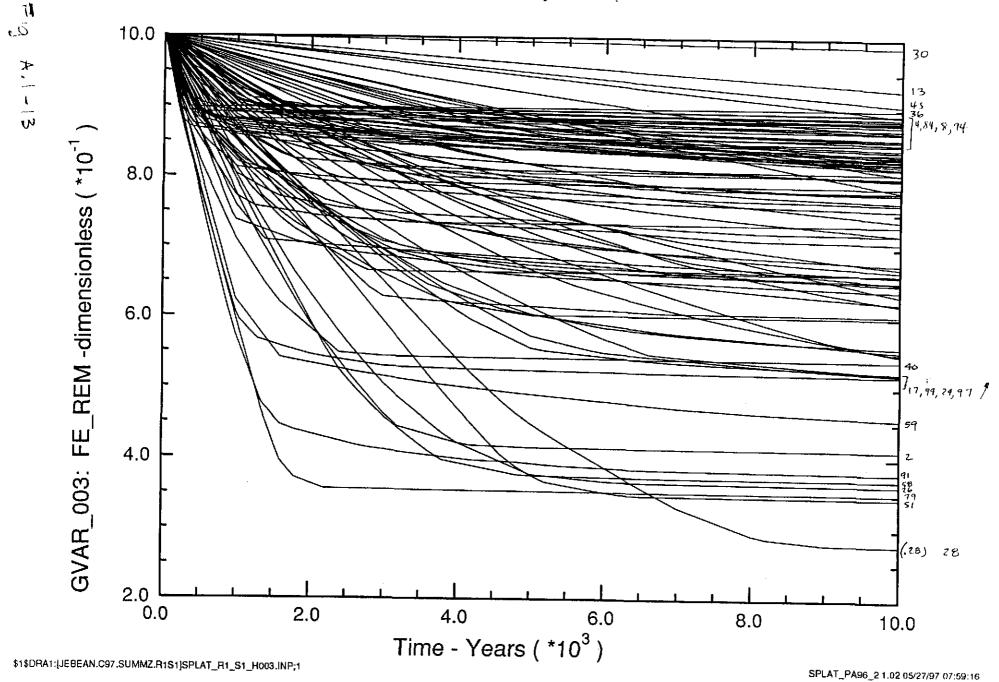


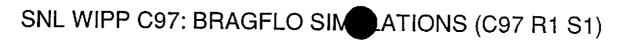
Volume-Averaged Brine Saturation in Waste Panel plus Rest of Repository



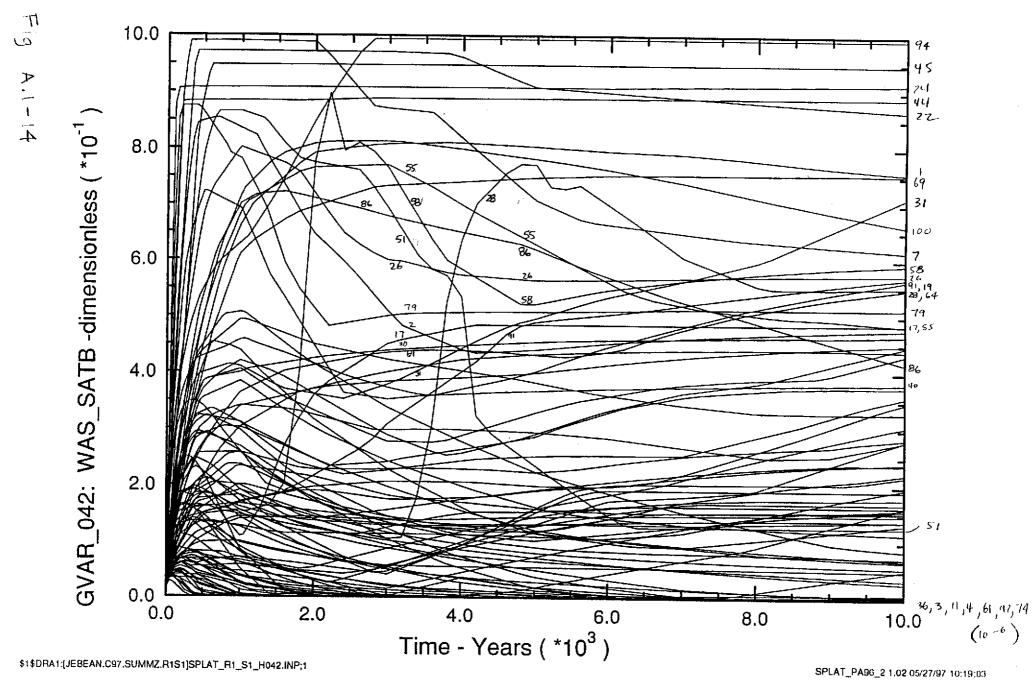


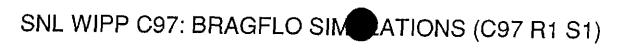




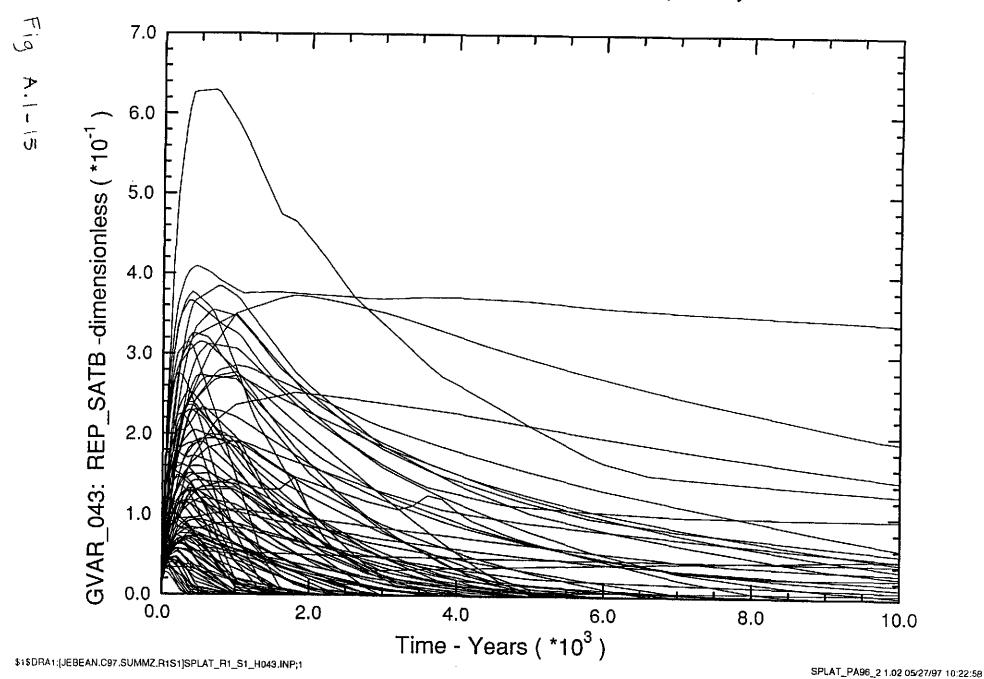


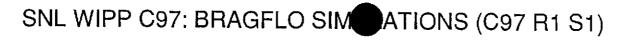
Volume-Averaged Brine Saturation in Waste Panel



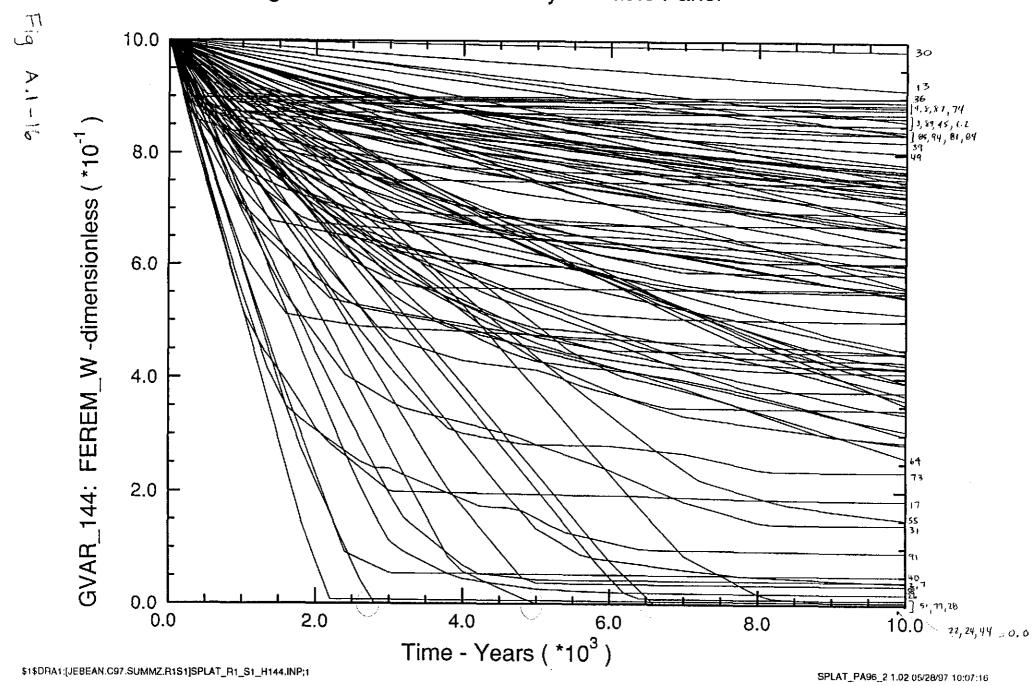


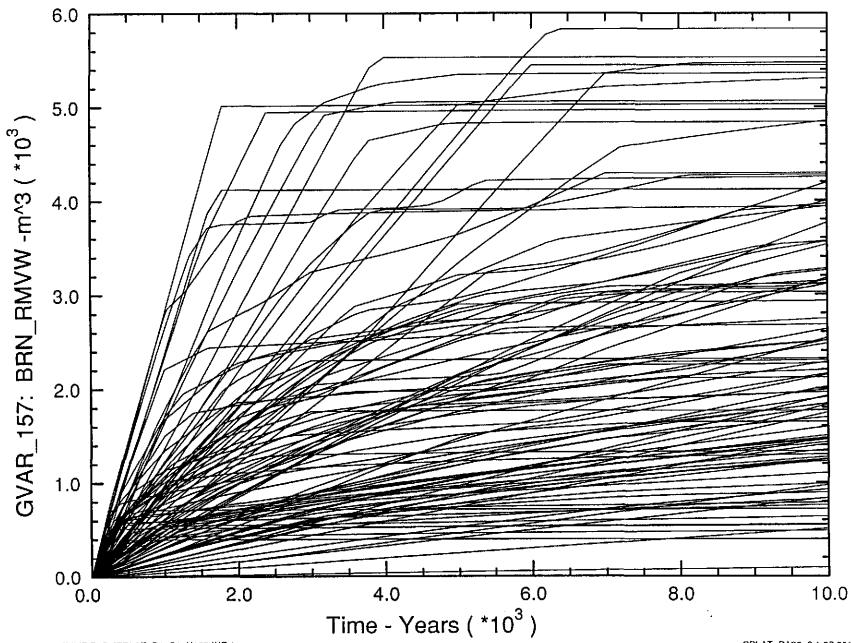
Volume-Averaged Brine Saturation in Rest of Repository

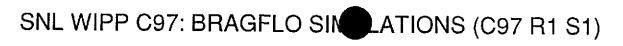




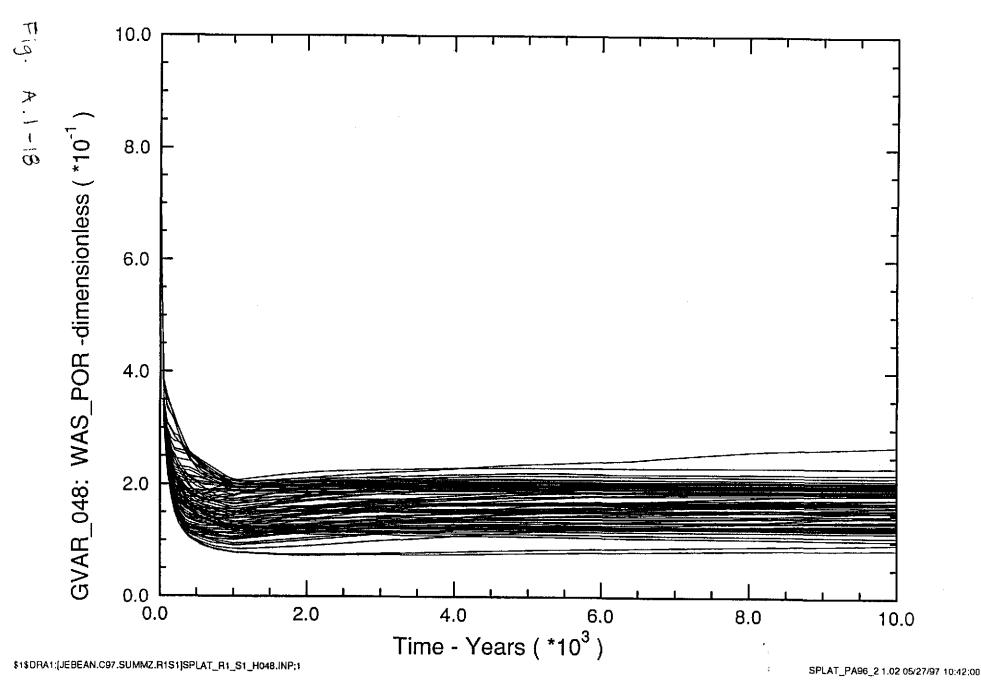
Remaining Fraction of Steel Inventory in Waste Panel

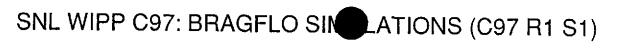




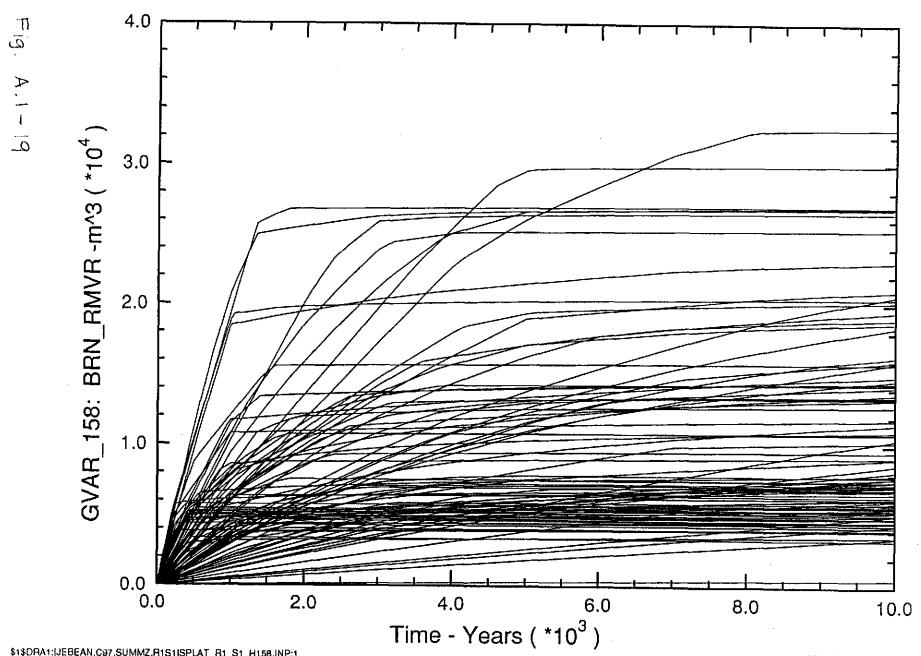






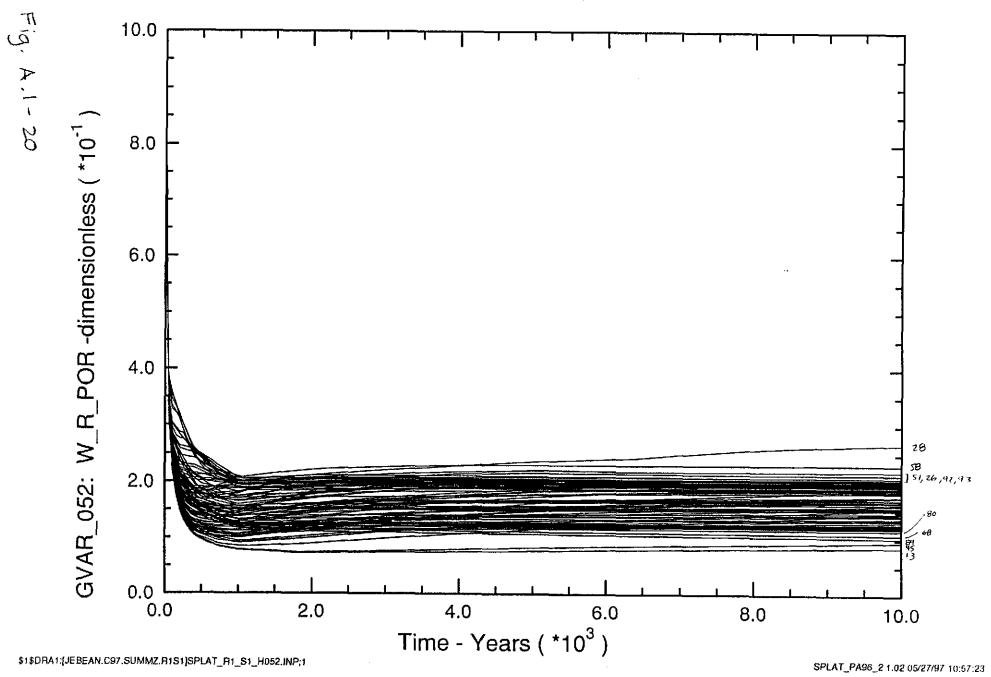


Brine Consumed in Rest of Repository



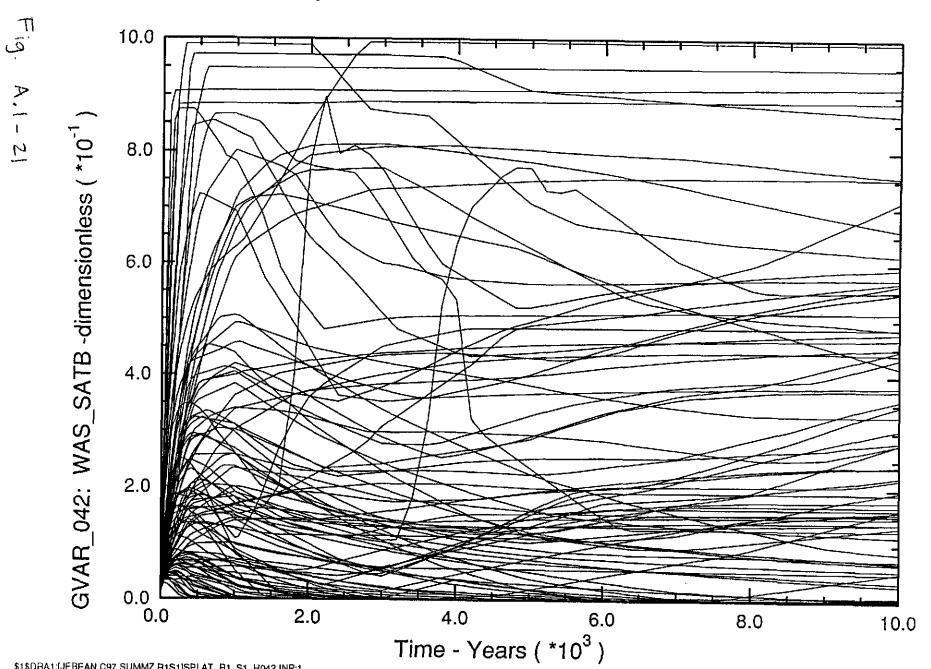


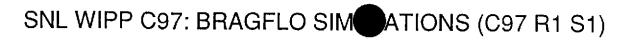
Volume-Averaged Porosity in Waste Panel plus Rest of Repository



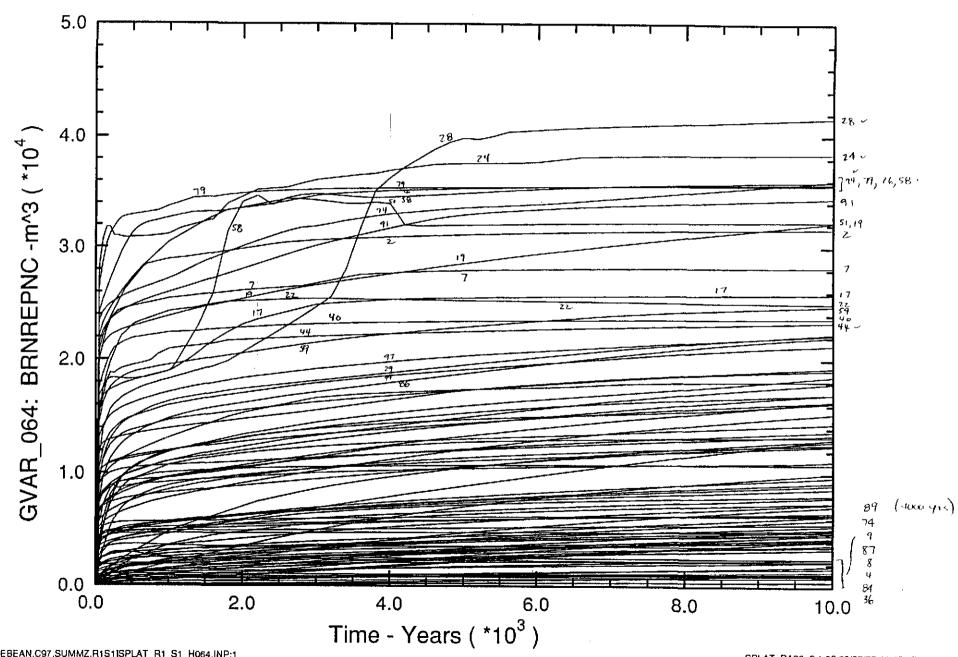
SNL WIPP C97: BRAGFLO SIN LATIONS (C97 R1 S1)

Volume-Averaged Brine Saturation in Waste Panel





Net Brine Flow into Repository



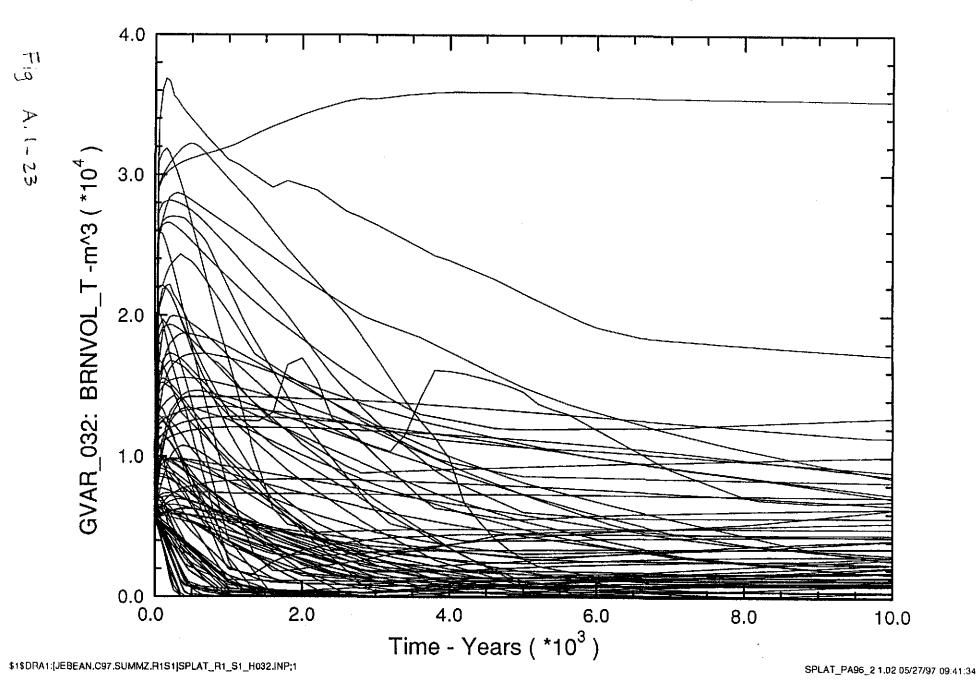
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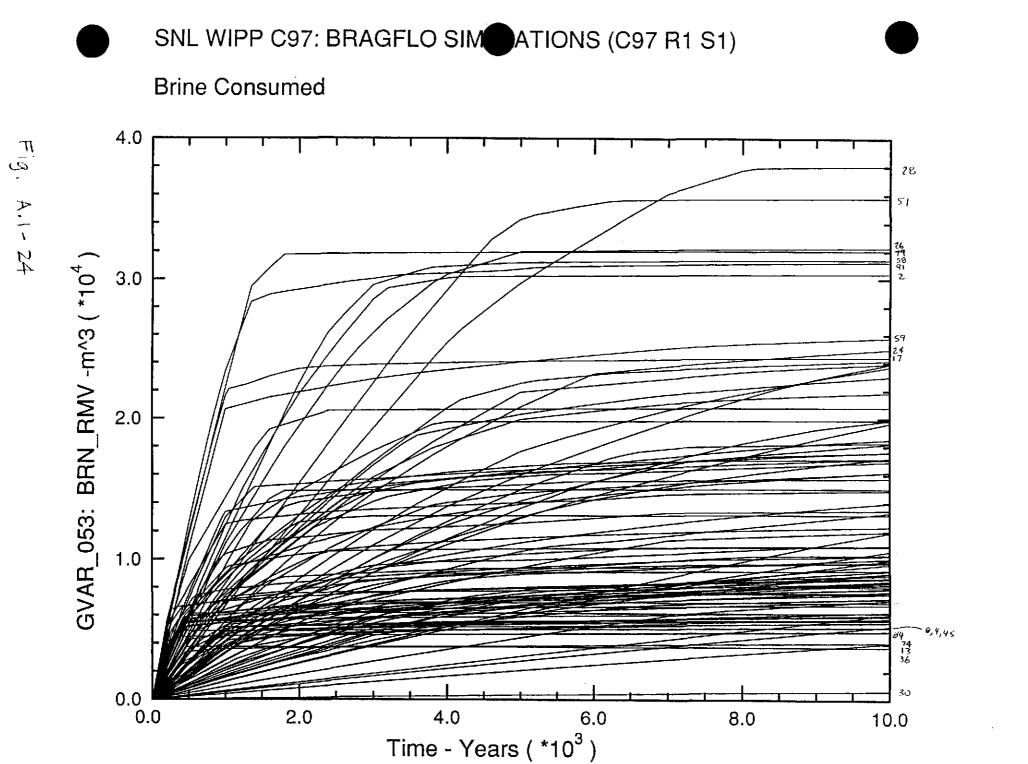
22

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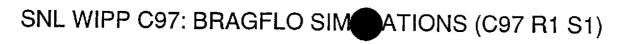
Brine Volume in Waste Panel and Rest of Repository



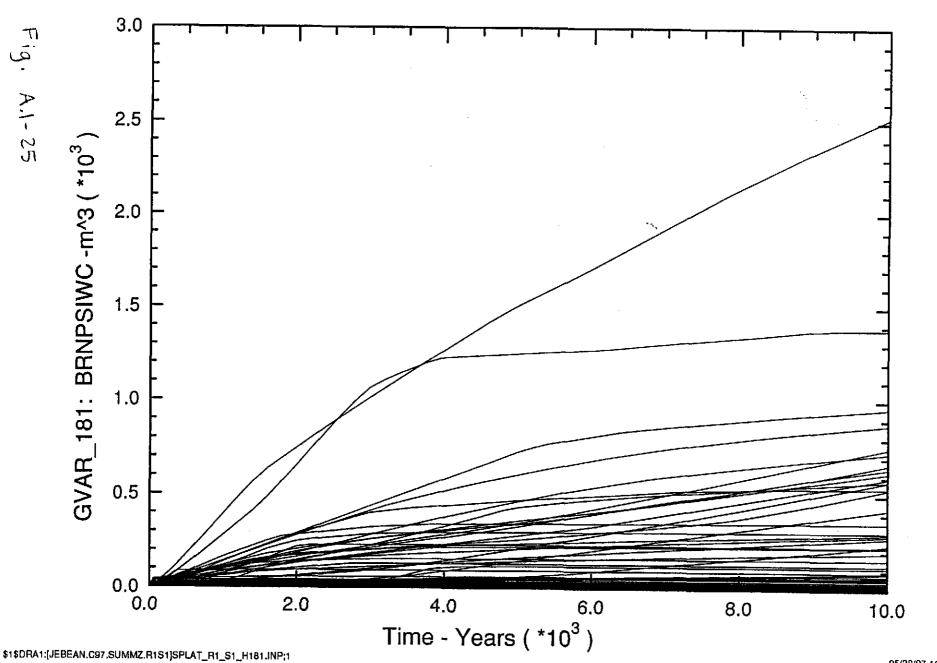


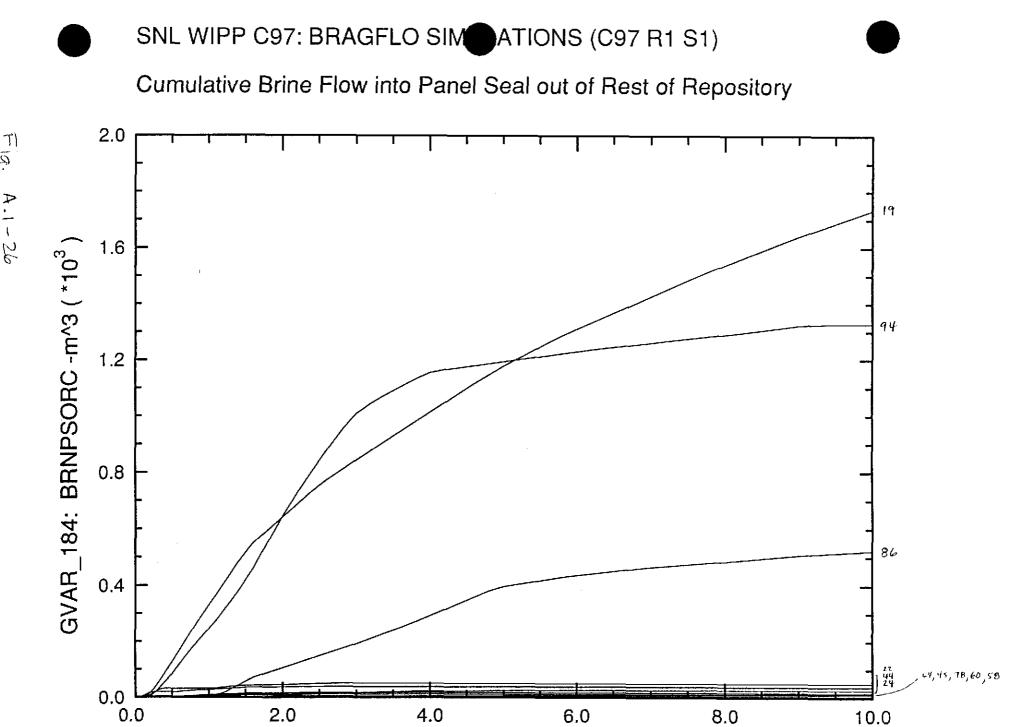
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Cumulative Brine Flow out of Panel Seal into Waste Panel





Information Only

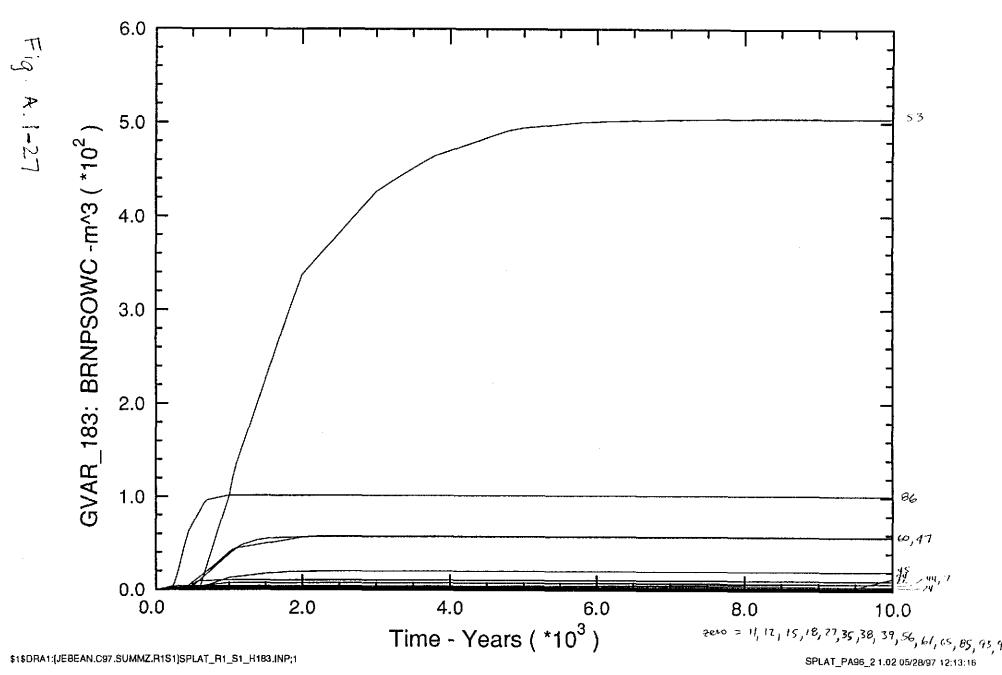
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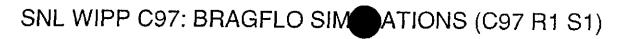
Time - Years (*103)

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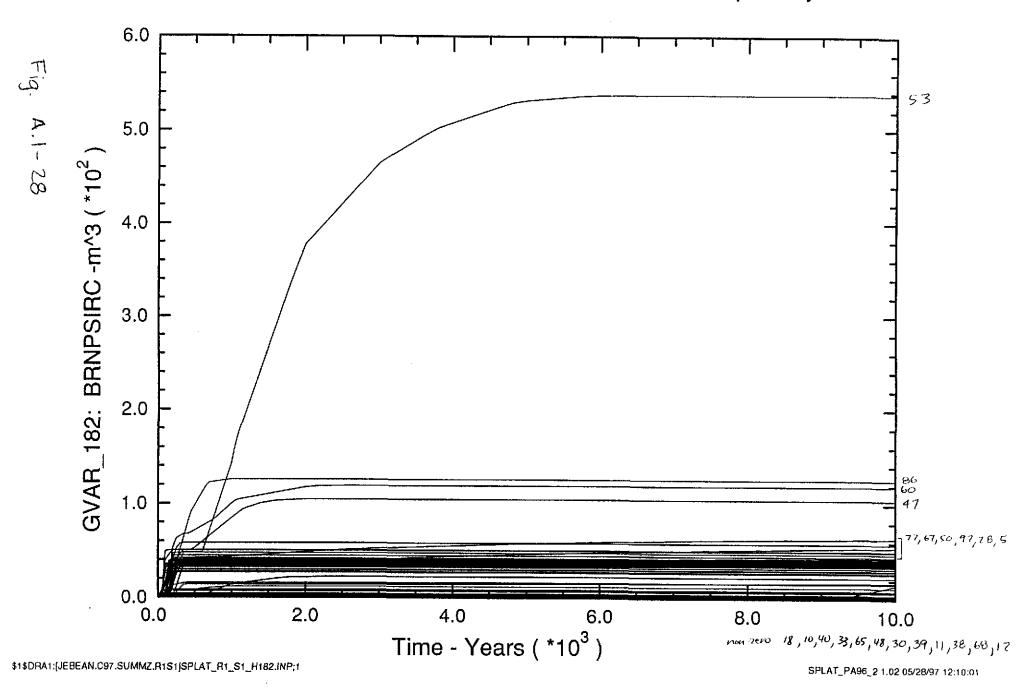
SNL WIPP C97: BRAGFLO SIMPLATIONS (C97 R1 S1)

Cumulative Brine Flow into Panel Seal out of Waste Panel





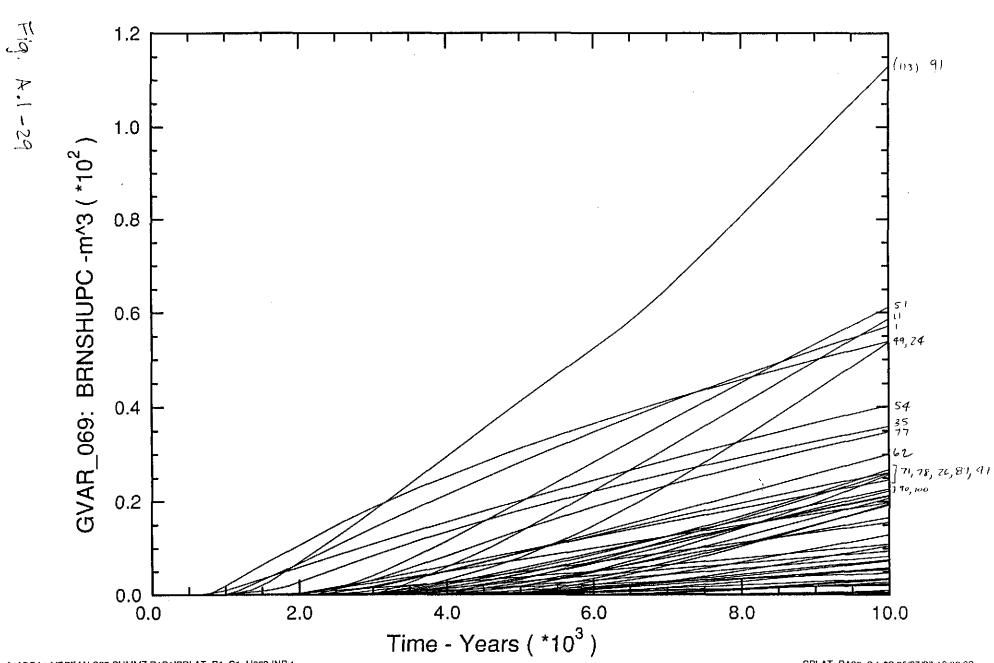
Cumulative Brine Flow out of Panel Seal into Rest of Repository



Information Only

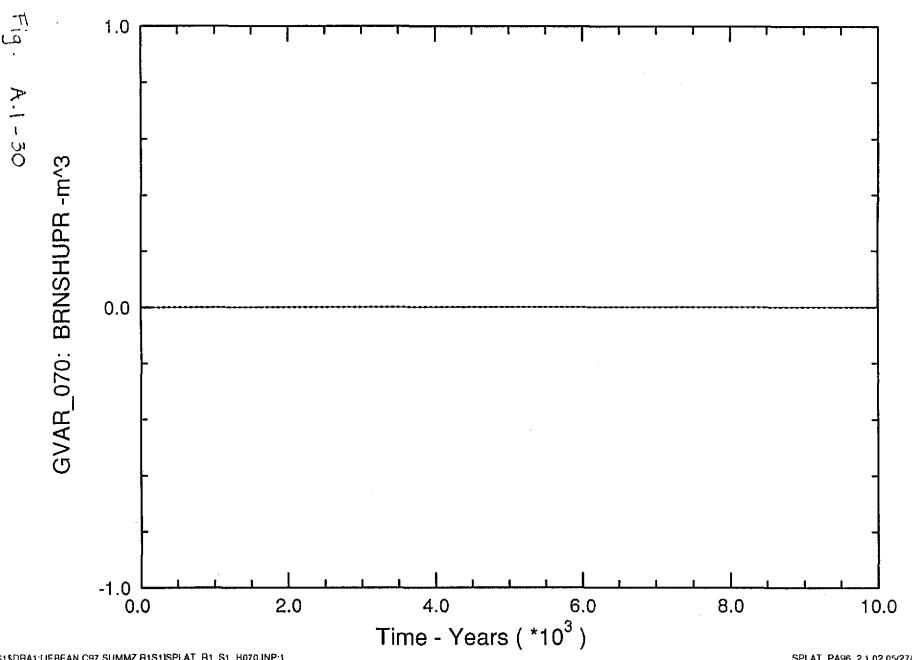


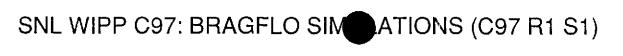
Cumulative Brine Flow up Shaft at top of Salado (E:661)



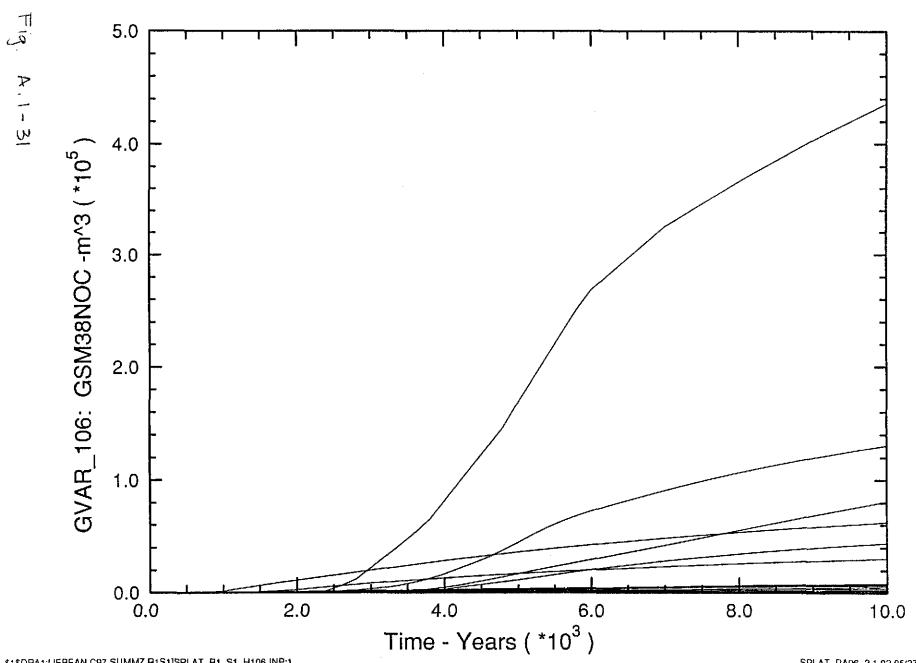
SNL WIPP C97: BRAGFLO SIME ATIONS (C97 R1 S1)

Cumulative Brine Flow up Shaft at top of Rustler (E:666)



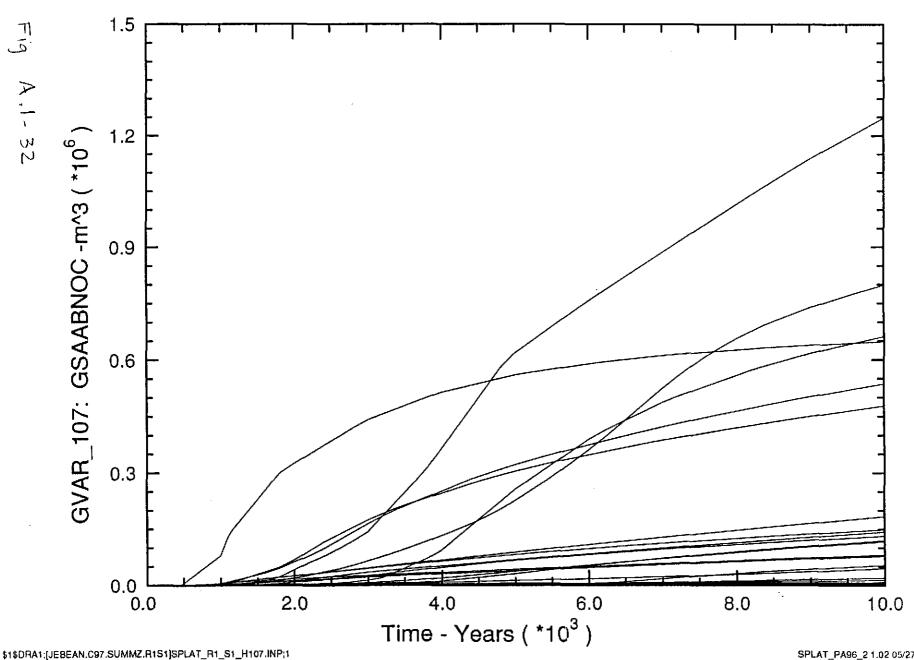


Cumulative Gas Flow from DRZ into North MB 138

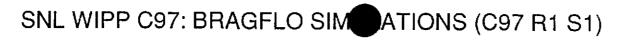




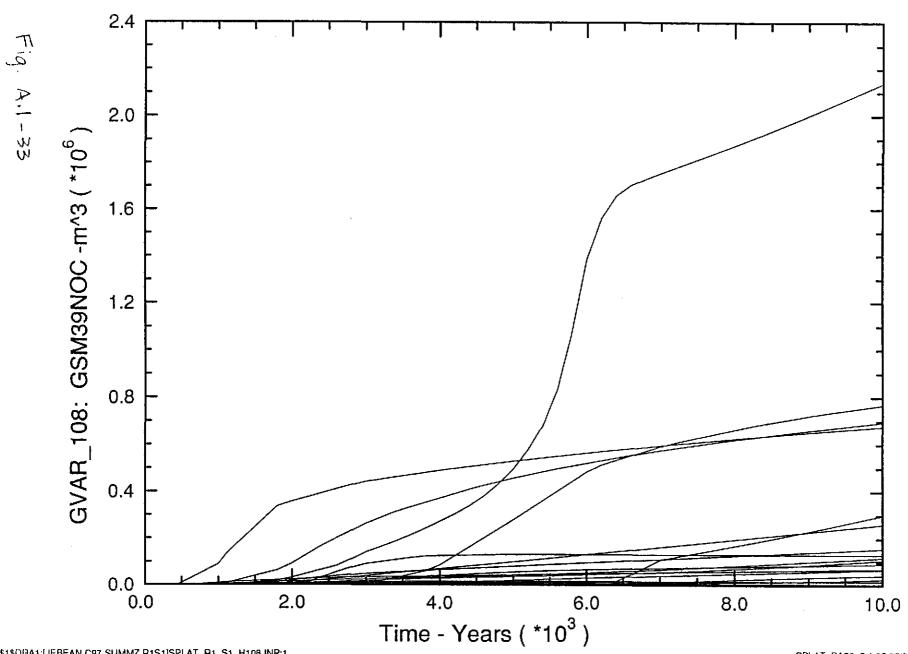
Cumulative Gas Flow from DRZ into North Anhydrite A/B



SPLAT_PA96_2 1.02 05/27/97 14:22:43



Cumulative Gas Flow from DRZ into North MB 139

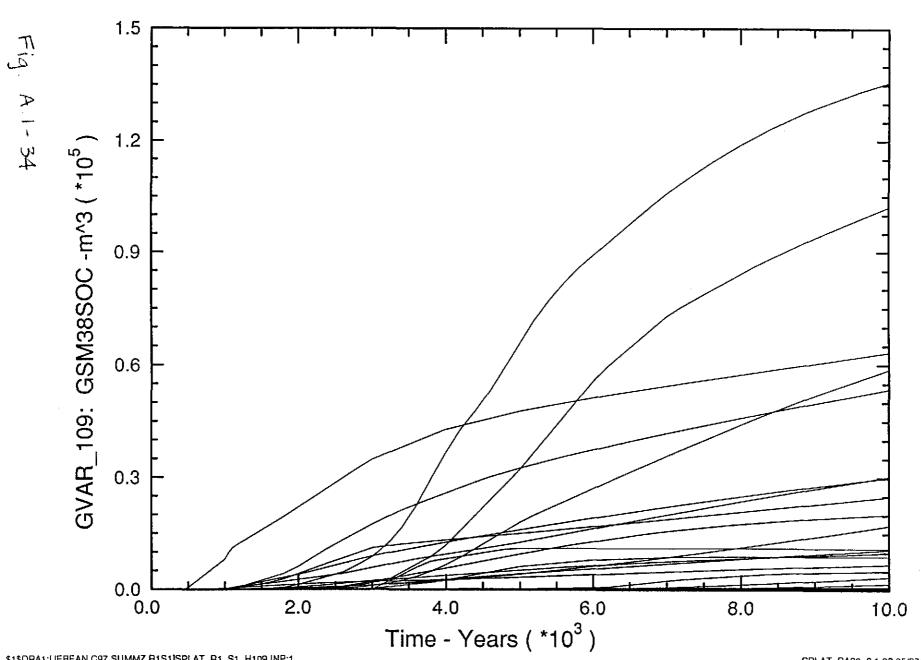


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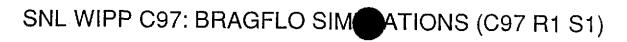


Cumulative Gas Flow from DRZ into South MB 138

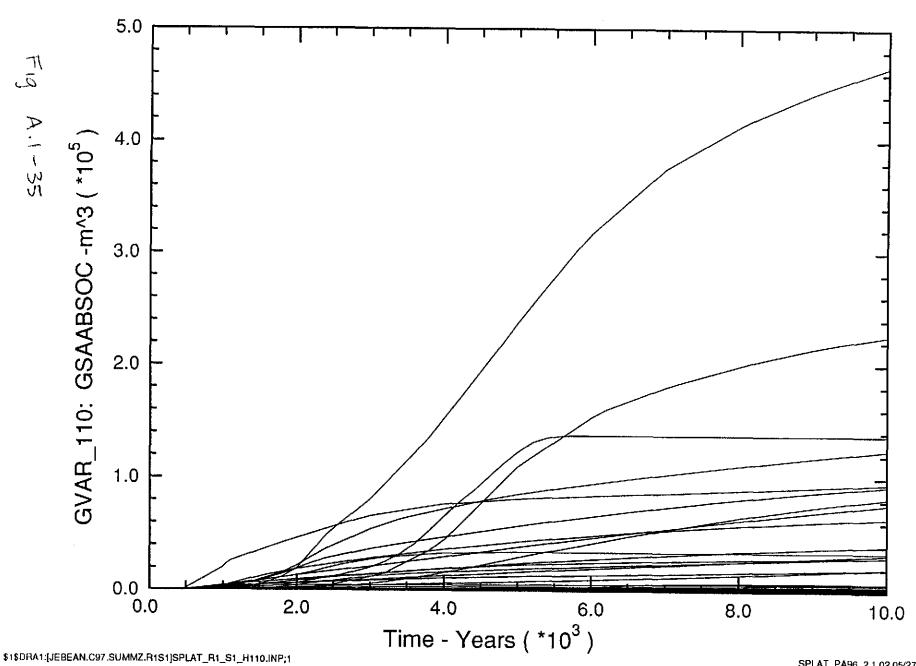


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Cumulative Gas Flow from DRZ into South Anhydrite A/B

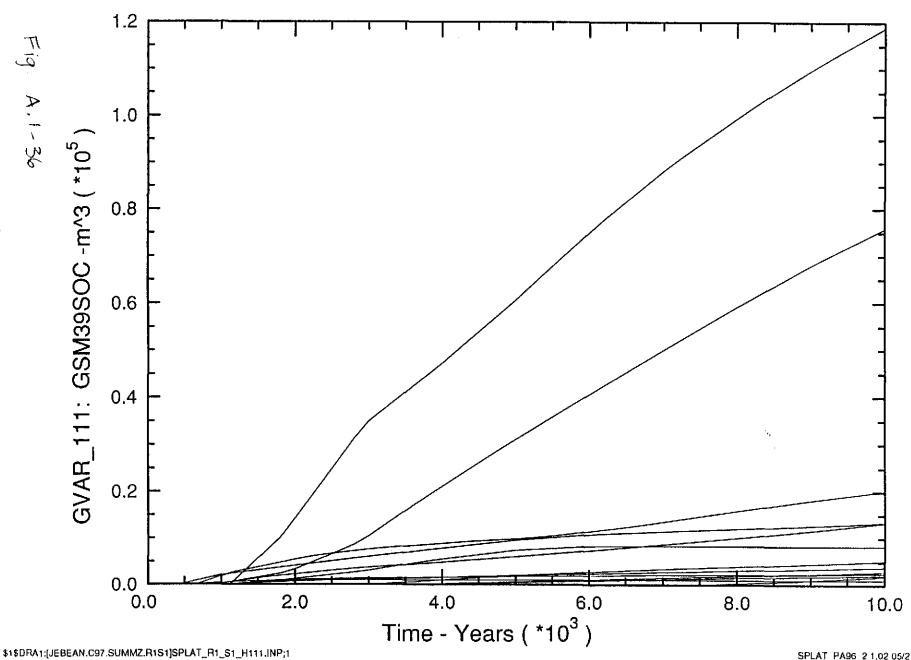


Information Only

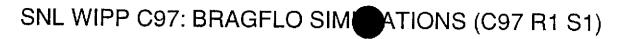
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SNL WIPP C97: BRAGFLO SIM ATIONS (C97 R1 S1)

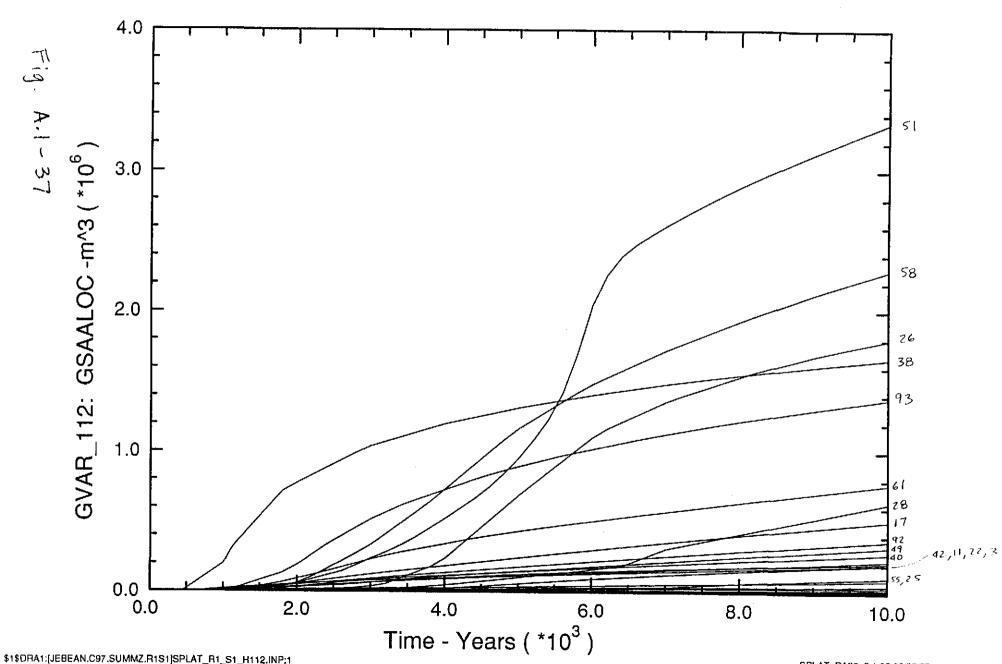
Cumulative Gas Flow from DRZ into South MB 139



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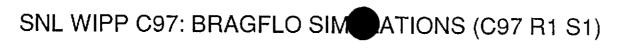


Cumulative Gas Flow from DRZ into Marker Beds

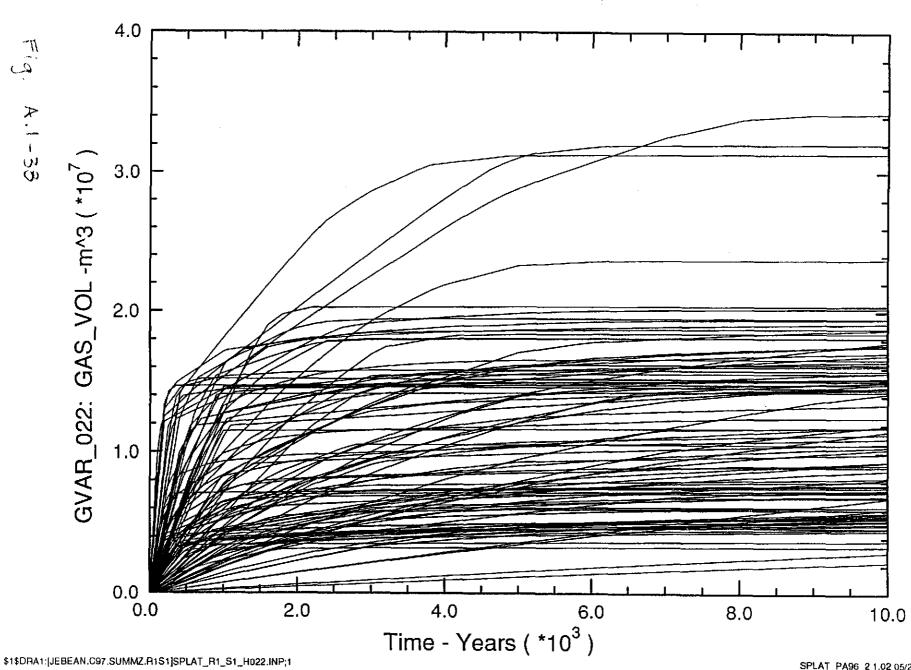


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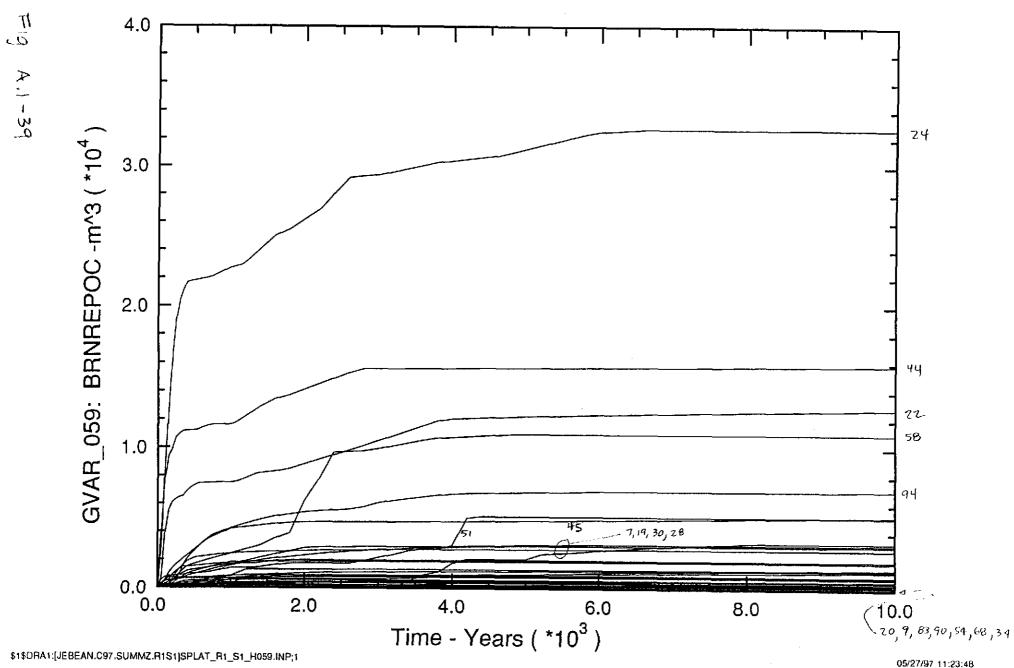




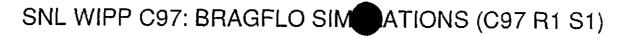


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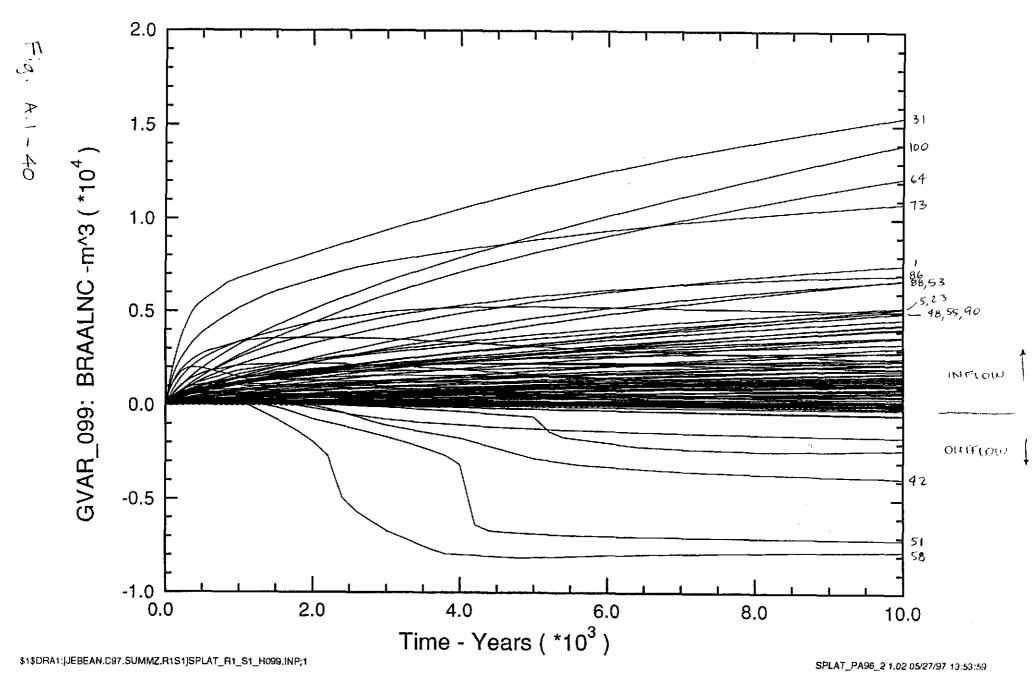


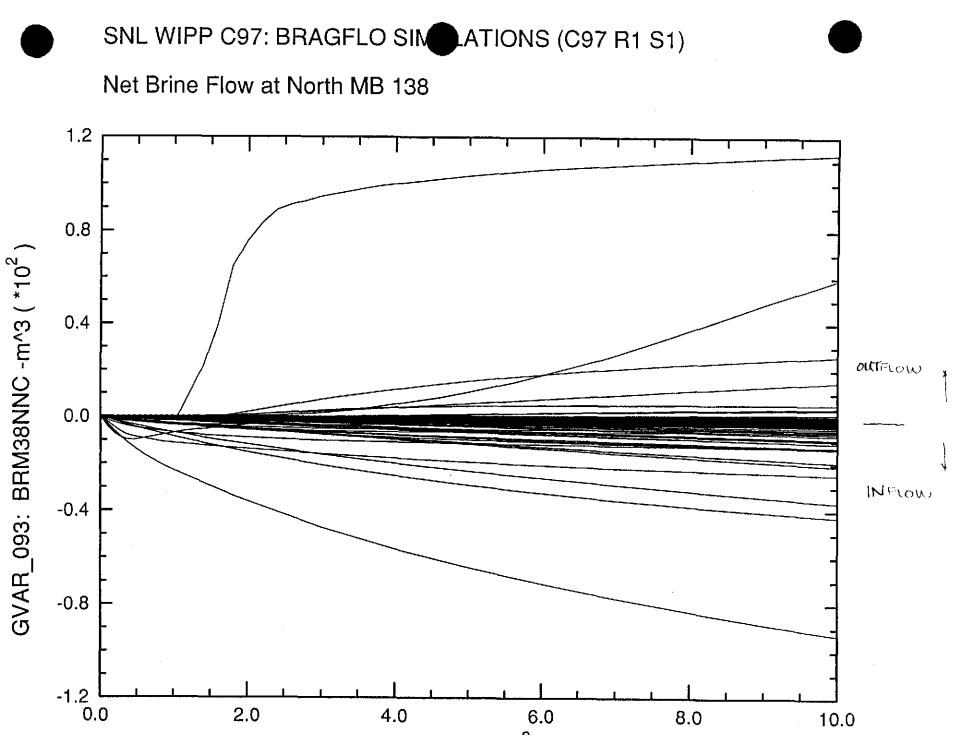


Information Only



Net Brine Flow into DRZ from All Marker Beds





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2.0

SPLAT_PA96_2 1.02 05/27/97 13:31:11

10.0

Time - Years (*10³)

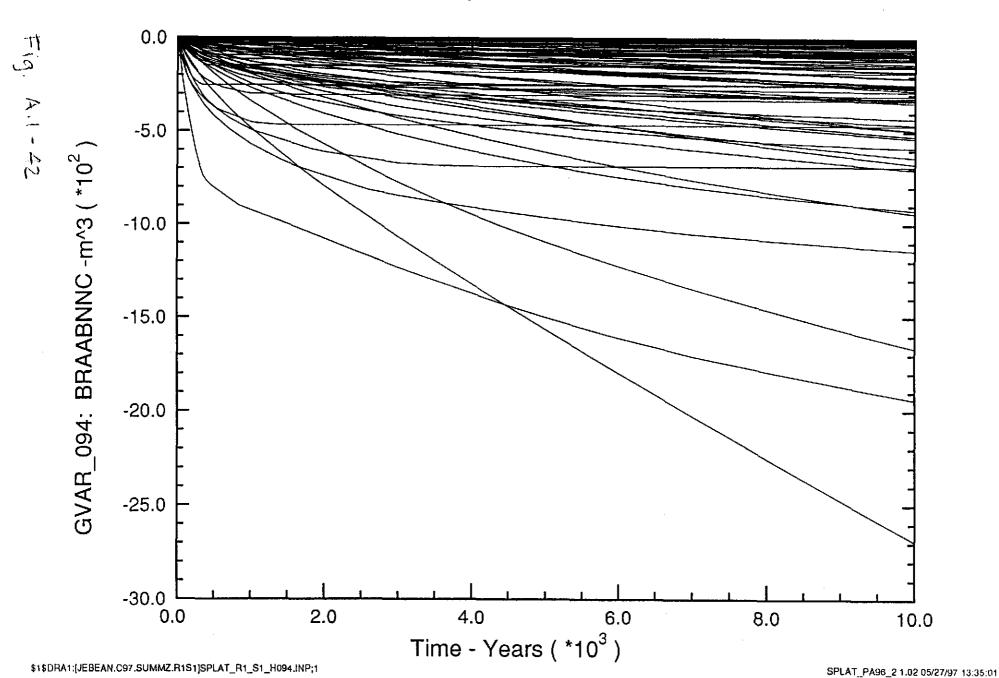
6.0

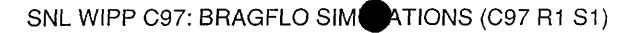
8.0

4.0

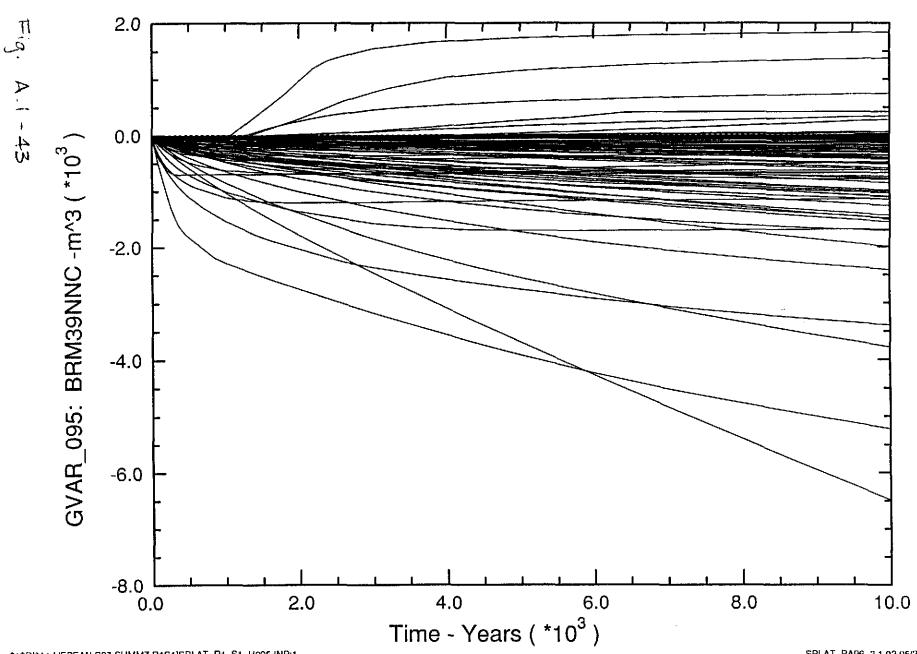


Net Brine Flow at North Anhydrite A/B





Net Brine Flow at North MB 139

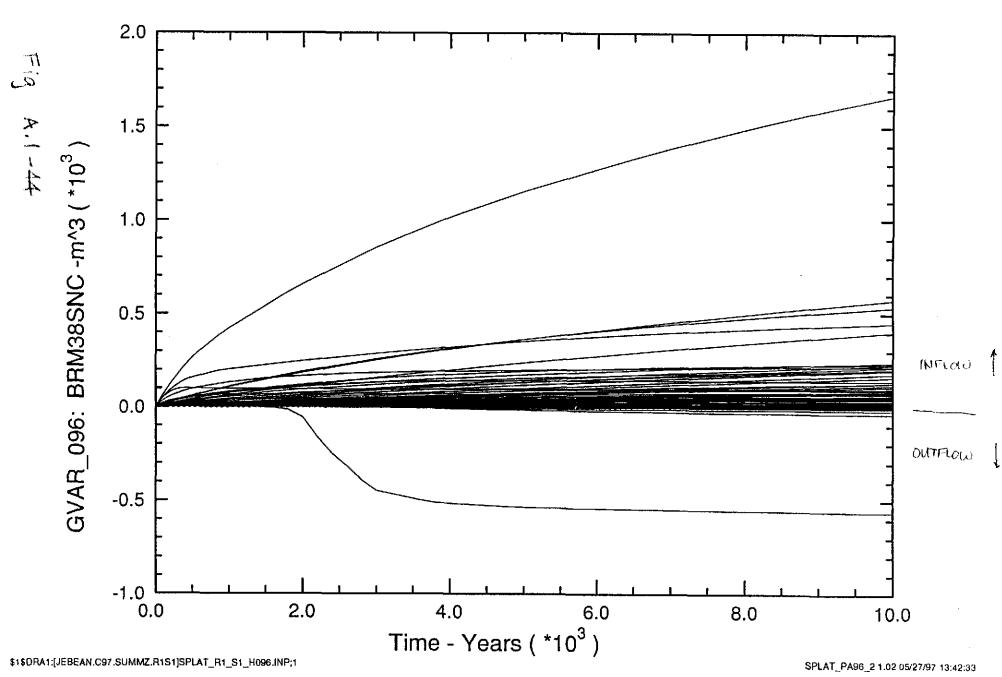


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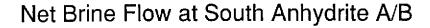
Net Brine Flow at South MB 138

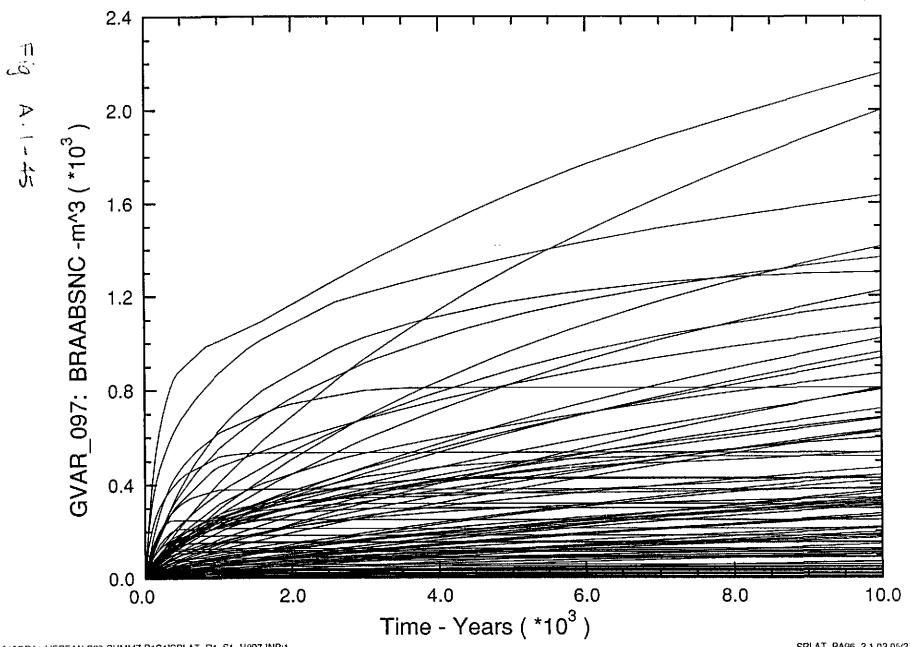


Information Only



SNL WIPP C97: BRAGFLO SIMU TIONS (C97 R1 S1)



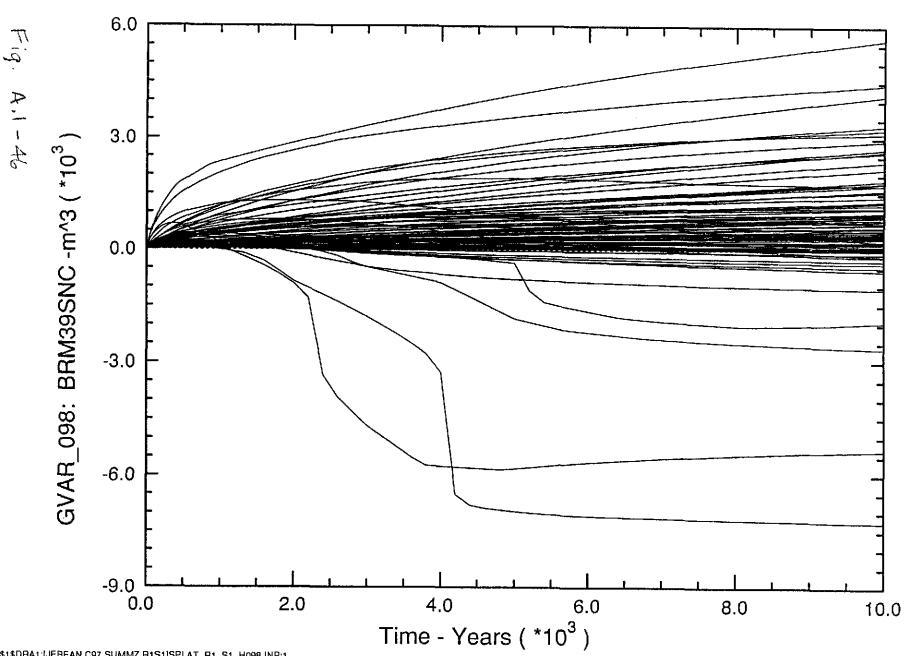


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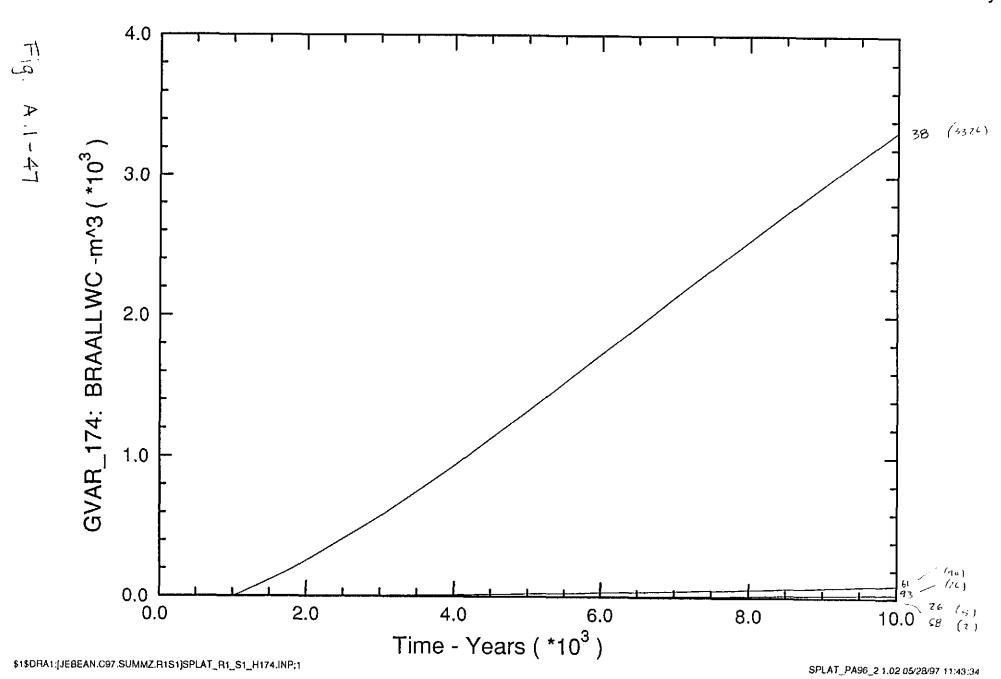
SNL WIPP C97: BRAGFLO SIMPLATIONS (C97 R1 S1)

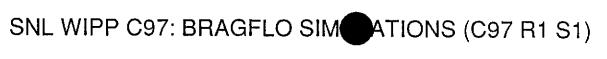
Net Brine Flow at South MB 139



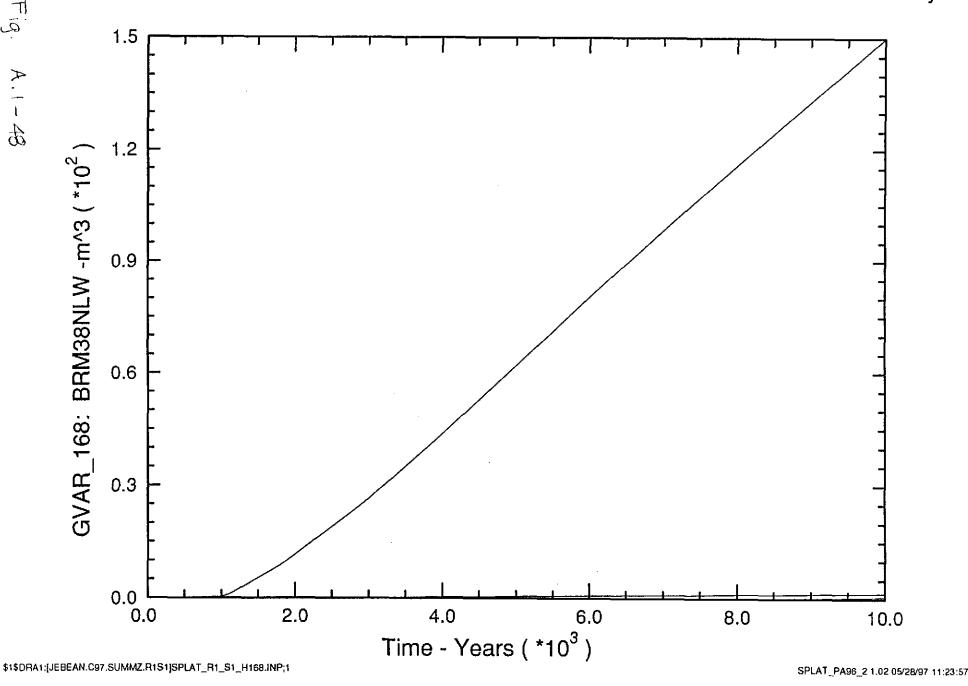


Cumulative Brine Flow Out of All Marker Beds Across Land-Withdrawal Boundary



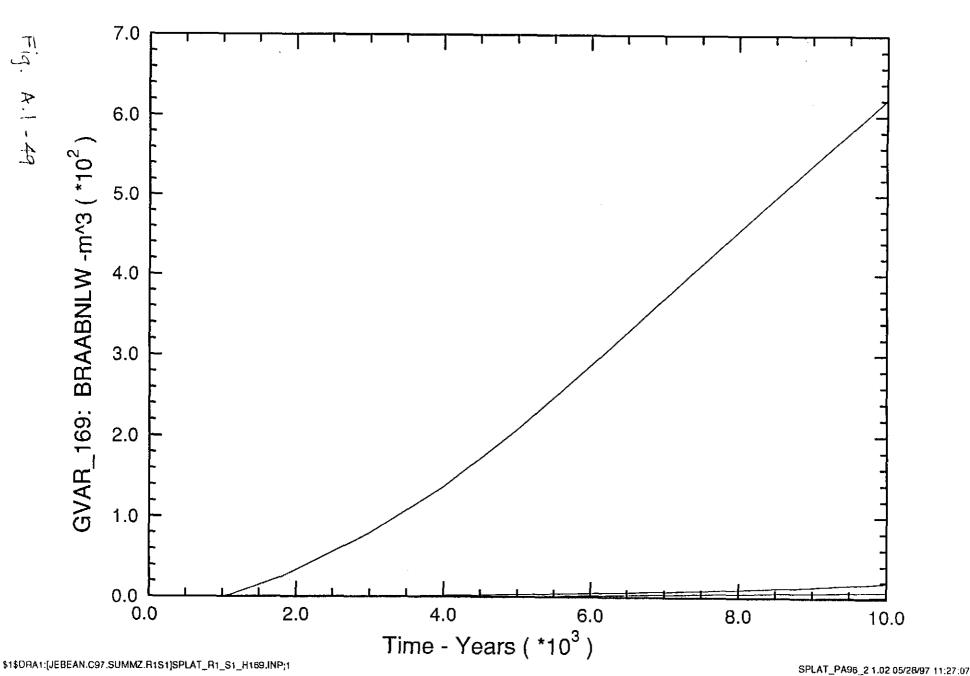






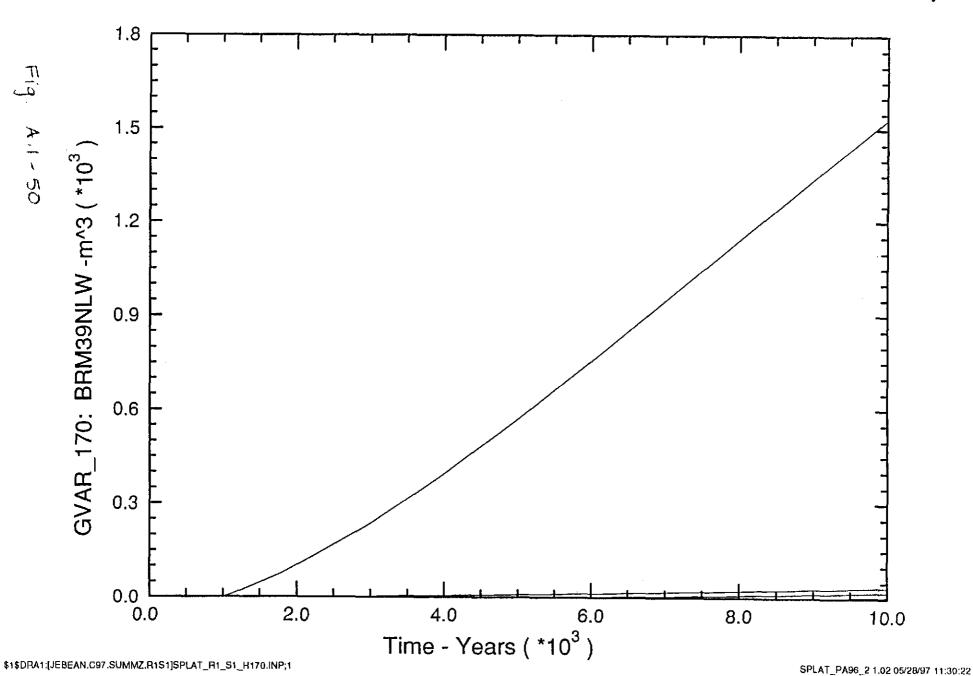


Cumulative Brine Flow Out North Anhydrite A/B Across Land-Withdrawal Boundary



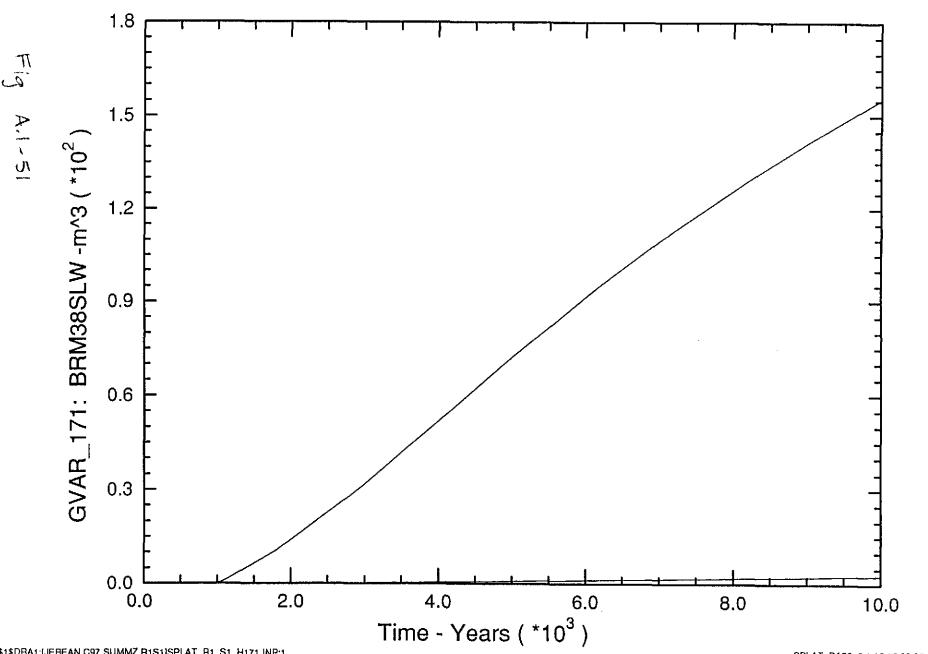


Cumulative Brine Flow Out North MB 139 Across Land-Withdrawal Boundary



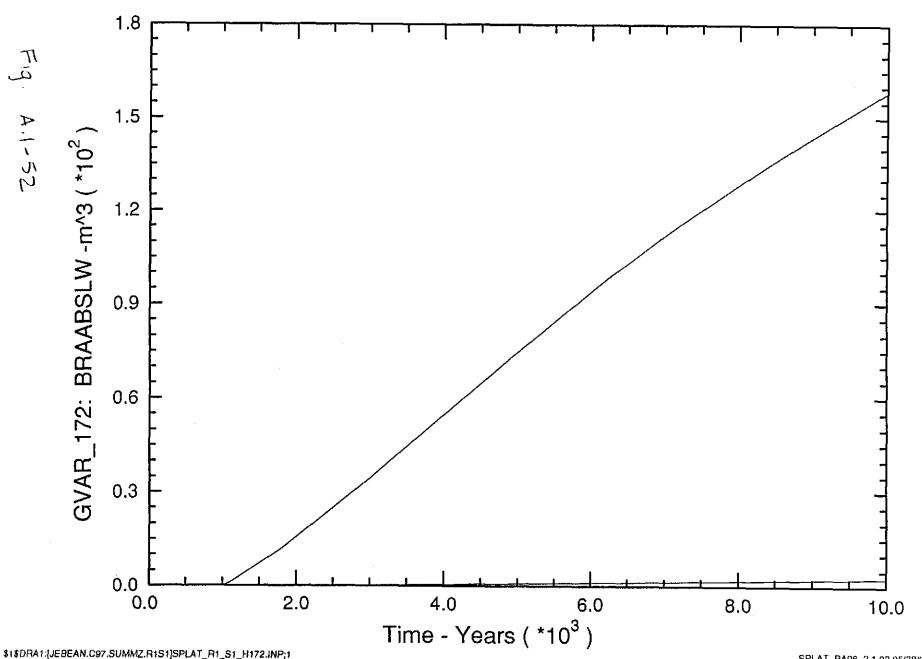


Cumulative Brine Flow Out South MB 138 Across Land-Withdrawal Boundary



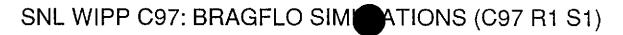
SNL WIPP C97: BRAGFLO SIM ATIONS (C97 R1 S1)

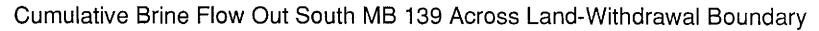
Cumulative Brine Flow Out South Anhydrite A/B Across Land-Withdrawal Boundary

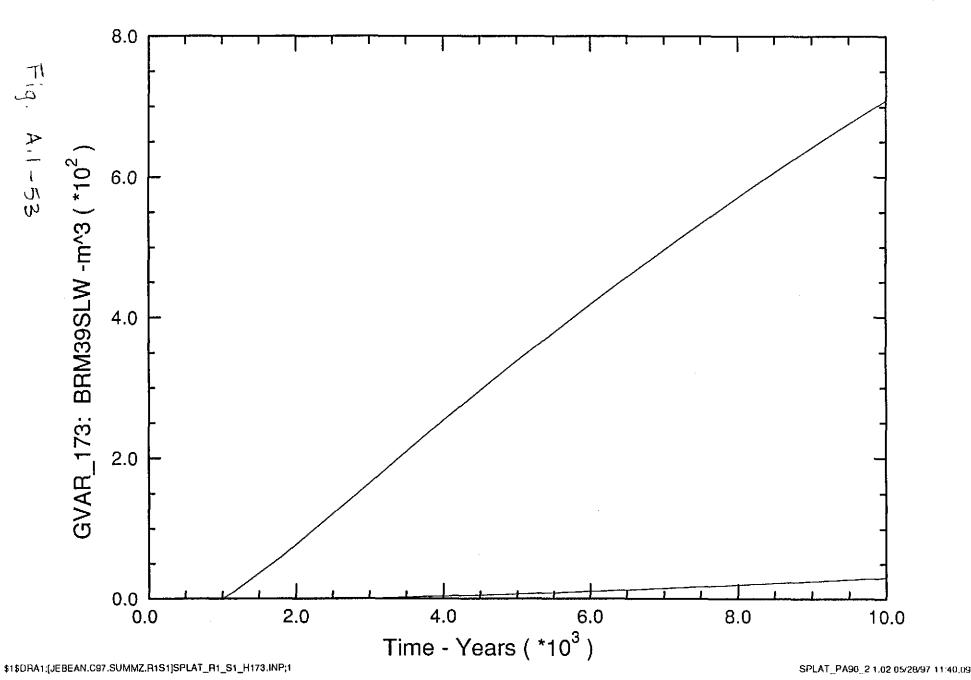


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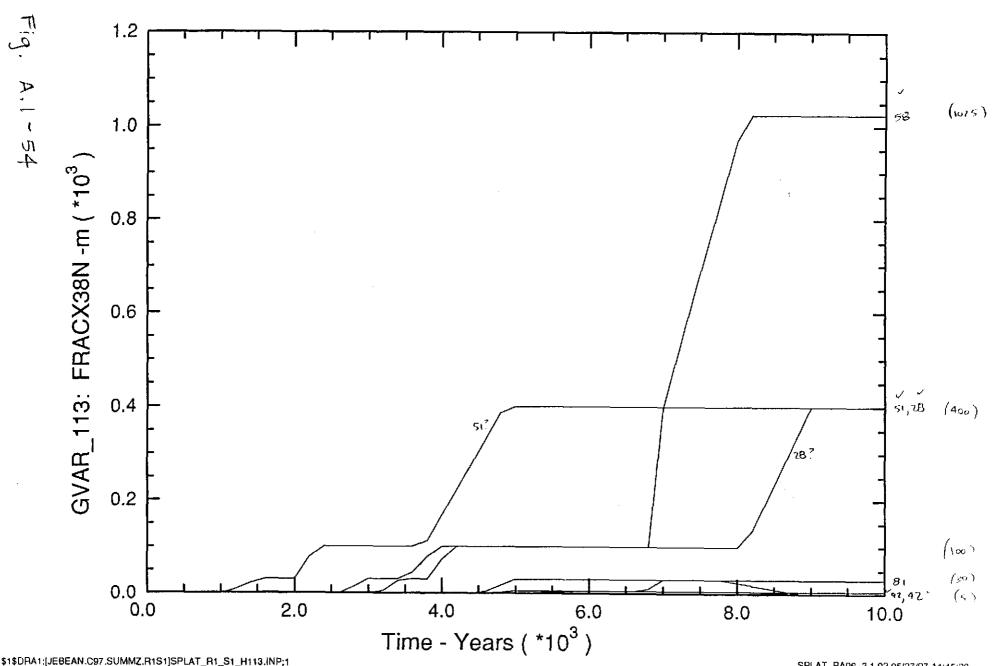






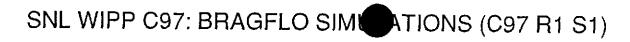
SNL WIPP C97: BRAGFLO SIM LATIONS (C97 R1 S1)

Length of Fractured Zone in North MB 138

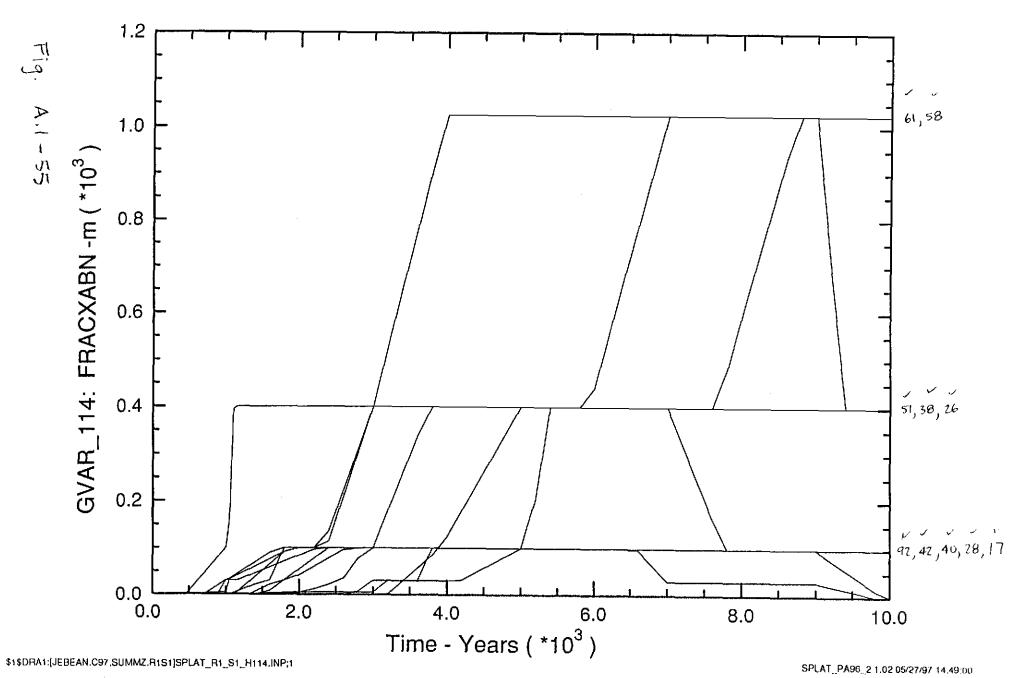


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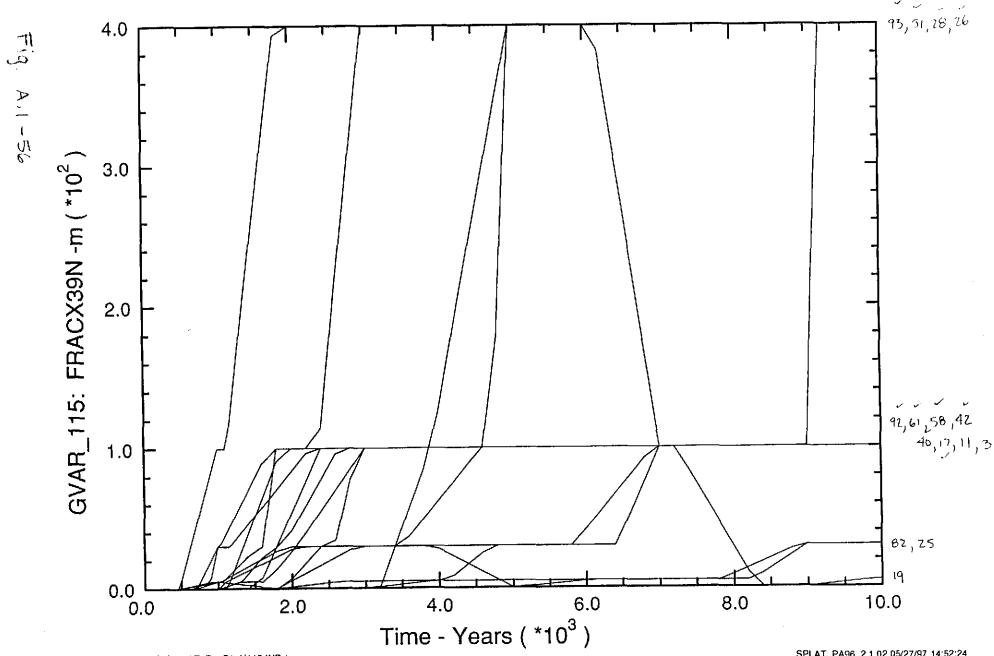


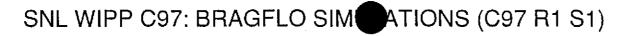
Length of Fractured Zone in North Anhydrite A/B



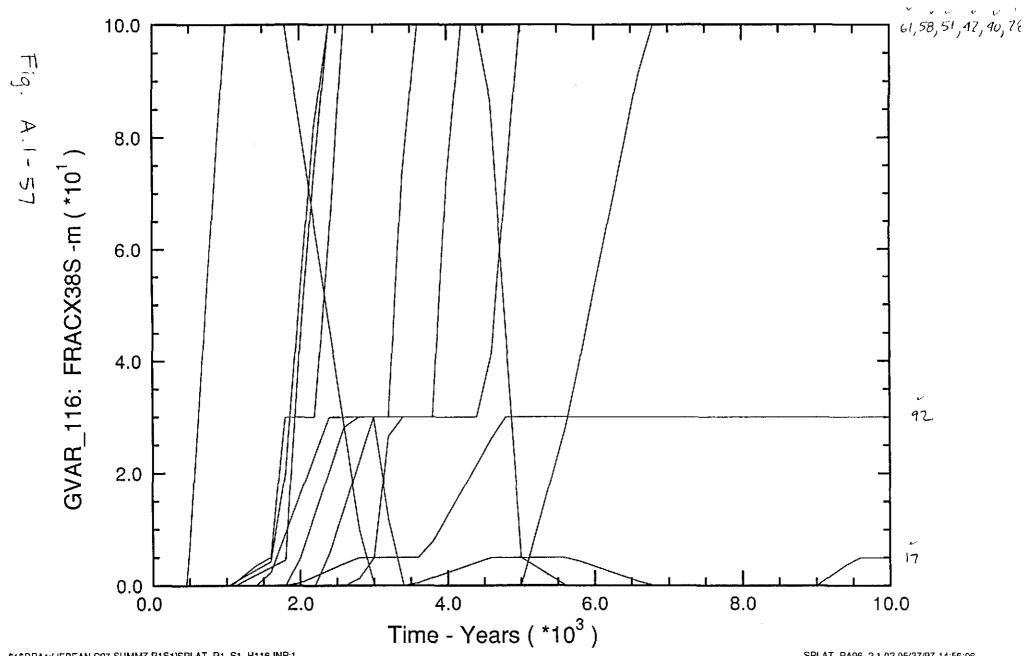


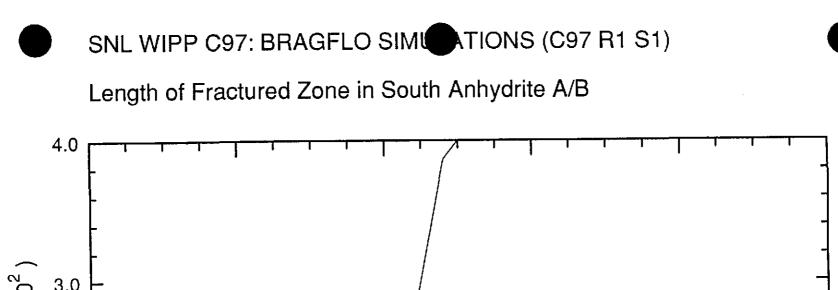
Length of Fractured Zone in North MB 139

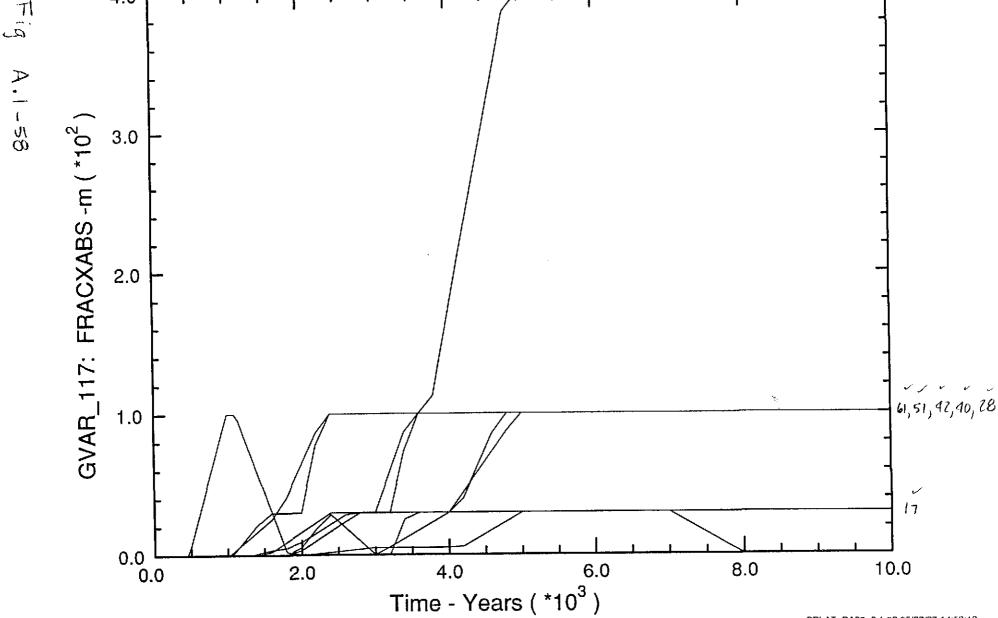




Length of Fractured Zone in South MB 138



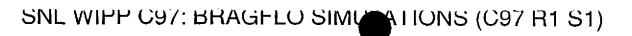




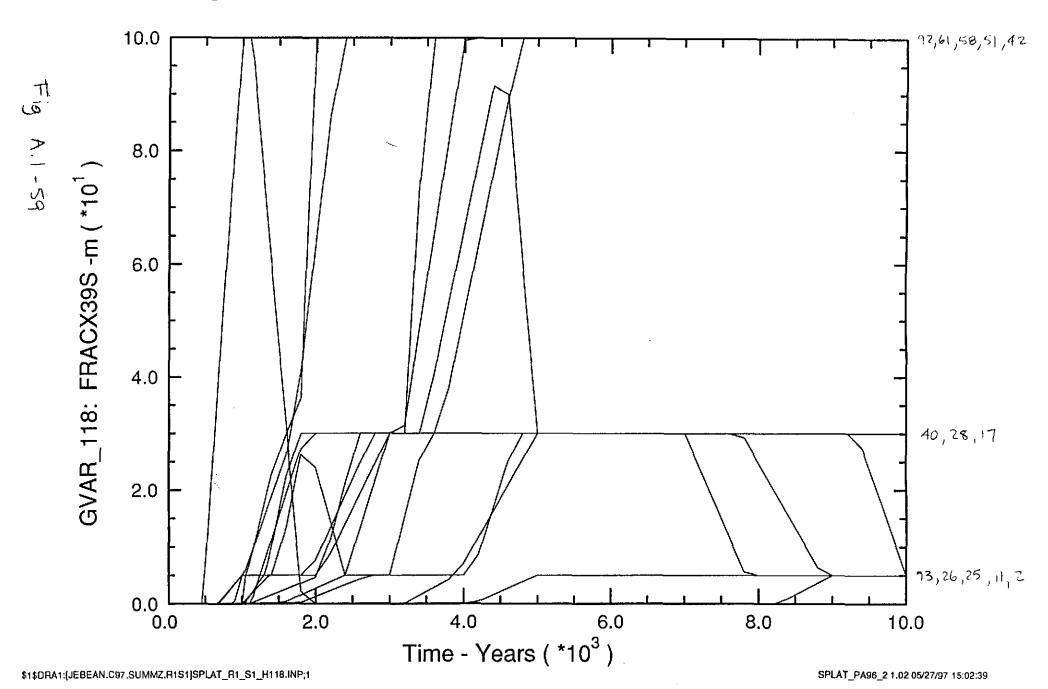
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58

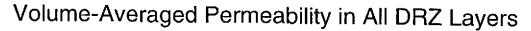


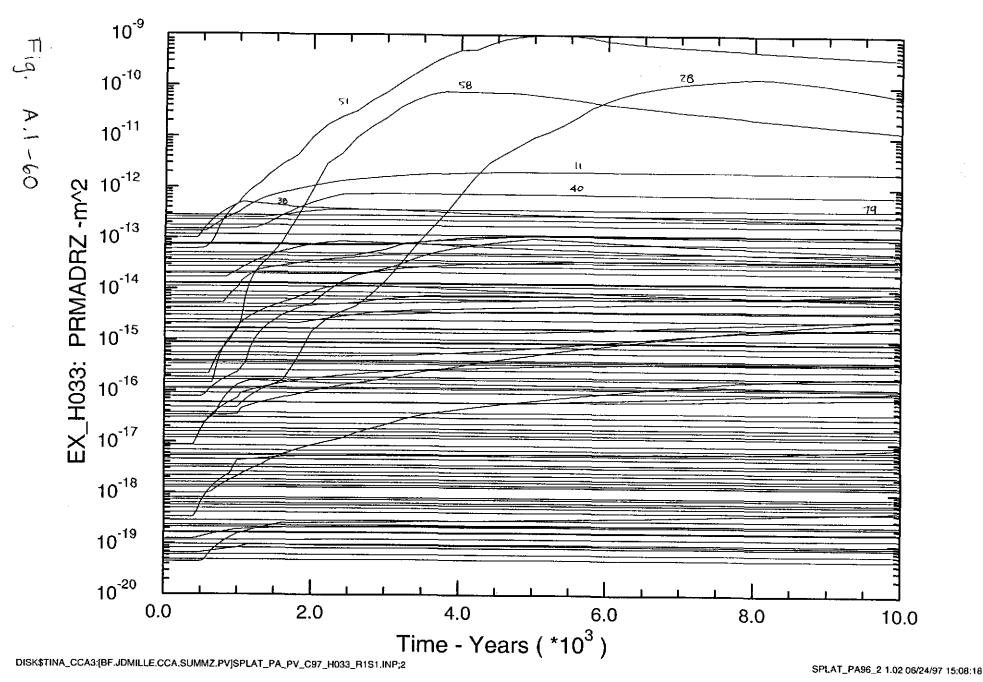
Length of Fractured Zone in South MB 139



Information Only

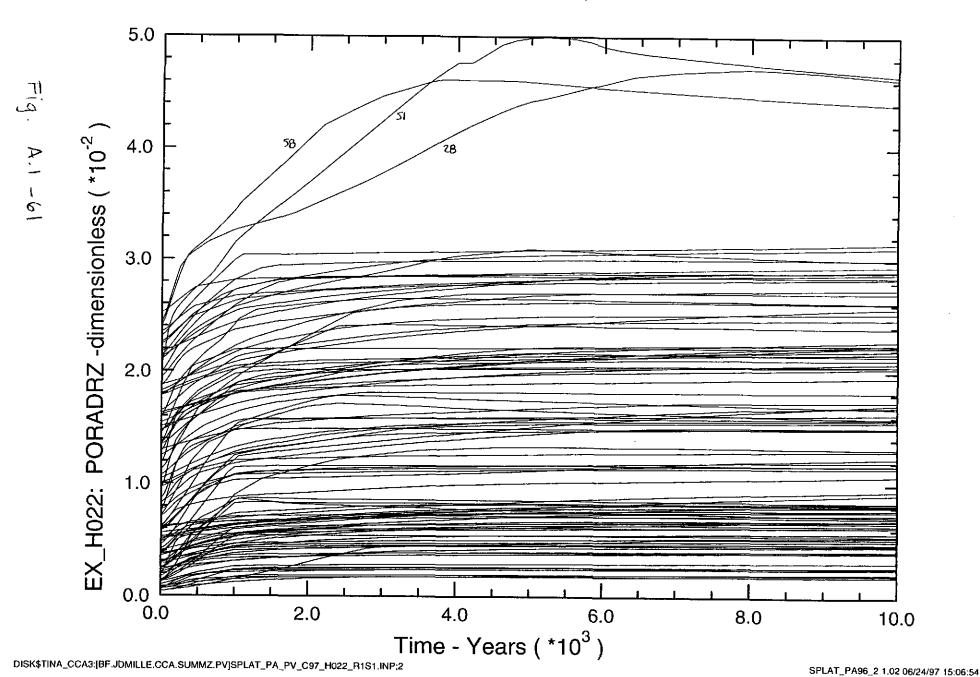
SNL WIPP PA: BRAGFLO SIMU TIONS (C97 R1 S1)





SNL WIPP PA: BRAGFLO SIMU TIONS (C97 R1 S1)





A.2 DISTURBED PERFORMANCE

This section examines repository behavior and the flow of brine and gas for three scenarios: the E1 scenario (Figure A.2-1), the E2 scenario (Figure A.2-2), and the E2E1 scenario (Figure A.2-3). Three potential pathways for migration of radionuclides in dissolved brine are considered. In the first and most likely pathway, contaminated brine may enter the intruding borehole and flow upward toward the Culebra Dolomite Member of the Rustler Formation. As in the undisturbed case, the quantity of brine reaching the Culebra is important because transport may then occur laterally in the Culebra toward the subsurface land withdrawal boundary. In the second pathway, brine may migrate through the panel seals and through the disturbed rock zone (DRZ) surrounding the repository to the shaft and then upward toward the Culebra. In the third pathway, brine may migrate from the repository through the DRZ and laterally toward the subsurface land withdrawal boundary within the anhydrite interbeds.

A.2.1 E1 Intrusion at 1000 Years (S3 Scenario)

In this E1 scenario, a borehole penetrates the waste panel and brine reservoir in the underlying Castile formation at 1000 years. The pressure in the brine reservoir is sampled from a range of 11.1 MPa to 17.0 MPa. It is assumed that the borehole is instantly emplaced and plugged at the time of intrusion. Except for the plugs, the borehole is assumed to have a porosity of 0.32, with the high permeability of 1.0×10^{-9} m² (see Section 3.9 Borehole Model). One plug extends from the top of the Salado formation up through the Unnamed member of the Rustler formation. The other plug extends downward from the surface through the Santa Rosa formation. The permeability of the two plugs is sampled from a range of 1.0×10^{-19} to 1.0×10^{-17} m². These conditions exist for 200 years. At 200 years after intrusion, the borehole material properties are modified to represent the impact of caving, sloughing, and plug degradation. At this time the borehole is assigned uniform properties, with a permeability sampled from a range of 5.0×10^{-17} to 1.0×10^{-11} m². These conditions remain in effect for 1000 years. Then, the section of the borehole from the bottom of the lower DRZ (i. e., the bottom of MB139) down through the Castile is assumed to have undergone creep closure. Creep closure is accounted for by reducing the sampled permeability by a factor of 10.

A.2.1.1 Replicate 1 Results and Discussion

A.2.1.1.1 Repository Behavior

As in the undisturbed scenario, repository behavior is characterized by interactions between creep closure, fluid flow, and gas generation. Creep closure of excavated regions begins immediately because of excavated induced loading. In the waste disposal region, waste consolidation will continue until back-stresses imposed by the compressed waste resist further closure or until fluid pressures become sufficiently high. Pressure in the disposal region is governed by the quantities of brine present in the disposal region, the rates of gas generation, and ease at which fluids can escape the repository. In the Undisturbed scenario, the extent of gas generation in many cases is

controlled by the availability of brine, the principal source of which is the halite and anhydrite layers surrounding the repository. In the E1 scenario, the borehole provides a pathway for additional sources of brine from two locations: (1) flow down the borehole from the Rustler and Dewey Lake Formations overlying the Salado, and (2) flow up the borehole from the pressurized brine reservoir in the Castile underlying the Salado. The rate and direction of brine flow in the borehole depends on the hydraulic properties of the borehole fill material and plugs and the head gradient between the Castile brine reservoir and the overlying strata. Because of the increased availability of brine in the repository, significant quantities of gas may be generated.

Pressures in the waste panel and rest of repository (Figures A.2.1-1 [GVAR_023] and A.2.1-2 [GVAR_024]) increase from their initial value of 1 atmosphere. As in the undisturbed scenario, pressure responses in the experimental and operation regions are nearly identical to those in the waste panel and rest of repository because the permeability of excavated regions, drift and panel seals are high and on the order of 10⁻¹⁵ m². In many realizations, pressure increases rapidly during the first 1000 years. This rapid increase in pressure is caused primarily by gas generation. In these realizations, plastics and rubbers are included in the inventory of biodegradables; this results in a higher net rate of gas generation during the first 1000 years. In some realizations, the pressure reaches a maximum during this initial period and gradually decrease during the remainder of the 10,000 year period. In contrast to this behavior, some realizations (near the bottom of the plot at 1,000 years) exhibit slowly increasing pressures. In these realizations, there is very little gas generation from corrosion (sampled corrosion rates are among the lowest) and none from biodegradation. The third type of behavior exhibited in Figures A.2.1-1 [GVAR_023] and A.2.1-2 [GVAR_024] is a moderately rapid initial rise in pressure. This behavior is a result of creep closure in combination with intermediate gas generation rates.

The observed pressure behavior in the repository prior to intrusion is similar in the PAVT and CCA, with a trend towards slightly higher pressures in the PAVT calculations because of increased corrosion rates. However, after intrusion some distinguishable differences occur because of four factors. Recall that at the time of intrusion the borehole has a high permeability of 1.0×10^{-9} m² everywhere except for two low permeability concrete plugs located above the Salado in the Santa Rosa and Unnamed Members. These borehole conditions remain for 200 years after intrusion, at which time the borehole plugs degrade. Note that in the CCA the concrete plugs had a constant permeability of 5.0×10^{-17} m². However, in the PAVT, concrete plug permeability is a sampled parameter with lower permeability values that range from 1.0 x 10⁻¹⁹ to 1.0 x 10⁻¹⁷ m². The second important factor is the much larger Castile brine reservoir that contains almost two orders of magnitude more brine than it did in the CCA. The third important factor is the higher corrosion rate and the generation of gas at a faster rate. In the PAVT, the inundated corrosion rate is nearly twice as large (uniform distribution in both PAs; range: 0.0 to 3.17×10^{-14} m/s versus 0.0 to 1.58×10^{-14} m/s) as that used in the 1996 calculations. The fourth important factor is the borehole permeability distribution that includes much lower permeability values; in this set of calculations borehole permeability is a sampled parameter that ranges from 5.0×10^{-17} to 1.0×10^{-11} m² versus 1.0×10^{-14} to 1.0×10^{-11} m² in the CCA. As a consequence of these four factors, pressures in the panel increase immediately after intrusion in all vectors

having low panel pressures (less than 7 MPa) at the time of intrusion. This behavior did not occur in the CCA. The range of panel pressures is also narrower and higher during the short 200 year period after intrusion than it was in 1996. Moreover, unlike the CCA, panel pressures in many vectors do increase significantly immediately after intrusion and continue to do so for the remainder of the 10,000 year regulatory period. Pressure behavior after intrusion is described in more detail below.

As in the CCA, three general types of pressure behavior occur after the concrete plugs degrade. In approximately 10% of the realizations, pressures decrease dramatically. In approximately another 10% or so of the realizations, pressures continue to gradually increase for several thousand years. In these realizations, the brine reservoir pressure (a sampled parameter ranging between 11.1 MPa and 17.0 MPa) is sufficiently high to force brine into the panel and maintain increasing pressure conditions. In contrast to the CCA, pressures in many of these vectors continue to increase over the full 10,000 years regulatory period and reach pressures that surpass the long-term pressures predicted in the CCA. Moreover, in the CCA, the highest pressures in the panel occurred prior to intrusion. However, in the PAVT, several vectors ultimately reach pressures that exceed or are near the highest pre-intrusion panel pressures. Corrosion also contributes to the pressure response since corrosion continues in many realizations over the full 10,000 year regulatory period. Gas generation due to microbial degradation in most cases ceases within 1500 years as the cellulose inventory becomes exhausted. Final pressures above hydrostatic pressure occur in those realizations having high corrosion rates and a relatively low borehole permeability that prevents gas from easily escaping the panel and repository. The third and less frequent type of response is for the pressure to rise relatively rapidly following a period of low or slowly decreasing pressure. The time lag between intrusion and repressurization lasts from 500 to over 6000 years. During this time, gas that has filled the panel is driven up the intrusion borehole as brine flows into the waste through the anhydrite layers and down the borehole. Once the borehole is filled with brine, the pressure in the waste reaches hydrostatic pressure relative to the water table in the Dewey Lakes, and then levels off. Pressures below hydrostatic occurs in those realizations where the sampled pressure in the brine reservoir is low and the borehole is filled predominately with gas.

The impact of the borehole on brine availability in the intruded panel and repository is apparent in Figures A.2.1-3 [GVAR_042] and A.2.1-4 [GVAR_046], where numerous realizations have increased brine saturation as compared to the Undisturbed scenario. Prior to the borehole intrusion, profiles of saturation with time are identical to the saturation profiles in the Undisturbed scenario. Note that because of the increased inundated corrosion rate used in the PAVT, repository brine saturations tend to be lower than those predicted in the CCA.

A.2.1.1.1.1 Gas Generation

In the Undisturbed scenario, the extent of gas generation in many realizations is controlled by the availability of brine. The principal source of brine is the halite and anhydrite layers surrounding the repository. In the E1 scenario, the borehole provides a pathway for additional brine.

Consequently, as much as 97% of the initial steel inventory is consumed by corrosion (Figure A.2.1-5 [GVAR_003]) as compared to the Undisturbed scenario where up to 80% of the initial steel inventory is consumed. In the CCA these quantities are 84 % and 60 %, respectively. As in the CCA, cellulose consumption by microbial decay in the E1 Scenario exhibits nearly identical behavior to that observed in the Undisturbed scenario. In all but approximately 10 realizations, the cellulose inventory (which, in 25 of the 100 realizations, includes plastics and rubbers) is completely consumed within 1500 years (Figure A.2.1-6 [GVAR_04]). In contrast to these results, only one realization in the CCA contained a significant amount of cellulose after 10,000 years. This difference in behavior is due in part to the increased corrosion rates in the PAVT and the increased number of vectors where brine is completely consumed in the interior cells of the rest of the repository.

As shown in Figure A.2.1-5 [GVAR_003], the fraction of steel inventory remaining after 10,000 years ranges from 3% to 98%. This wide range in remaining inventories, coupled with the fact that brine saturation in the repository is relatively high in the majority of realizations (Figure A.2.1-4 [GVAR_046]), indicates that the corrosion rate, and not just the availability of brine, plays an important role in determining how much corrosion occurs. This observation was also made in the CCA.

The importance of corrosion rate is also observed in the Undisturbed scenario. In the Undisturbed scenario, steel is present in the panel at the end of 10,000 years in all vectors. In the CCA steel was completely consumed in one vector. In the E1 scenario, the steel inventory in the panel is fully consumed in several realizations because of enhanced brine availability in the intruded down-dip panel via the borehole intrusion (Figure A.2.1-7 [GVAR_144]). In the rest of the repository (Figure A.2.1-8 [GVAR_159]), brine is not as readily available as in the panel for three reasons. First, brine that enters the repository tends to pool in the lower regions and is not available for corrosion in those cells where steel remains. Second, the repository is located updip from the intruded panel. Because of gravity effects, this configuration favors the flow of brine from the repository to the intruded panel and the flow of gas from the panel to the up-dip repository. Third, the panel seal, although highly permeable with a permeability of 10⁻¹⁵ m², does partially inhibit flow between the panel and repository.

The total gas volume generated by corrosion over 10,000 years ranges from about 6×10^5 m³ to 3.05×10^7 m³ (Figure A.2.1-9 [GVAR_017]). In the CCA, the total gas volume generated by corrosion over 10,000 years ranges up to 2.65×10^7 m³. Comparing these quantities with the Undisturbed scenario, in which the amount of gas generated by corrosion ranges from 5×10^5 m³ to 2.28×10^7 m³, it is apparent that the increased availability of brine increases the amount of gas generated by corrosion by approximately 35% (40%). The volume of brine consumed by corrosion in the panel ranges from about 100 m³ to more than 5800 m³ (Figure A.2.1-10 [GVAR_157]). In the rest of the repository, it ranges from 1000 m³ to 42,600 m³ (Figure A.2.1-11 [GVAR_158]). The corresponding values in the CCA range from 100 m³ to 5800 m³ in the panel and from 1000 m³ to 39,000 m³ in the rest of the repository.

As in the CCA, cellulose consumption by microbial decay in the E1 scenario exhibits very similar behavior to that observed in the Undisturbed scenario, essentially the same amount of microbial gas is generated in the E1 scenario as in the Undisturbed scenario: 3.5×10^6 - 3.7×10^6 m³ (3.6×10^6 - 3.7×10^6 m³) at reference conditions (Figure A.2.1-12 [GVAR_020]) when plastics and rubbers are not included and 8.5×10^6 - 1.2×10^7 m³ (1.2×10^7 - 1.2×10^7 m³) when plastics and rubbers are included. Note that approximately 10 vectors do not coincide with the two plateaus representing complete cellulose consumption, these are the vectors noted previously that are limited by the availability of brine. In the CCA, gas generated by microbial degradation was limited in only one vector.

In a plot of total gas generated by corrosion and biodegradation (Figure A.2.1-13 [GVAR_022]), three different types of behavior can be seen. Many curves, especially at the bottom of the plot, increase smoothly, and very slowly. These are realizations in which there is no biodegradation occurring, only the comparatively slower but steady corrosion of iron. A second group of curves rise steeply at first. Most of these result from biodegradation, particularly those realizations in which plastics and rubbers are included in the cellulose inventory. Once biodegradation is complete, in most cases within the first 1500 years, the rate of gas generation decreases sharply as corrosion continues at a slower rate. A third group of realizations, having high corrosion rates, are jump-started by the inflowing brine from the intrusion borehole and exhibit relatively high rates of gas generation after intrusion. This latter behavior is more evident in the panel because the influx of brine immediately after the intrusion affects the panel much more than the rest of the repository (Figure A.2.1-14 [GVAR_146]). These three groups of behavior were also observed in the CCA. In addition, the quantities of gas generated are similar in both PAs with the maximum amount of gas generated being 4.18 x 10⁷ and 3.61 x 10⁷ m³ in the PAVT and CCA, respectively.

A.2.1.1.1.2 Halite Creep

Creep closure of the repository and consolidation of the waste behaves similarly in all realizations as it did in the CCA. In all cases, a very rapid reduction in porosity (Figure A.2.1-15 [GVAR_052]) occurs during the first 300 - 500 years. At the time of intrusion, the waste porosity has mostly leveled off at values ranging from 8% to 20%, depending on the pressure in the waste. When the pressure is high, the porosity remains higher as fluid pressures resist further closure. When the intrusion occurs, the borehole connects the panel with the Castile brine reservoir. However, low permeability plugs located above the Salado in the Santa Rosa and Unnamed Members (see Section 3.3.7) effectively prevent communication with overlying formations for two hundred years subsequent to intrusion. The immediate response depends on the borehole permeability and the Castile brine reservoir pressure relative to the waste pressure. Typically, the borehole has a relatively high permeability and the Castile pressure is higher than the pressure in the waste. The result is an increase in pressure in the waste, in turn causing the porosity to rise slightly at 1000 years.

After 200 years, the plugs in the borehole degrade, raising the borehole permeability to the same sampled value as in the lower portion of the borehole. This increase in permeability generally allows gas and brine to escape up the borehole and reduce pressure in the waste. This pressure reduction causes the waste porosity to decrease. In some cases, the repository pressure and porosity are prevented from decreasing significantly because the borehole permeability is sufficiently low and the gas generation rate is sufficiently high. In other cases, the pressure continues to increase after intrusion. After about 2000 years, the pressure and porosity in the waste generally stabilize. Porosity tends to level off very slowly over time, ranging from 6% up to 22 % of the initial excavated volume by 10,000 years. This range of porosities is slightly broader than that (5 % to 17 %) predicted in the CCA.

As predicted in the CCA, some realizations display more rapid transient responses at later times. In some cases where brine influx is slow but steady, the portion of the borehole above the repository remains gas-filled for hundreds or thousands of years. This gas-filled connection to the overlying formations and ground surface keeps the repository at near-atmospheric pressures. If enough brine flows in, all of the gas (down to residual gas saturation) is eventually driven out of the panel and the panel and borehole fill with brine. This gas is either driven up the borehole or forced up-dip into the rest of the repository and DRZ. As the panel and borehole fill with brine, the pressure in the repository will increase fairly rapidly until hydrostatic pressure relative to the water table in the Dewey Lakes is reached. This relatively rapid increase in pressure, and the resulting increase in porosity, can be seen in some realizations at around 6000 years, both in the pressure plot (Figure A.2.1-1 [GVAR_023]) and in the porosity plot (Figure A.2.1-15 [GVAR_052]). In many other realizations, this process takes place over a much shorter period of time, during the 1000 - 2000 years period following the intrusion. Many realizations tend toward hydrostatic pressures of about 7 MPa and resulting porosities in the range of 11% to 12%.

A.2.1.1.1.3 Fluid Flow

Immediately following the borehole intrusion, there is little upward flow of gas (Figure A.2.1-16 [GVAR_101]) or brine (Figure A.2.1-17 [GVAR_073]) from the panel because the borehole plugs emplaced in the Unnamed and Santa Rosa formations are fairly tight (a sampled parameter from a range of 1.0 x 10⁻¹⁹ to 1.0 x 10⁻¹⁷ m² in the CCA this parameter is a constant 5 × 10⁻¹⁷ m²). However, brine flows rapidly up from the Castile reservoir into the panel (Figure A.2.1-18 [GVAR_072]) in several realizations. In these realizations, the brine reservoir pressure (a sampled parameter from a range of 11.1 MPa to 17.0 MPa) is appreciably higher than the pressure in the panel. The amount of brine flowing immediately into the panel ranges from 0.0 m³ to a maximum of nearly 87,000 m³ (fourth highest vector, #45). The maximum amount is approximately double the maximum amount (44,000 m³) calculated in the CCA. After 200 years, when the plugs degrade, the rate of inflow tends to decrease sharply.

Another group of realizations shows continual flow from the Castile into the panel after intrusion (Figure A.2.1-18 [GVAR_072]). The maximum amount that flows upward in these vectors is 112,000 m³ (#28). This maximum amount is approximately 2.5 times the maximum amount

(44,000 m³) calculated in the CCA. In most of these realizations, brine flow is small prior to plug degradation, and the panel is already pressurized as a result of gas generation. These realizations typically have high corrosion rates and include plastics and rubbers in the cellulose inventory. When the borehole intrudes at 1000 years, the pressure in the Castile is not high enough to drive brine up into the pressurized panel. Only after the plugs degrade, which allows gas to escape up the borehole and reduce the panel pressure, can brine flow upwards from the Castile. At 2200 years, when creep closure reduces the permeability of the section of the borehole between the Castile and the panel by an order of magnitude, the brine flow from the Castile drops off significantly.

There does seem to be a correlation between Castile reservoir pressure, borehole permeability, and the amount of brine that flows up the borehole (Figure A.2.1-17 [GVAR_073]). The top four realizations (#28, #54, #57,#72) have high borehole permeabilities (ranks of 100, 94, 99, 93, respectively) and high initial Castile reservoir pressures (ranks of 83, 96, 80, 79, respectively). The realizations that show immediate flow into the panel tend to have a low borehole permeability, high Castile pressure, and low panel pressure at the time of intrusion. For example the top two immediate flow realizations, #45 and #69, have Castile pressures at the time of intrusion that rank 95 and 98, borehole permeabilities that rank 30 and 41, and panel pressures that rank 2 and 43.

In many cases, once the borehole plugs degrade (at 1200 years), substantial quantities of brine (up to 18,500 m³ compared to 47,000 m³ in the CCA) from the Culebra, Magenta, and Dewey Lakes formations flow downward into the panel (Figures A.2.1-19 [GVAR_140] and A.2.1-20 [GVAR_141]). Lower downward flows in the PAVTas compared to the CCA appear to occur because of the range of lower borehole permeabilities in combination with relatively higher panel pressures at the time of intrusion.

In many realizations, substantial amounts of brine (up to 102,000 m³) flow up the borehole beyond the top of the panel (Figure A.2.1-17 [GVAR_073]). Only very small amounts (at most 1 m³) ultimately reach the top of the Rustler (Figure A.2.1-21 [GVAR_075]). Salado transport results (Section 3.3) show that these small amounts of brine were uncontaminated. In many of these vectors, all of the flow occurs over a very short period (less than 100 years) after the borehole plugs disintegrate at 1200 years. In another 20 or so realizations, brine flow continues upwards in the borehole during the remainder of the 10,000 year regulatory period. Brine flow up the borehole into the bottom of the panel exhibited this same behavior (Figure A.2.1-18 [GVAR_072]). In fact, the three highest borehole flows at the top of the panel (vectors #28, #54, and #57) correspond to the three highest flows at the bottom of the panel (vectors #28, #54, and #57). This behavior is different than that observed in the CCA where the top realization resulted from a combination of high borehole permeability, high marker bed permeability, and low gas generation rate. These characteristics produced the following responses. The low gas generation rate left the panel at low pressure when the intrusion occurred. The low panel pressure, in combination with the high borehole permeability, allowed a large quantity of brine to flow down into the panel from the Culebra, Magenta, and Dewey Lakes and fill the panel

relatively quickly. The high marker bed permeability enhanced the flow of brine in from the marker beds, which forced the large amount of brine occupying the panel back up the borehole.

Flows up the borehole at the top of the DRZ (i. e., at the bottom interface of MB138) (Figure A.2.1-22 [GVAR_078]) are similar (both in magnitude and trend) to flows up the borehole beyond the top of the panel (Figure A.2.1-17 [GVAR_073]). For example, the top four realizations (#28 (1.02 x 10⁵ m³), #54(7.5 x 10⁴ m³), #57 (6.6 x 10⁵ m³), and #72 (6.5 x 10⁵ m³)) for flows at the top of the DRZ correspond, to the top four realizations for flows at the top of the panel (#28 (1.01 x 10⁵ m³), #54(7.5 x 10⁴ m³), #57 (6.6 x 10⁵ m³), and #72 (6.5 x 10⁵ m³)). Note, however, the absence of the realizations that produce, after intrusion, immediate flows beyond the top of the panel. In the CCA, flows up the borehole at the top of the DRZ were substantially lower with maximum quantity at 10,000 yrs of 3.5 x 10⁴ m³.

Gas flow down the borehole and into the Castile reservoir occurs in only six realizations (Figure A.2.1-23 [GVAR_103]). These six realizations are all high gas producers with low initial Castile reservoir pressures. Gas flow takes place during the 200 years following the intrusion, when the section of the borehole between the Castile and the panel is fully open, with a permeability of 1.0×10^{-9} m². The amount of gas that flows into the Castile ranges up to 3×10^{6} m³ (versus up to 1.4×10^{5} m³ in the CCA) resulting in average gas saturations in the brine reservoir ranging from 0.0001 to 0.0038 (Figure A.2.1-24 [GVAR_041]). After 1200 years, gas flow into the Castile ceases. Only a small fraction of the gas that flows into the Castile flows back out (Figure A.2.1-25 [GVAR_104]): about 400 to 2100 m³.

In the CCA, Latin Hypercube Sampling of Castile brine reservoir properties produced five discrete Castile brine reservoir volumes approximately equal to 3.2 x 10⁴ m³, 6.4 x 10⁴ m³, 9.6 x 10⁴ m³, 12.8 x 10⁴ m³, and 16 x 10⁴ m³. Figure A.2.1-26 [GVAR_139] shows the volumes of brine in the Castile reservoir with time used in the PAVT. Recall that these brine volumes are inversely correlated with the compressibility of the Castile reservoir. Note that brine volumes are approximately two orders of magnitude higher in the PAVT as compared to the CCA. Because brine volumes are so large, the reduction in brine volume at the time of intrusion is relatively insignificant (recall that the largest value of brine flow into the bottom of the panel is 1.12 x 10⁵ m³) and almost undetectible on the plot. The pressure in the Castile reservoir (Figure A.2.1-27 [GVAR_028]) shows a drop in pressure after intrusion followed by a gradual pressure decline in approximately 20% of the realizations or very little pressure decline in the remaining realizations. A few realizations exhibit a slight increase in pressure at the time of intrusion, in these cases the panel pressure at the time of intrusion is sufficiently higher than the initial Castile pressure to force some fluid to flow downward to the Castile.

Brine flow up the shaft (Figure A.2.1-28 [GVAR_069]) is small compared to the flow up the borehole, ranging from 0 m³ to 67 m³ (versus 48 m3 in the CCA). It is interesting to note that brine flow up the shaft does not begin until after the borehole intrusion. As in the CCA, this brine is believed to originate in the upper section(s) of the shaft. This conclusion is based on

examination of flows at different locations in the shaft for individual realizations and cannot be verified until Salado transport simulations are analyzed.

Small amounts of brine flow in continuously from the panel seal into the panel (Figure A.2.1-29 [GVAR_181]), primarily as a result of the panel being down-dip from both the rest of the repository and the DRZ beneath the repository. In some instances, flow from the seal into the panel stops or is reversed when intrusion occurs and the panel becomes pressurized with Castile brine. The largest flows seen in (Figure A.2.1-29 [GVAR_181]) are a result of brine entering the panel and rest of the repository from either the Castile or the Culebra, or both, and then, at subsequent times, inflow from the marker beds drives brine back through the panel seal and up the borehole. Most flow from the panel seal into the rest of the repository occurs following the intrusion (Figure A.2.1-30 [GVAR_182]) as Castile or Culebra brine fills the excavated regions with brine. Consequently, cumulative brine flows across the panel seal and out of the panel are very similar to cumulative brine flow across the panel seal and into the rest of the repository (Figures A.2.1-30 [GVAR_182] and A.2.1-31 [GVAR_183]): they both show flow in the northerly direction, from the panel towards the rest of the repository. Also, flow from the repository into the panel seal (Figure A.2.1-32 [GVAR_184]) is similar to flow across the panel seal and into the panel (Figure A.2.1-29 [GVAR_181]). The characteristics of the panel seal flows described above are very similar to thos predicted in the CCA.

A.2.1.1.2 Behavior in Formations Surrounding the Repository

A.2.1.1.2.1 Two-Phase Flow

Gas flows into the interbeds are presented in Figures A.2.1-33 [GVAR 106] to A.2.1-39 [GVAR_112]. Relatively few realizations (compared to the Undisturbed scenario) result in gas flow from the DRZ into the marker beds. In MB138, the largest of seven realizations shows 36,000 m³ (versus 40,000 m³ in the CCA) flowing to the north (Figure A.2.1-33 [GVAR_106]) and 62,000 m³ (versus 35,000 m³ in the CCA) flowing to the south (Figure A.2.1-36 [GVAR_109]). In Anhydrite a and b (Figures A.2.1-34 [GVAR_107] and A.2.1-37 [GVAR_110]), many realizations show small flows of gas (less than 6,000 m³). In eight (versus 3 in the CCA) realizations more than 10,000 m³ flow out; the maxima are 400,000 m³ to the north and 130,000 m³ to the south (versus 133,000 m³ and 77,000 m³, respectively, in the CCA). In MB139, a maximum of 800,000 (versus 11,400 m³ in the CCA) flows to the north (Figure A.2.1-35 [GVAR_108]); to the south, there is substantial gas flow in only two realizations, the larger flow being 66,000 m³ (versus 9,400 m³ in the CCA) (Figure A.2.1-38 [GVAR_111]). At the end of the 10,000 year regulatory period, a maximum of 1.25 x 10^6 m³ (versus 2.9×10^5 m³ in the CCA) has flowed from the DRZ into the marker beds (Figure A.2.1-39 [GVAR_112]). Note that in several realizations, the flow of gas out into the interbeds continues well after the borehole penetrates the panel. This behavior is in contrast to the behavior observed in the CCA, where the flow of gas out into the interbeds in all realizations stopped when the borehole plugs degraded.

Once the borehole plugs degrade at 1200 years, large volumes of gas [up to 1.85×10^7 m³(8.5×10^6 m³)] are vented up the borehole (Figure A.2.1-16 [GVAR_101]). In several realizations, gas flow from the panel continues as long as gas is generated. In the CCA, gas flow from the panel generally occurred over a shorter period of time, about 500 years. Larger volumes of gas flow up the borehole from the DRZ (Figure A.2.1-40 [GVAR_102]]). The total amount of gas vented up the borehole ranges up to 38×10^6 m³ (32×10^6 m³). The maximum total amount of gas generated is 42×10^6 m³ (36×10^6 m³) (Figure A.2.1-13 [GVAR_022]). Thus, as in the CCA, a large fraction of the gas generated eventually flows up the borehole. Very little gas flows up the shaft. Figure A.2.1-41 [GVAR_100] shows that a maximum of 25 m³ (22 m³) flows up the shaft at the interface between the Salado and Rustler formations. A detailed examination of gas flows at different locations in the shaft found that this gas came exclusively from the asphalt shaft seal immediately below this interface. None of this gas originates from lower elevations in the shaft, including the repository. Thus, the shaft seals are very effective in keeping gas from flowing up the shaft.

In addition to the shaft and borehole pathways, potentially contaminated brine can get to the land withdrawal boundary by flowing from the repository through the DRZ and into one of the permeable anhydrite layers (MB138 or 139 or the combined Anhydrite a and b). These flows are examined next.

Cumulative net brine flows into and out of the DRZ region surrounding the repository from all anhydrite layers is shown in Figure A.2.1-42 [GVAR_099] and are listed in Table A.2.1-1. In this figure, positive values indicate flow inward. Net inward flow occurs in all but three (zero) realizations, with the maximum being 32,000 m³ (64,000 m³). The distribution of net brine flows among the various anhydrite layers to the north and south of the repository are shown in Figures A.2.1-43 [GVAR_093] to A.2.1-45 [GVAR_095] and Figures A.2.1-46 [GVAR_096] to A.2.1-48 [GVAR_098]. In these figures, positive flows are to the north and negative flows are to the south. These figures show that almost all net flows are inward with less than five exceptions.

Table A.2.1-1. Cumulative Net Interbed Brine Flows for E1 Intrusion at 1000 Years (S3 Scenario)

Marker Bed	Max. Net Brine Flow from MB into DRZ, m ³	Max. Net Brine Flow from DRZ into MB, m ³
MB138 North	40(300)	40(4)
MB138 South	1,080(3,700)	0(0)
Anhydrite a & b North	4,180(8,800)	0(0)
Anhydrite a & b South	5,000(9,800)	0(0)
MB139 North	10,700(20,200)	1,000(100)
MB139 South	10,800(21,200)	2,800(200)
All Marker Beds	32,800(64.000)	3,800(304)

The maximum amount of brine that flows in from the marker beds is about 70% (50%) smaller

(greater) than the maximum that flows up the borehole from the Castile, $32,800 \text{ m}^3(64,000 \text{ m}^3)$ vs. $112,000 \text{ m}^3(44,000 \text{ m}^3)$. Note that in the CCA this flow condition was reversed with the maximum amount of brine flow from the marker beds 50% greater than the maximum that flows up the borehole from the Castile.

The corresponding cumulative flows out all anhydrite layers and across the land withdrawal boundary are summarized in Figure A.2.1-49 [GVAR_174] and Table A.2.1-2. Flows in individual layers are presented in Figures A.2.1-50 [GVAR_168] to A.2.1-55 [GVAR_173]. As shown, brine flow out across the land withdrawal boundary occurs in only one vector (#38) and the majority of flow occurs northward. The maximum volume released in all marker beds over the 10,000 years regulatory period is 2,630 m³(1.28 m³). Note that this amount is much larger than was calculated in the CCA. An examination of the sampled parameter values for vector #38 indicate that this vector had the highest sampled MB139 permeability in combination with the 7th highest sampled DRZ permeability and the 17th lowest borehole permeability. This vector also had a very low DRZ porosity and a low far-field pressure. However, this brine does not come from the repository since at most 1315 m³ flows to the north into MB139 from the DRZ, which is far less than the pore volume of MB139 which is 155,500 m³ between the repository and the land withdrawal boundary. This conclusion is verified by the Salado transport calculations analysis.

Table A.2.1-2. Cumulative Interbed Brine Flows Outward Across Land Withdrawal Boundary for E1 Intrusion at 1000 Years (S3 Scenario).

Marker Bed	Maximum Brine Outflow across Land Withdrawal Boundary, m ³
MB138 North	106(0.19)
MB138 South	120(0.0)
Anhydrite a & b North	488(0.27)
Anhydrite a & b South	118(0.0)
MB139 North	1,315(0.82)
MB139 South	483(0.0)
All Marker Beds	2630(1.28)

A.2.1.1.2.2 Mechanical Response

In most realizations, gas is not generated at sufficiently high rates to reach fracture pressures prior to the intrusion at 1000 years. After the intrusion, the borehole prevents pressures from building up in all but a few realizations to the point where fracturing could again take place. As a consequence, fracturing in the interbeds occurs in only a few realizations (A.2.1-56 [GVAR_113] to A.2.1-61 [GVAR_118]). The most extensive fracturing (vector #78) occurs to the north in

Anhydrite a and b and Marker Bed 139, the fracture length is 400 m. In the CCA, most of the fracturing occurs to the north in Marker Bed 138 and Anhydrite a and b, the fracture length up to 100 m. In these layers, the fracture length is 100 m. Other realizations displayed fracturing only in Anhydrite a and b to the north, and in Marker Bed 139, both north and south. In these realizations, the maximum extent was 30 m. Note that fracture curves that go to zero indicate fracture closure as pressures decrease.

DRZ fracturing occurs in about 20 vectors, however, in most vectors DRZ fractures close in less than 500 years after the borehole intrusion. Significant fracturing in the DRZ after intrusion occurs in only about 5 realizations, as indicated by increasing DRZ permeability (Figure A.2.2-62 [EX_H033]). Vector #78 exhibits the largest DRZ permeability increase (vector with highest permeability after 2000 years). This vector had a low borehole permeability (rank of 5), a low marker bed permeability (rank of 8), and a relatively high initial DRZ porosity (rank of 61). Note that this vector also produced the most extensive marker bed fracturing. DRZ porosity increases, indicative of DRZ fracturing are also evident in several realizations (Figure A.2.2-63 [EX_H022]). Only one realization (#78) results in a long-term DRZ permeability greater than 1x10⁻¹¹ m² and porosity greater than 0.035. Mean, median, and maximum values for DRZ permeability and porosity are shown in Table A.1-3.

A.2.1.2 Comparison with Other Intrusion Time [350-year version of E1 (S2 Scenario)]

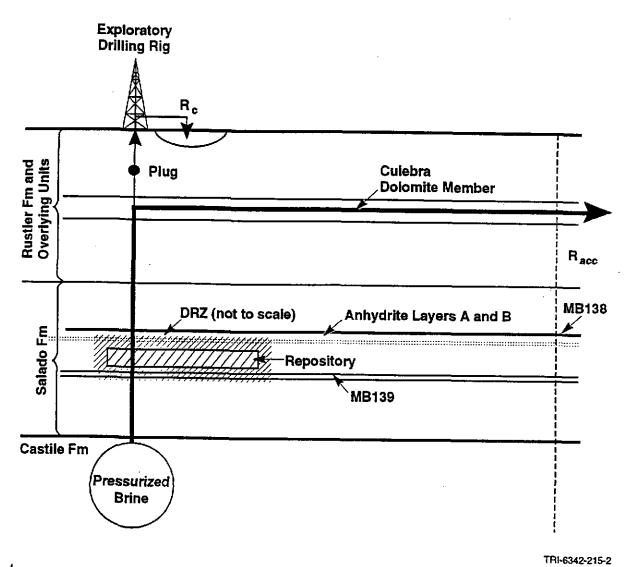
The S2 Scenario is another E1 scenario in which the intrusion occurs at 350 years instead of 1000 years. The borehole properties are the same as in the 1000-year intrusion, but changes take place 650 years earlier. At 350 years, the borehole is open with a permeability of 1.0×10^{-9} m² from the Castile brine reservoir up to the surface, except for two plugs, each having a permeability that is sampled from a range of 1.0×10^{-19} to 1.0×10^{-17} m² (5.0×10^{-17} m²). The plugs are located in the Unnamed Member of the Rustler Formation and in the Santa Rosa Formation. After 200 years, the plugs degrade into silty sand and the rest of the borehole becomes filled silty sand; the entire borehole has a sampled permeability that ranges from 5.0×10^{-17} to 1.0×10^{-11} m² (1.0×10^{-14} m² to 1.0×10^{-11} m²). These conditions persist for 1000 years. At 1550 years, the segment of the borehole from the Castile to the waste panel undergoes creep closure, resulting in a decrease in permeability by a factor of 10 from the sampled value. These conditions remain in effect for the remainder of the 10,000 years.

Since the intrusion time is earlier (350 years), not as much gas is generated prior to intrusion. As a result, the pressure in the waste does not build up as high prior to intrusion as in the 1000-year intrusion scenario. The peak pressure observed in the waste panel at the 350-year intrusion is 12.4 MPa (12.2 MPa), compared with 14.0 MPa (14.1 MPa) in the 1000 yr intrusion scenario (S3). However, at later times the peak pressure in S2 is 16.7 MPa versus 15.5 MPa in S6. Because of higher repository pressure at later times, increased fracturing of the marker beds occur. Note that in the CCA, peak repository pressures in the S2 scenario were less than those in the S6 scenario and as a result fracturing did not occur. In the PAVT S2 scenario, the maximum fracture length is 1900 m to the north in MB139 and MB a and b compared to 400 m in S6.

Although peak pressures are higher in S2 than in S3, approximately the same amount of gas is generated over the 10,000 years. The reason for this behavior appears to be that the additional brine provided by the earlier intrusion is used to drive reactions faster. After 1000 years, approximately the same amount of brine is available for the reactions regardless of whether the intrusion occurs at 350 years or 1000 years. The cellulose inventory is again fully consumed in most vectors, as it is in the 1000 yr case, in all but the same 8-10 realizations.

Except for some transients between 350 and 1200 years, the porosity in the waste differs very little from the later intrusion. After the first few hundred years, the porosity is a damped response to pressure and tracks the waste pressure very closely. After about 1200 years, the pressure in the waste behaves similarly in both the earlier and later intrusions. Because the pressure in the waste panel is less at the time of intrusion when the intrusion occurs at 350 years, more brine is able to flow immediately into the panel from the Castile — a maximum of 115,000 m³ (53,000 m³) compared with 87,000 (44,000 m³) immediately following the 1000-year intrusion. However, maximum brine flow up the borehole from the top of the DRZ is approximately the same because the long-term flows, which are the largest, are controlled primarily by the large Castile brine pocket. As in the S3 scenario, only very small amounts of uncontaminated brine (<1.2 m³) flowed upward in the borehole beyond the top of the Rustler. Since the amount of gas generated is approximately the same regardless off intrusion time, the lower initial pressure results in a correspondingly lower driving force for brine up the borehole. As in all other scenarios and replicates, very little brine flows up the borehole beyond the Rustler in any realization in this scenario; almost all of it flows into the Culebra.

Net brine flow into the DRZ from the marker beds is about the same for the 350-year intrusion as for the 1000-year intrusion. The maximum amount is slightly lower at 26,000 m³ in S2 than the 32,800 m³ in S3 (in the CCA the corresponding volumes were 62,000 m³ vs. 64,000 m³ in the 1000-year intrusion). Conversely, net brine flow out of the DRZ and into the marker beds is higher in the earlier intrusion. The maximum outflow is 8200 (233 m³), compared with 3800 m³ (670 m³) after the later intrusion. The maximum brine outflow in all marker beds across the land withdrawal boundary is similar in both S2 and S3, 2500 m³ (0.8 m³) and 2600 m³ (1.3 m³), respectively.



A.2-1

Figure 7.2-1. Conceptual model for scenario E1. Arrows indicate assumed direction of flow. Exploratory borehole penetrates pressurized brine below the repository horizon. R_c is the release of material directly from the drilling operation. R_{acc} is the release at the subsurface boundary of the accessible environment. A plug above the Culebra Dolomite Member is assumed to remain intact for 10,000 years.

Information Only

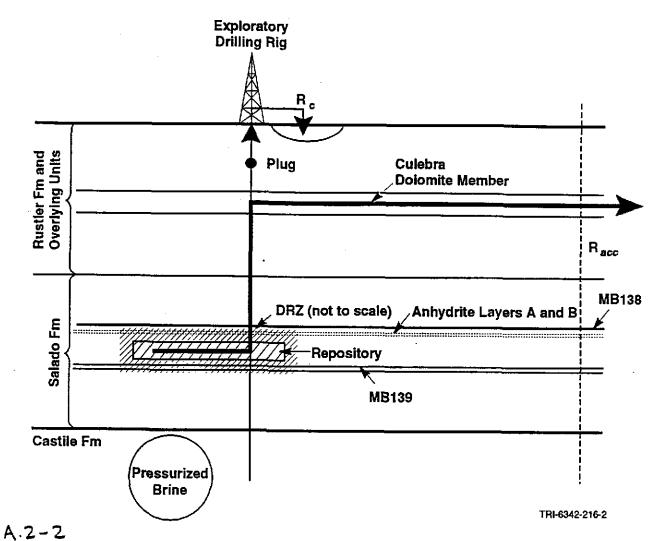
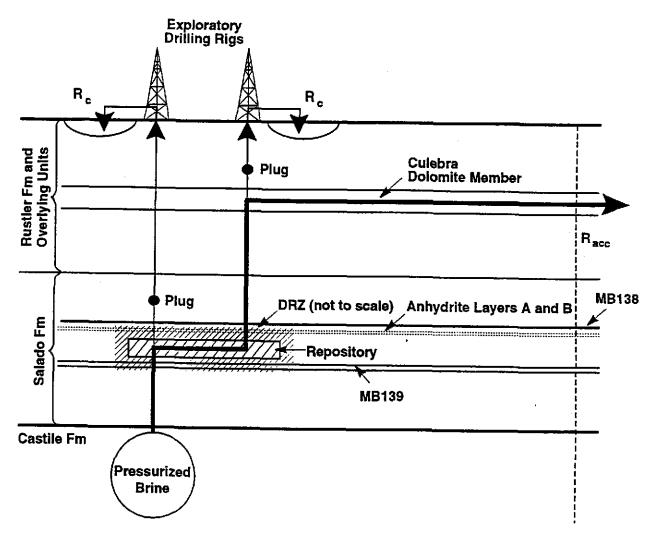


Figure 7.2-2. Conceptual model for scenario E2. Arrows indicate assumed direction of flow. Exploratory borehole does not penetrate pressurized brine below the repository horizon. R_c is the release of material directly from the drilling operation. R_{acc} is the release at the subsurface boundary of the accessible environment. A plug above the Culebra Dolomite Member is assumed to remain intact for 10,000 years.

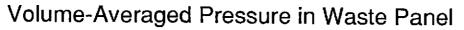


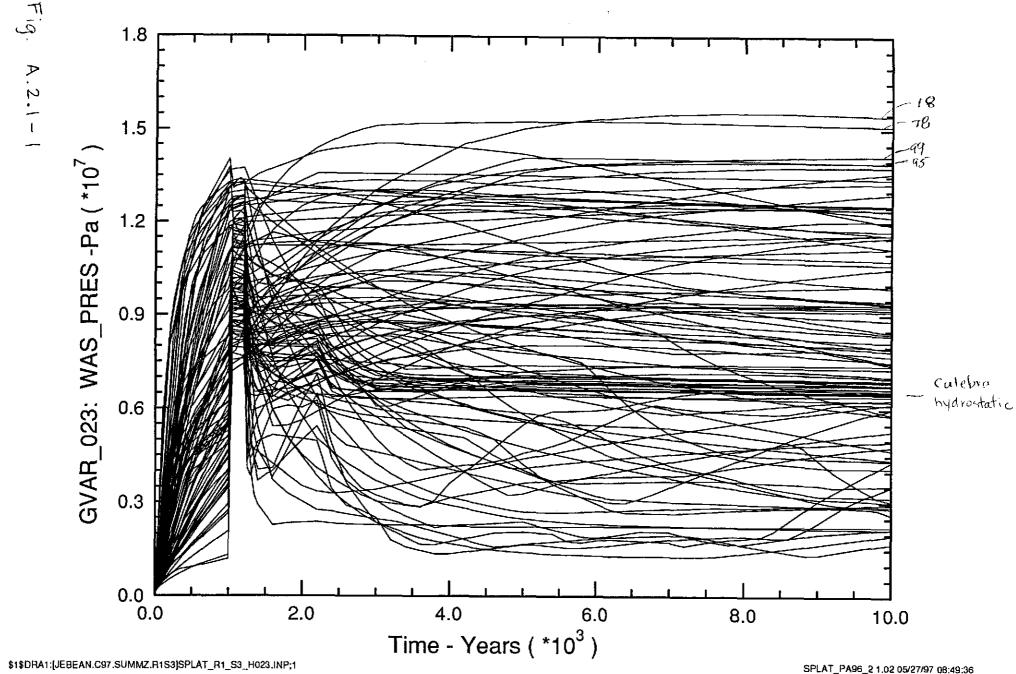
A.Z-3

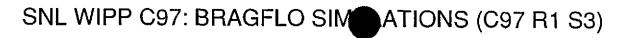
Figure 7.2-3. Conceptual model for scenario E1E2. Arrows indicate assumed direction of flow. One exploratory borehole penetrates pressurized brine below the repository horizon a plug between the repository and the Culebra Dolomite Member is assumed to remain intact for 10,000 years. The second borehole does not penetrate pressurized brine below the repository; a plug above the Culebra Dolomite Member is assumed to remain intact for 10,000 years. R_c is the release of material directly from the drilling operation. R_{acc} is the release at the subsurface boundary of the accessible environment.

Information Only

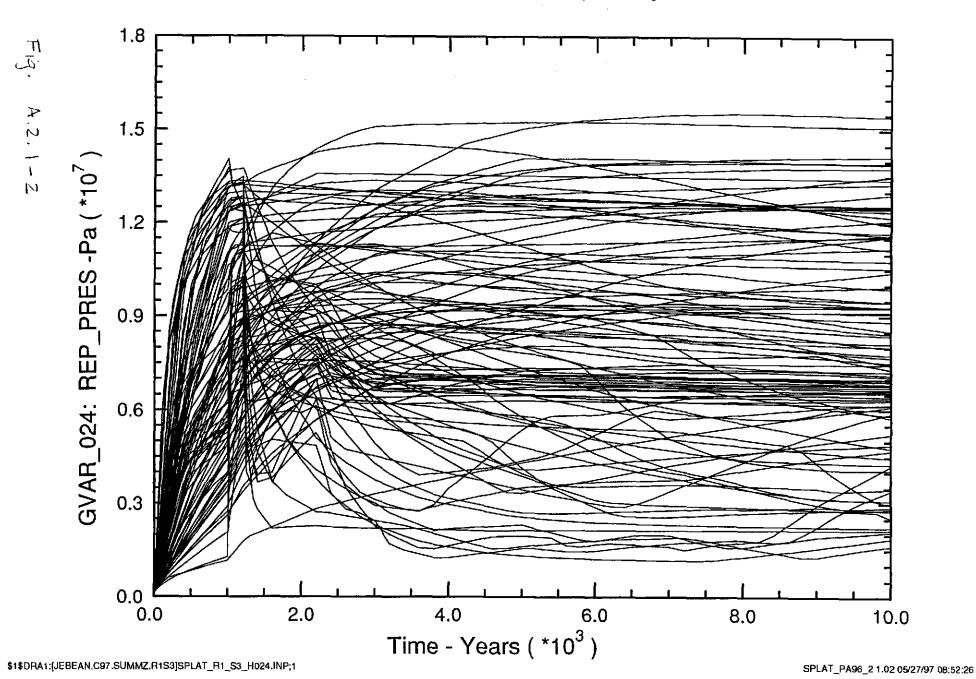




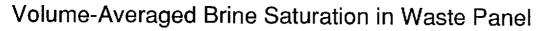


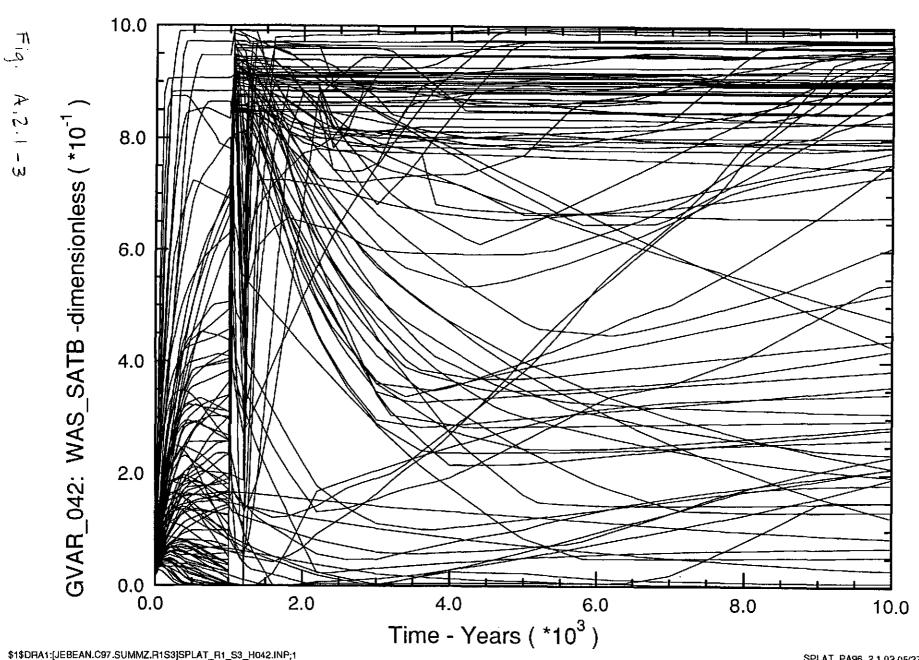


Volume-Averaged Pressure in Rest of Repository



SNL WIPP C97: BRAGFLO SIM ATIONS (C97 R1 S3)





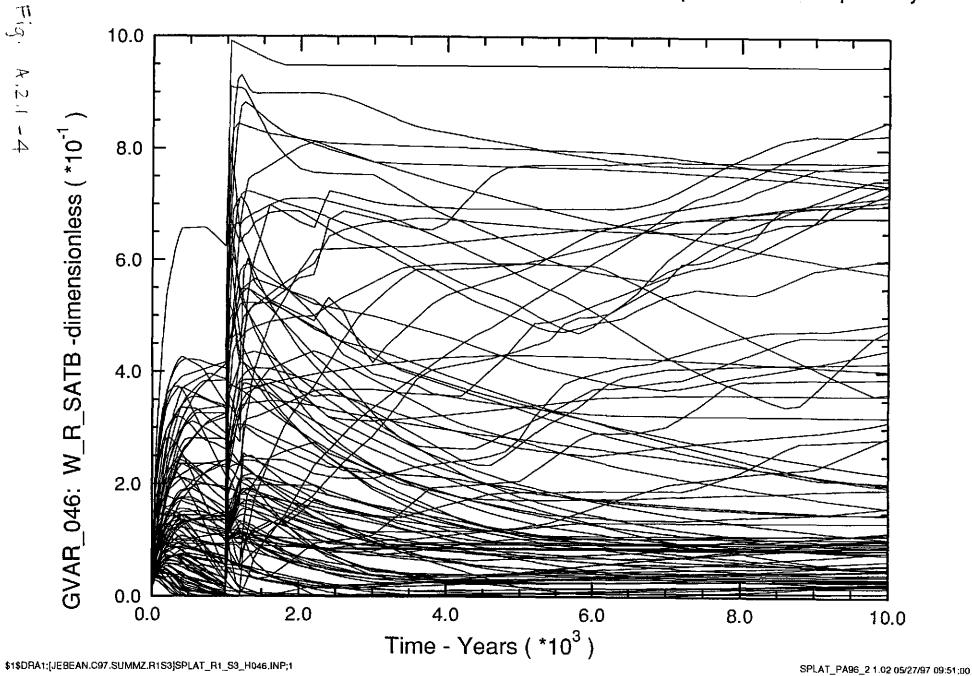
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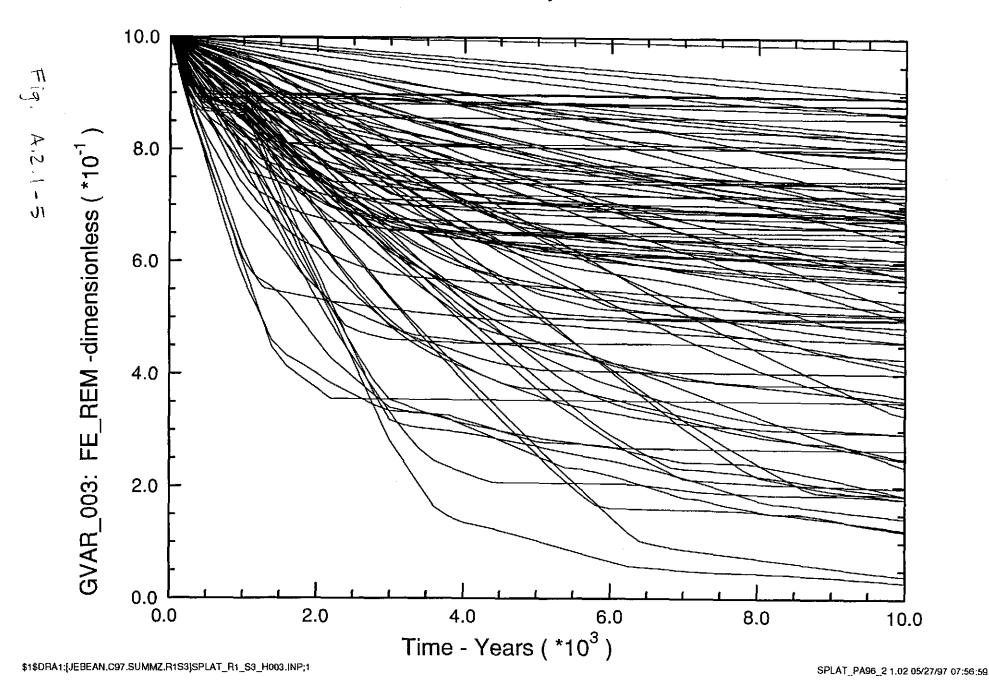


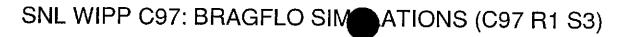
Volume-Averaged Brine Saturation in Waste Panel plus Rest of Repository



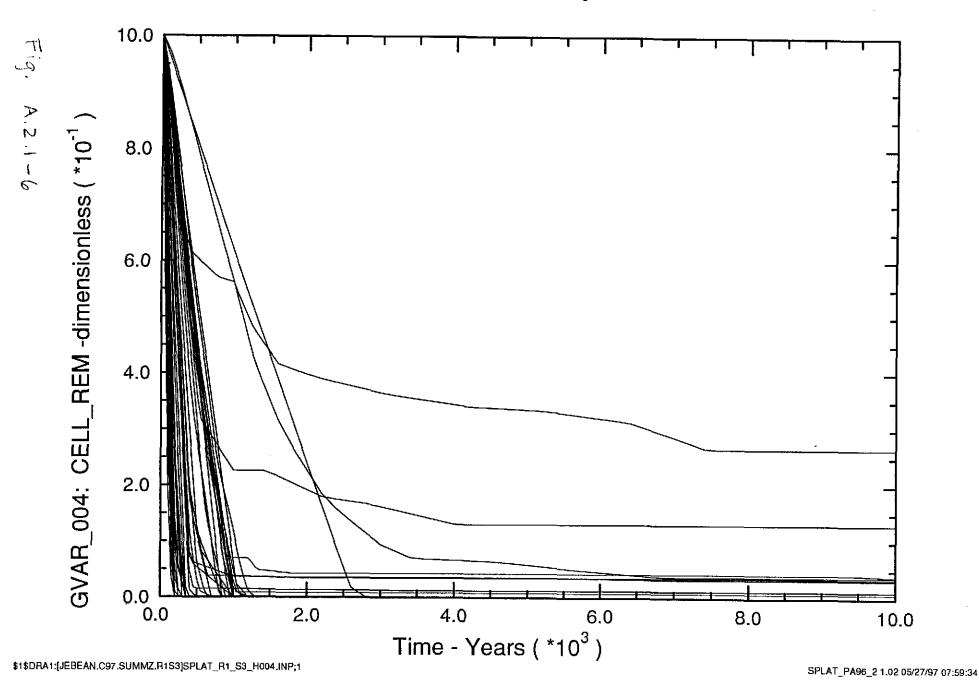


Remaining Fraction of Steel Inventory

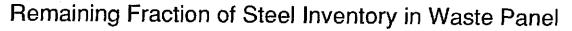


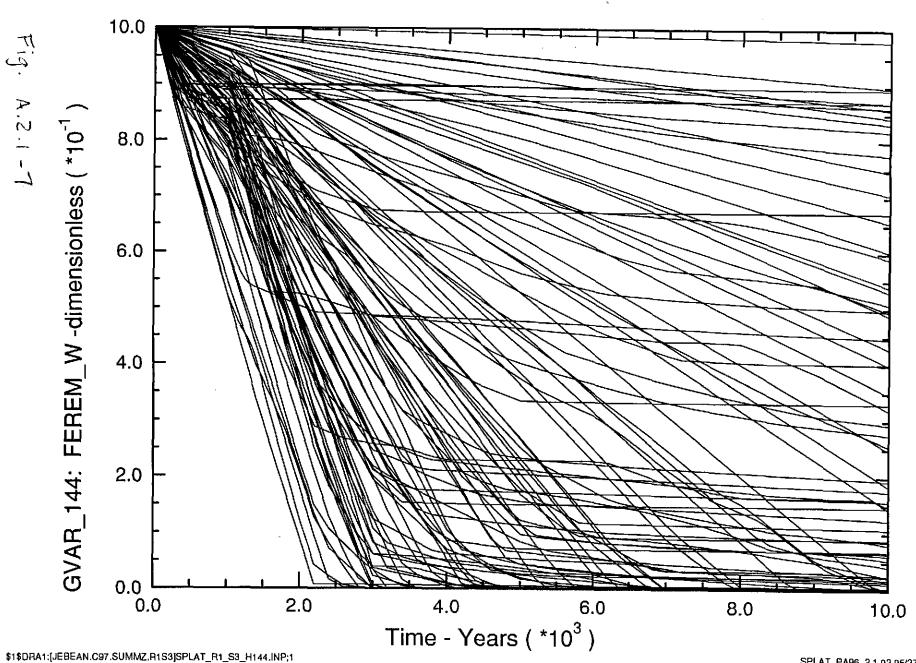


Remaining Fraction of Cellulose Inventory



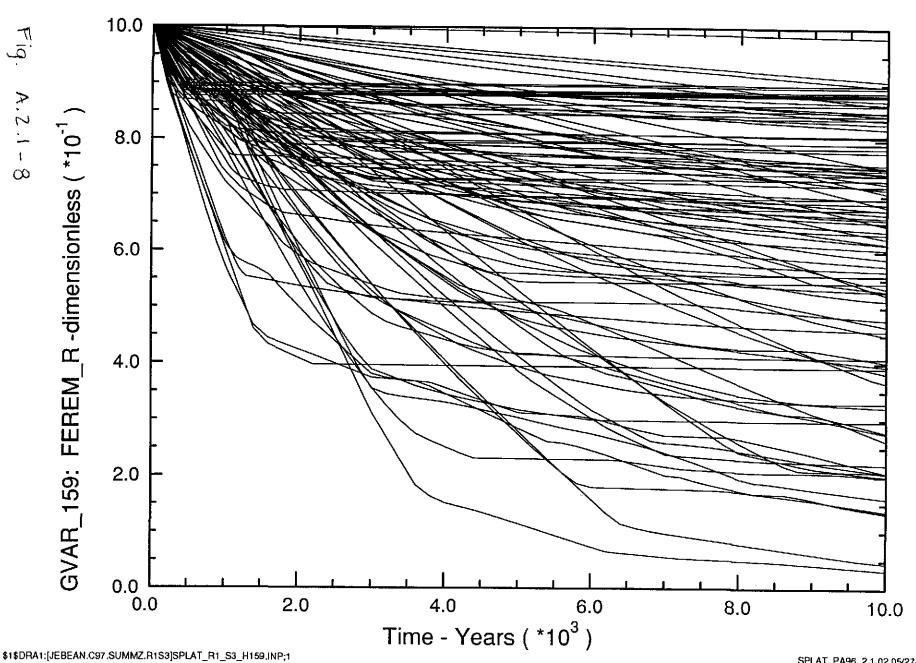
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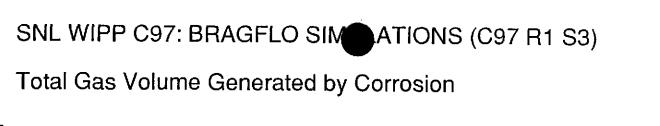


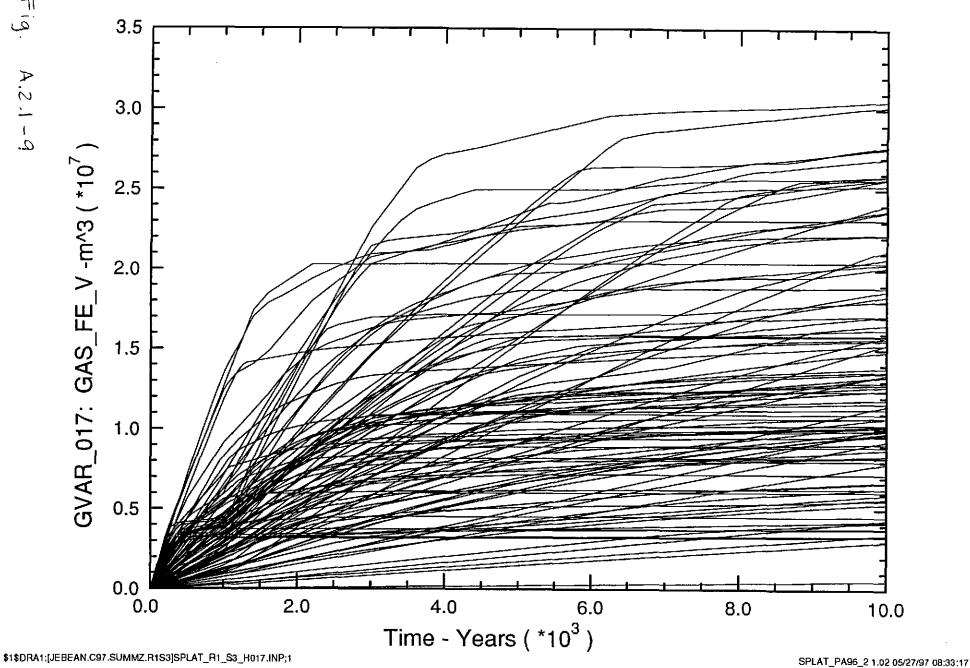






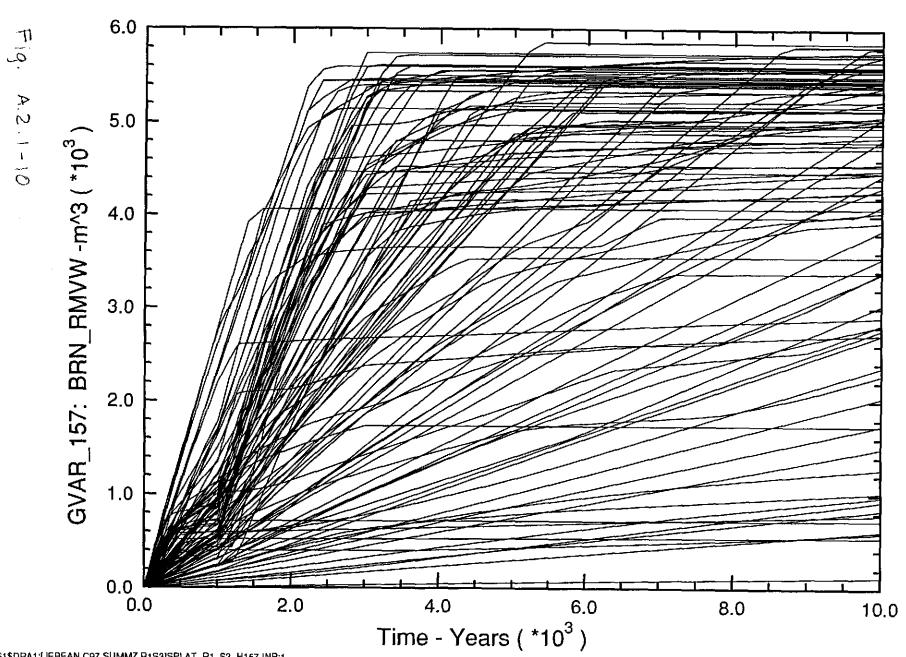


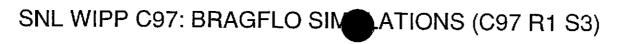




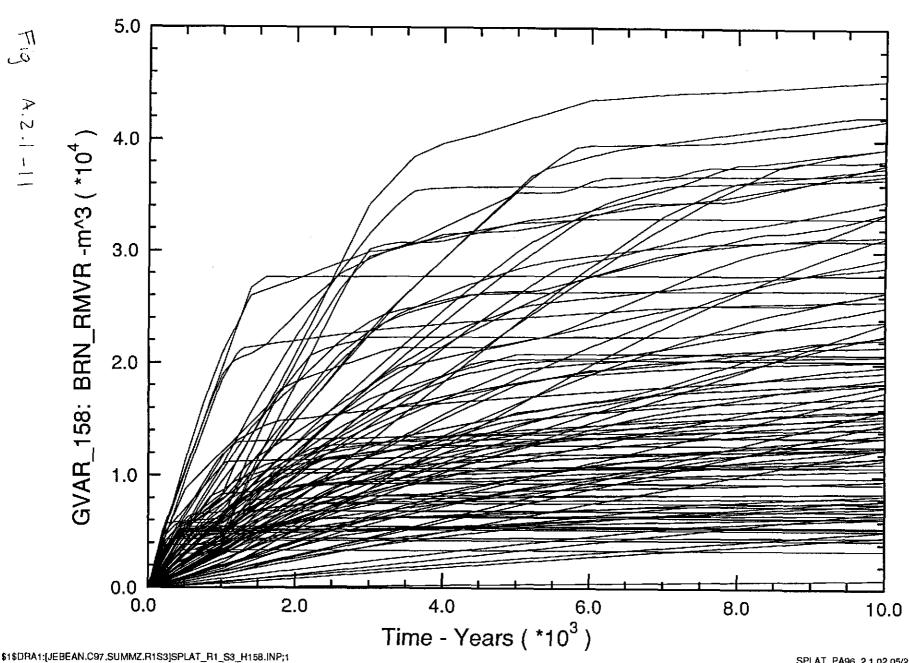
SNL WIPP C97: BRAGFLO SIM ATIONS (C97 R1 S3)

Brine Consumed in Waste Panel





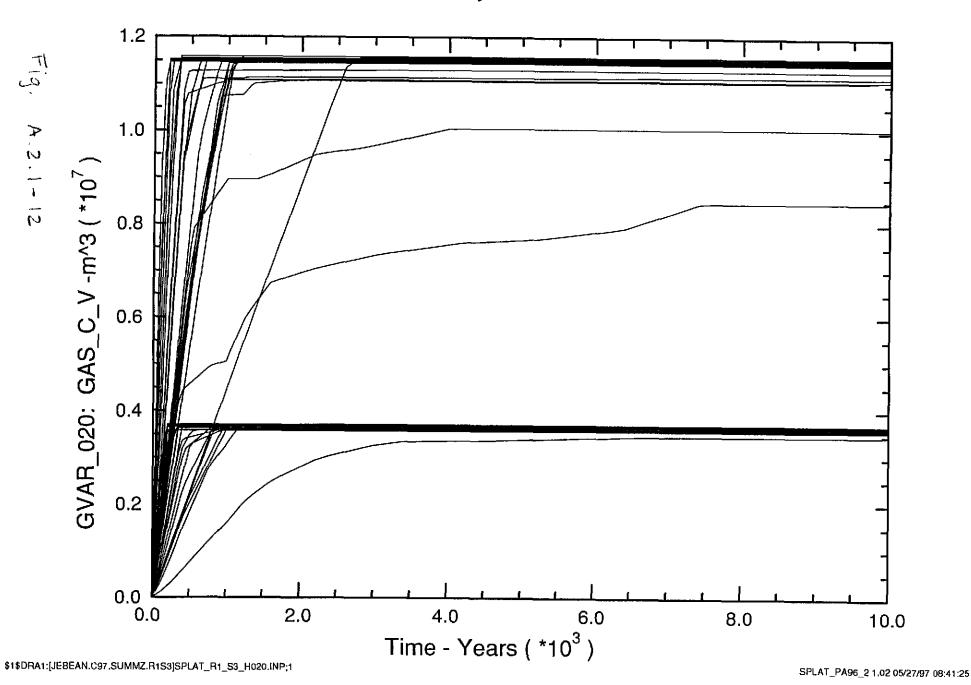




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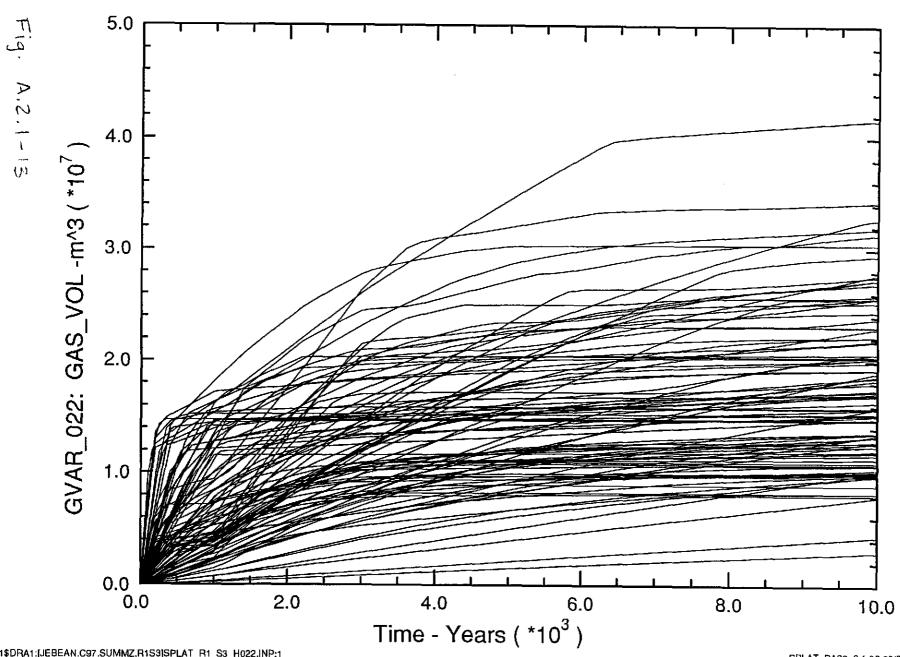


Total Gas Volume Generated by Microbial







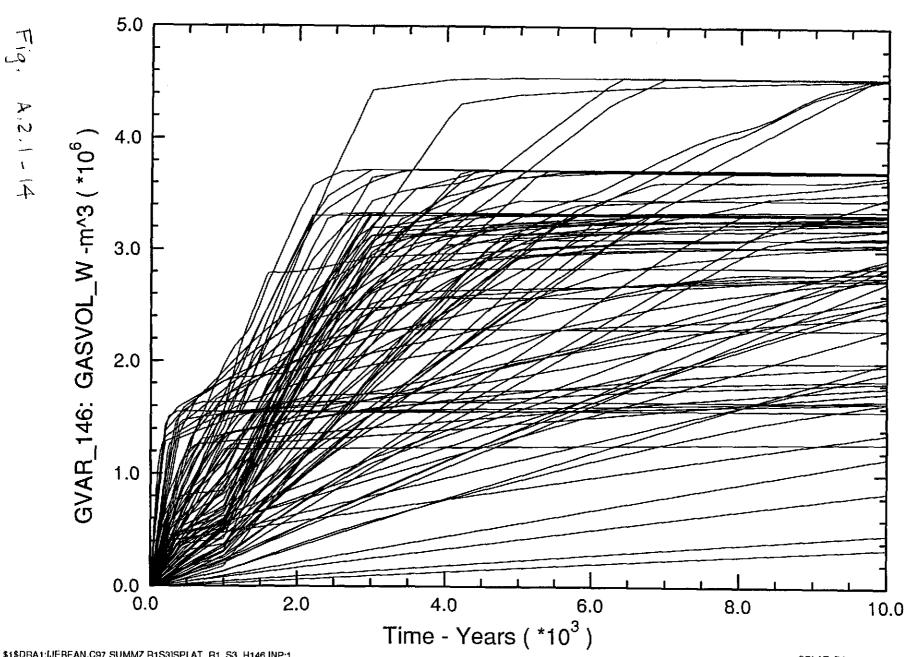


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Total Gas Volume Generated in Waste Panel

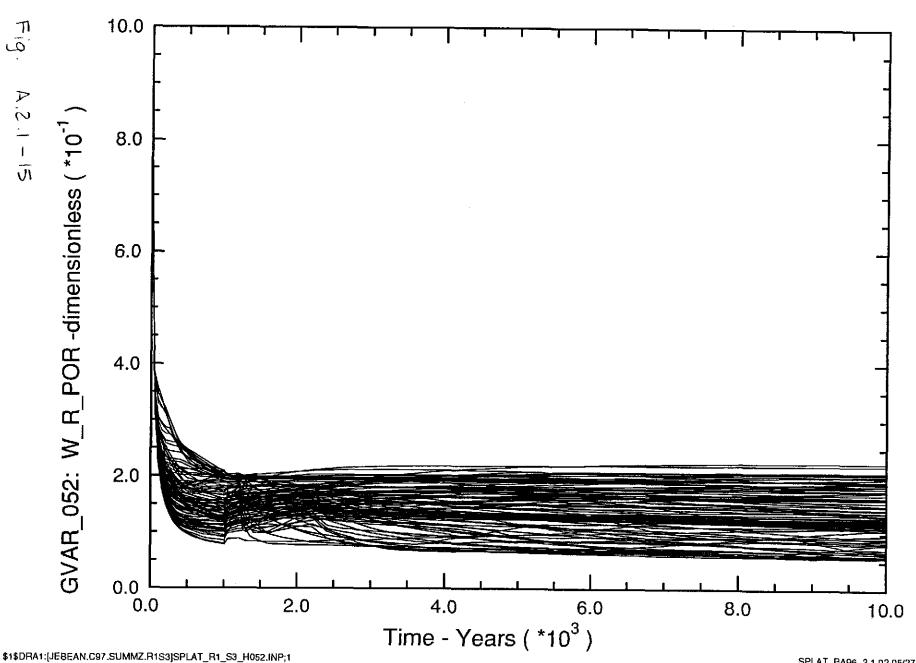


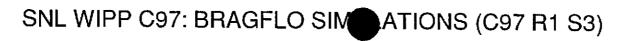
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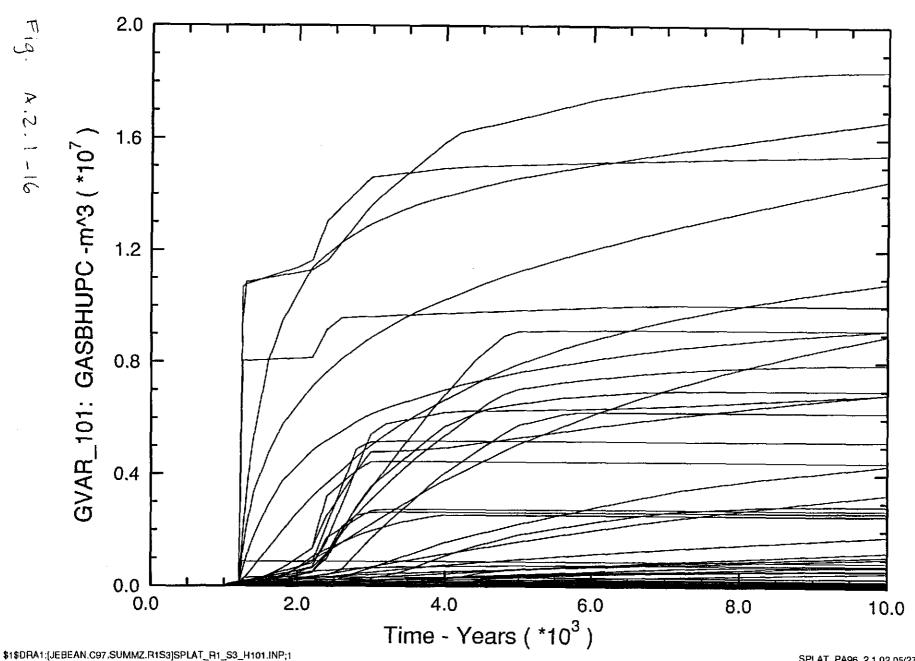


Volume-Averaged Porosity in Waste Panel plus Rest of Repository





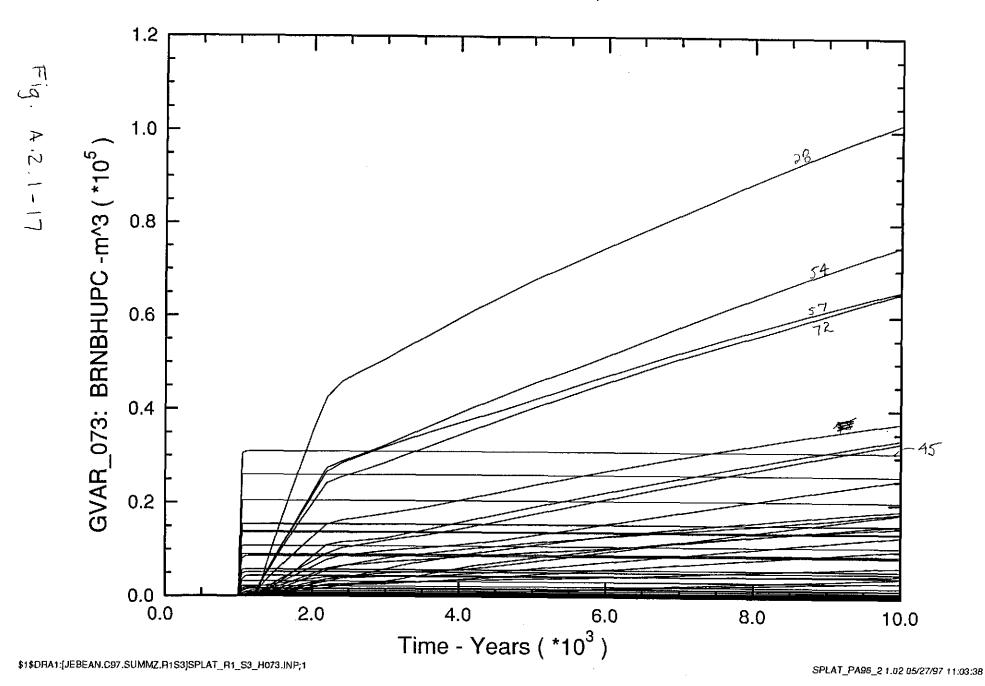
Cumulative Gas Flow up Borehole at Top of Panel (E:471)



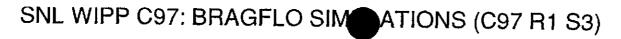
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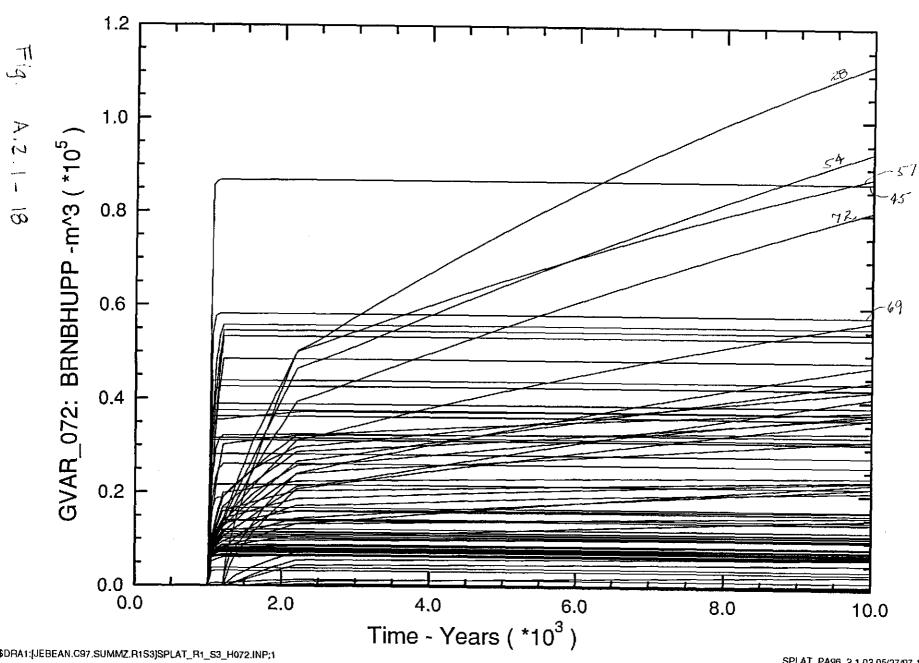
Cumulative Brine Flow Up Borehole at Top of Panel



Information Only

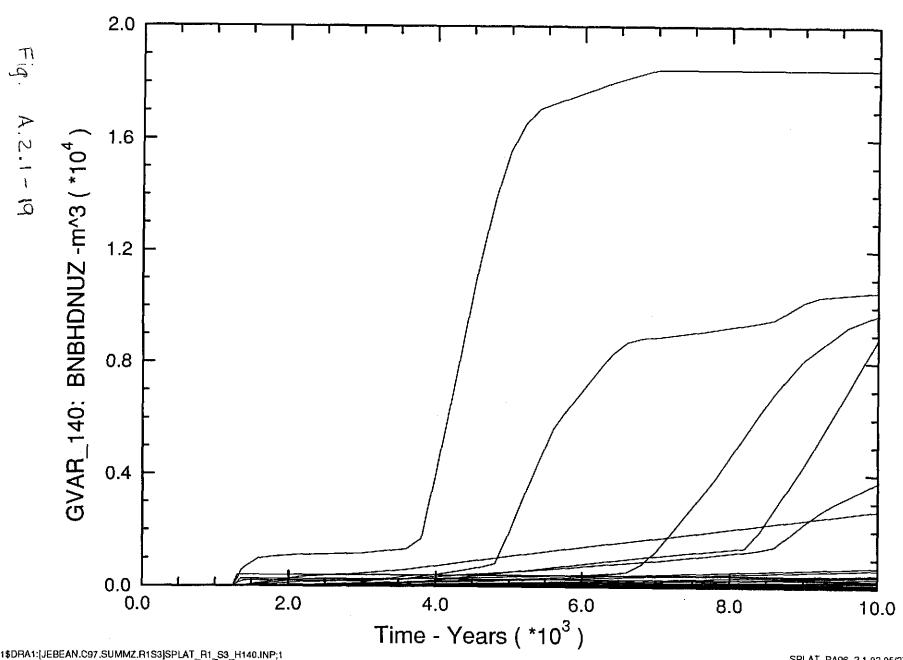


Cumulative Brine Flow up Borehole at Bottom of Panel (E:599)



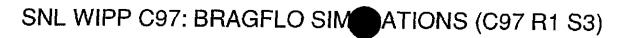


Cumulative Brine Flow Down Borehole at MB 138 (E:223)

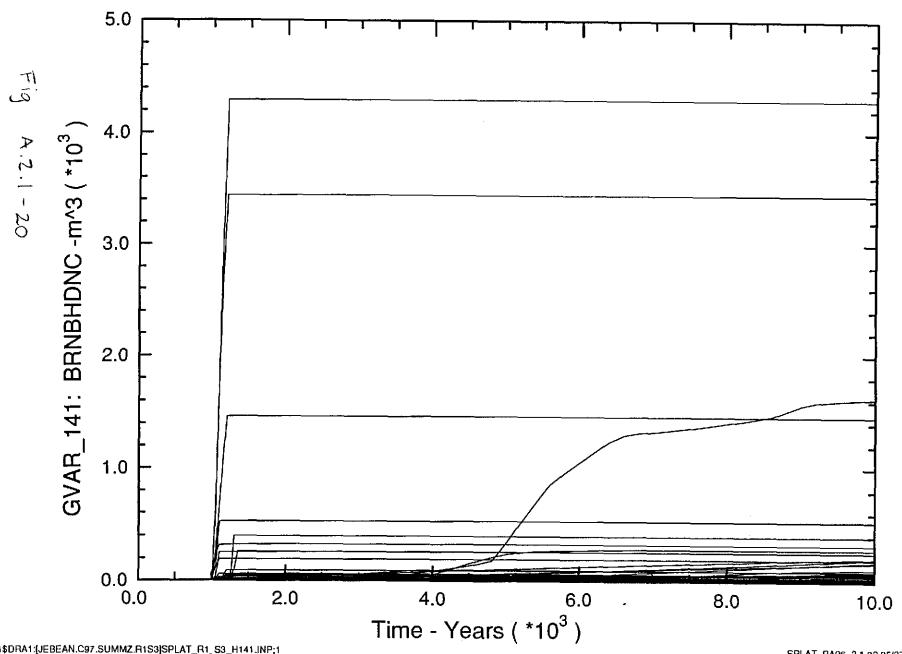


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Cumulative Brine Flow Down Borehole at Top of Panel (E:471)

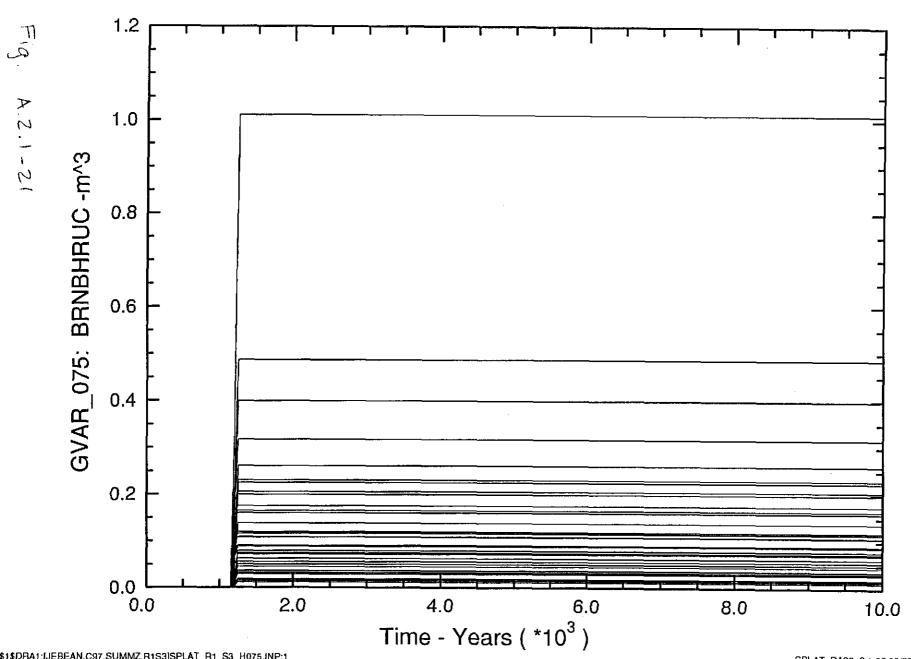


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Cumulative Brine Flow up Borehole at Top of Rustler (E:841)

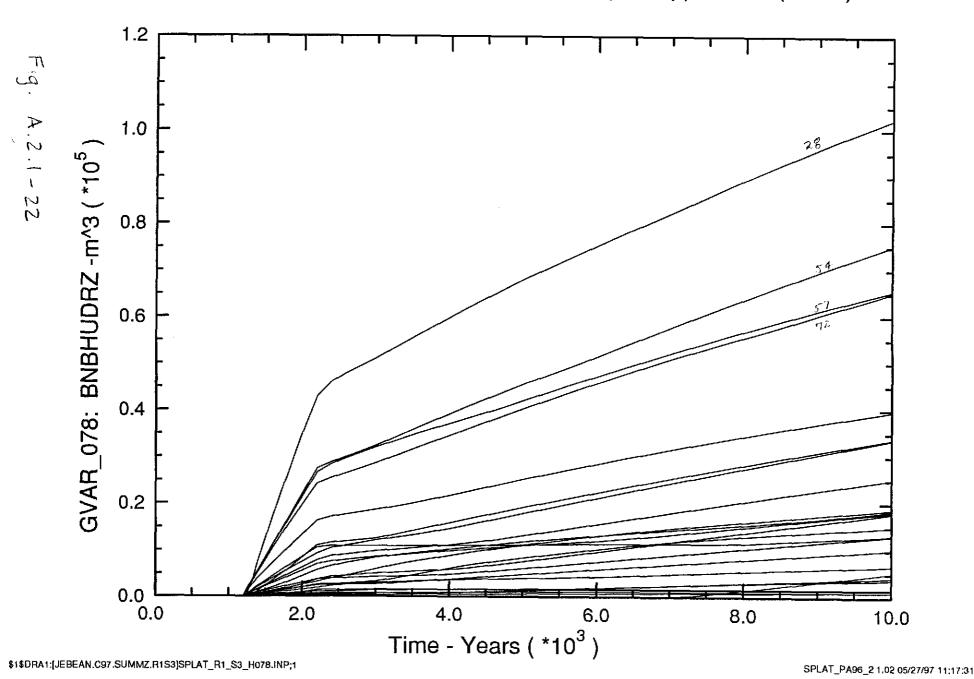


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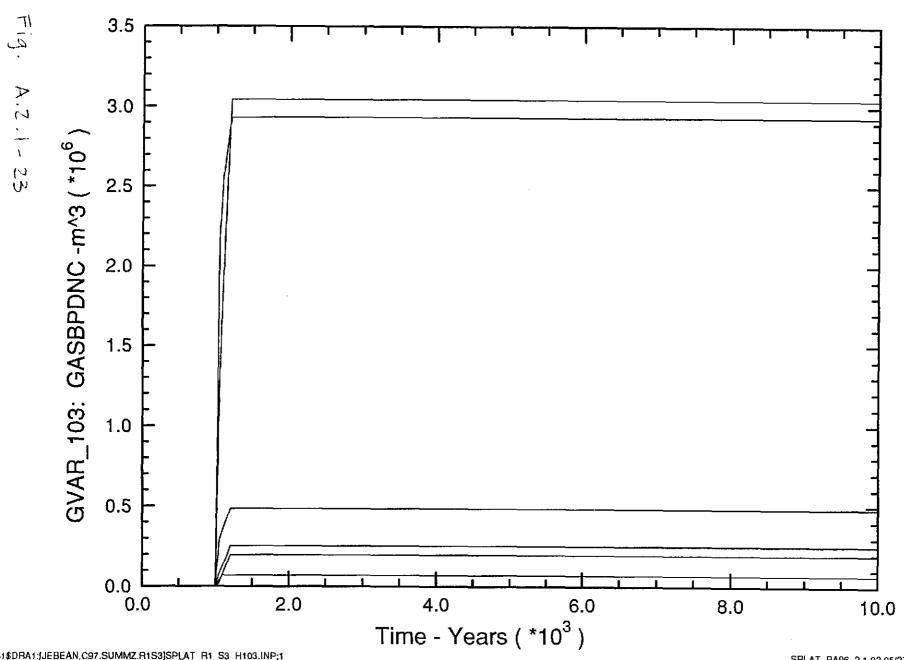


Cumulative Brine Flow up Borehole from Top of Upper DRZ (E:575)





Cumulative Gas Flow into Brine Pocket (E:985)

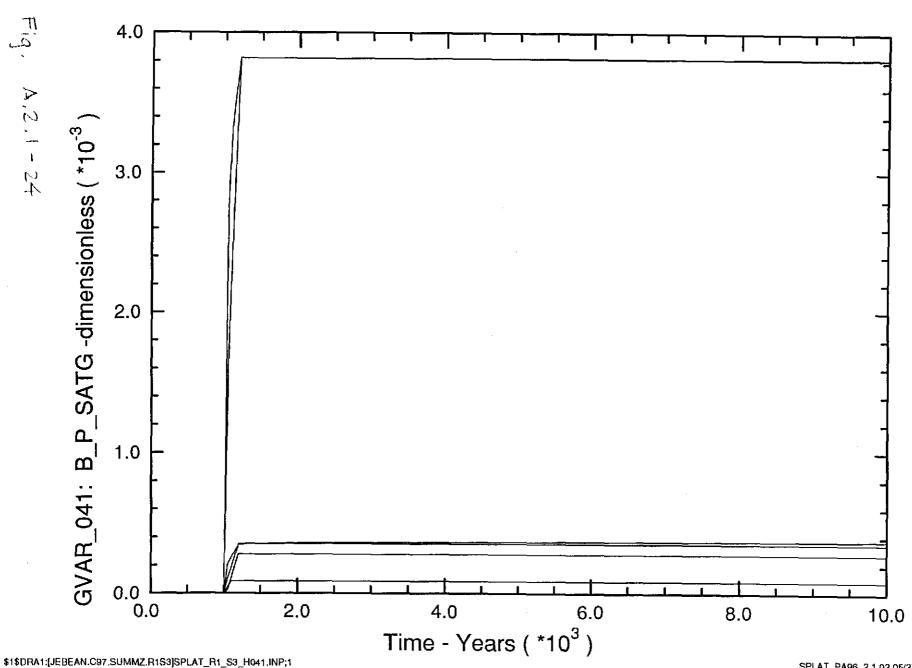


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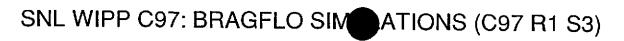


Gas Saturation in Brine Pool

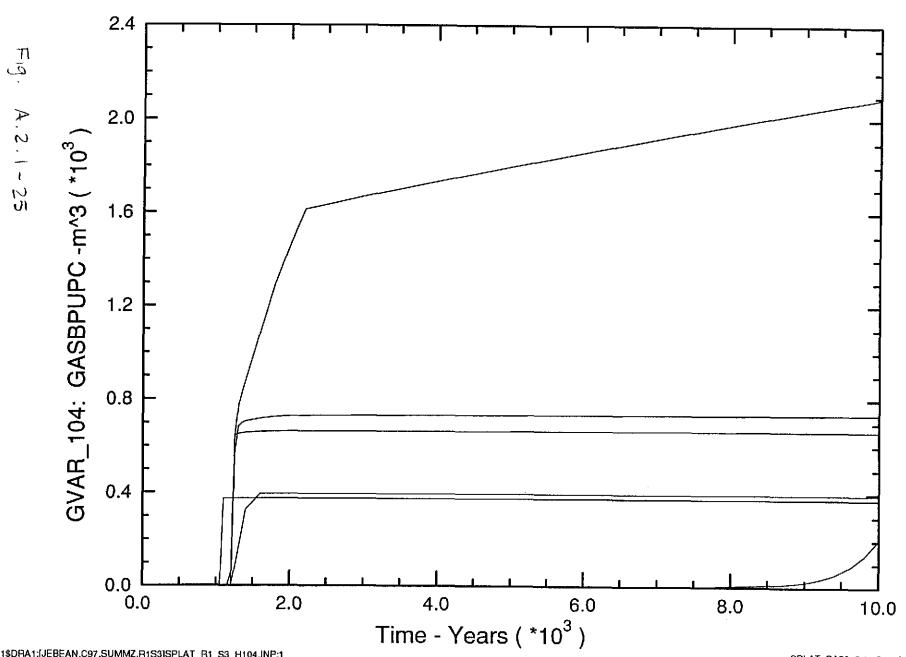


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Cumulative Gas Flow Out of Brine Pocket (E:985)

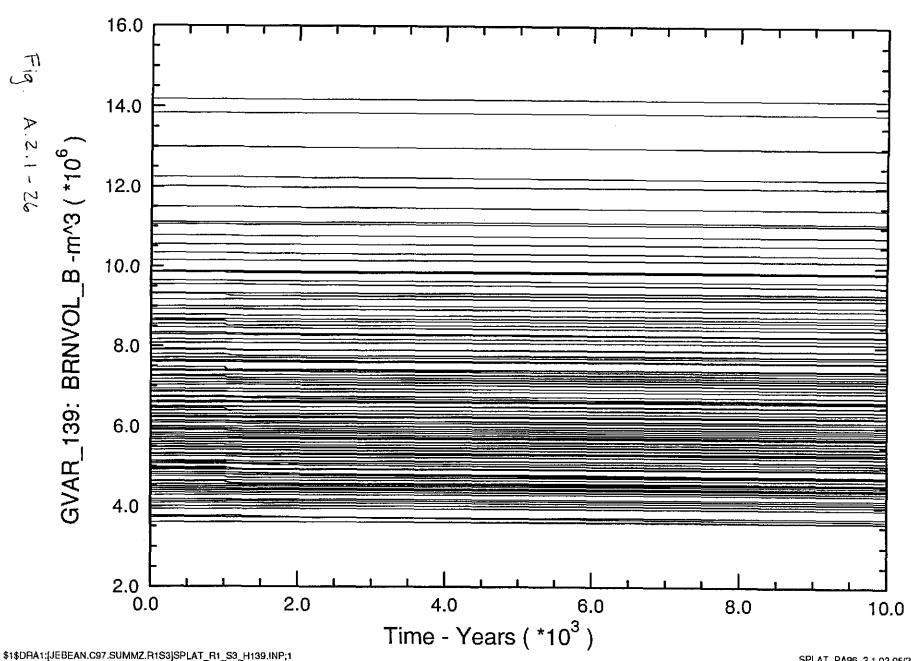


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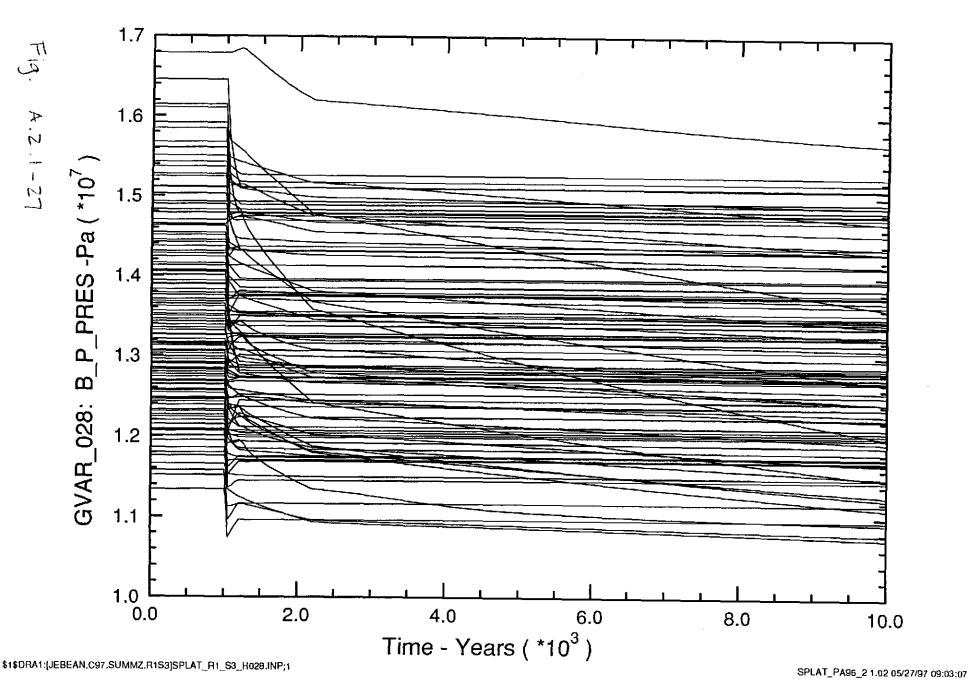
Brine Volume in Brine Pocket

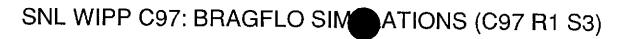


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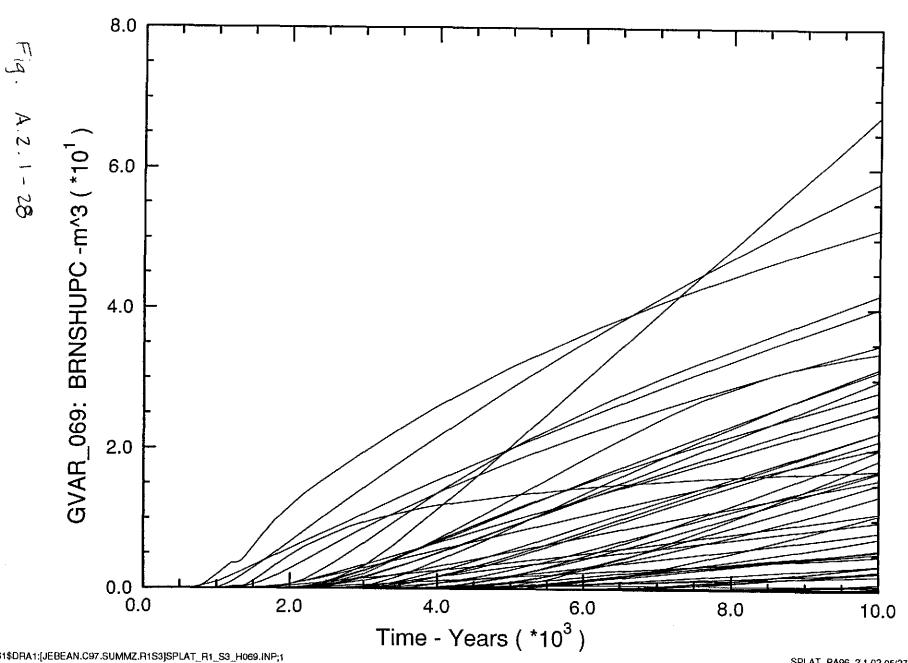


Volume-Averaged Pressure in Brine Pocket



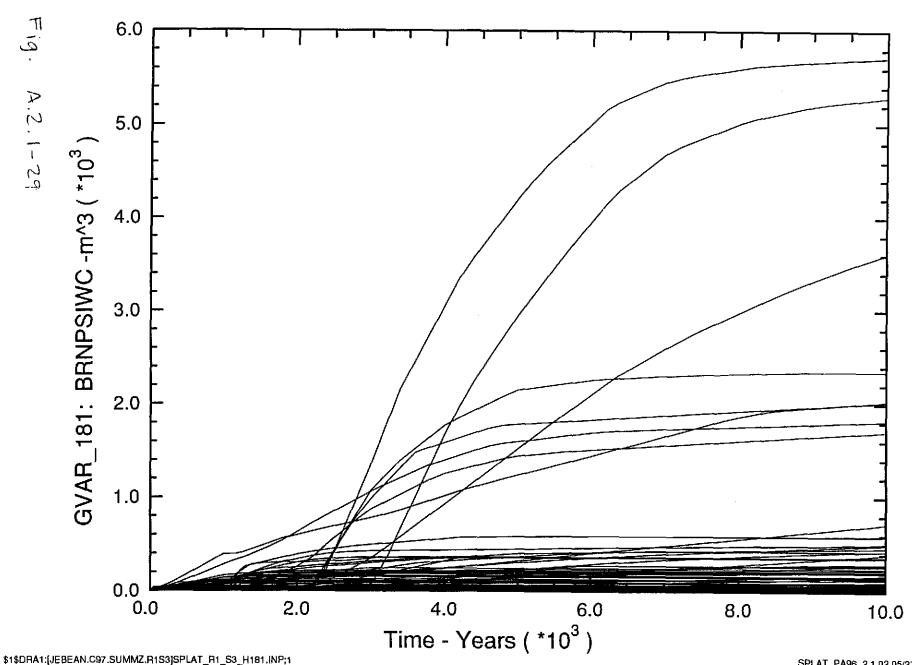


Cumulative Brine Flow up Shaft at top of Salado (E:661)



SNL WIPP C97: BRAGFLO SIM ATIONS (C97 R1 S3)

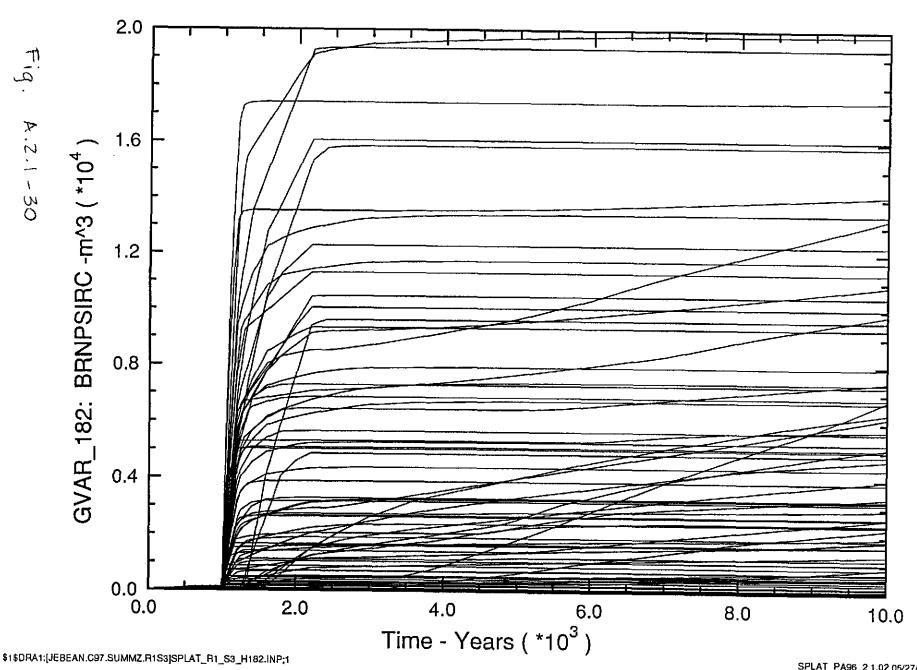
Cumulative Brine Flow out of Panel Seal into Waste Panel



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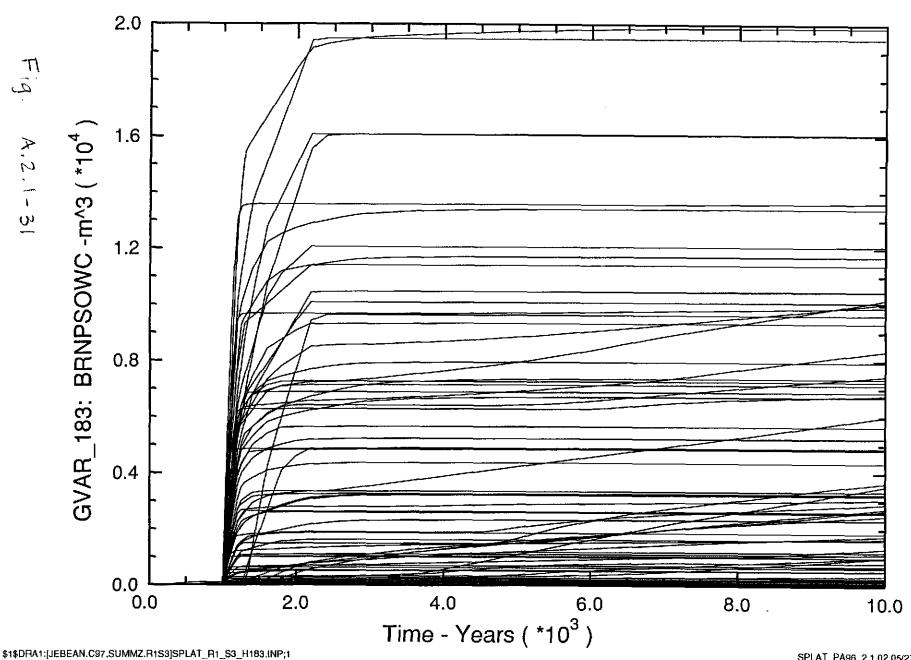


Cumulative Brine Flow out of Panel Seal into Rest of Repository



SNL WIPP C97: BRAGFLO SIM ATIONS (C97 R1 S3)

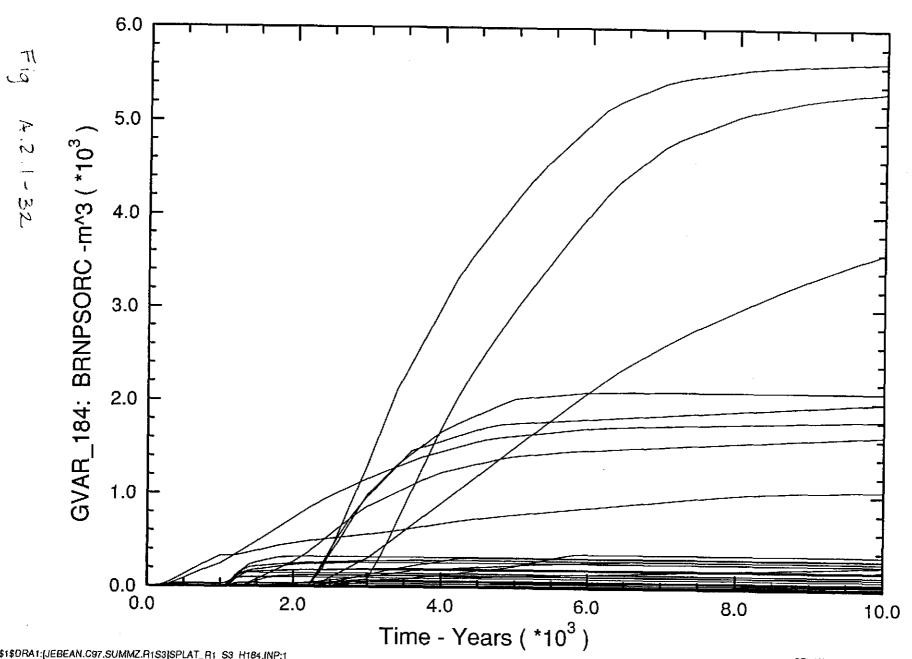
Cumulative Brine Flow into Panel Seal out of Waste Panel



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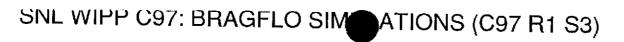


Cumulative Brine Flow into Panel Seal out of Rest of Repository

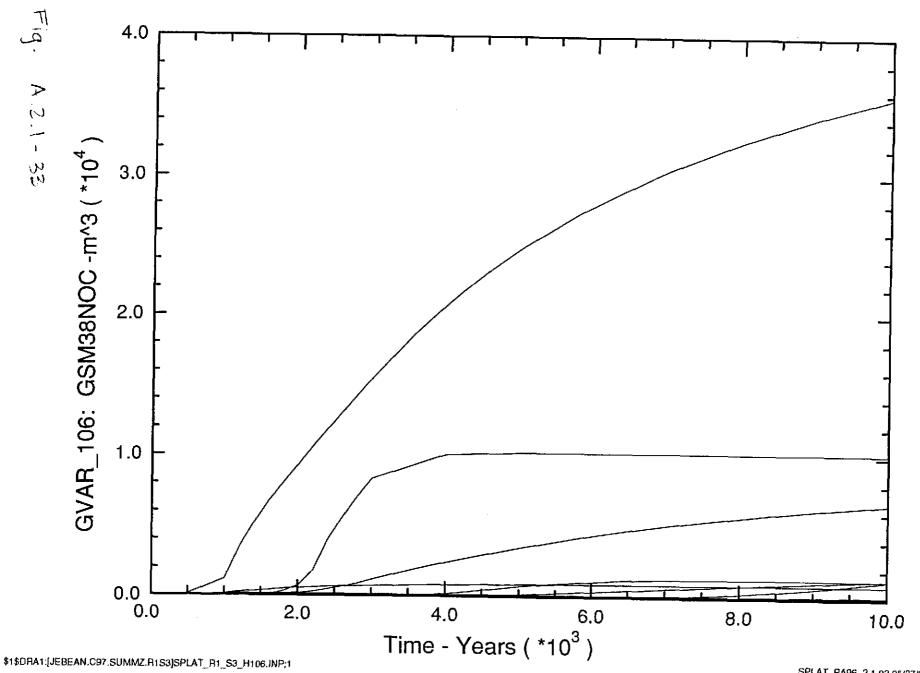


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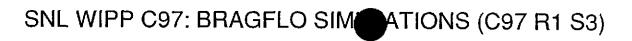


Cumulative Gas Flow from DRZ into North MB 138

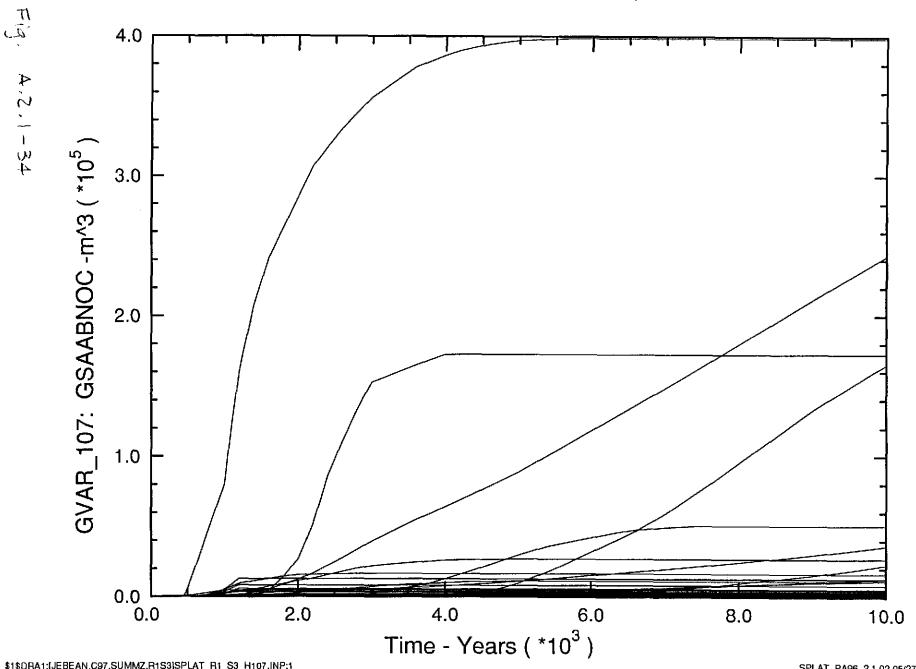


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Cumulative Gas Flow from DRZ into North Anhydrite A/B

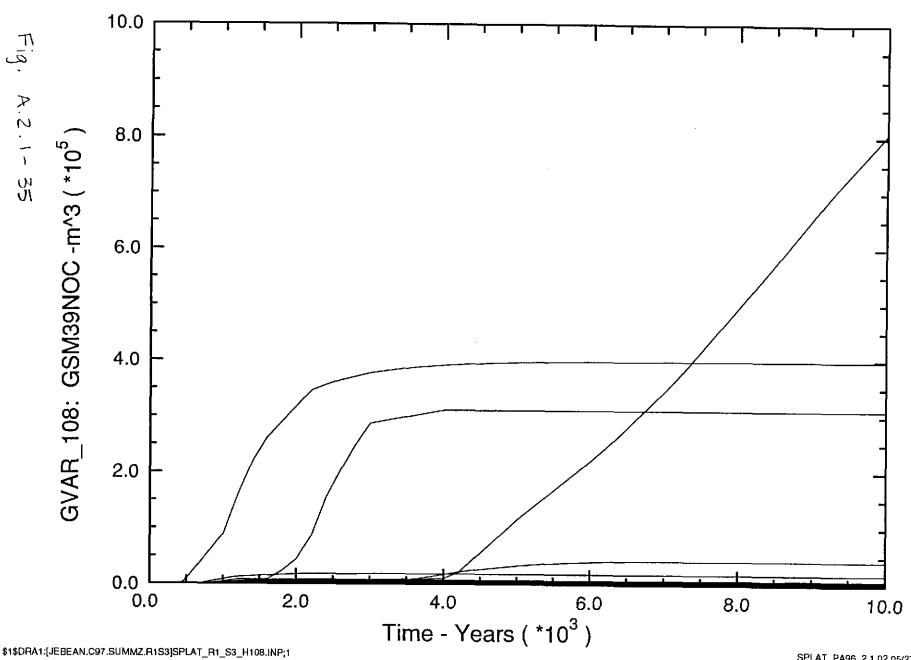


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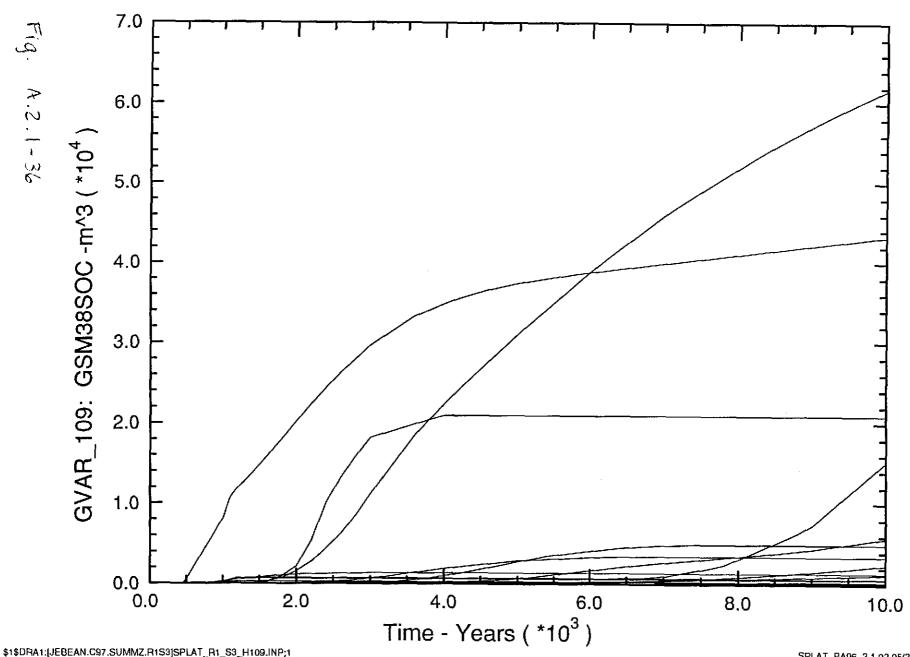
Cumulative Gas Flow from DRZ into North MB 139



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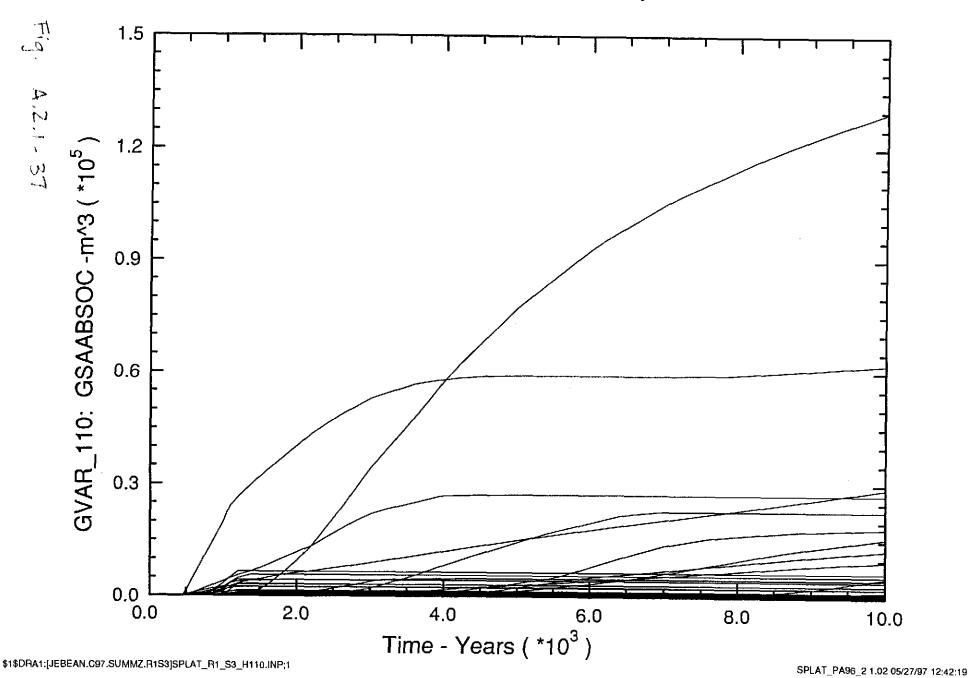
Cumulative Gas Flow from DRZ into South MB 138

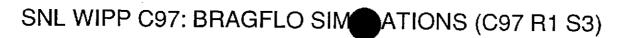


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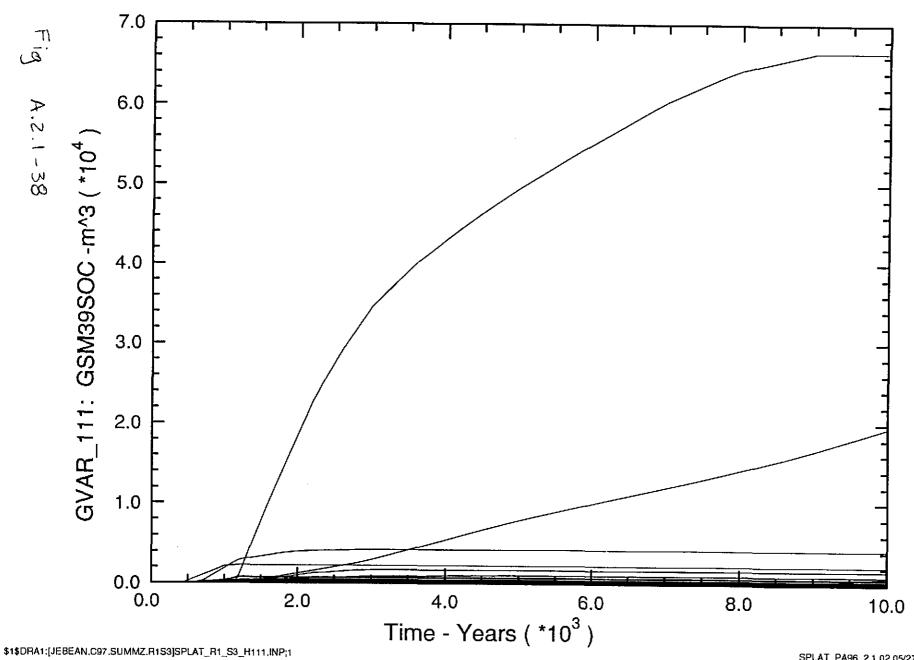


Cumulative Gas Flow from DRZ into South Anhydrite A/B



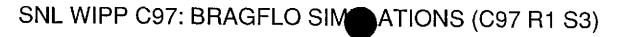


Cumulative Gas Flow from DRZ into South MB 139

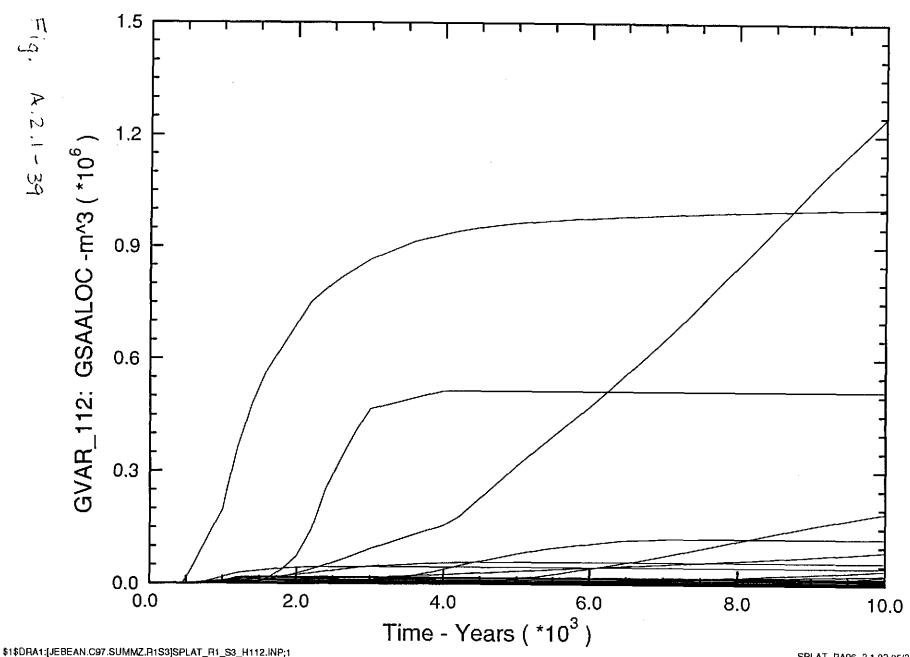


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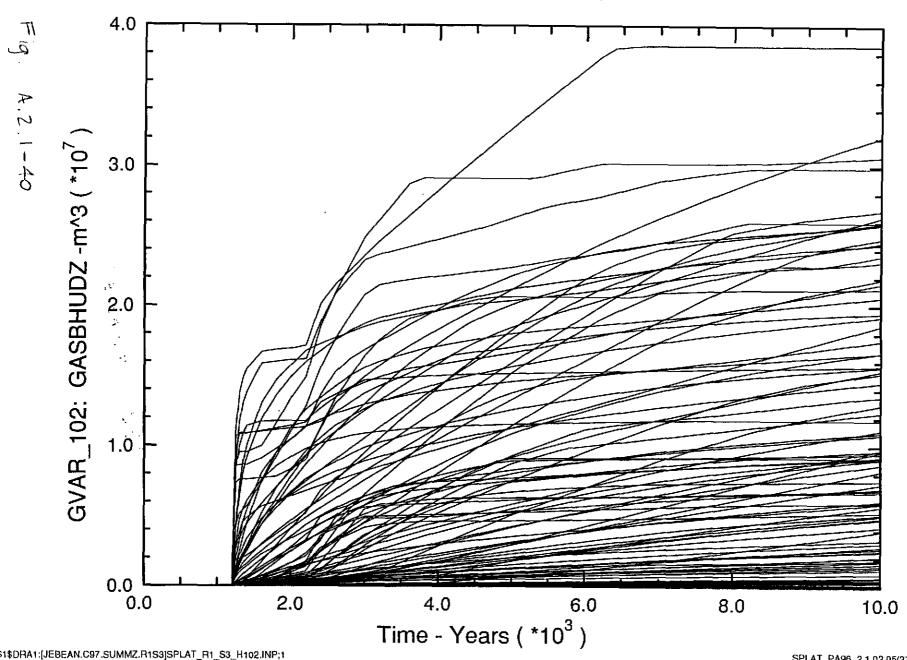
Cumulative Gas Flow from DRZ into Marker Beds



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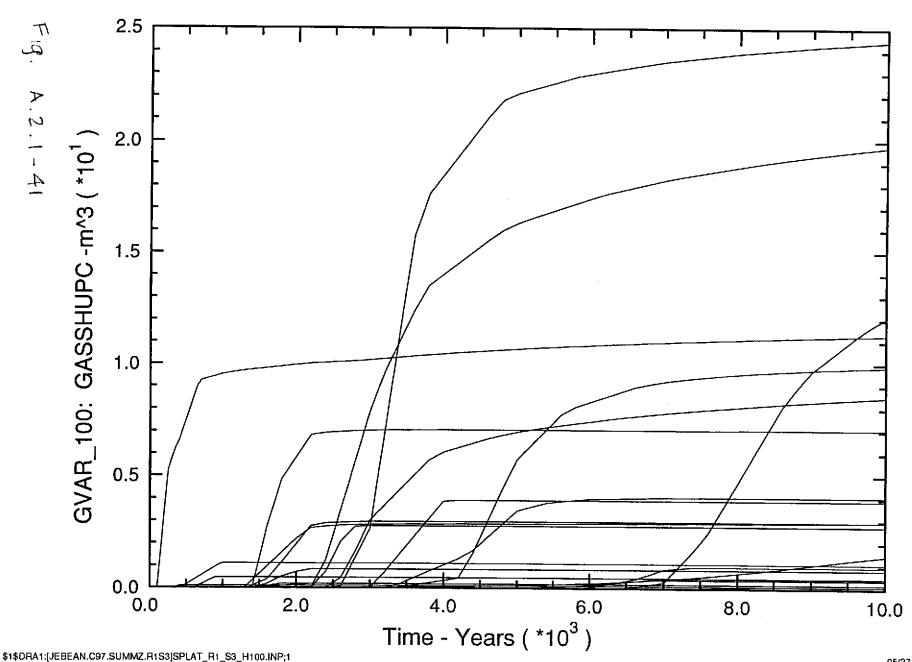


Cumulative Gas Flow Out of Upper DRZ at Borehole (E:575)



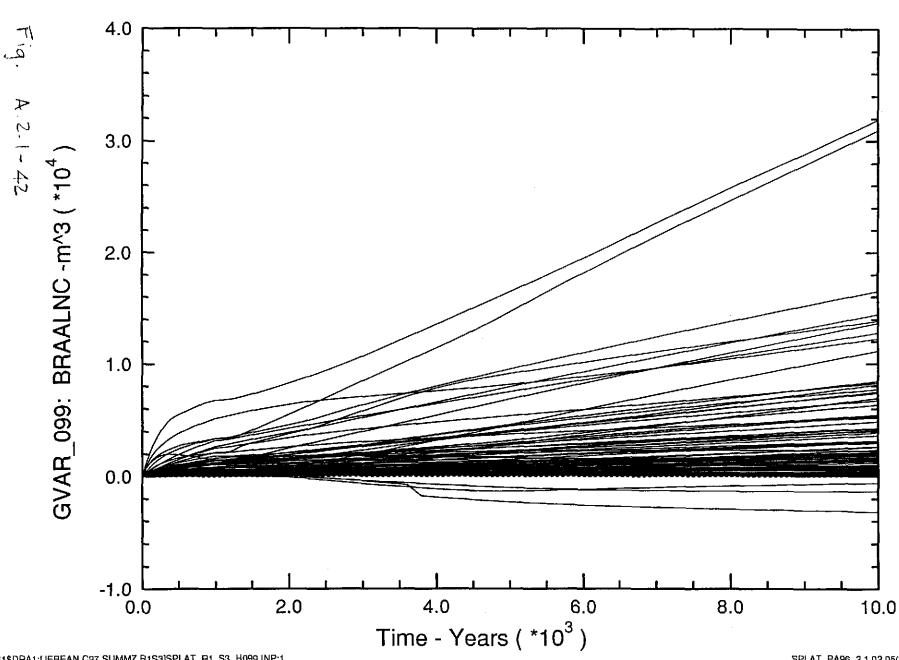


Cumulative Gas Flow up Shaft at Top of Salado (E:661)



SNL WIPP C97: BRAGFLO SIM ATIONS (C97 R1 S3)

Net Brine Flow into DRZ from All Marker Beds

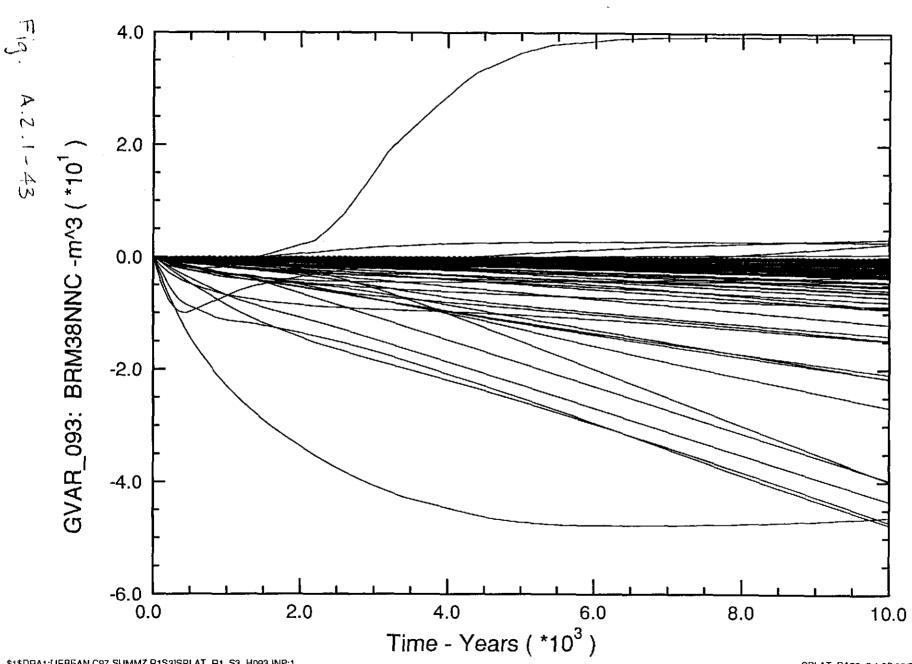


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Net Brine Flow at North MB 138

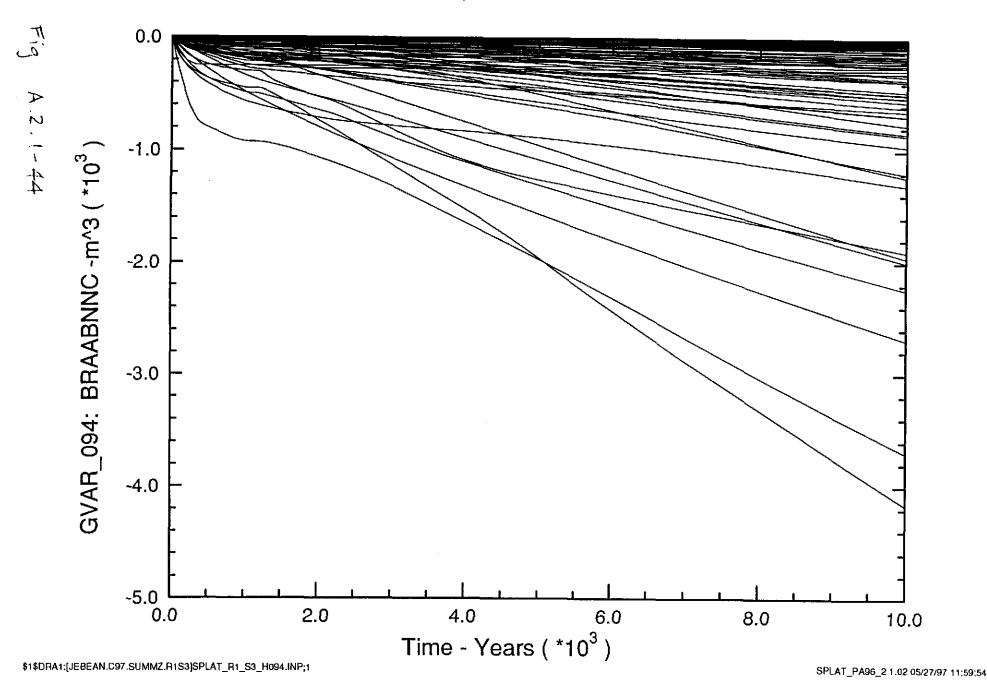


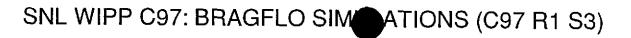
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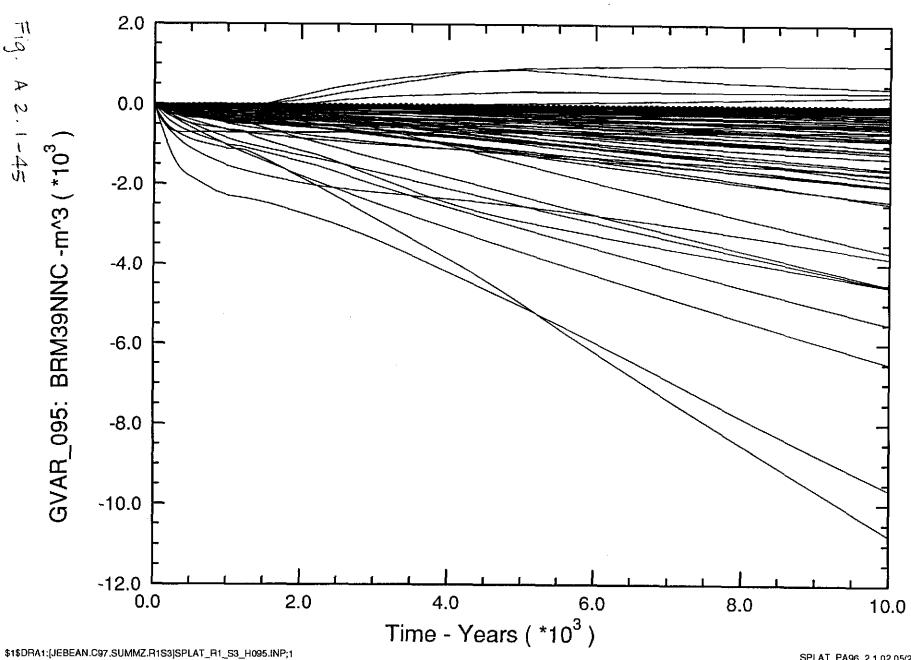
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Net Brine Flow at North Anhydrite A/B



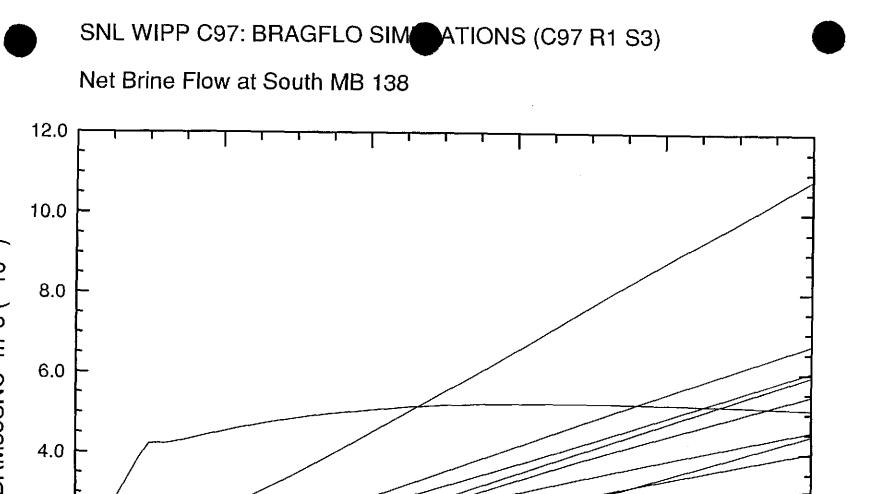


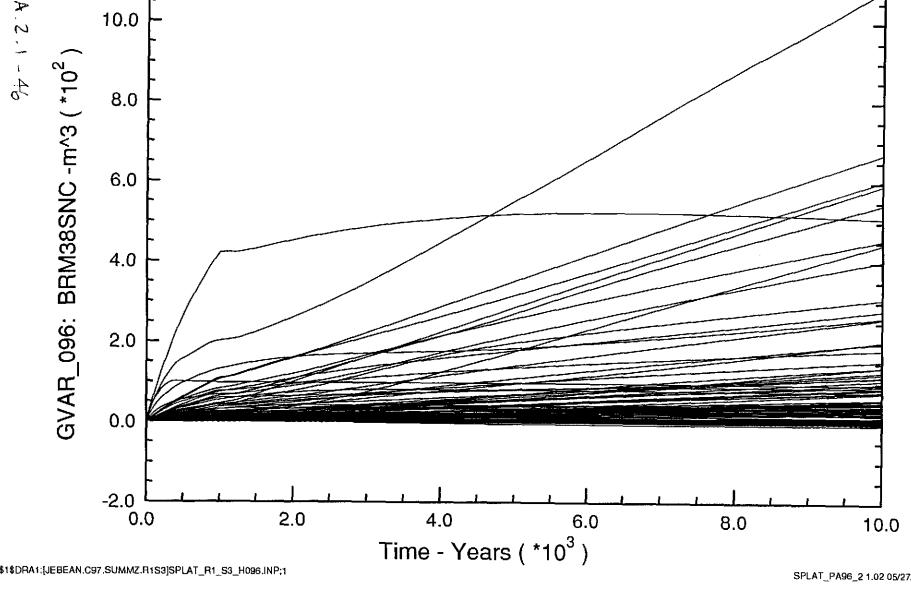
Net Brine Flow at North MB 139



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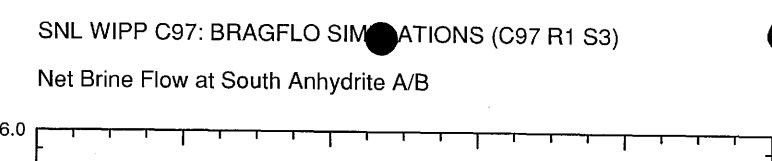
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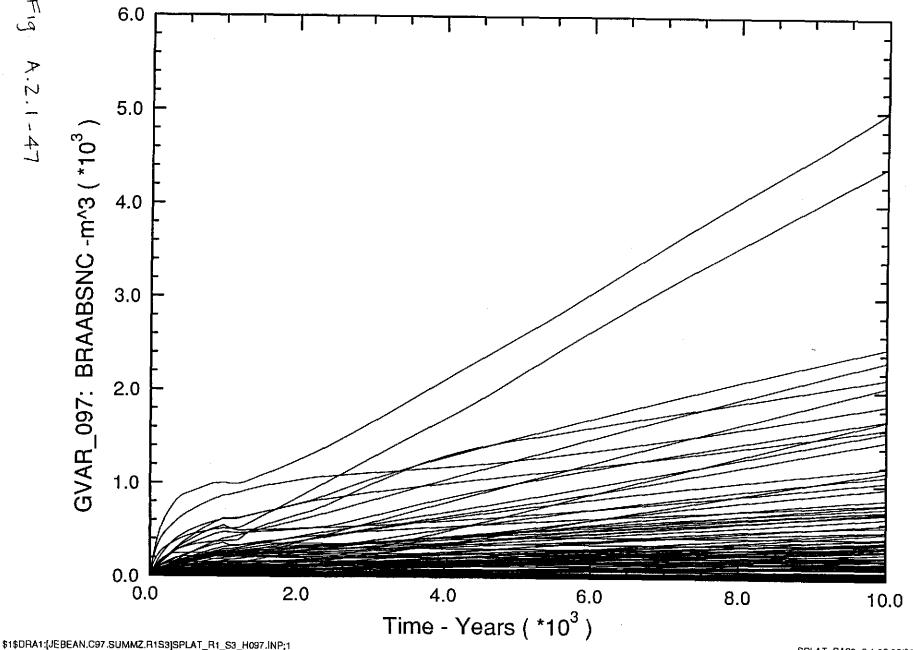




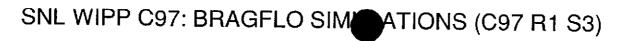
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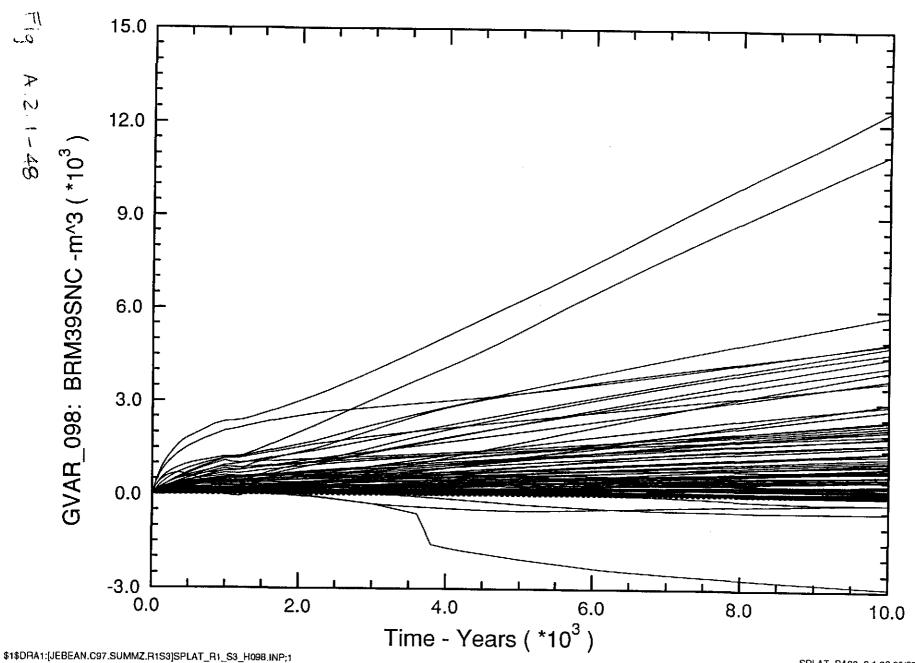




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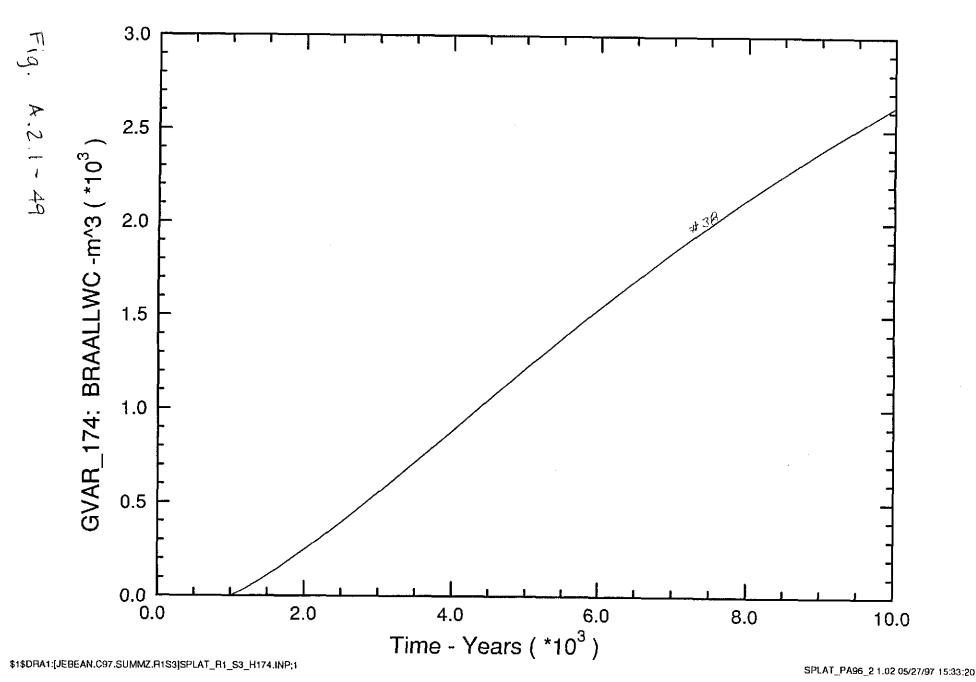
Net Brine Flow at South MB 139

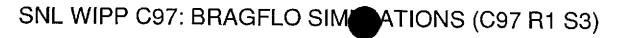


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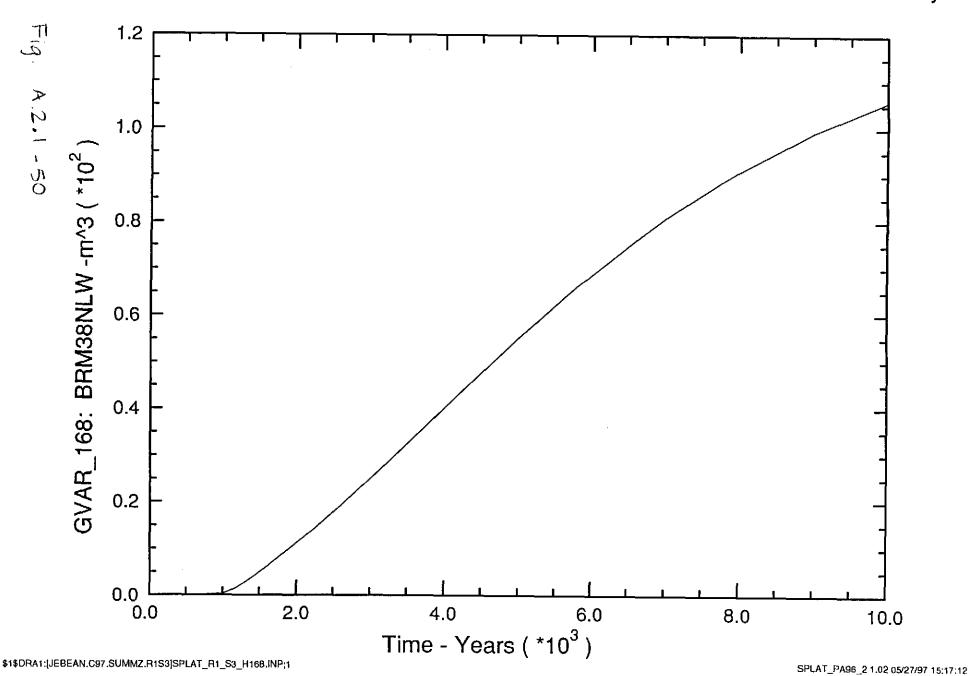
Cumulative Brine Flow Out of All Marker Beds Across Land-Withdrawal Boundary





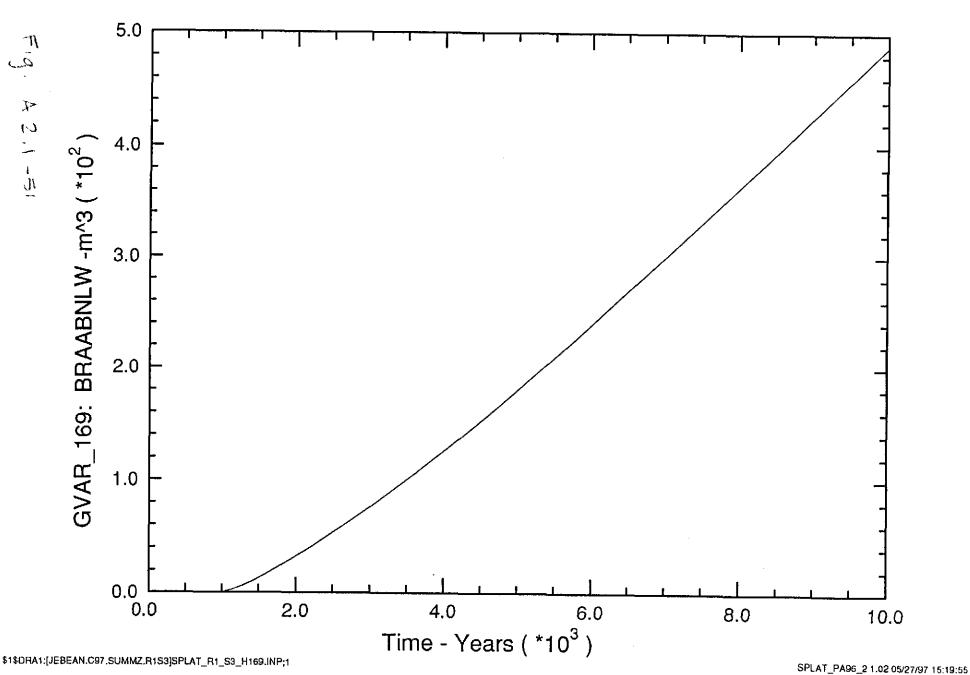


Cumulative Brine Flow Out North MB 138 Across Land-Withdrawal Boundary





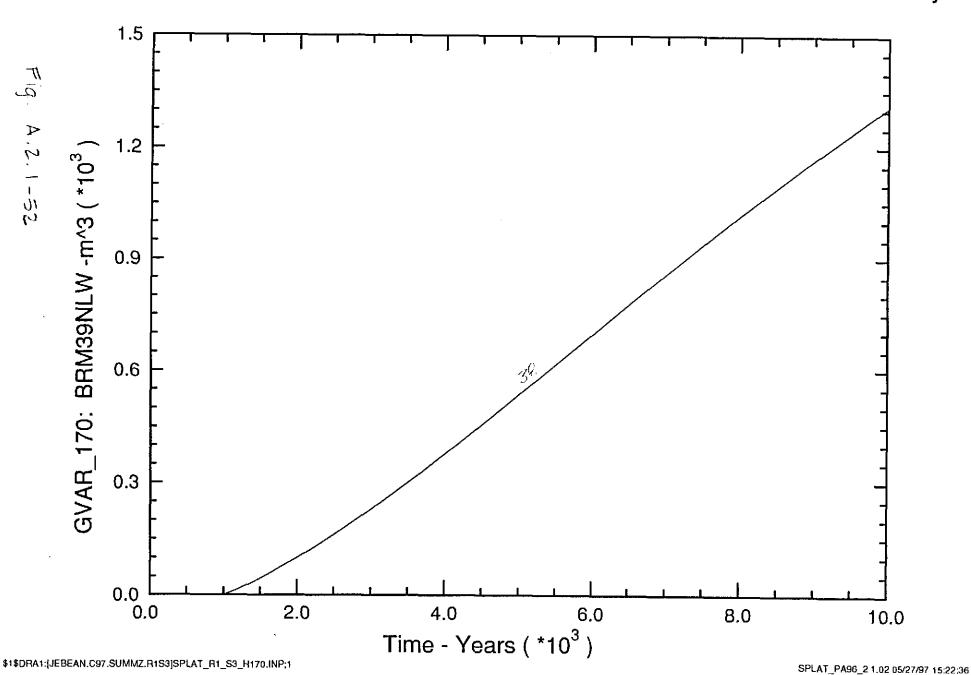
Cumulative Brine Flow Out North Anhydrite A/B Across Land-Withdrawal Boundary



Information Only

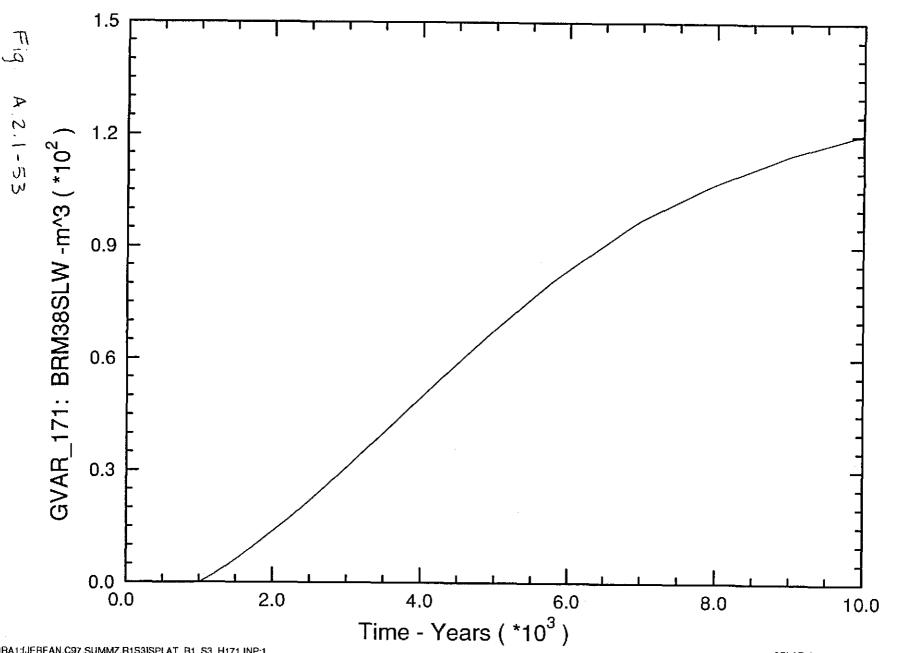






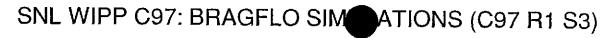




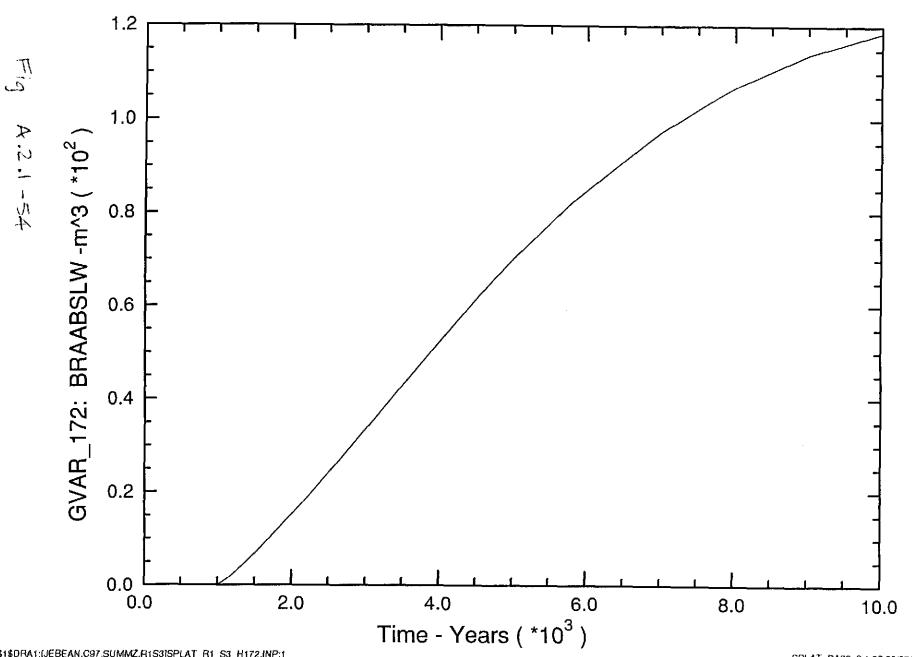


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Cumulative Brine Flow Out South Anhydrite A/B Across Land-Withdrawal Boundary

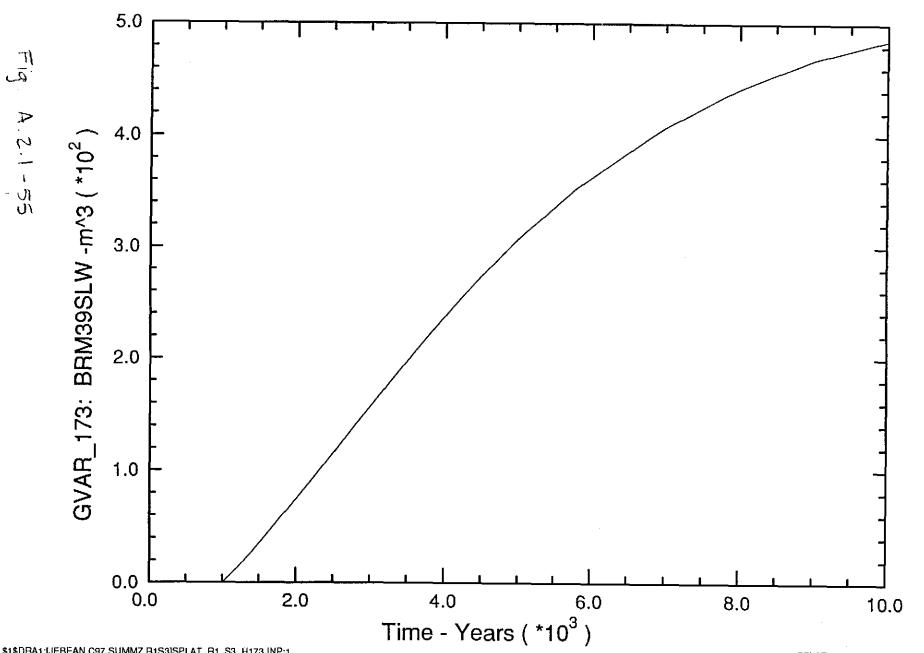


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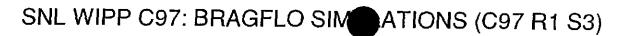


Cumulative Brine Flow Out South MB 139 Across Land-Withdrawal Boundary

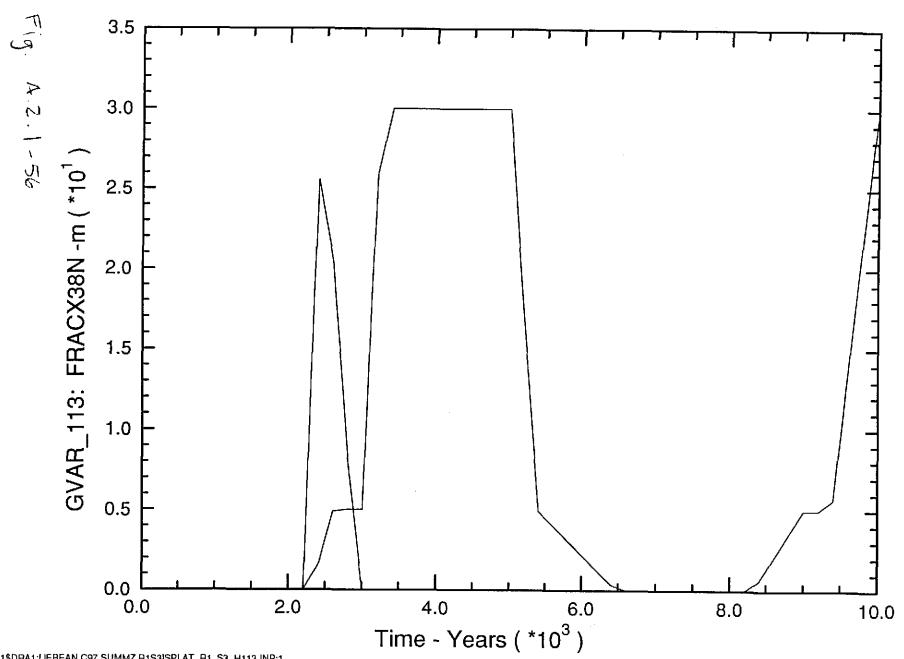


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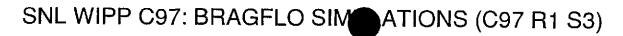


Length of Fractured Zone in North MB 138

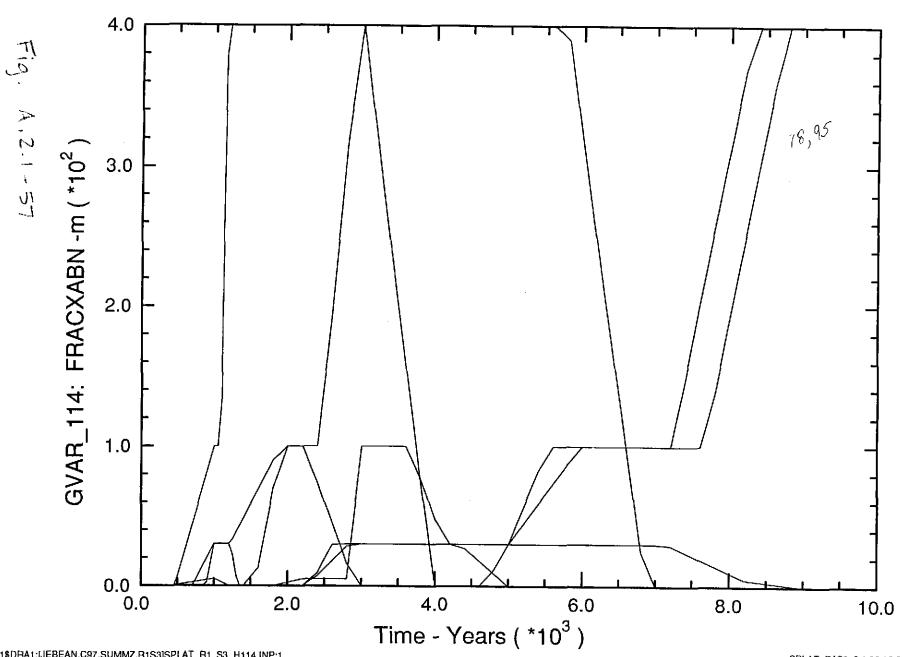


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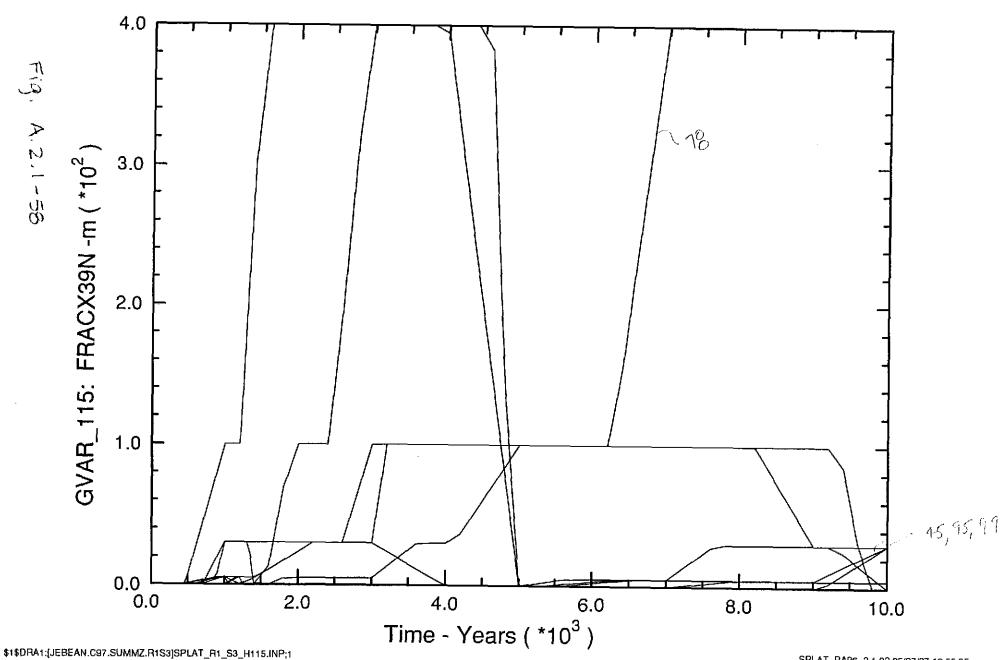


Length of Fractured Zone in North Anhydrite A/B

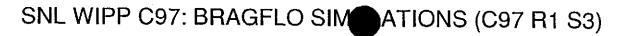




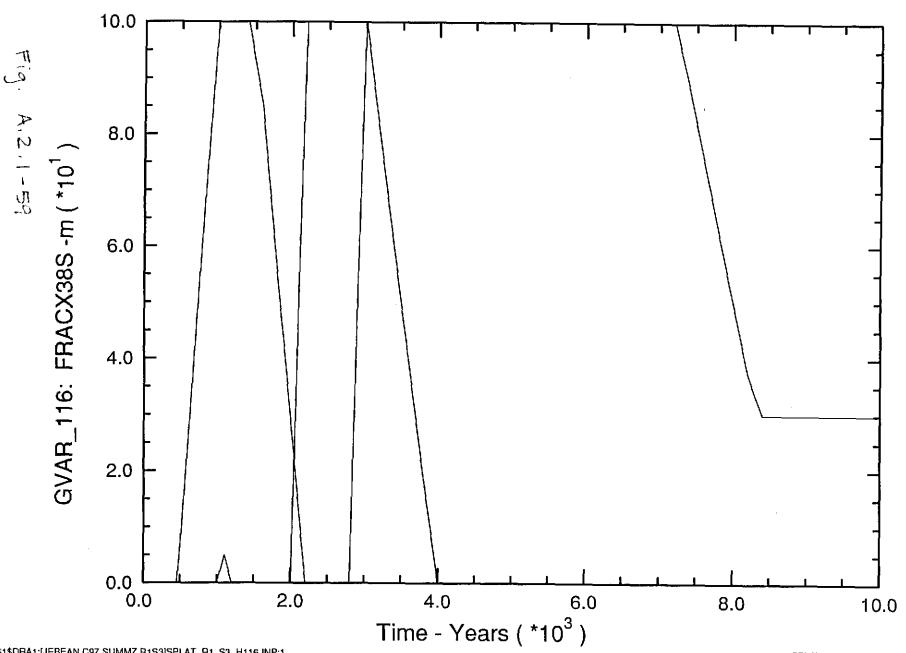
Length of Fractured Zone in North MB 139



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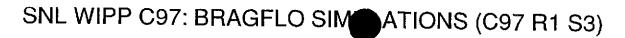


Length of Fractured Zone in South MB 138

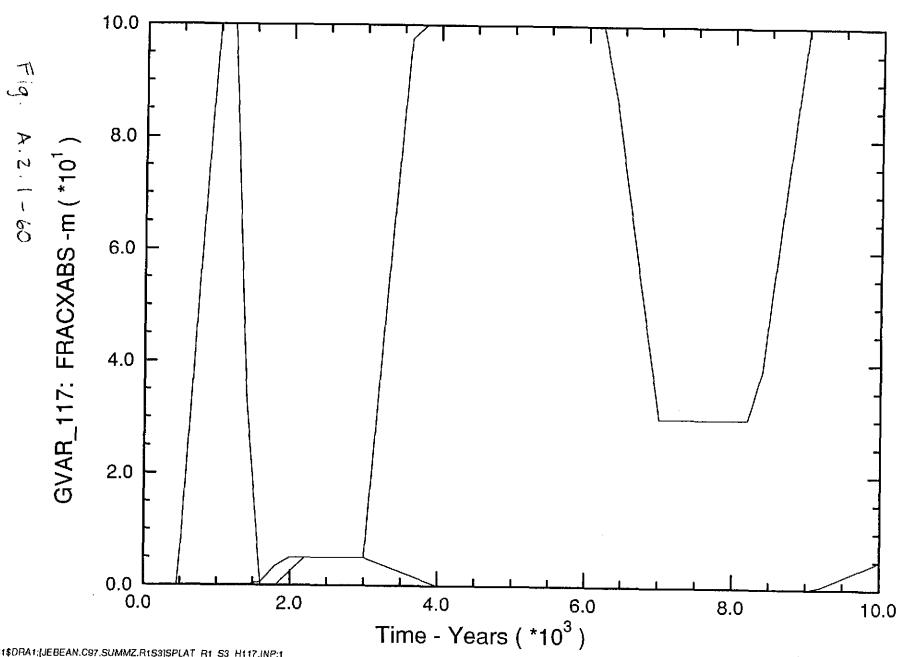


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Length of Fractured Zone in South Anhydrite A/B

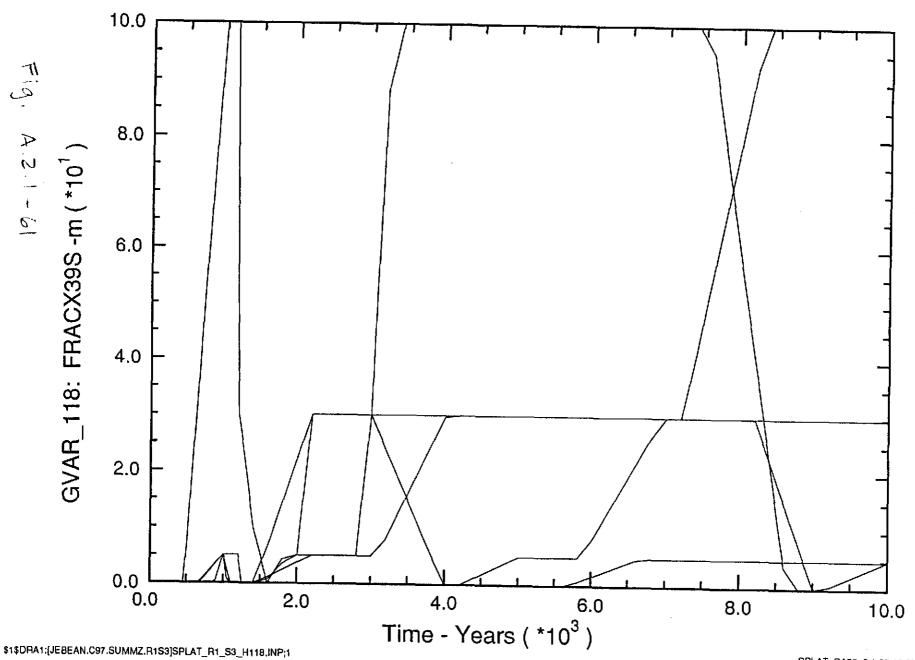


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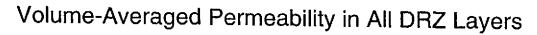


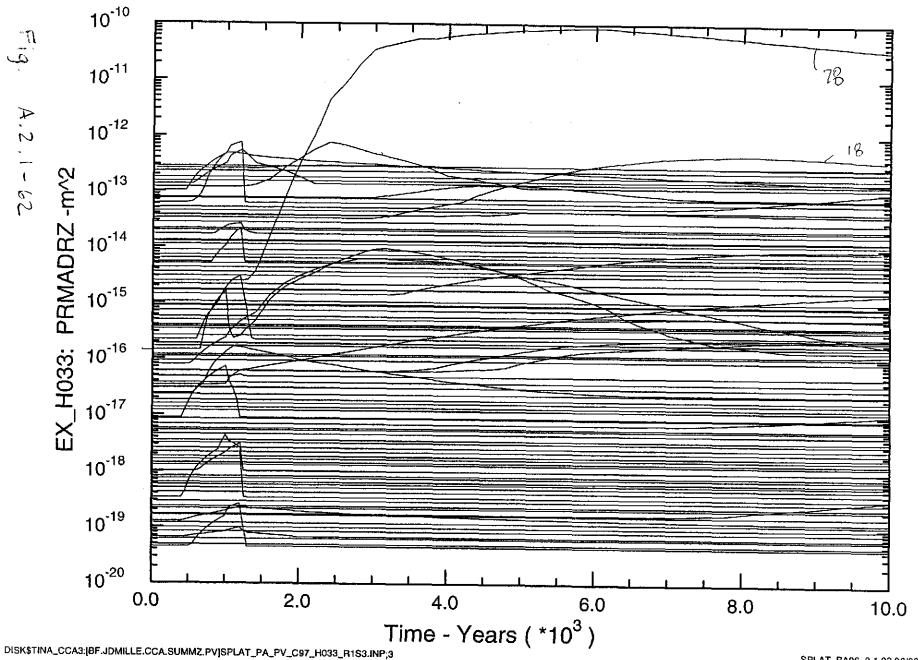
Length of Fractured Zone in South MB 139

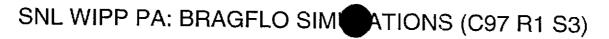


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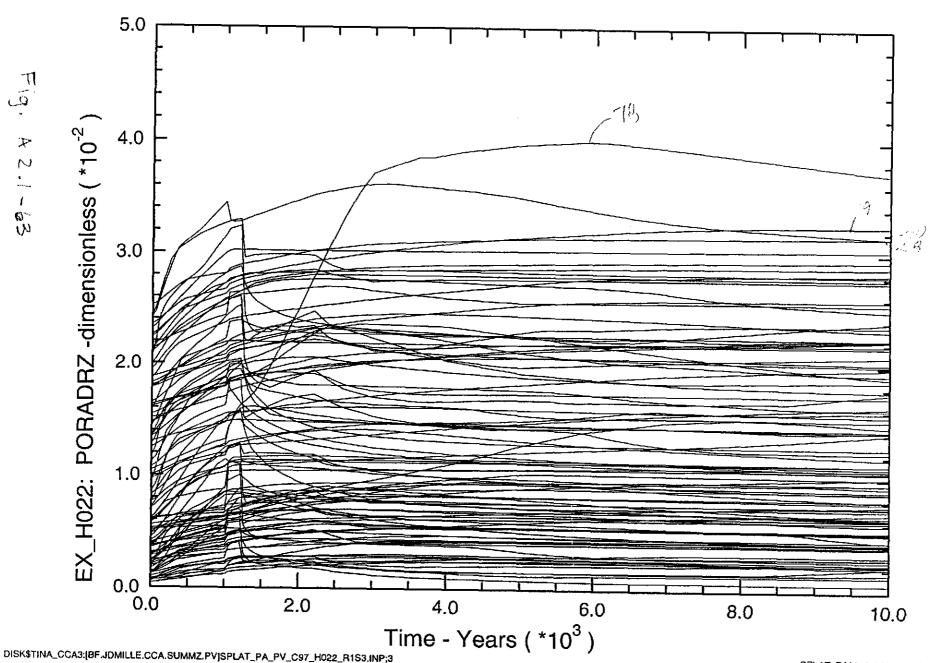
SNL WIPP PA: BRAGFLO SIM ATIONS (C97 R1 S3)







Volume-Averaged Porosity in All DRZ Layers



A.2.2 E2 Intrusion at 1000 Years (S5 Scenario)

Scenario E2, like Scenario E1, also involves a borehole that penetrates the waste-filled panel. Unlike the E1 scenario, however, the borehole does not go beyond the panel and into the underlying brine reservoir. The borehole is assumed to be emplaced instantaneously and plugged at the time of intrusion. Except for the plugs, the borehole is assumed to have a porosity of 0.32, with the high permeability of 1.0×10^{-9} m². One plug extends from the top of the Salado formation up through the Unnamed member of the Rustler formation. The other plug extends downward from the surface through the Santa Rosa formation. The permeability of the two plugs ranges from 1.0×10^{-19} to 1.0×10^{-17} m² (is 5.0×10^{-17} m²). These conditions exist for 200 years. At 200 years after intrusion, the borehole material properties are modified to represent the impact of caving, sloughing, and plug degradation. At this time the borehole is assigned uniform properties, with a permeability sampled from a range of 5×10^{-17} to 1×10^{-11} m² (10^{-14} to 10^{-11} m²). These conditions persist for the remainder of the 10,000 years.

A.2.2.1 Replicate 1 Results and Discussion

A.2.2.1.1 Repository Behavior

The time dependence of pressures in the waste panel and rest of repository are shown in Figures A.2.2-1 [GVAR_023] and A.2.2-2 [GVAR_024]. As in the E1 scenario, pressure responses in the experimental and operation regions are nearly identical to those in the waste panel and rest of repository because the permeability of excavated regions, drift and panel seals, and the DRZ are high and on the order of 10-15 m². In a few realizations where the DRZ or lower shaft permeability is low, on the order of 10⁻¹⁸ m², the experimental area shows a slower pressure response, however, this behavior does not influence the rest of the repository or the surrounding formations. In many realizations, pressures increase rapidly during the first 1000 years. These rapid increases in pressure are caused by a high gas generation rate coupled with creep closure. In these realizations, plastics and rubbers are included in the inventory of biodegradables; this results in a higher net rate of gas generation during the first 1000 years. In some realizations, the pressure reaches a maximum. In contrast to this behavior, some realizations (near the bottom of the plots) exhibit slowly increasing pressures. In these realizations, there is very little gas generation from corrosion (sampled corrosion rates are among the lowest) and none from biodegradation. The third type of behavior exhibited in Figures A.2.2-1 [GVAR_023] and A.2.2-2 [GVAR_024] is a moderately rapid initial rise in pressure. This behavior is a result of creep closure in combination with intermediate gas generation rates.

After intrusion, the rate of pressure increase tends to decrease slightly for 200 years. Recall that at the time of intrusion, the borehole has a high permeability of 1.0×10^{-9} m² everywhere except for two concrete plugs having a permeability ranging from 1.0×10^{-19} to 1.0×10^{-17} m² (5.0×10^{-17} m²). These plugs are located above the Salado in the Santa Rosa and Unnamed Members. These borehole conditions remain for 200 years after intrusion, at which time the borehole plugs degrade. Four (Three) general types of pressure behavior then follow. In approximately 20% of

the realizations, pressures decrease dramatically. In approximately 10% (5%) of the realizations, pressures continue to gradually increase for several thousand years followed by a period of decreasing pressure. In these realizations, sufficient quantities of brine flow into the panel to maintain relatively high gas generation rates due to corrosion and increasing pressure conditions. Corrosion continues in many realizations over the full 10,000 years regulatory period. Gas generation due to microbial degradation, however, has largely ceased as the cellulose inventory has been exhausted, generally within 1500 years. The third type of response is for the pressure to rise relatively rapidly following a period of low or slowly decreasing pressure. The time lag between intrusion and repressurization lasts from 500 to over 5000 years. During this time gas that has filled the panel is driven up the intrusion borehole as brine flows into the waste through the anhydrite layers. Once the borehole is filled with brine, the pressure in the waste reaches hydrostatic pressure relative to the water table in the Dewey Lakes, and then levels off. Note that in the E2 scenario more realizations take longer for the pressure in the repository to rise to hydrostatic pressure than did in the E1 scenario. Final pressures above hydrostatic pressure occur in those realizations having high corrosion rates and a relatively low borehole permeability (sampled parameter ranging from 5.0×10^{-17} to 1.0×10^{-11} m² (1.0×10^{-14} to 1.0×10^{-11} m²)) that prevents gas from easily escaping the panel and repository. Pressures below hydrostatic occur in those realizations where the borehole is filled predominately with gas. The fourth type of response (approximately 15% of the realizations) is for the pressure to remain relatively constant following intrusion. This behavior is centered in two pressure ranges, 8-9 MPa and 12-13 MPa. The driving factors for this fourth type of behavior are similar to the third type, the difference being that for the fourth type post-intrusion pressures are already above hydrostatic.

A.2.2.1.1.1 Gas Generation

The fraction of the initial steel inventory that remains after 10,000 years (Figure A.2.2-3 [GVAR_003]) ranges from about 3% to 98% (3% to 82%), compared with 3 % to 97% (3% to 84%) in the E1 scenario. The profiles of steel consumption with time are also very similar to the E1 results. Approximately one third of the realizations show slow but steady corrosion over the full 10,000 years, indicating that corrosion is controlled by the corrosion rate rather than by the availability of brine. In numerous other realizations, steel consumption slows significantly after varying lengths of time, indicating that corrosion eventually becomes controlled by the amount of brine available, rather than the corrosion rate. In some realizations, corrosion slows fairly early, between 1000 and 2000 years, and the rate never picks up again. It is also interesting to note that the intrusion has an insignificant impact on corrosion in the majority of realizations.

The consumption of cellulose (Figure A.2.2-4 [GVAR_004]) is nearly identical to both the E1 and Undisturbed scenarios. As in these preceding scenarios, the biodegradation rate is much faster than the corrosion rate and nearly all of the cellulose is reacted before corrosion consumes the brine needed for reactions to take place. Only in nine (two) realizations does any appreciable amount of cellulose remain after the intrusion.

The total amount of gas generated is similar to that generated in the E1 scenario, ranging from

about 2.4×10^6 m³ to 3.5×10^7 m³ (1.5×10^6 m³ to 3.6×10^7 m³) at reference conditions over 10,000 years. The distribution of amounts generated differs slightly, with the mean gas volume being higher in the E1 scenario (1.72×10^7 m³ (1.74×10^7 m³)) than in the E2 scenario (1.39×10^7 m³ (1.60×10^7 m³)), reflecting the greater availability of brine from the Castile Formation. Similar amounts of brine are consumed in the E2 and E1 scenarios, a maximum of 49,600 m³ (41,000 m³) in the E2 scenario compared with 48,400 m³ (44,000 m³) in the E1 scenario.

A.2.2.1.1.2 Halite Creep

Creep closure of the repository and consolidation of the waste behaves similarly in all realizations, as it did in the E1 scenario. In all cases, a very rapid reduction in porosity (Figure A.2.2-5 [GVAR_052]) occurs during the first 300 - 500 years. At the time of intrusion, the waste porosity has mostly leveled off at values ranging from 8% to 22% (8% to 20%), depending on the pressure in the waste. When the pressure is high, the porosity remains higher as fluid pressures resist further closure. When the intrusion occurs, the borehole connects the panel with the overlying formations and atmosphere. However, the low permeability plugs located above the Salado in the Santa Rosa and Unnamed Members effectively prevent communication with overlying formations for two hundred years subsequent to intrusion. After 200 years, the plugs in the borehole degrade, raising the borehole permeability to the sampled value. This increase in permeability allows gas and brine to escape up the borehole, reducing the pressure in the waste, and causing the porosity to further decrease. In some cases, the repository pressure and porosity are prevented from decreasing significantly because the borehole permeability is sufficiently low and the gas generation rate is sufficiently high. In other cases, the pressure continues to increase after intrusion. After about 2000 years, the pressure and porosity in the waste generally stabilize. The minimum porosity tends to drift very slowly downward over time, reaching approximately 5% by 10,000 years. This porosity is just slightly greater than the minimum porosity computed by SANTOS for a repository at low pressure. The maximum porosities level off at about 21% (18%), corresponding to pressures ranging up to 14 MPa (9 MPa).

Some realizations display more rapid transient responses at later times. In some cases where brine influx is slow but steady, the portion of the borehole above the repository remains gas-filled for hundreds or thousands of years. This gas-filled connection to the overlying formations and the surface keeps the repository at near-atmospheric pressures. If enough brine flows in, all of the gas (down to residual gas saturation) is eventually driven out of the panel and both the panel and borehole fill with brine. This gas is either driven up the borehole or forced up-dip into the rest of the repository and DRZ. As the panel and borehole fill with brine, the pressure in the repository will increase fairly rapidly until hydrostatic pressure relative to the water table in the Dewey Lakes is reached. This relatively rapid increase in pressure, and the resulting increase in porosity, can be seen in some realizations between 2000 and 8000 years, both in the pressure plot (Figure A.2.2-1 [GVAR_023]) and in the porosity plot (Figure A.2.2-5 [GVAR_052]).

A.2.2.1.1.3 Fluid Flow

Cumulative brine flow into the repository is shown in Figure A.2.2-6 [GVAR_054]. Amounts of brine entering the repository during the first 1000 years range from nearly zero to about 35,000 m³ (30,000 m³) with one extreme realization (#24) having almost 55,000 m³. Most of this inflow occurs very early, as the repository equilibrates with the surrounding formations. At 1200 years, when the borehole plugs degrade and their permeability increases, the rate of brine inflow increases in several realizations. In most cases, this increase is caused by brine flowing down the borehole from the overlying Culebra and Dewey Lakes Formations. The majority of realizations exhibit a slow but steady increase in brine inflow, reflecting the continual inflow from the marker beds. Those realizations that display a rapid increase in brine inflow over the 2000 years following the intrusion eventually experience a rather sharp decline in inflow rate. This decline in inflow rate occurs when the panel and rest of the repository fill, to the extent possible, with brine flowing down the borehole. Thereafter, the rate of inflow is an indication of the sampled permeability of the marker beds. After 10,000 years, the cumulative brine inflow ranges from 240 to 133,000 m³ (3,000 to 137,000 m³).

Brine outflow from the repository (Figure A.2.2-7 [GVAR_059]) shows similar behavior to brine inflow except that the outflow is delayed by the amount of time needed to fill the repository and is much lower in quantity, ranging from zero to 45,000 m³ (91,000 m³) at 10,000 years. Those realizations in which large amounts flow in by way of the borehole also have a lot of brine flowing out by way of the borehole. The amount flowing out of the repository reflects a combination of brine being driven out (either up the borehole or simply into the DRZ) by continual brine inflow from the interbeds and by gas generated by corrosion. Brine outflow is reduced when high corrosion rates consume brine. In many realizations, the brine consumption rate is high enough that all brine inflow is consumed, keeping the brine outflow at or near zero.

Brine flow up the shaft ranges from 0 m³ to 57 m³ (0 m³ to 48 m³) (Figure A.2.2-8 [GVAR_069]). There is no upward flow of brine from the repository level.—This brine is believed to originate in the upper section(s) of the shaft. This conclusion is based on examination of flows at different locations in the shaft for individual realizations and is verified in Section 3.0 describing the Salado transport analysis.

Flow up the borehole at the top of the panel (Figure A.2.2-9 [GVAR_073]) occurs in 20 (5) realizations, in amounts ranging from less than 1 m³ to 4,400 m³ (120 m³ to 21,900 m³). The realizations with the highest flows up the borehole all have a very high borehole permeability and a low DRZ permeability. Brine flow up the borehole at the elevation of the Culebra (Figure A.2.2-10 [GVAR_074]) is similar to flow at the top of the panel. At most 0.7 m³ (5.3 m³) of brine flows up past the top of the Rustler (Figure A.2.2-11 [GVAR_075]), and none reaches the surface.

A.2.2.1.2 Behavior in Formations Surrounding the Repository

A.2.2.1.2.1 Two-Phase Flow

Once the borehole plugs degrade at 1200 years, large volumes of gas (up to $1.6 \times 10^7 \, \text{m}^3$) (up to $9.5 \times 10^6 \, \text{m}^3$) are vented up the borehole (Figure A.2.2-12 [GVAR_101]). Large amounts continue to flow from the DRZ for as long as gas is generated (Figure A.2.2-13[GVAR_102]). The total amount of gas vented up the borehole ranges from about 300 m³ up to $35 \times 10^6 \, \text{m}^3$ (1.0 $\times 10^6 \, \text{m}^3$ up to $32 \times 10^6 \, \text{m}^3$). The maximum total amount of gas generated is $35 \times 10^6 \, \text{m}^3$ (36 $\times 10^6 \, \text{m}^3$) (Figure A.2.2-14 [GVAR_022]). Thus, a large fraction of the gas generated eventually flows up the borehole. Very little gas (less than 25 (22) m³) flows up the shaft (Figure A.2.2-15 [GVAR_100]).

Gas flow into the interbeds occurs in only 10 to 20% of the (a few) realizations, and the amounts are very small compared to flow up the borehole. In MB138, the largest of the realizations shows 38,000 m³ (40,000 m³) flowing to the north (Figure A.2.2-16 [GVAR_106]) and 44,000 m³ (35,000 m³) flowing to the south (Figure A.2.2-17 [GVAR_109]). In Anhydrite a and b (Figures A.2.2-18 [GVAR_107] and A.2.2-19 [GVAR_110]), several realizations show small flows of gas (less than 3,000 m³), but only in six (three) realizations does more than 10,000 m³ flow out; the maximum is 430,000 m³ (133,000 m³) to the north. In MB139, a maximum of 420,000 m³ (11,000 m³) flows to the north (Figure A.2.2-20 [GVAR_108]); to the south, the maximum flow is 550,000 m³ (4,000 m³) (Figure A.2.2-21 [GVAR_111]).

Brine flow into and out of the marker beds in the E2 scenario are similar to that in the E1 scenario (Figures A.2.2-22 [GVAR_079] to A.2.2-42 [GVAR_099]). The maximum net flows (Table A.2.2-1) are similar in the two scenarios. The highest flows out of the DRZ are into Marker Bed 139, with about half as much flowing northward as to the south. Compared to the amount that flows into the DRZ, outflows are very small, about 10% (less than 1%) as large as inflows.

Table A.2.2.-1. Cumulative Net Interbed Brine Flows for E2 Intrusion at 1000 Years (S5 Scenario)

Marker Bed	Max. Net Brine Flow from MB into DRZ, m ³	Max. Net Brine Flow from DRZ into MB, m ³
MB138 North	90 (300)	100 (4)
MB138 South	1650 (3700)	17 (0)
Anhydrite a & b North	4300 (8800)	0 (0)
Anhydrite a & b South	5300 (9800)	0 (0)
MB139 North	11,100 (20,200)	1700 (100)
MB139 South	12,600 (21,200)	3300 (100)
All Marker Beds	34,000 (64,000)	5200 (200)

The cumulative flows out all anhydrite layers and across the land withdrawal boundary are summarized in Figure A.2.2-43 [GVAR_174] and Table A.2.2-2. Flows in individual layers are presented in Figures A.2.2-44 [GVAR_168] to A.2.2-49 [GVAR_173]. As shown, only one realization (#38) has brine flow out across the land withdrawal boundary. The maximum volume released in all marker beds over the 10,000 years regulatory period is 2735 m³ (1.28 m³). The high flow across the land withdrawal boundary in vector #38 is due to the combination of low borehole permeability, very high DRZ and marker bed permeabilities, a very low DRZ porosity, and a low far-field pressure. The brine that flows across the land withdrawal boundary does not originate in the repository; rather, it is brine that is initially present in the marker beds, as is demonstrated in Section 3.0 describing the Salado transport analysis. This result is not surprising since the pore volume of Marker Bed 139 (which provides most of the flow in vector #38) between the repository and the land withdrawal boundary is greater than 155,000 m³.

Table A.2.2-2. Cumulative Interbed Brine Flows Across Land Withdrawal Boundary for E2 Intrusion at 1000 Years (\$5 Scenario)

Marker Bed	Maximum Brine Outflow across Land Withdrawal Boundary, m ³
MB138 North	110 (0.19)
MB138 South	125 (0.0)
Anhydrite a & b North	520 (0.27)
Anhydrite a & b South	120 (0.0)
MB139 North	1350 (0.82)
MB139 South	510 (0.0)
All Marker Beds 2735 (1.28)	

A.2.2.1.2.2 Mechanical Response

As in the E1 scenario, gas is not generated at sufficiently high rates in most realizations to reach fracture pressures prior to the intrusion at 1000 years. After the intrusion, the borehole prevents pressures from building up to the point where fracturing could again take place. As a consequence, fracturing occurs in less than 10 (only four) realizations (Figures A.2.2-50 [GVAR_113] to A.2.2-55 [GVAR_118]). Only two realizations, #58 and #38, have significant fracturing. In realization #58 fracture lengths are 400 m in Anhydrite a and b north and 100 m in other marker beds. In realization #38 fracture lengths are 400 m in Anhydrite a and b north and Marker Bed 139 north. All marker bed fractures in realization #38 close up before 10,000 years.

Significant fracturing in the DRZ occurs in only about 3 realizations, as indicated by increasing DRZ permeability (Figure A.2.2-56 [EX_H033]). Note that the permeability increase around

1000 years in all realizations with permeability less than about 10^{-16} m² is an artifact of the volume averaging scheme (which includes the 10^{-9} m² borehole) and is not indicative of fracturing. DRZ porosity increases, indicative of lesser DRZ fracturing are also evident in some of the realizations (Figure A.2.2-57 [EX_H022]). Only one realization (#58) results in DRZ permeabilities greater than 1×10^{-12} m² and porosities greater than 0.03. Mean, median, and maximum values for DRZ permeability and porosity are shown in Table A.1-3.

A.2.2.2 Comparison with Other Intrusion Time [350-year version of E2 (S4 Scenario)]

The S4 scenario is another E2 scenario in which the intrusion occurs at 350 years instead of at 1000 years as in the S5 scenario. The borehole properties are the same as in the 1000-year intrusion, but changes take place 650 years earlier.

Because the S4 intrusion time is earlier (350 years), not as much gas is generated prior to intrusion, and the pressure in the waste does not build up as high prior to intrusion as in the S5 1000-year intrusion. The peak pressure observed in the waste panel in the 350-year intrusion is 10.5 MPa, compared with 14.0 MPa in the 1000 yr intrusion case. By 10,000 years nearly the same amount of gas is generated. The reason for this is that sufficient brine is available for both corrosion and biodegradation to proceed at their full rates for at least 1000 years without requiring any supplemental brine from outside sources. Therefore, the earlier intrusion does not provide any additional brine that can be used to drive the reactions faster. After 1000 years, approximately the same amount of brine is available for the reactions regardless of whether the intrusion occurs at 350 years or 1000 years. The cellulose inventory is again fully consumed, as it is in the later intrusion case, within 1000 years in all but the same 8-10 realizations.

Except for some transients between 350 and 1200 years, the porosity in the waste differs very little from the later intrusion. After the first few hundred years, the porosity is a highly damped response to the pressure, and the waste porosity tracks the waste pressure very closely. After about 1200 years, the pressure in the waste behaves similarly in both the earlier and later intrusions.

The largest brine outflows occur in realizations in which large amounts of brine first flow down the borehole from overlying formations. This initial downflow is greater in the S4 scenario because the pressure in the waste is lower. Maximum brine flow up the borehole at the Rustler/Culebra interface is 4800 m³ for S4 and 4500 m³ for S5. As in all other scenarios and replicates, none of the brine flowing up the borehole reaches the surface in any realization in this scenario; almost all of it flows into the Culebra.

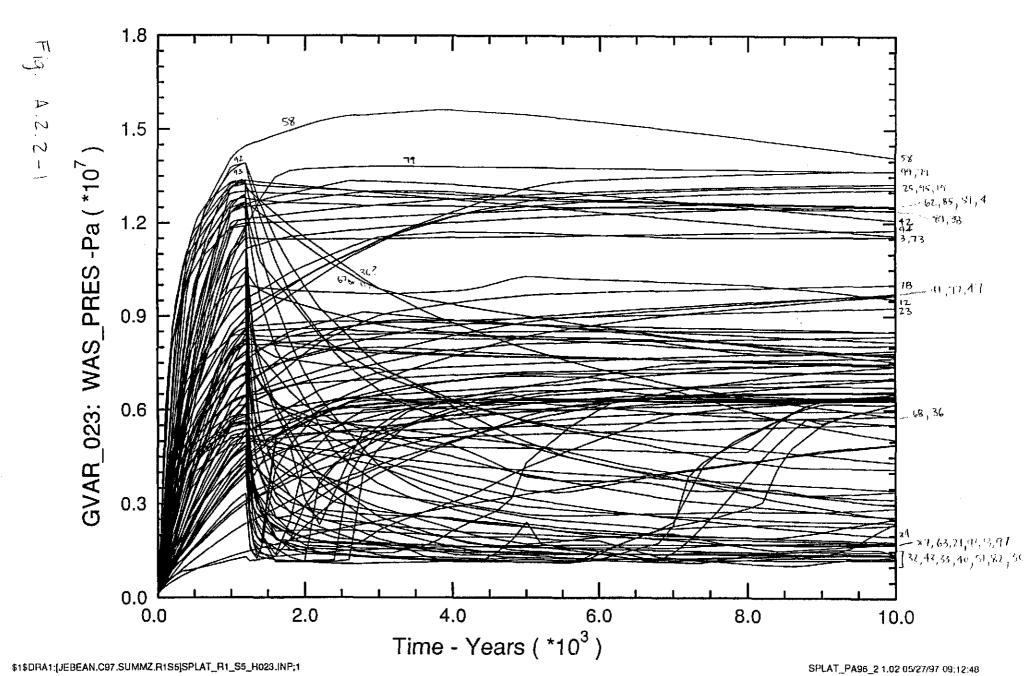
Brine flow into the DRZ from the marker beds is slightly higher (about the same) for the 350-year intrusion as for the 1000-year intrusion. The maximum is 35,000 m³ for S4 vs. 34,000 m³ for S5. Brine flow out of the DRZ into the marker beds is lower in the earlier intrusion. The maximum outflow is 4500 m³, compared with 5200 m³ after the later intrusion. The maximum brine outflow in all marker beds across the land withdrawal boundary is about

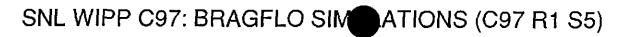
 $2600~\text{m}^3$ for S4 and about $2700~\text{m}^3$ for S5. The outflow across the LWB in all other realizations in both scenarios is insignificant.

Gas flow up the borehole at the top of the panel is slightly greater than in the later intrusion, with a maximum of 1.96×10^7 m³ (at reference conditions), compared with 1.94×10^7 m³ in the 1000-year intrusion. The maximum gas flow from the DRZ into the marker beds is also similar (more than an order of magnitude lower than with the 1000-year intrusion). Because the shaft seals are very effective in preventing brine or gas flow up the shaft, gas flow at the top of the Salado originating in the asphalt seal is essentially independent of repository behavior, so those flows are virtually identical (and insignificant at 24 m³) in both intrusion times.

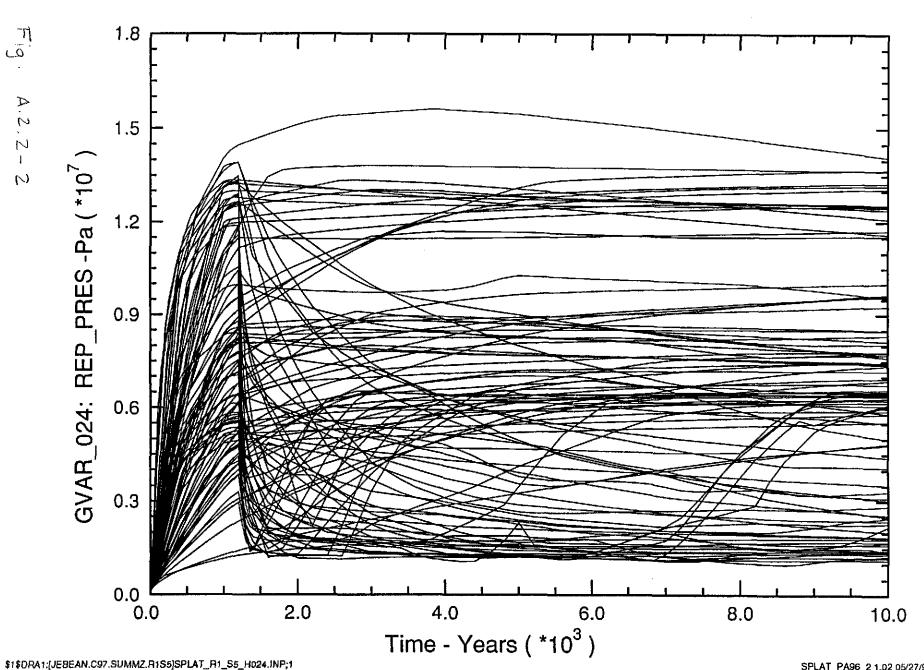






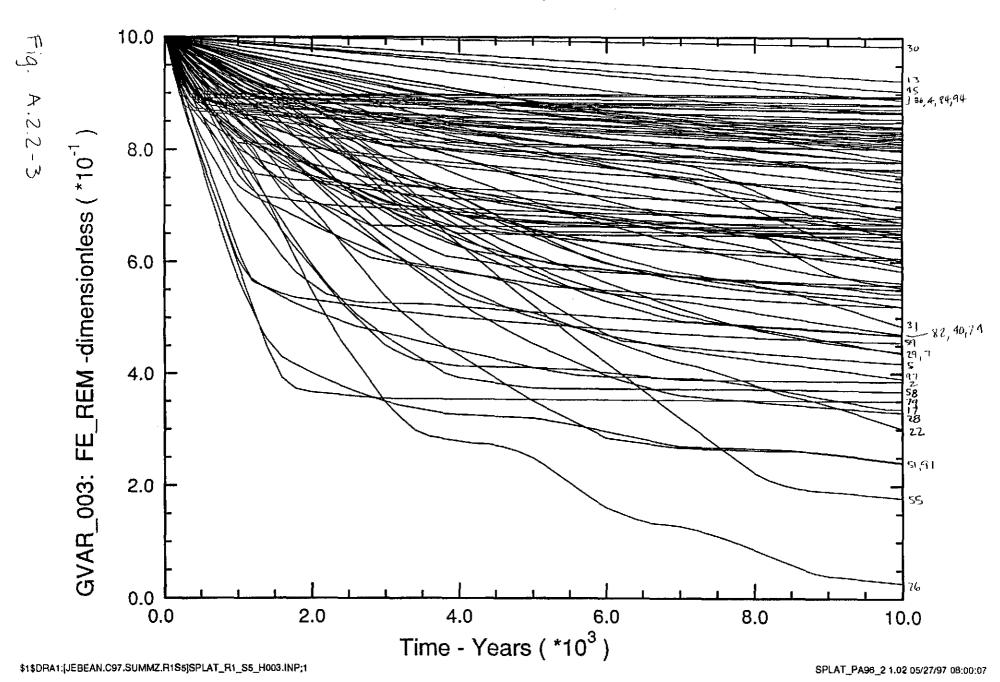


Volume-Averaged Pressure in Rest of Repository

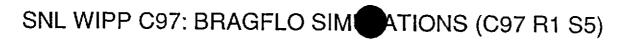


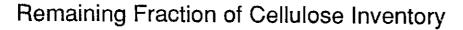


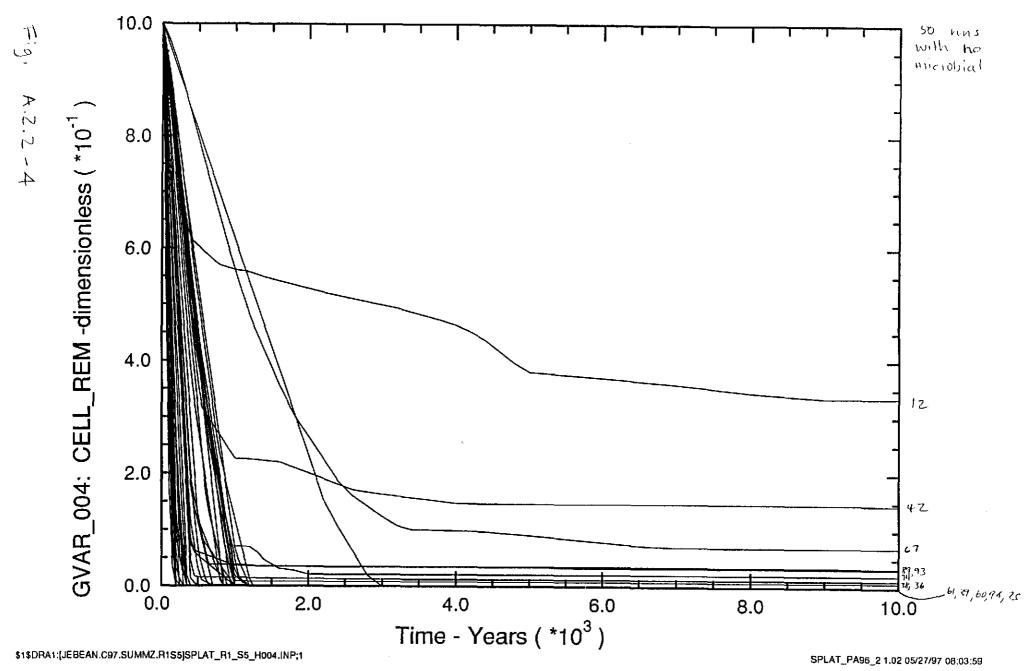
Remaining Fraction of Steel Inventory



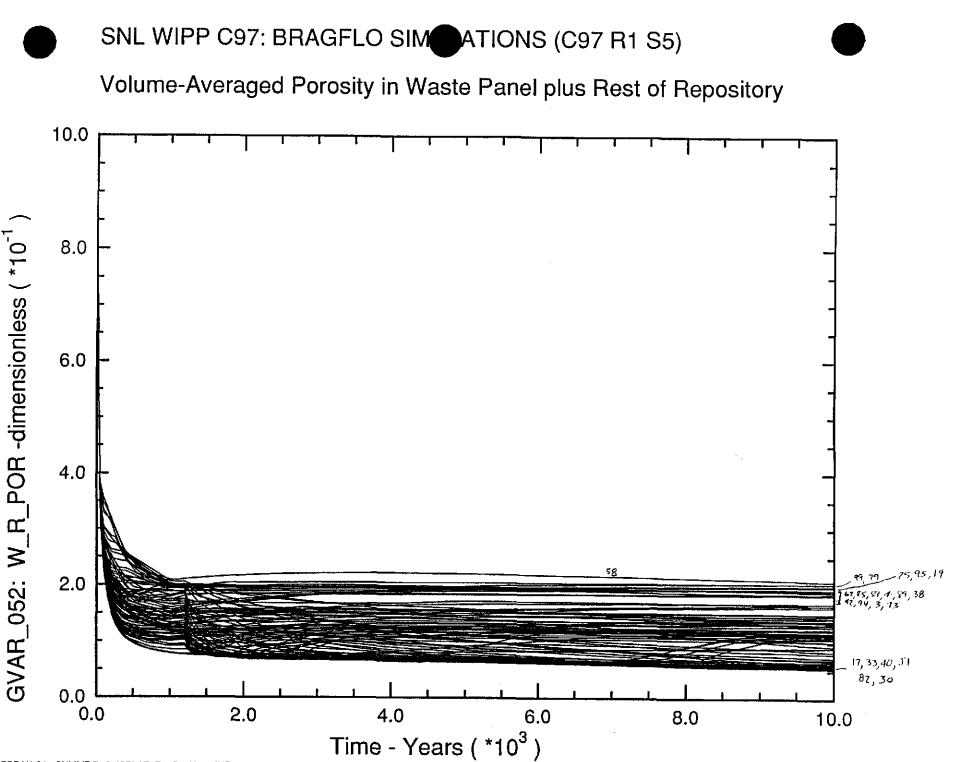
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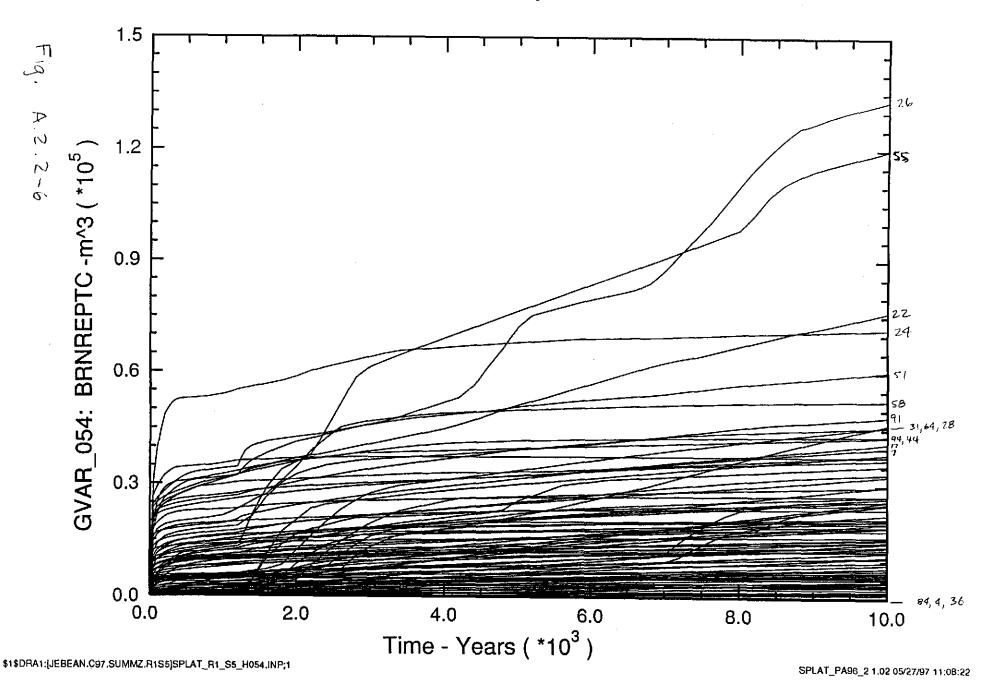
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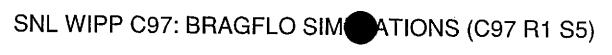
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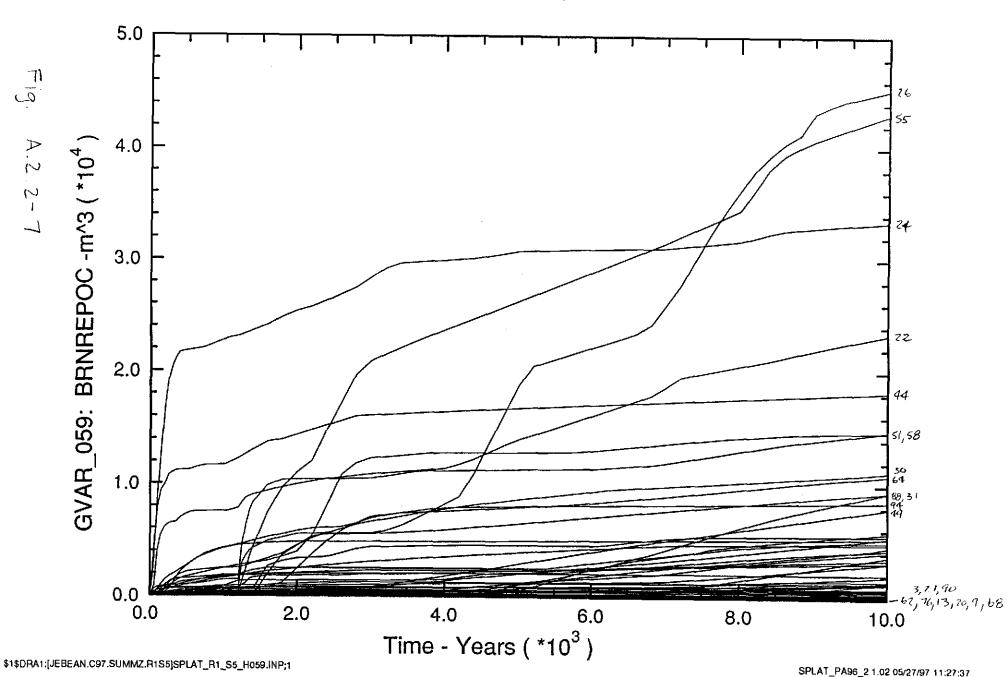
Cumulative Brine Flow into Repository



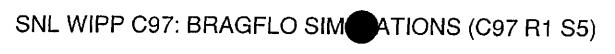
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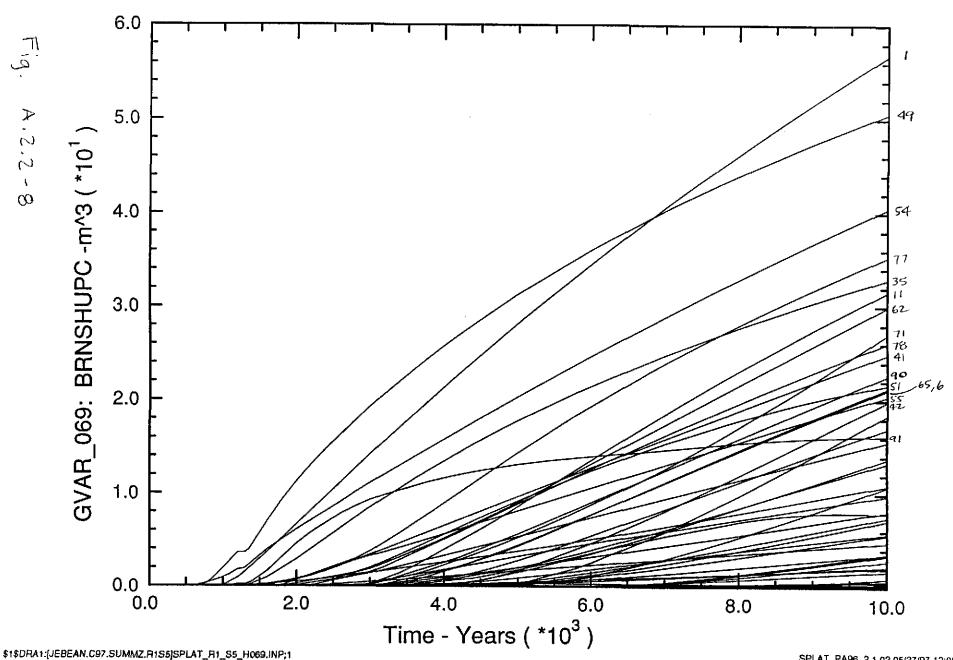
Cumulative Brine Flow Out of Repository



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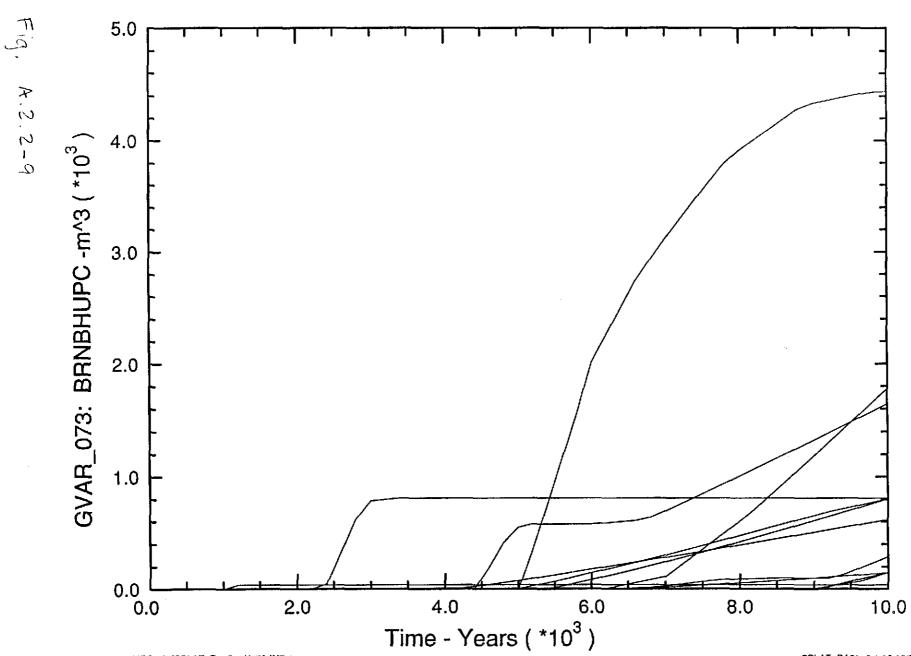
Cumulative Brine Flow up Shaft at top of Salado (E:661)



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Cumulative Brine Flow Up Borehole at Top of Panel

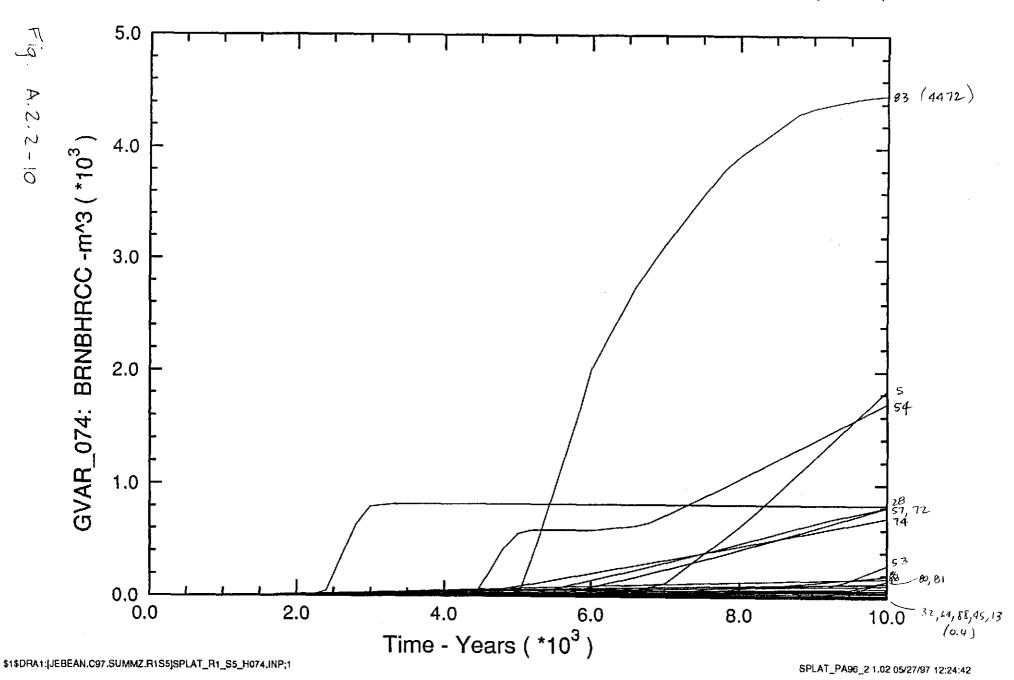


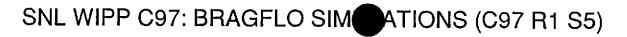
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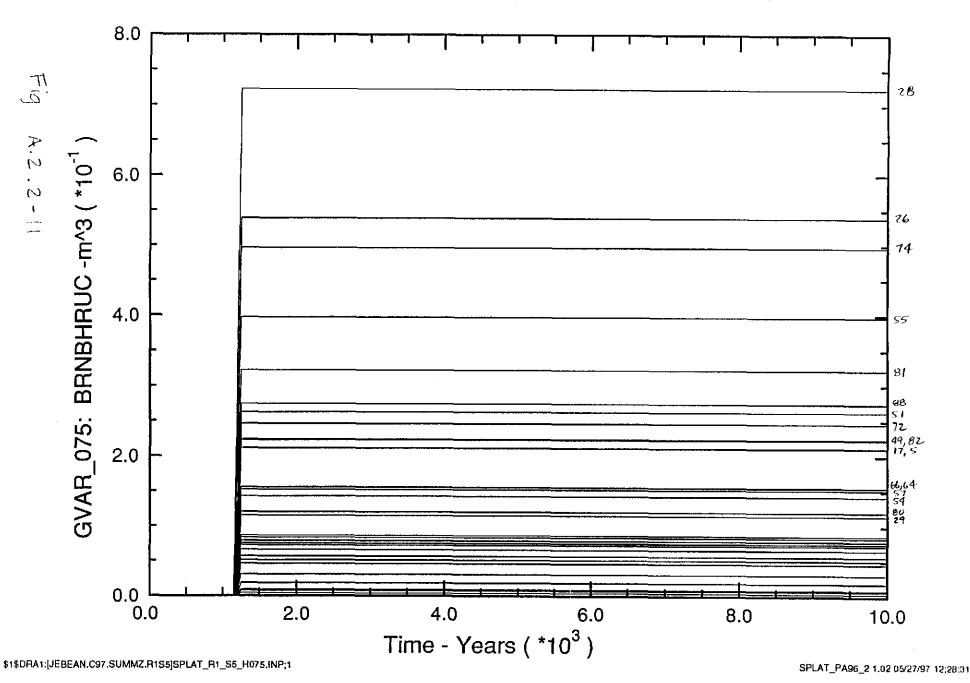


Cumulative Brine Flow up Borehole at Rustler/Culebra Interface (E:713)



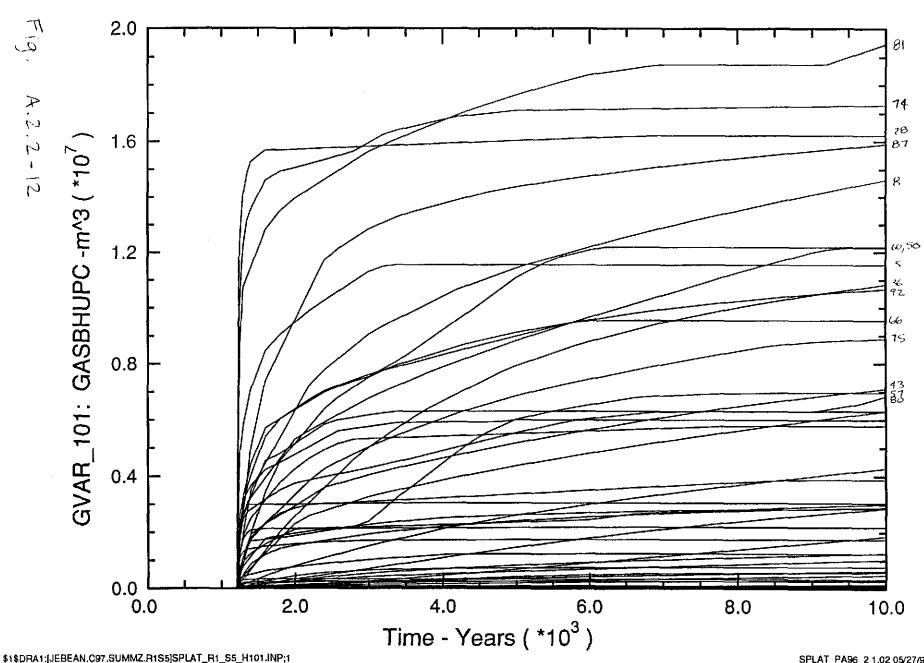


Cumulative Brine Flow up Borehole at Top of Rustler (E:841)

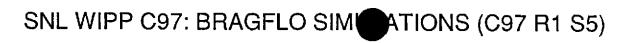




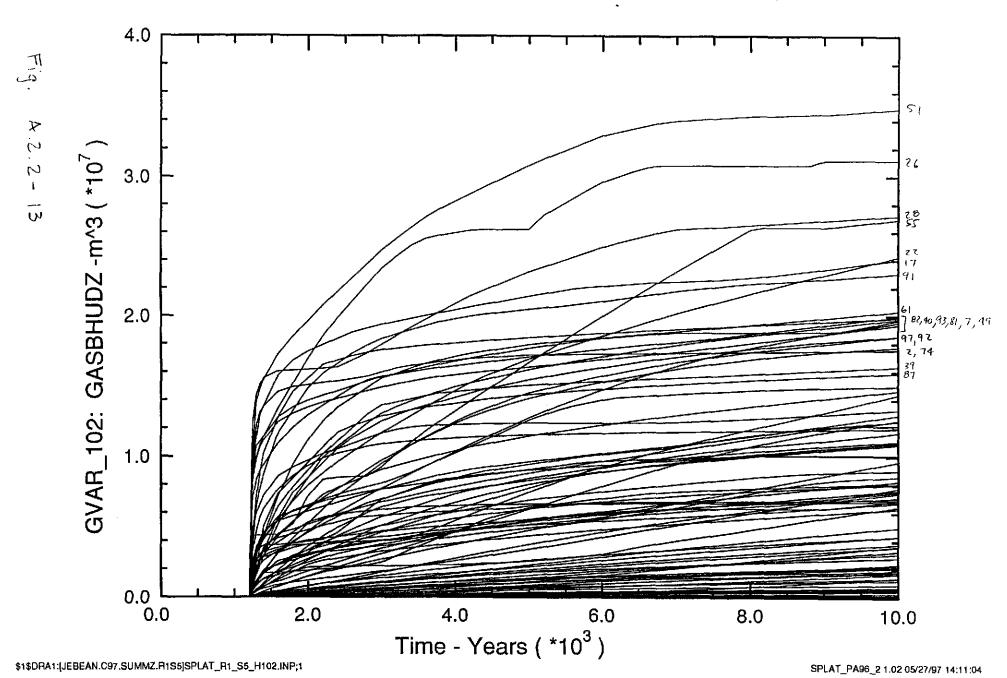
Cumulative Gas Flow up Borehole at Top of Panel (E:471)

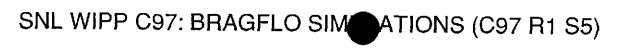


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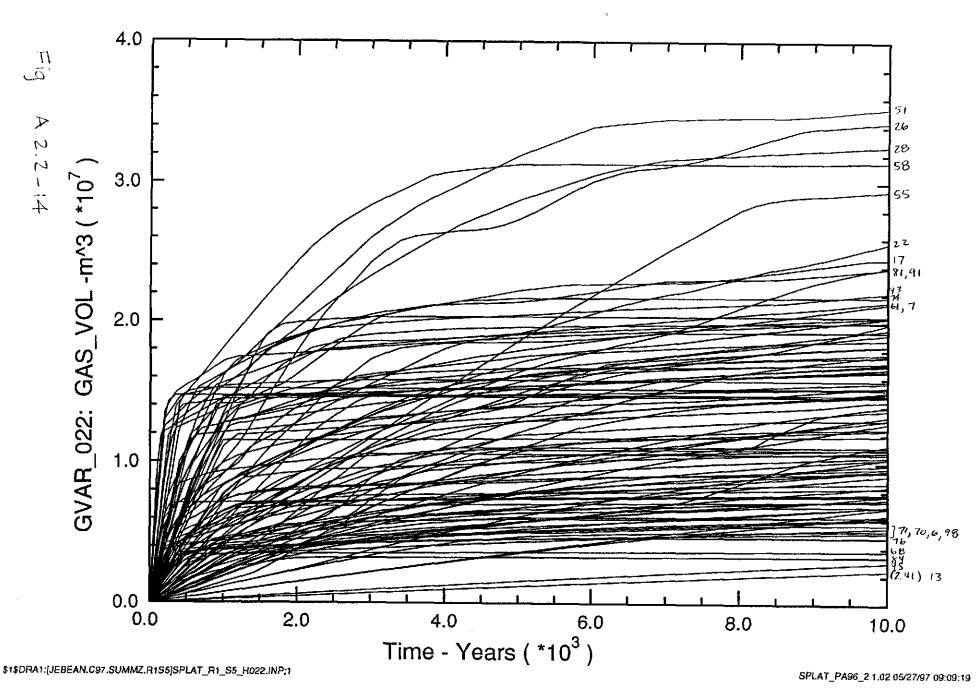


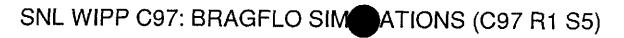
Cumulative Gas Flow Out of Upper DRZ at Borehole (E:575)



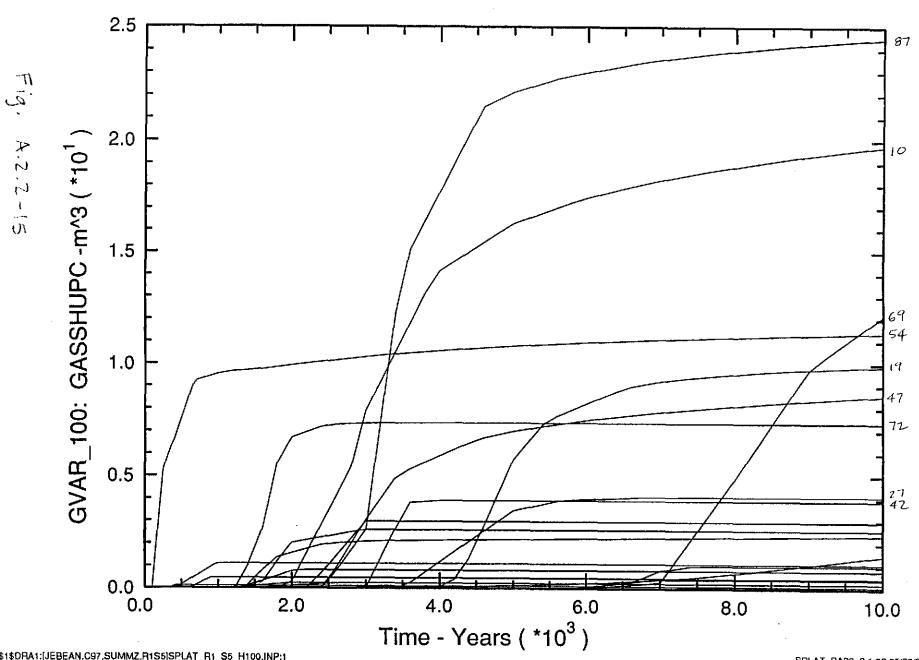


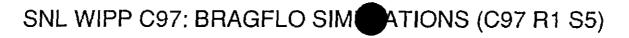




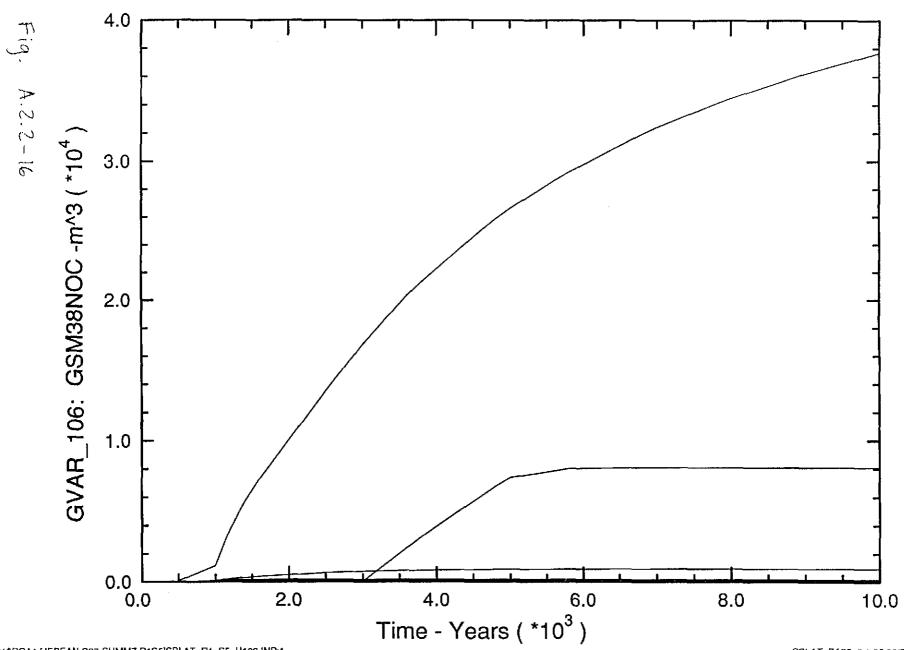


Cumulative Gas Flow up Shaft at Top of Salado (E:661)



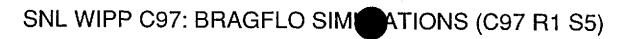


Cumulative Gas Flow from DRZ into North MB 138

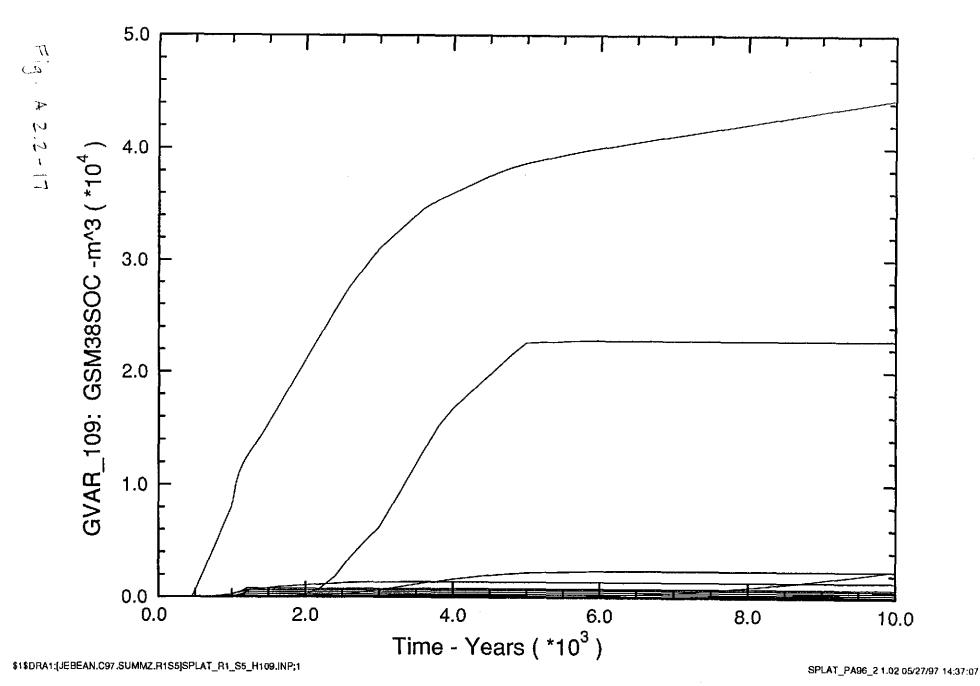


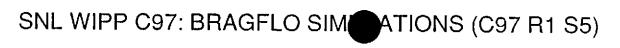
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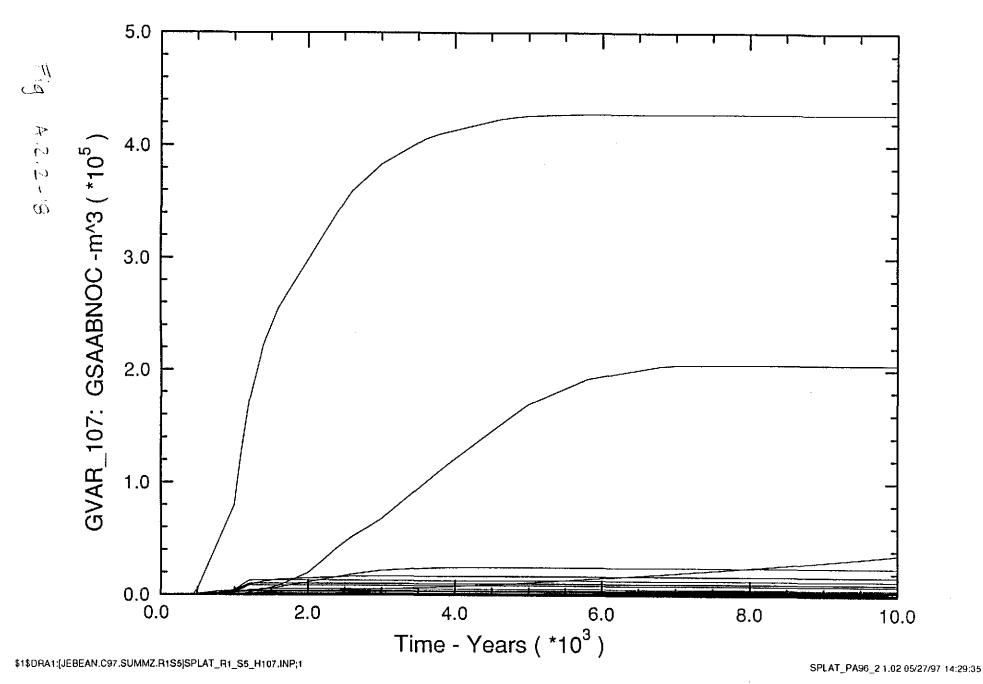


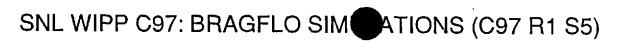
Cumulative Gas Flow from DRZ into South MB 138



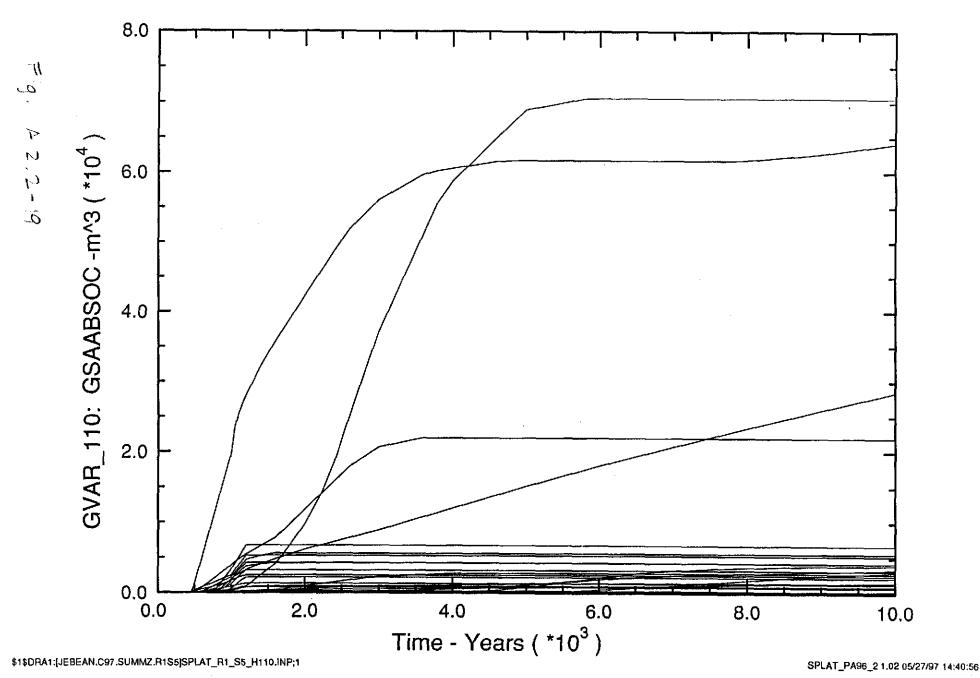


Cumulative Gas Flow from DRZ into North Anhydrite A/B



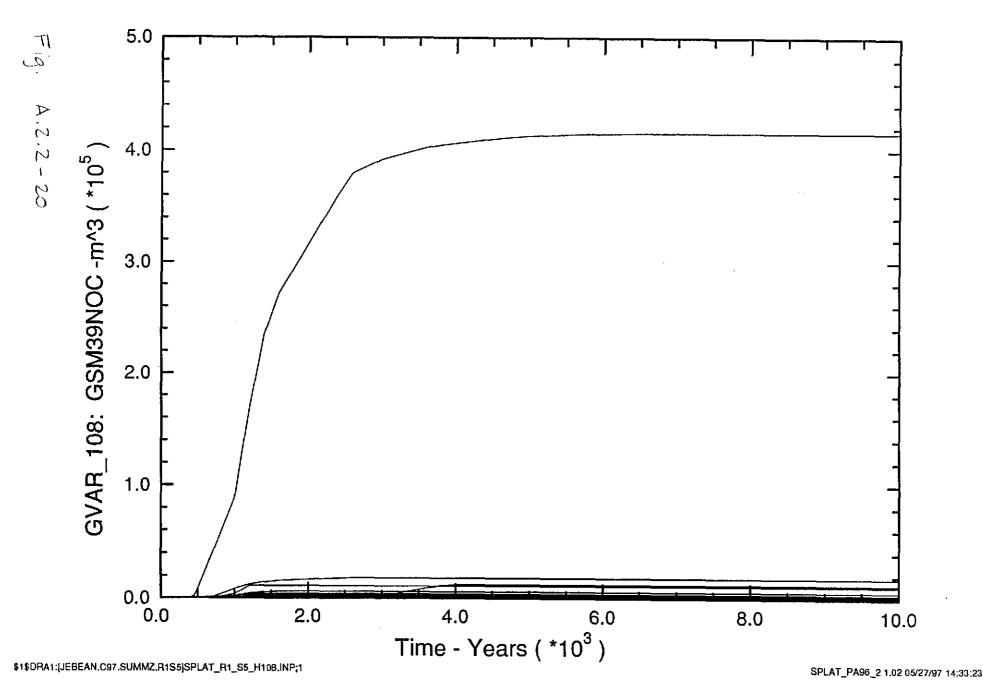






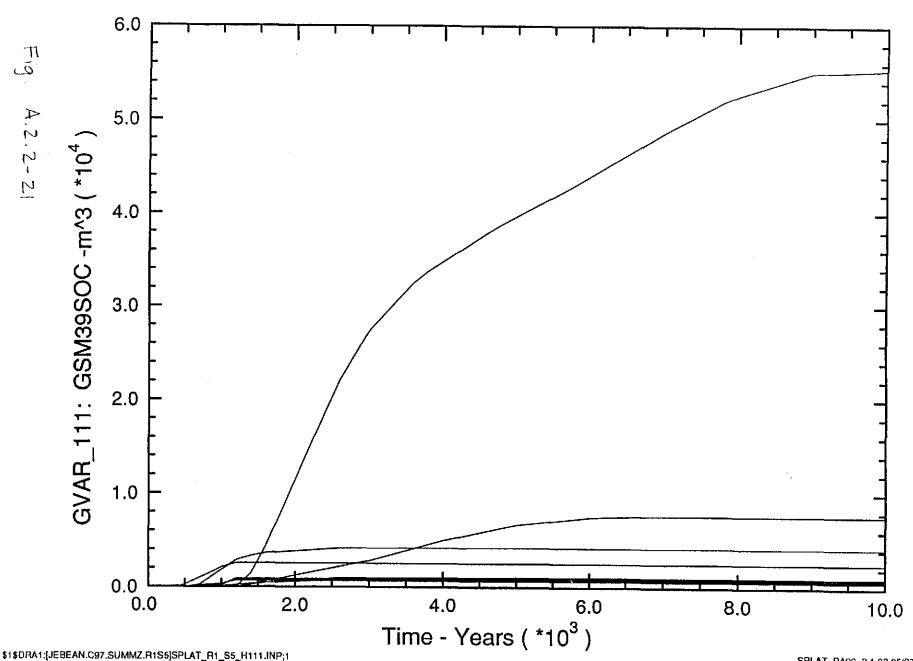
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Cumulative Gas Flow from DRZ into North MB 139





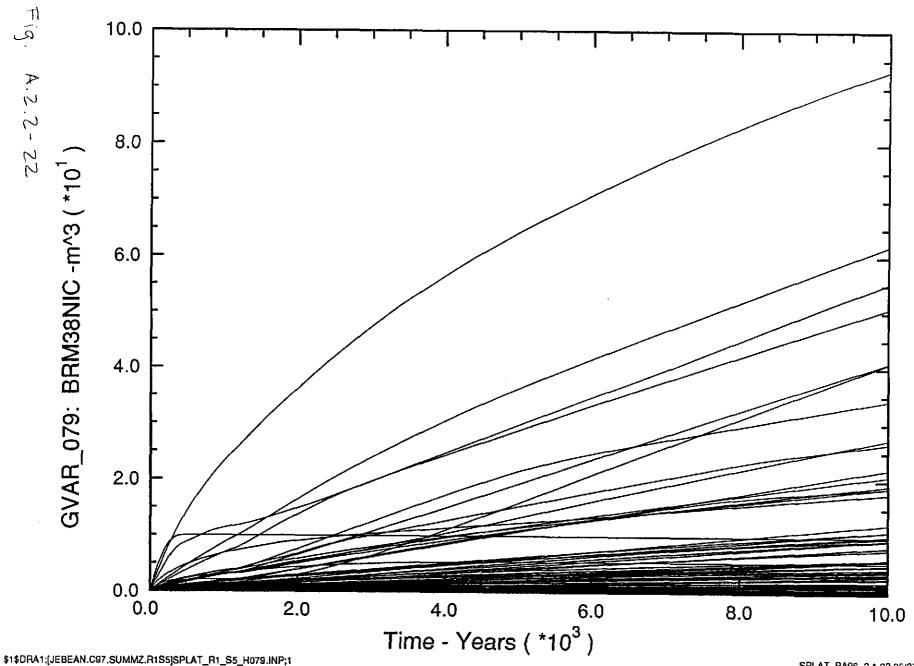
Cumulative Gas Flow from DRZ into South MB 139



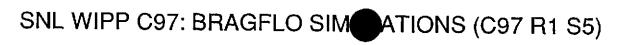
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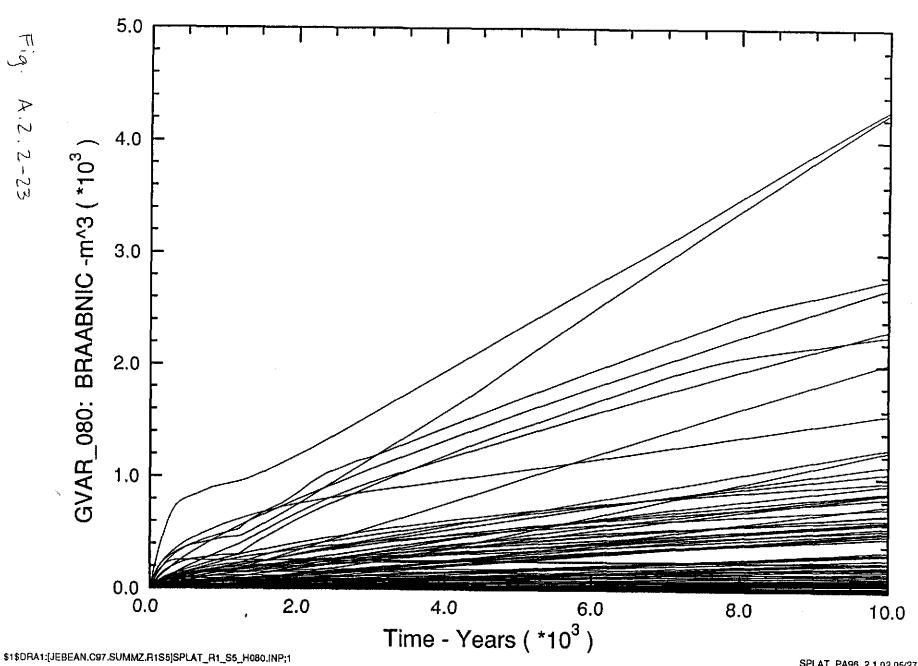
Cumulative Brine Flow Out of North MB 138 into DRZ



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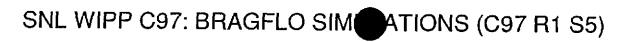


Cumulative Brine Flow Out of North Anhydrite A/B into DRZ

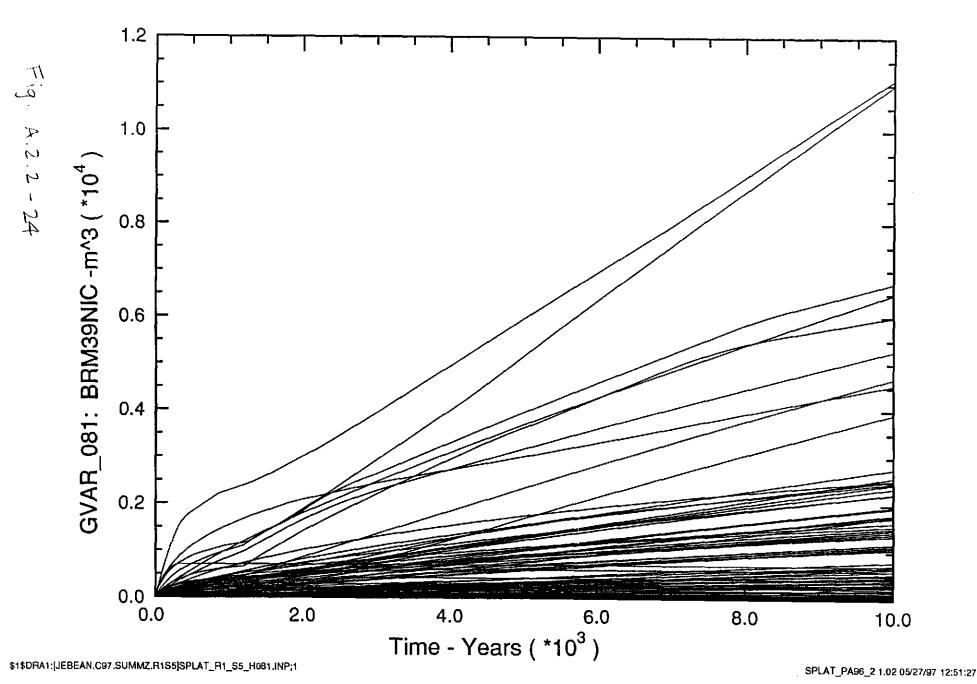


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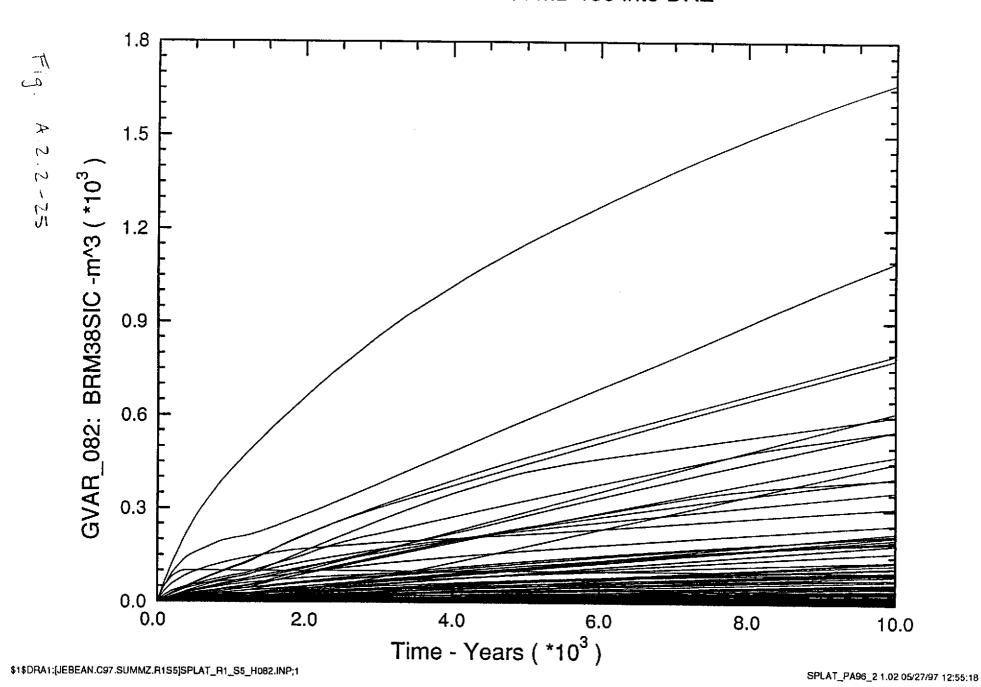


Cumulative Brine Flow Out of North MB 139 into DRZ

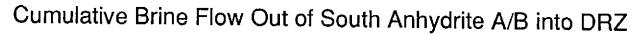


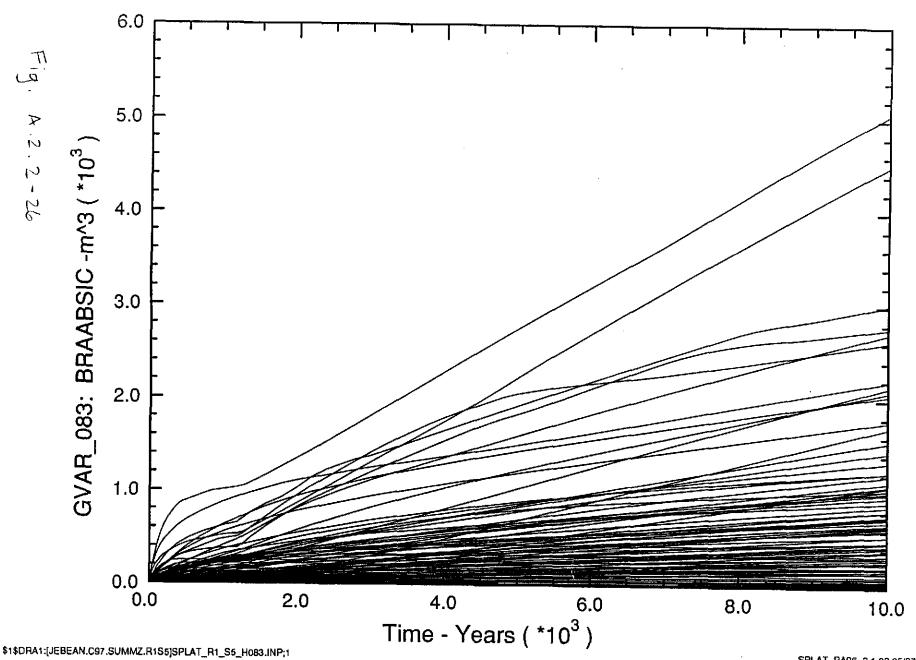
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Cumulative Brine Flow Out of South MB 138 into DRZ



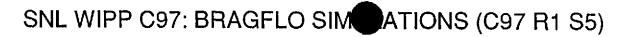




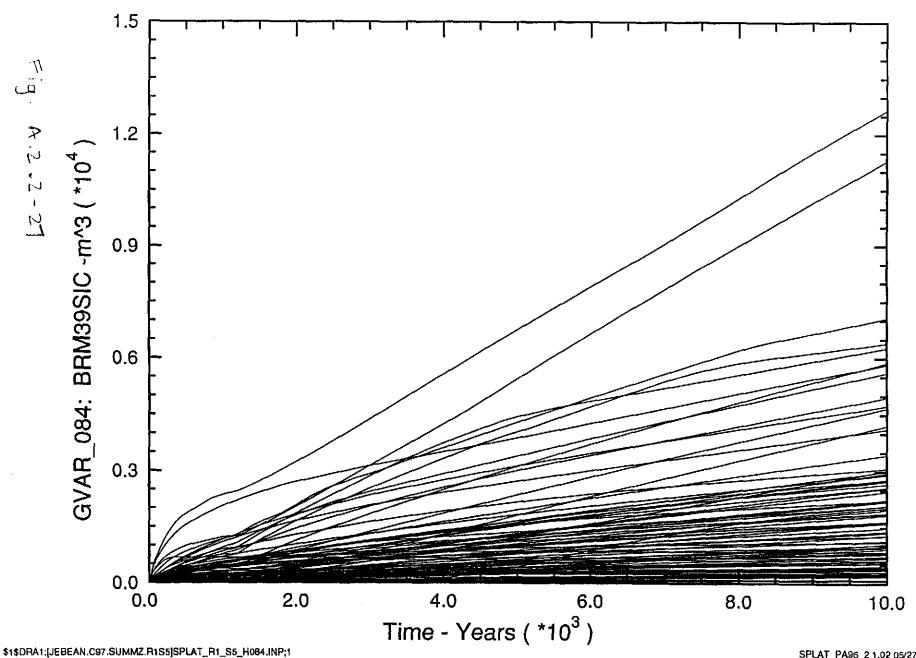


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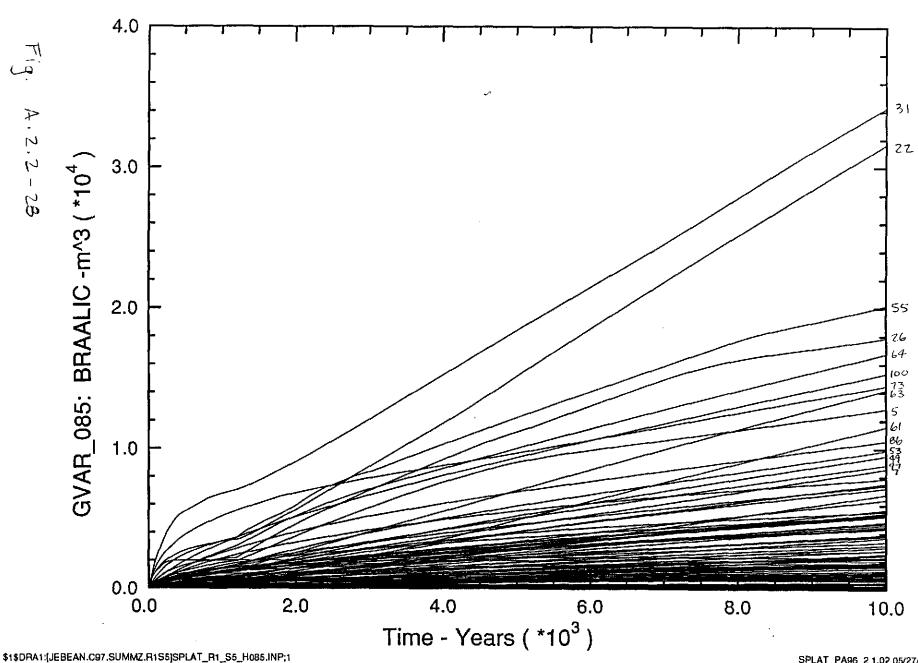
Cumulative Brine Flow Out of South MB 139 into DRZ



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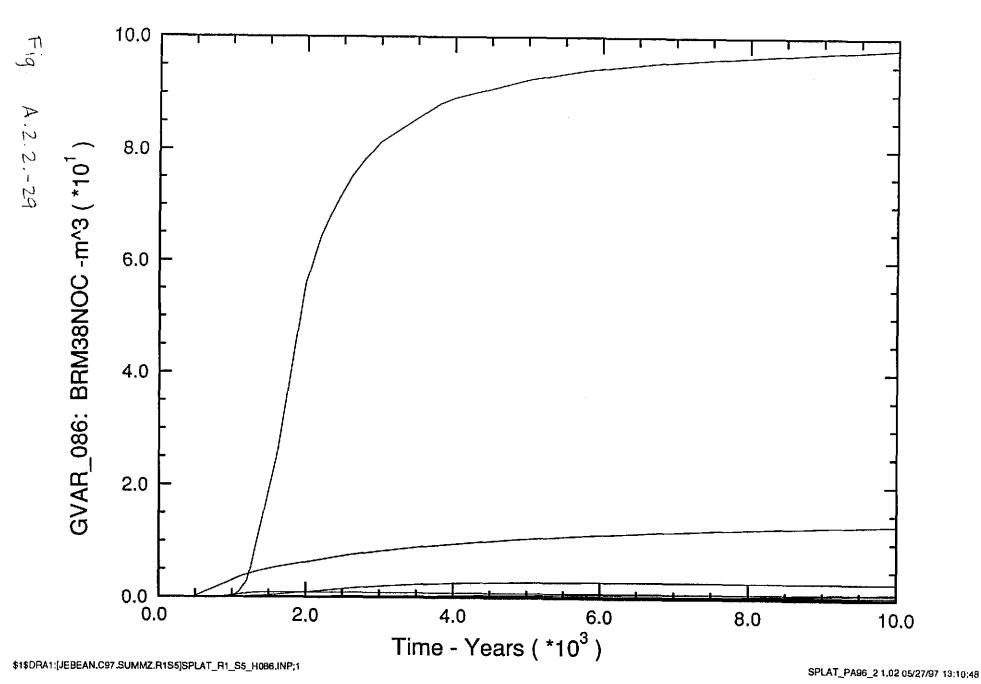
Cumulative Brine Flow into DRZ from All Marker Beds

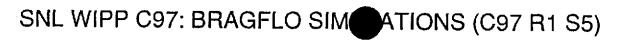


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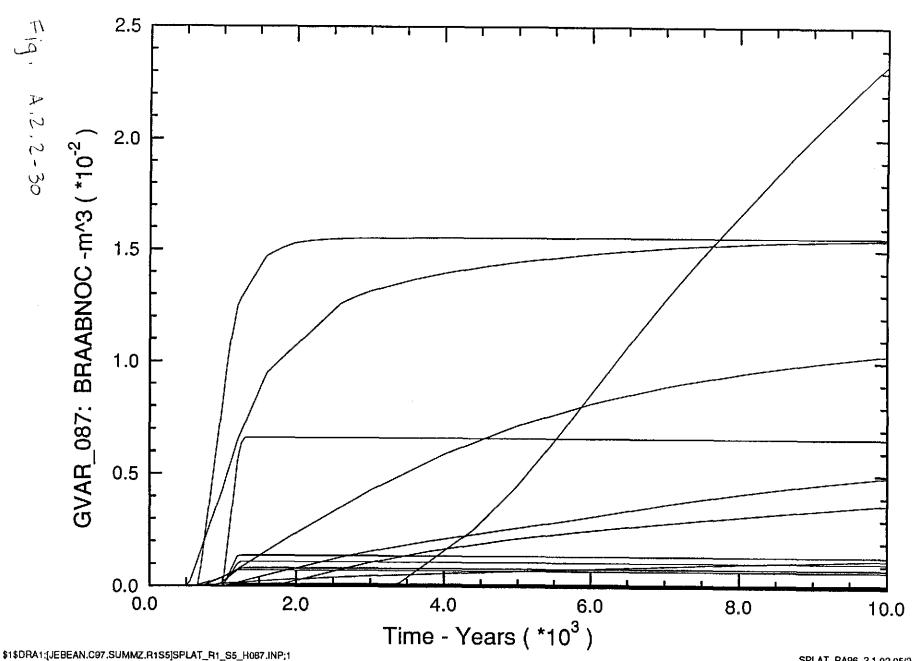
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Cumulative Brine Flow Out of DRZ into North MB 138

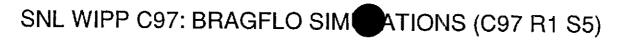


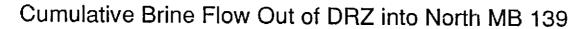


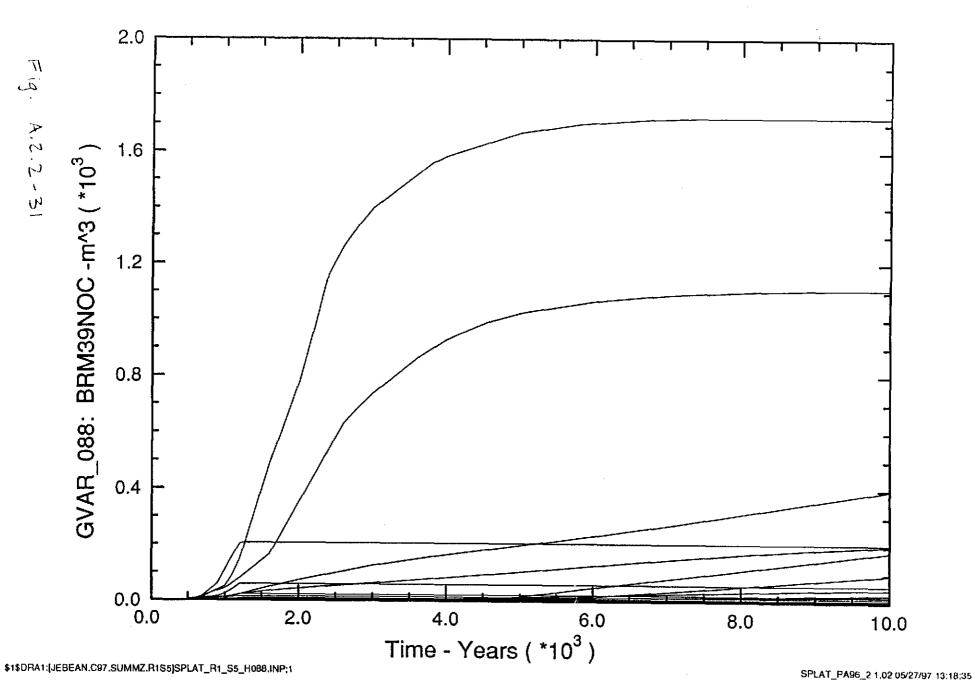
Cumulative Brine Flow Out of DRZ into North Anhydrite A/B



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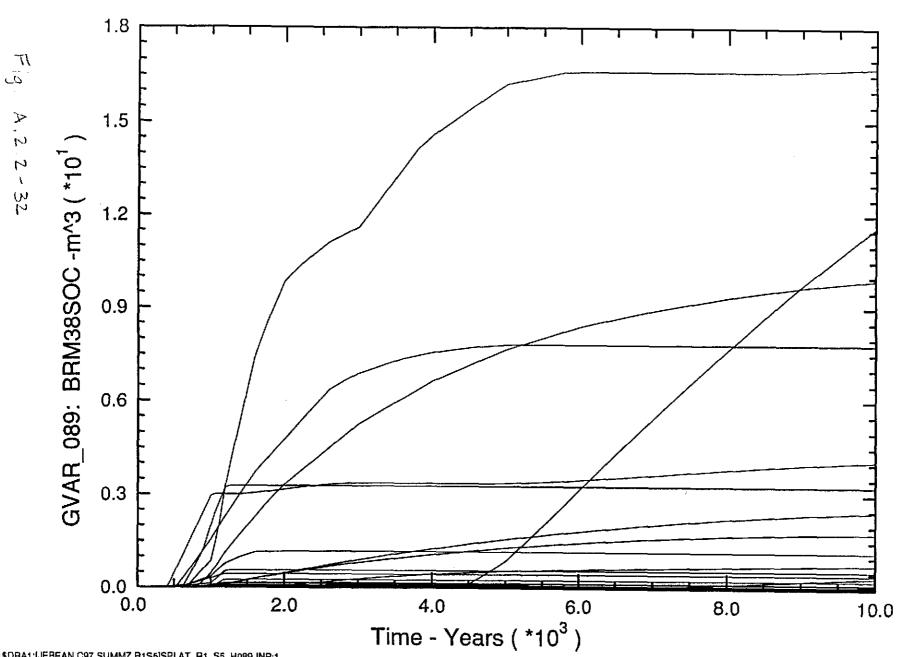






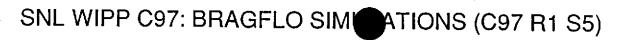
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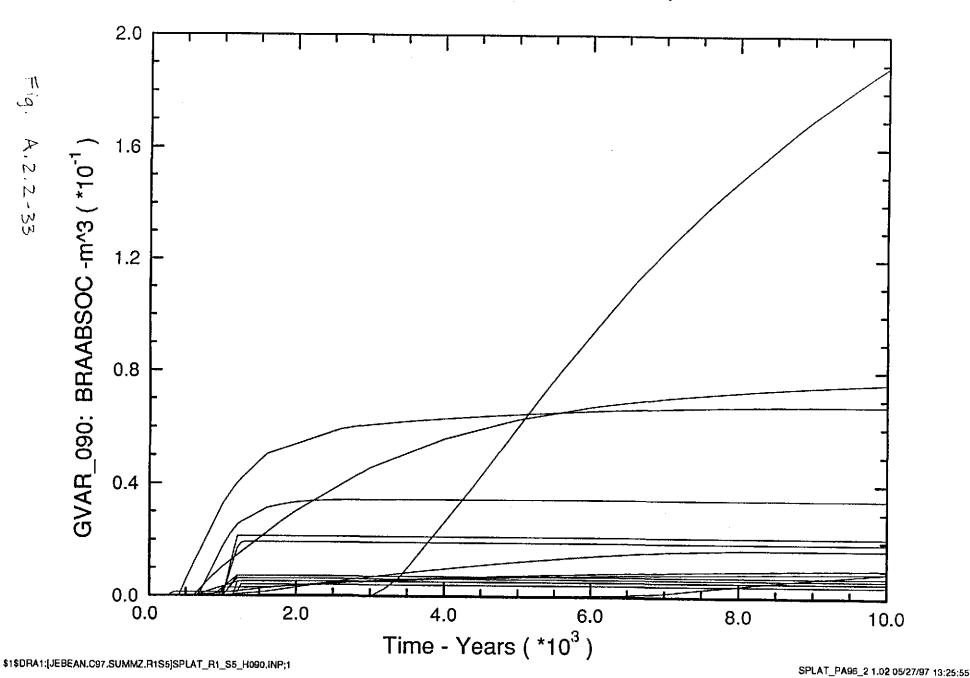


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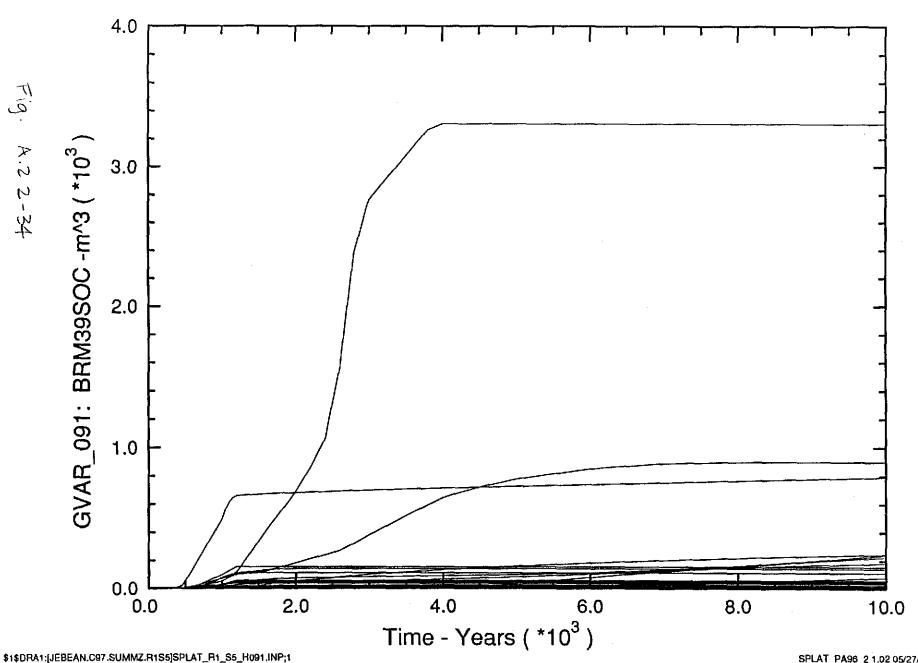


Cumulative Brine Flow Out of DRZ into South Anhydrite A/B

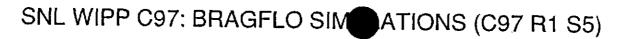




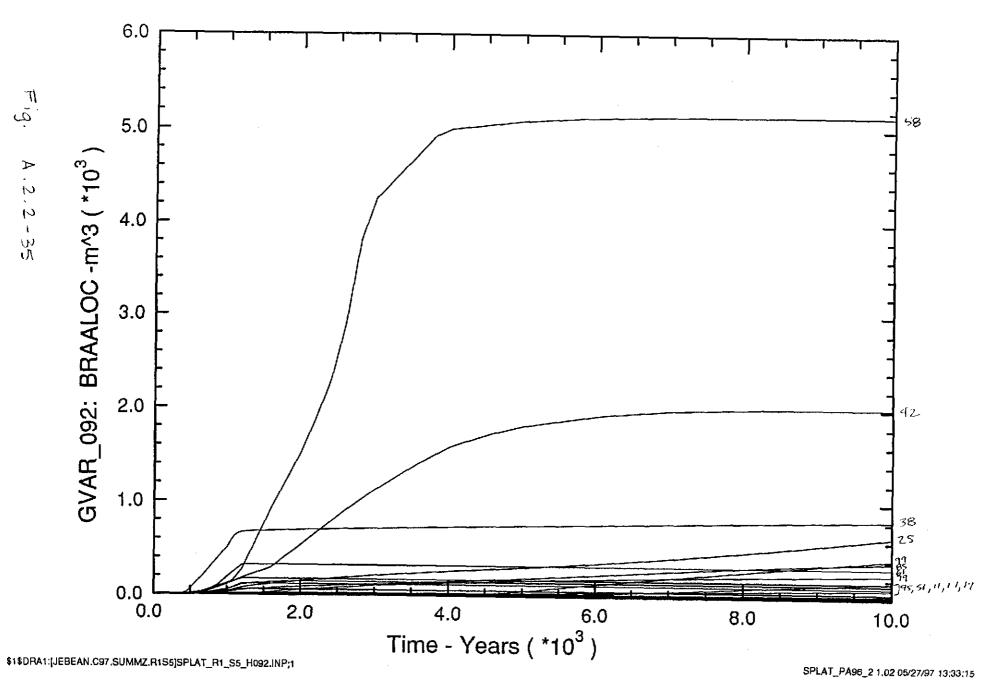
Cumulative Brine Flow Out of DRZ into South MB 139

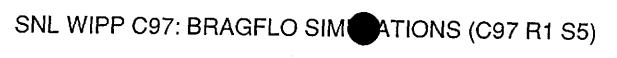


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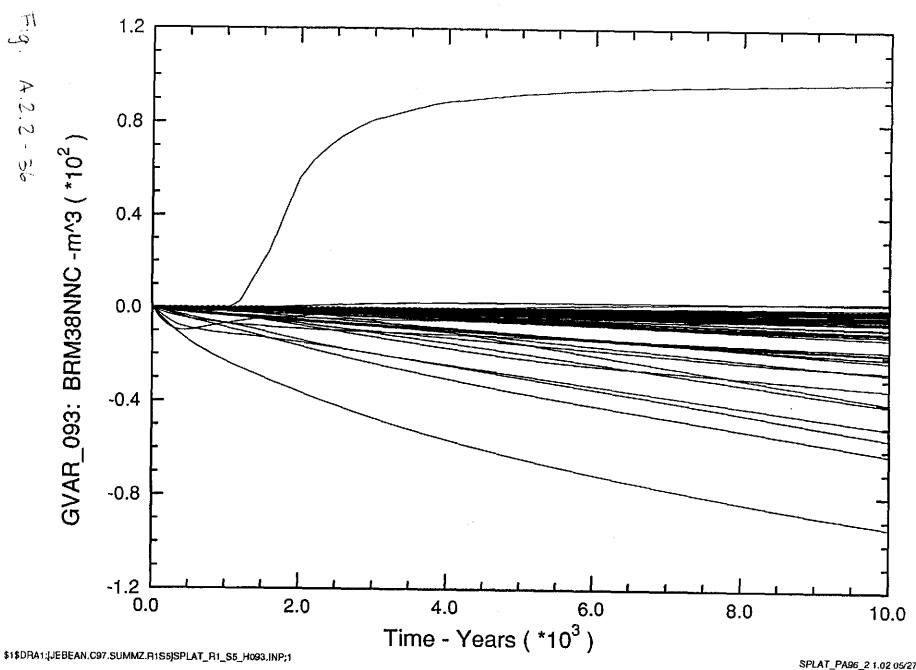


Cumulative Brine Flow Out of DRZ into All Marker Beds

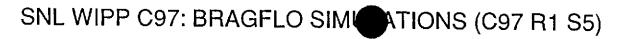




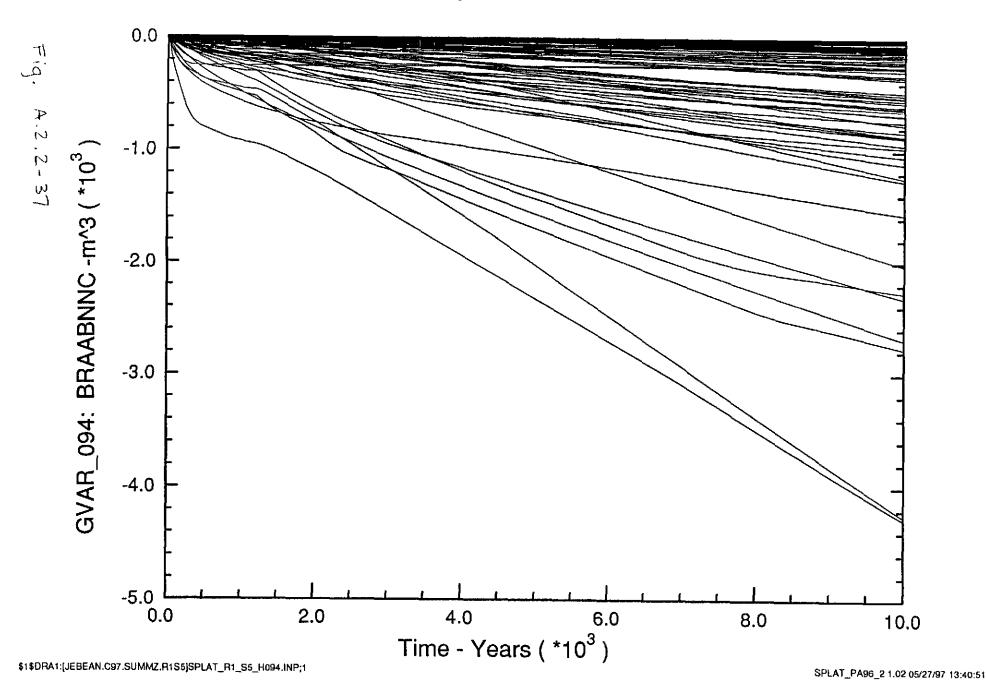
Net Brine Flow at North MB 138

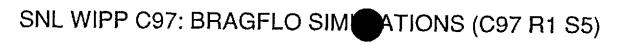


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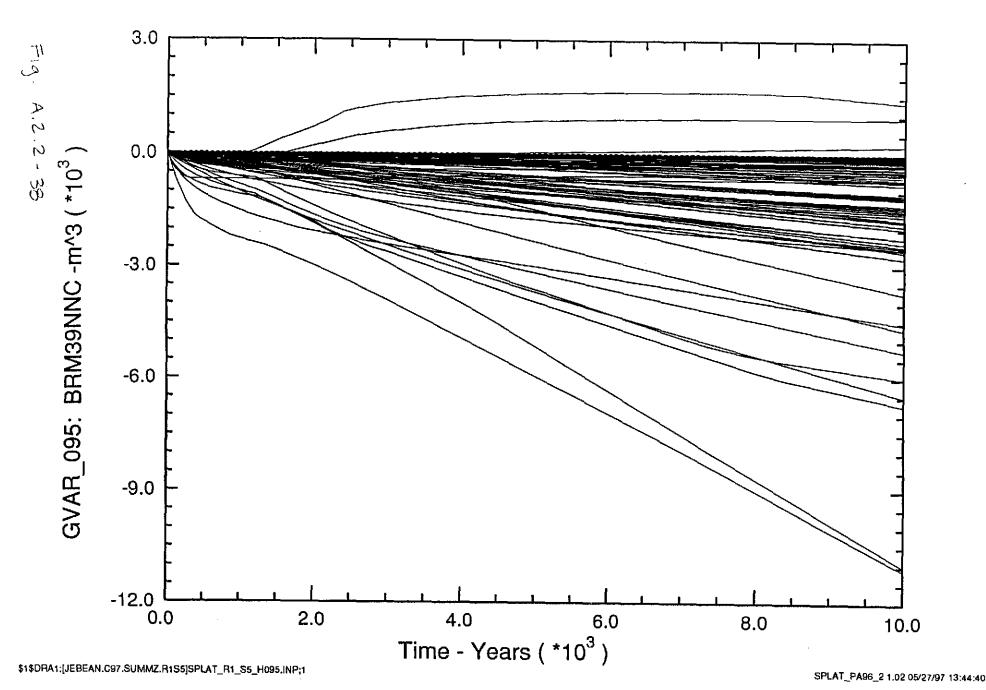


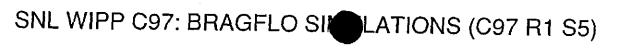
Net Brine Flow at North Anhydrite A/B

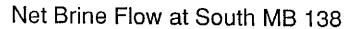


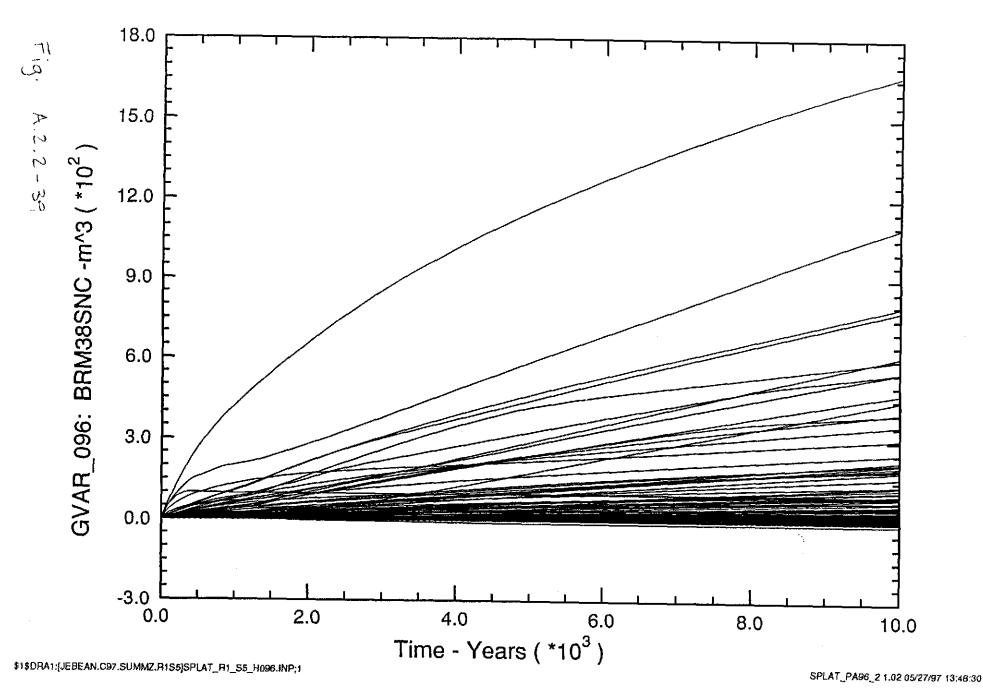


Net Brine Flow at North MB 139

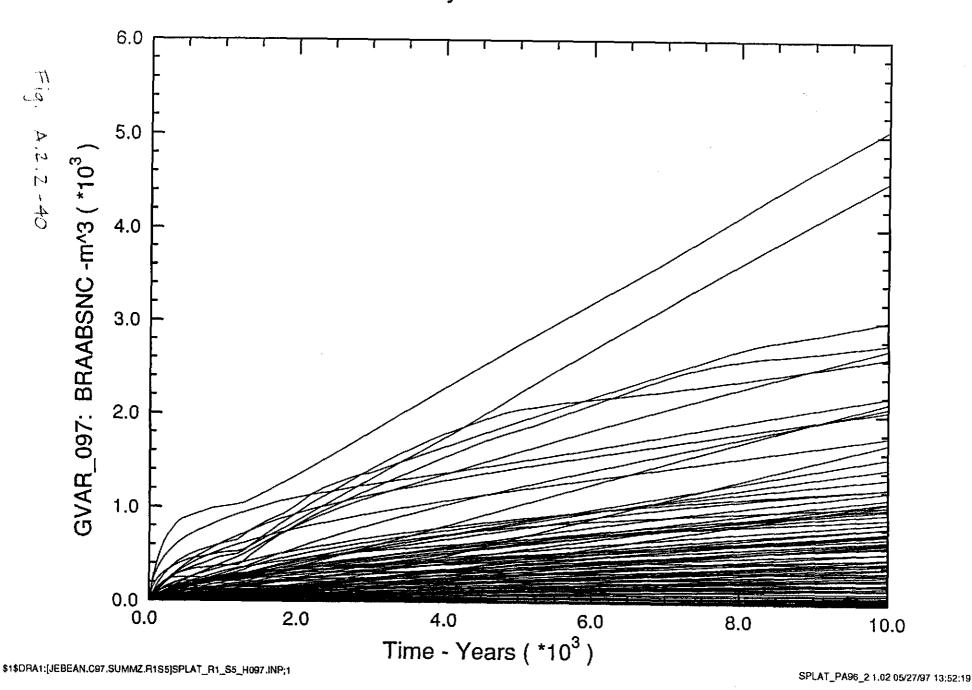


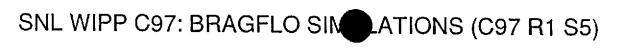




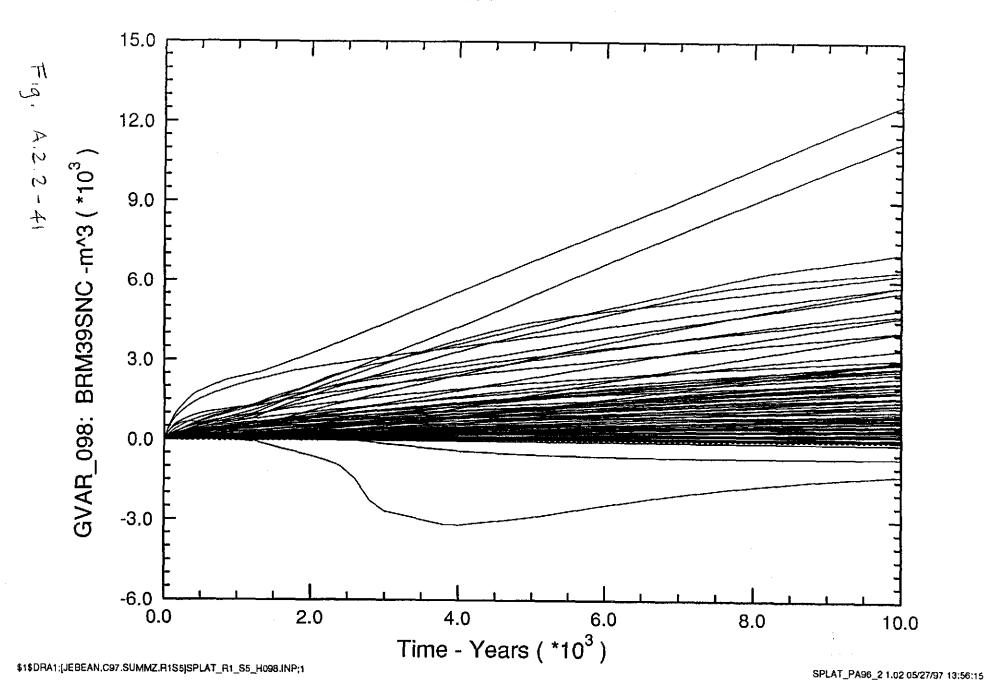


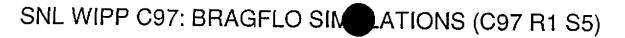




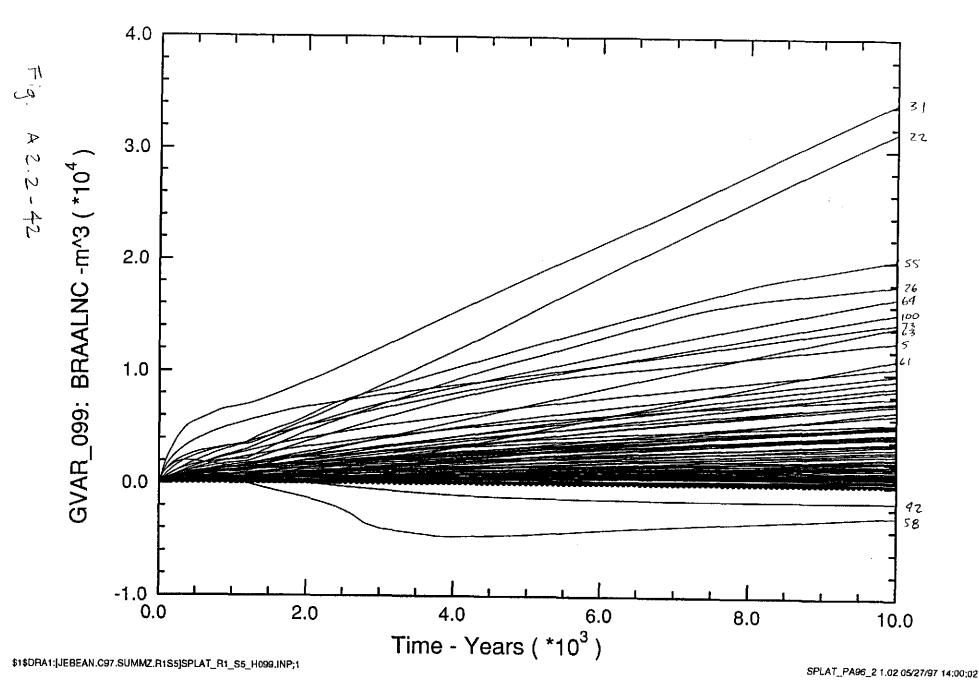


Net Brine Flow at South MB 139



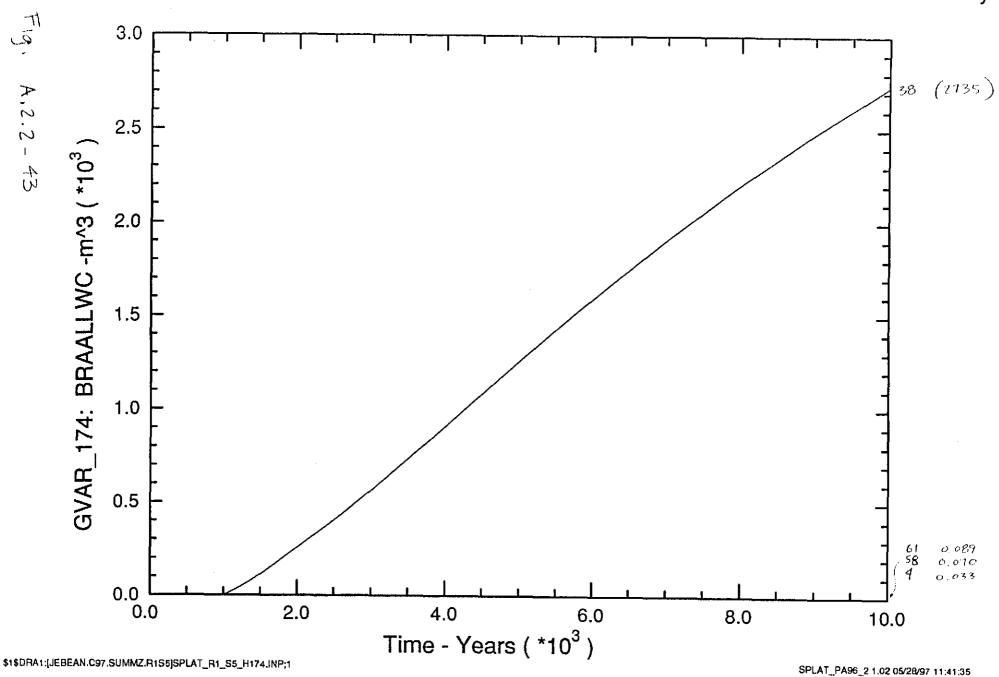


Net Brine Flow into DRZ from All Marker Beds



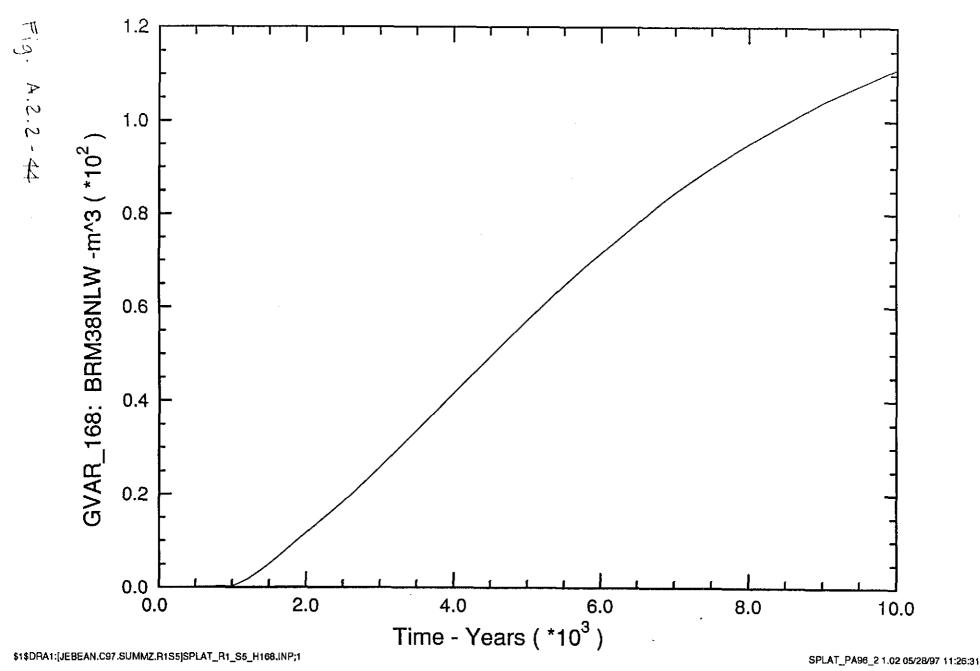


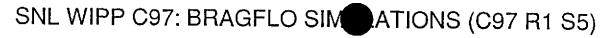
Cumulative Brine Flow Out of All Marker Beds Across Land-Withdrawal Boundary



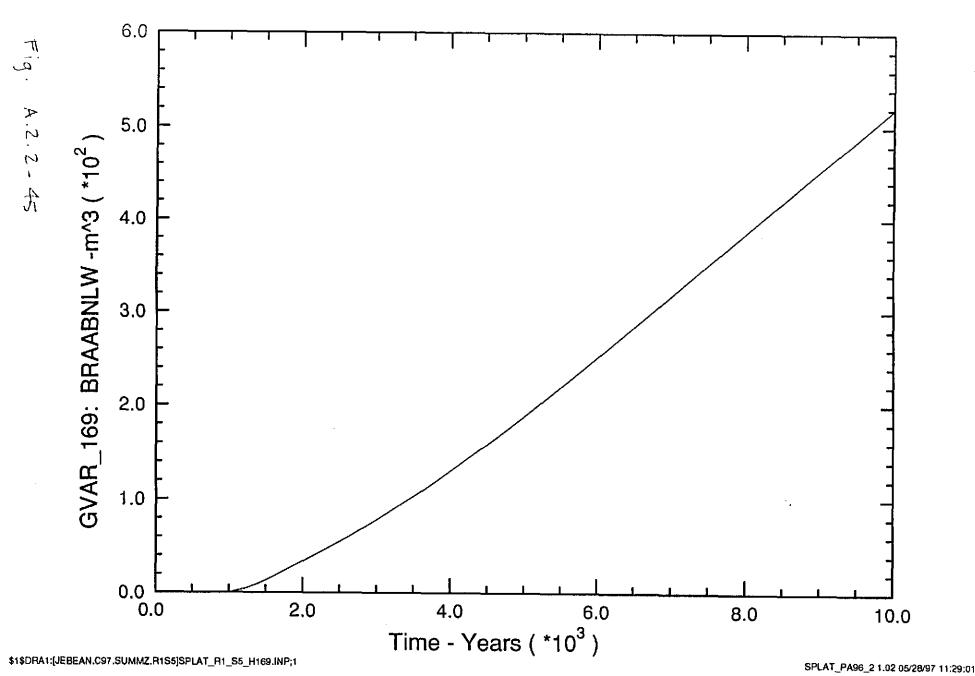
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Cumulative Brine Flow Out North MB 138 Across Land-Withdrawal Boundary



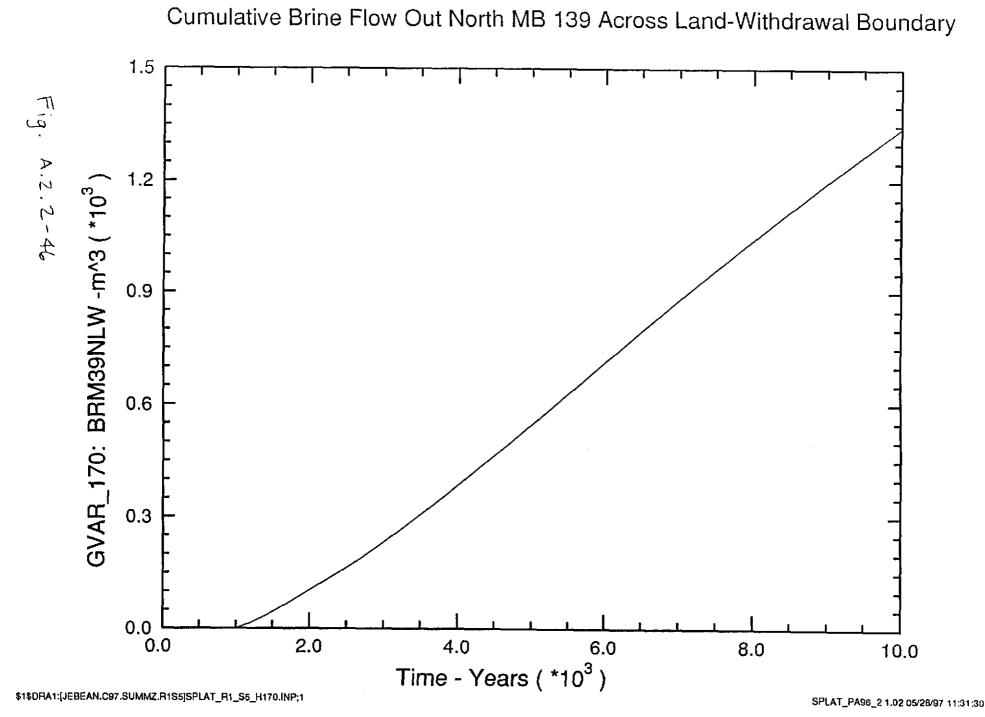


Cumulative Brine Flow Out North Anhydrite A/B Across Land-Withdrawal Boundary

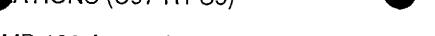




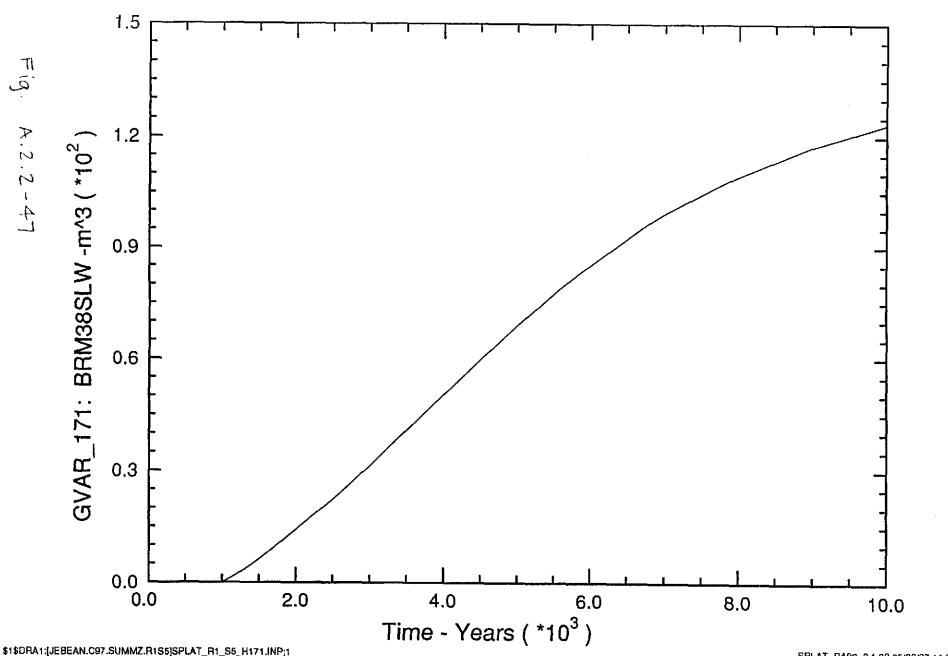






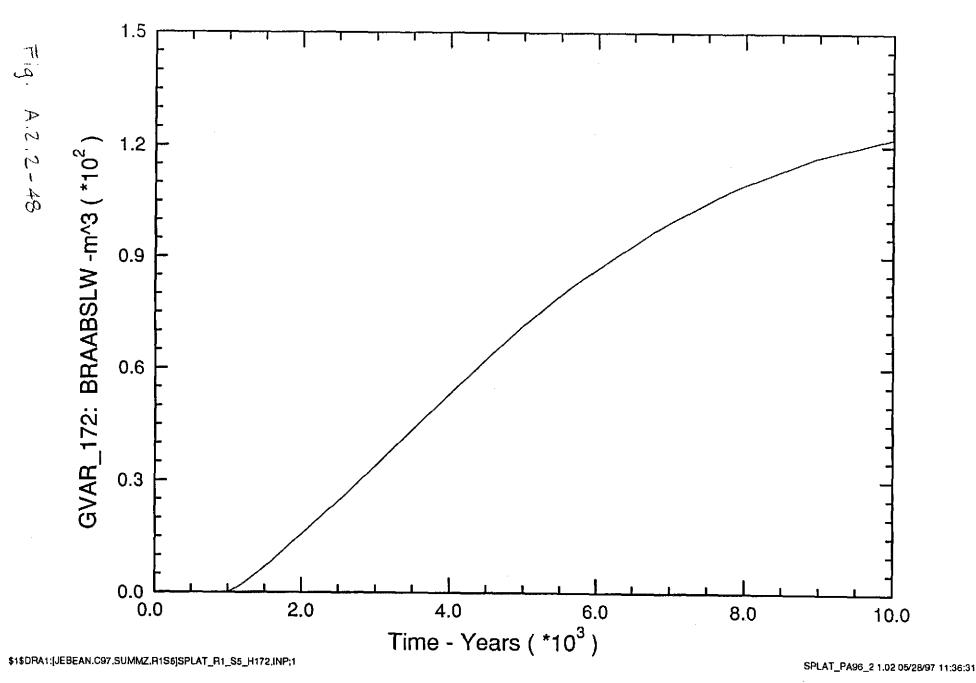


Cumulative Brine Flow Out South MB 138 Across Land-Withdrawal Boundary



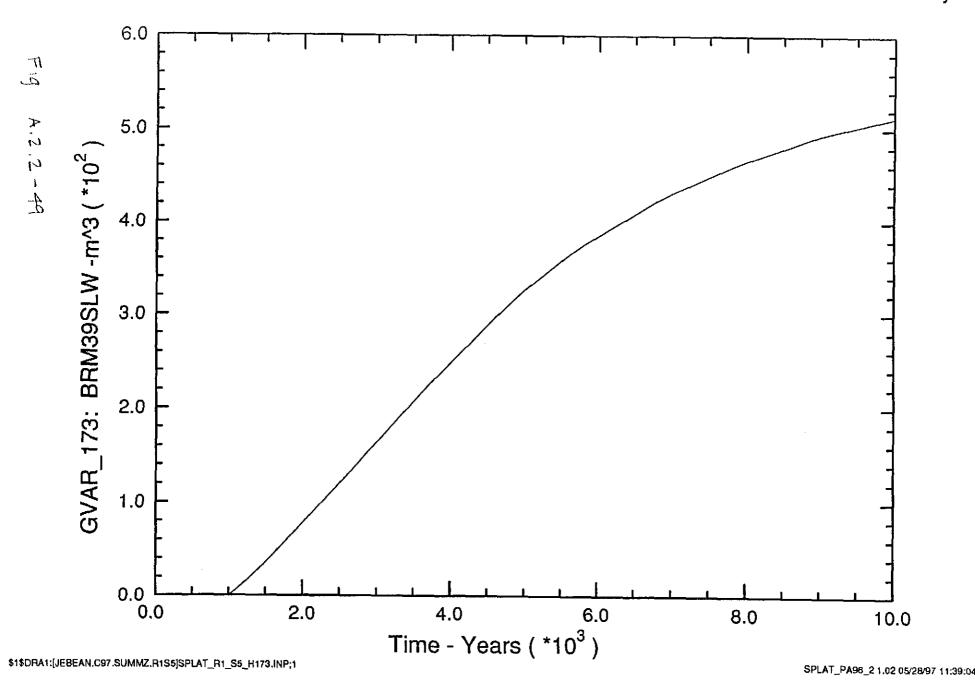


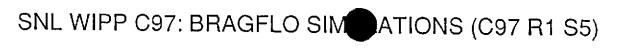
Cumulative Brine Flow Out South Anhydrite A/B Across Land-Withdrawal Boundary



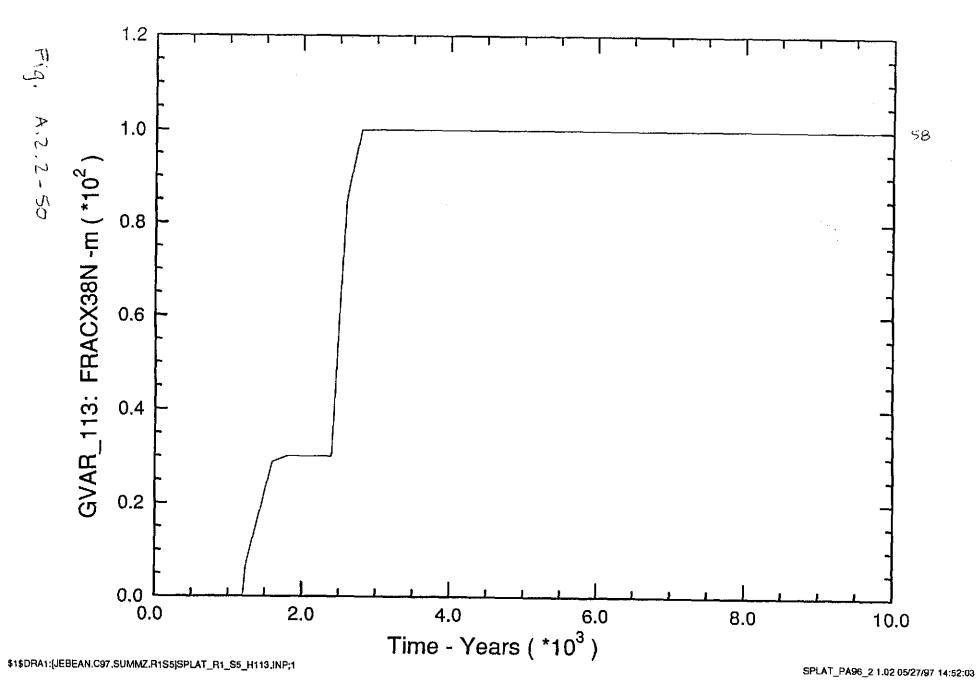


Cumulative Brine Flow Out South MB 139 Across Land-Withdrawal Boundary





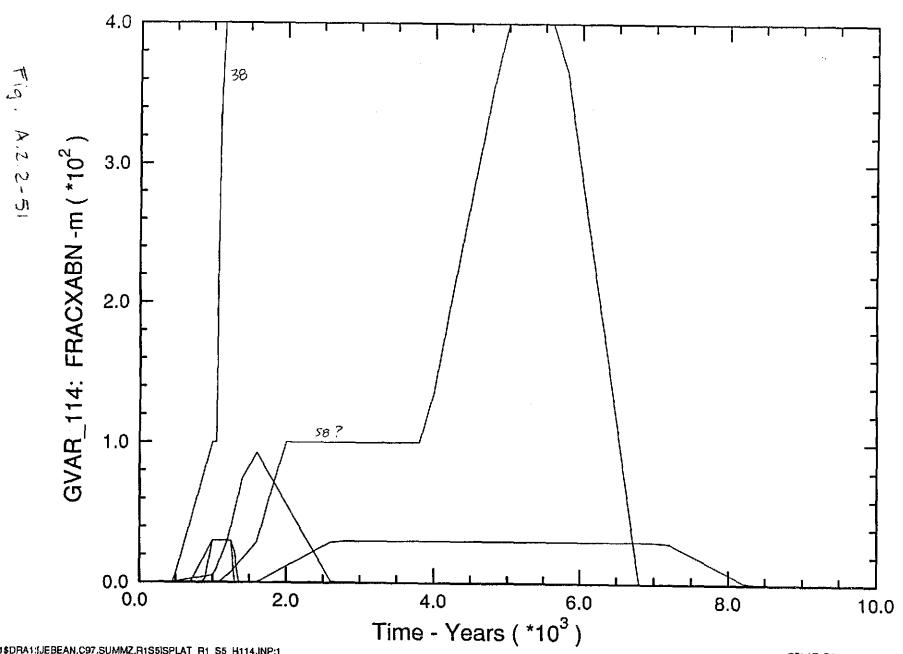
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Information Only

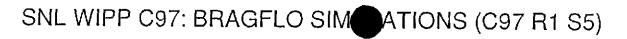


Length of Fractured Zone in North Anhydrite A/B

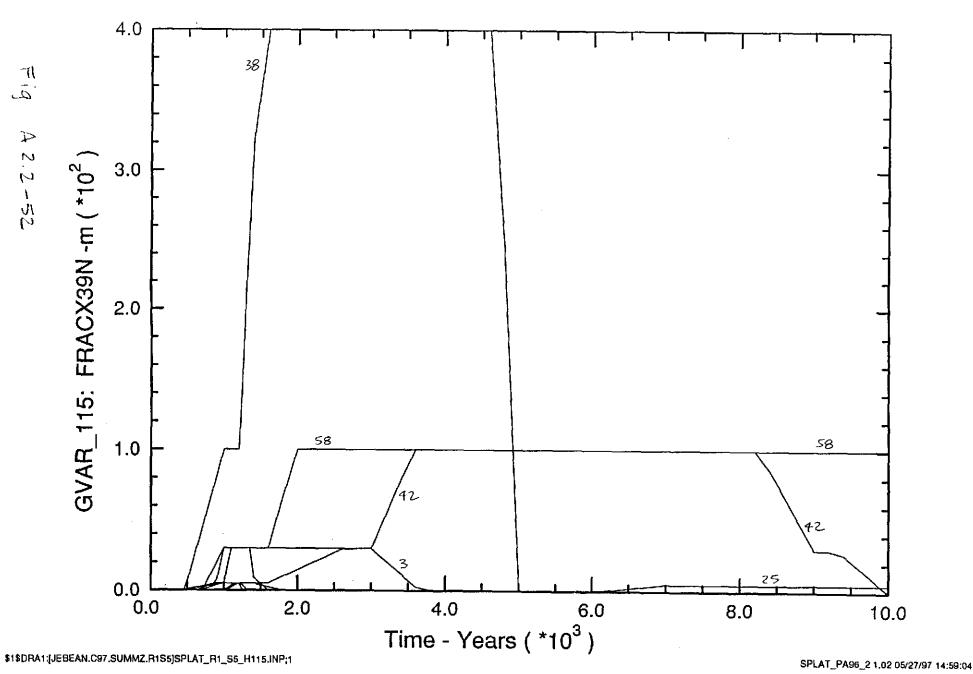


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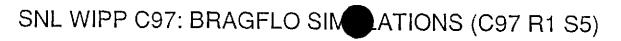
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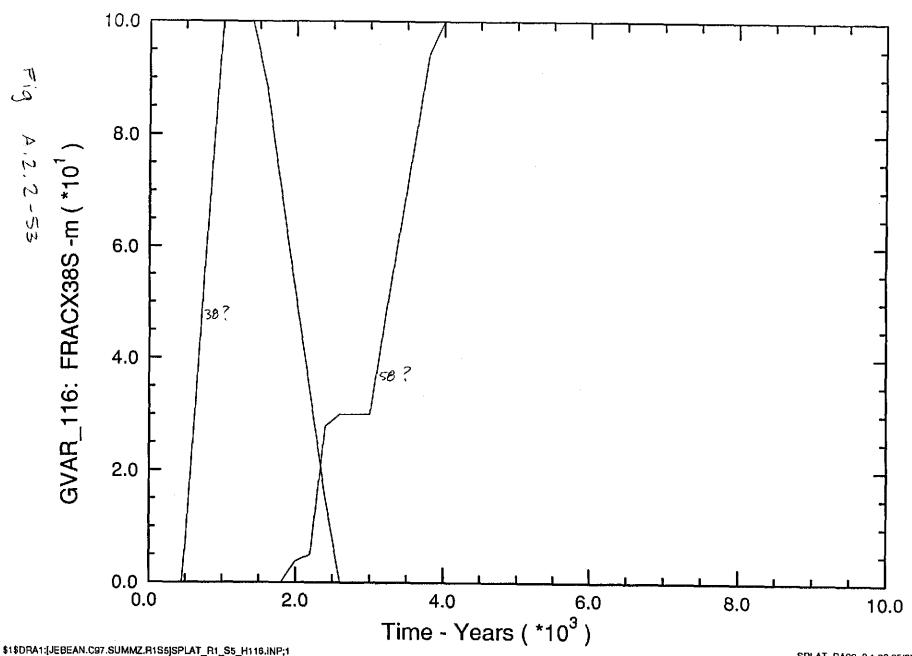
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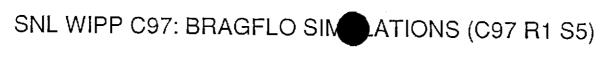


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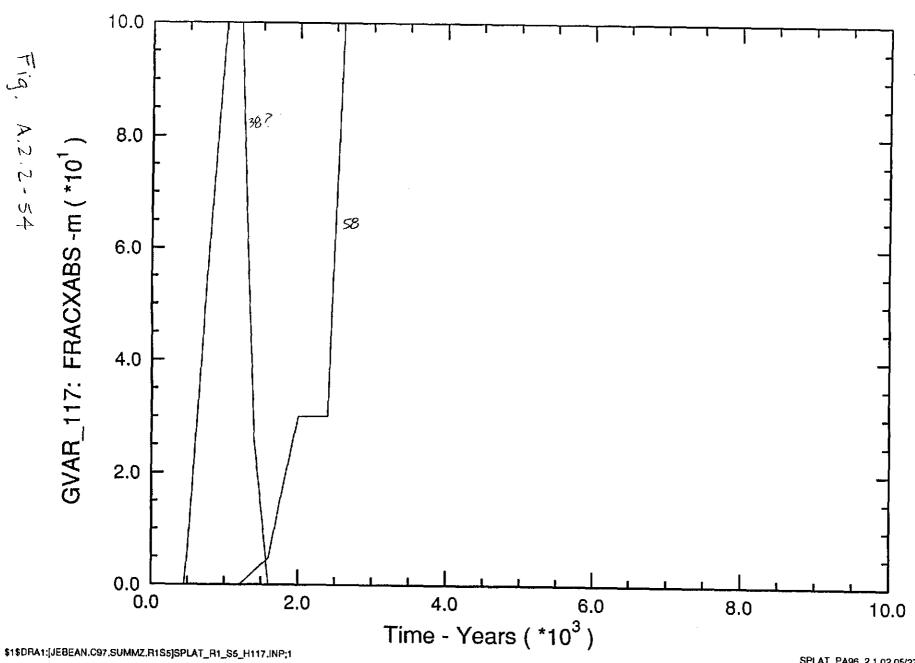


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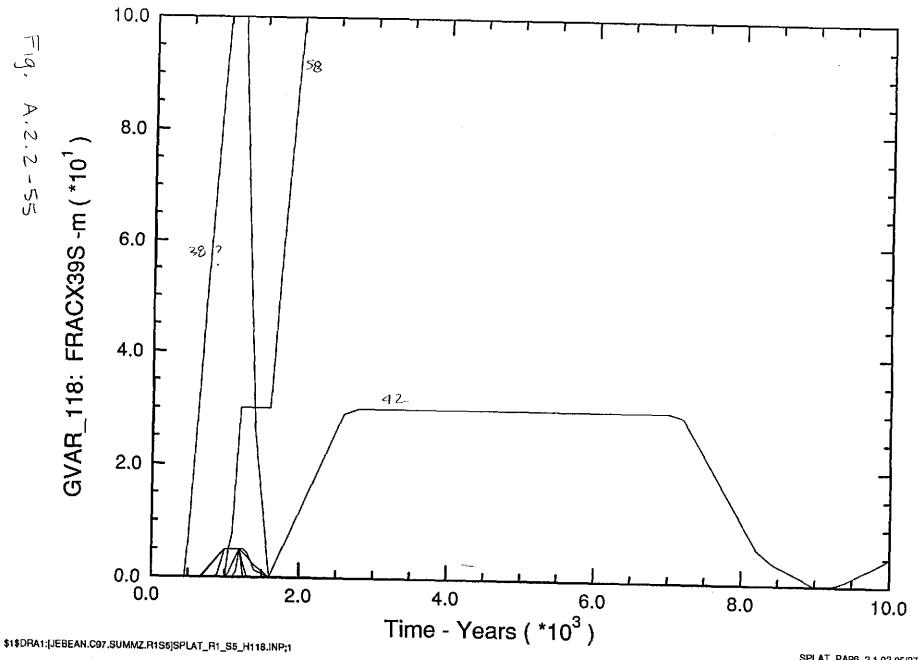
Length of Fractured Zone in South Anhydrite A/B



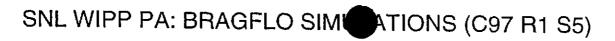
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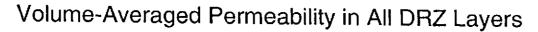


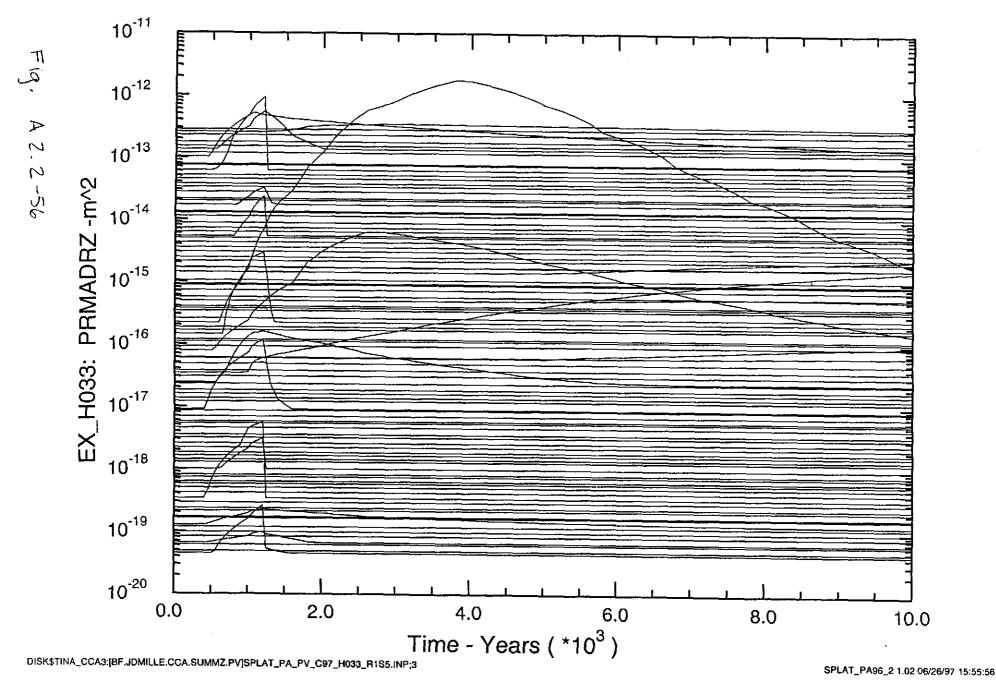
Length of Fractured Zone in South MB 139

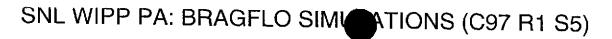


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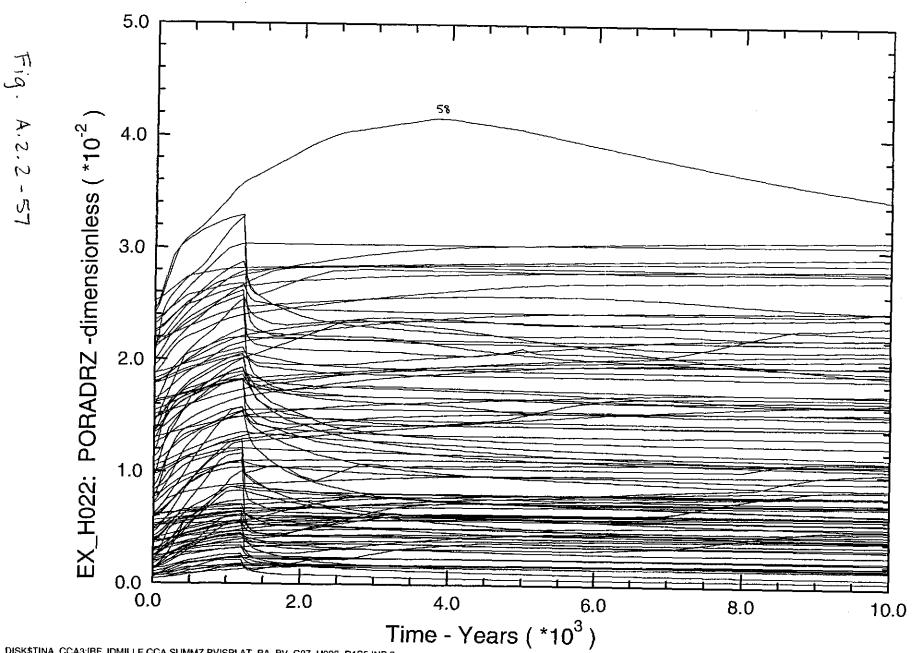








Volume-Averaged Porosity in All DRZ Layers



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A.2.3 E2E1 Intrusion (S6 Scenario)

In the S6 scenario, one borehole penetrates the waste-filled panel at 1000 years (an E2 intrusion) and a second borehole, drilled at the same location, penetrates the panel and underlying Castile brine reservoir at 2000 years (an E1 intrusion). The borehole from the panel to the surface is assumed to be sand-filled from 1000 years to 10,000 years. At 2000 years, an additional borehole segment is emplaced that extends from the bottom of the panel to the Castile brine reservoir. This lower segment is assumed to be an open borehole for 200 years and sand-filled borehole from 2200 years to 3200 years. At 3200 years, as in an E1 intrusion (S3 and S2 scenarios), the segment of the borehole that extends from the Castile brine reservoir up to the bottom of MB139 is assumed to creep shut, attaining a lower permeability. The different time periods and borehole conditions are summarized in Table A.2.3-1.

Time (years)	Borehole Portion	Behavior	Permeability (m²)
0 - 1000	All	Undisturbed conditions	Undisturbed conditions
1000 - 2000	Above panel	Silty sand	10 ^{-16.3} - 10 ⁻¹¹
	Below panel	Undisturbed conditions	Undisturbed conditions
2000 - 2200	Above panel	Silty sand	10 ^{-16.3} - 10 ⁻¹¹
	Below panel	Open borehole	10 ⁻⁹
2200 - 3200	Above panel	Silty sand	10 ^{-16.3} - 10 ⁻¹¹
	Below panel	Silty sand	10 ^{-16.3} - 10 ⁻¹¹
3200 - 10,000	Above panel Below panel	Silty sand Tight silty sand	$10^{-16.3} - 10^{-11}$ $10^{-17.3} - 10^{-12}$

Table A.2.3-1. Changes in Borehole Properties in E2E1 Intrusion Scenario (S6)

A.2.3.1 Replicate 1 Results and Discussion

A.2.3.1.1 Repository Behavior

The time dependence of pressures in the waste panel is shown in Figure A.2.3-1 [GVAR_023]. As in the previous scenarios, pressure responses in the experimental and operation regions are nearly identical to those in the waste panel and rest of repository because the permeability of excavated regions, drift and panel seals, and the DRZ are high, on the order of 10^{-15} m². Up to the time of the first intrusion, 1000 years, the behavior is identical to that in the other scenarios. In most cases, the pressure rises steadily, at widely varying rates, until the intrusion occurs. During the time between the first and second intrusion, the behavior differs insignificantly from the S5 scenario (E2 intrusion at 1000 years). The slight differences arise from the presence of two low permeability plugs in the borehole in the S5 scenario. In the majority of realizations, the pressure undergoes rapid transients immediately following the first intrusion. In some cases, there is a

relatively rapid depressurization when the intrusion borehole connects the pressurized panel with the lower-pressure Dewey Lakes Formation. In other cases, pressures level off or increase after the first intrusion. Another type of response is for the pressure to rise from a very low pressure relatively rapidly following the first intrusion. In these realizations, brine flows into the waste from the overlying formations and through the anhydrite layers, and as the borehole is filled with brine, the pressure in the waste tends toward hydrostatic pressure until the time of the second intrusion, 2000 years.

The repository behavior described thus far is not significantly different than the behavior predicted in the CCA, with the exception of repository pressures at the time of both intrusions tending to be slightly higher in the PAVT calculations because of increased corrosion rates. However, as was observed in the S3 scenario (E1 intrusion at 1000 years), after the borehole penetrates the brine reservoir some distinguishable differences do occur. These differences include the following. Pressures in the panel increase immediately after intrusion in all vectors having low panel pressures (less than 7 MPa) at the time of intrusion. This behavior did not occur in the CCA. The range of panel pressures is also narrower and higher during the short 200 year period after the second intrusion than it was in the CCA. Moreover, unlike the CCA, panel pressures in many vectors do increase significantly immediately after intrusion and continue to do so for the remainder of the 10,000 year regulatory period. In several cases (e.g., vectors #38 and #3), the second intrusion has no significant impact on pressure and pressure continues to either gradually decrease or increase for several thousand years. In these realizations, the borehole permeability is low and sufficient quantities of brine flow into the panel from the DRZ and through the anhydrite layers to maintain relatively high gas generation rates and increasing pressure conditions. Pressure behavior after intrusion is described in more detail below.

At the time of the second intrusion, many realizations again undergo rapid transients. In some cases, the pressure in the waste increases suddenly when the borehole connects the panel with the pressurized Castile brine reservoir. In these realizations, the brine reservoir pressure (a sampled parameter from a range of 11.1 MPa to 17.0 MPa) is appreciably higher than the pressure in the panel. A less frequent type of response is for the pressure to rise following a period of low or slowly decreasing pressure. The time lag between intrusion and repressurization lasts from 500 to over 4000 years. During this time, gas that has filled the panel is driven up the intrusion borehole as brine flows into the waste through the anhydrite layers and down the borehole. Once the borehole is filled with brine, the pressure in the waste approaches hydrostatic pressure relative to the water table in the Dewey Lakes. Note that final pressures above hydrostatic pressure occur in those realizations having relatively high corrosion rates and a low borehole permeability (sampled parameter ranging from $1.0 \times 10^{-16.3}$ to 1.0×10^{-11} m²) that prevents gas from easily escaping the panel and repository. Pressures below hydrostatic occur in those realizations where the sampled pressure in the brine reservoir is low and the borehole is filled predominately with gas.

The E2E1 intrusion scenario generally results in more brine being present in the repository (Figure A.2.3-2 [GVAR_046]) than in an E1 intrusion, even though the E1 intrusion has the same

borehole properties after 3200 years. This behavior was observed in the CCA as well and for the following two reasons. First, in those realizations in which most of the brine inflow to the repository is from flow down the borehole, the E2E1 (S6) scenario has an additional 200 years during which brine is readily available. Recall that the E1 (S3 and S2) scenarios have low permeability plugs emplaced in the borehole for two hundred years following intrusion. Second, in realizations where the Castile is the principal source of brine, the 1000-year period between intrusions with an open borehole allows the pressure in the repository to drop, so that when the borehole to the Castile opens, the amount of flow from the Castile is greater.

A.2.3.1.1.1 Gas Generation

Profiles of total gas generated with time (Figure A.2.3-3 [GVAR_022]) are similar to those in the E1 (S3) and E2 (S5) scenarios. The 25 realizations in which plastics and rubbers are included in the cellulose inventory again display the most rapid gas generation during the first 1000 years. Once all of the cellulose is consumed (in less than 1750 years, and much sooner, in most cases, as in the S5 scenario), the rate of gas generation tends to drop off in a large fraction of the realizations. In realizations in which the cellulose inventory is zero, gas generation tends to proceed at a very uniform rate (the curves are smooth and more-or-less straight), unless the corrosion rate is high enough to deplete the brine in parts of the waste. In these cases, there are breaks in the curves indicating that gas generation has stopped or decreased in some grid cells. This same behavior occurs when the steel inventory has been consumed in some parts of the waste region. Overall, more gas is generated in this scenario than in the other intrusion scenarios. The maximum amount generated is slightly higher, almost 4.3×10^7 m³ $(3.9 \times 10^7$ m³)(at reference conditions), compared with 3.5×10^7 m³ in S5 and 3.1×10^7 m³ in S3 $(3.6 \times 10^7$ m³ in S5 and 2.7× 10⁷ m³ in S3) in the other intrusion scenarios. Slightly more steel is consumed in S6 than in any other scenario, to a maximum of 100% (96%) versus 97% (83 %) in S3. In the panel, the entire steel inventory (less than 1% remaining) is consumed in 42 (48) of the realizations, compared with 41 (43) realizations in the E1(S3) Scenario. As noted in the preceding section, brine saturations in the repository are generally higher in this scenario than in the other intrusion scenarios. When corrosion is controlled by the rate, the amount of gas generated by corrosion is less, and the results are nearly indistinguishable from other scenarios.

A.2.3.1.1.2 Halite Creep

The reduction in porosity resulting from halite creep is similar to other intrusion scenarios, except for some transients between 1000 and 3000 years. After the initial rapid change in porosity during the first 300 - 500 years, the porosity tracks the pressure response in the waste very closely. After 3000 years, the porosities again range from 7 % to 21% (7 % to 18%), and, after 10,000 years, from 7 to 23 % (5% to 17%).

A.2.3.1.1.3 Fluid Flow

Immediately following the first borehole intrusion, there is substantial upward flow of gas

(Figure A.2.3-4 [GVAR_101]) and no upward flow of brine (Figure A.2.3-5 [GVAR_073]) from the panel. However, brine flows rapidly down the borehole from overlying formations in several realizations (Figure A.2.3-6 [GVAR 140]). The maximum flow down the borehole from overlying formations is similar to that in other scenarios, 16,500 m³ (49,000 m³), compared with 18,500 m³ (47,000 m³) in E1(S3) and 46,480 m³ (48,000) in E2 (S5), although the behavior of individual realizations differs greatly among the three scenarios. Although brine could flow up the borehole starting at 1000 years, none does flow upward until after the Castile intrusion at 2000 years (Figure A.2.3-7 [GVAR_078]). In only a few realizations, inflow from the marker beds is sufficient to drive small amounts of brine up the borehole without any contribution from the Castile. However, in most cases, without the Castile flow, not enough brine will flow into the repository over 10,000 years to cause brine flow up the borehole. This behavior was also observed in 1996. Profiles of brine flow into the panel from the Castile are shown in Figure A.2.3-8 [GVAR 072]. Note that brine flows rapidly up from the Castile reservoir into the panel in several realizations. In these realizations, the brine reservoir pressure (a sampled parameter from a range of 11.1 MPa to 17.0 MPa) is appreciably higher than the pressure in the panel. The amount of brine flowing immediately into the panel ranges from 0.0 m³ to a maximum of nearly 90,000 m³ (fourth highest vector, #45). The maximum amount is approximately 1.5 times greater than the maximum amount (60,000 m³) calculated in the CCA. As was noted in the S3 scenario, the realizations that show immediate flow into the panel tend to have a low borehole permeability, high Castile pressure, and low panel pressure at the time of intrusion. In S6, the top two immediate flow realizations, #51 and #17, have Castile pressures at the time of intrusion that rank 100 and 87, borehole permeabilities that rank 79 and 80, and panel pressures that rank 19 and 18. In this scenario, the borehole permeabilites of the top two realizations are not low indicating that there may be another factor involved that reduces upwards flow into the panel after intrusion. Low Castile compressibility may be a contributor to reducing upward flow after intrusion; Castile compressibility in realizations # 51 and #17 rank 6 and 59, respectively.

As in the S3 scenario, one group of realizations shows continual flow from the Castile into the panel after the second intrusion. Again, this behavior did not occur in the CCA. The maximum amount that flows upward in these vectors is 120,000 m³ (66,000 m³). This maximum amount is slightly larger than the 112,000 m³ calculated in S3 and approximately two times the maximum amount (66,000 m³) calculated in the CCA. In most of these realizations, brine flow is small prior to plug degradation, and the panel is already pressurized as a result of gas generation. These realizations typically have high corrosion rates and include plastics and rubbers in the cellulose inventory. When the borehole intrudes at 2000 years, the pressure in the Castile is not quite high enough to immediately drive large quantities of brine up into the pressurized panel. At 3200 years, when creep closure reduces the permeability of the section of the borehole between the Castile and the panel by an order of magnitude, the brine flow rate drops off significantly.

The plot of brine flow up the borehole at the top of the panel (Figure A.2.3-5 [GVAR_073]) is again dominated by four realizations, #28, #54, #57, and #72. As noted in the S3 scenario, these top four realizations have high borehole permeabilities (ranks of 100, 94, 99, 93, respectively)

and high initial Castile reservoir pressures (ranks of 83, 96, 80, 79, respectively). These four vectors also correspond to the top four continual flows into the bottom of the panel (Figure A.2.3-8 [GVAR_072]) indicating that these flows are primarily comprised of Castile brine. The maximum flow up the borehole is 108,000 m³ (22,500 m³). Note that flows up the borehole at both the bottom and top of the panel are larger in the S6 scenario than in the S3 scenario. The reason for this increase in flow is the fact that the panel has a longer period to depressurize before the Castile flow started; with the greater initial pressure drop between the Castile and the panel, more brine flows up from the Castile and continues upwards toward the Culebra. As in the S3 scenario, the brine flow up the borehole at the top of the DRZ is nearly equal (only slightly higher) to the borehole flow at the top of the panel. The maximum flow at this location in this scenario (Figure A.2.3-7 [GVAR_078]) is slightly higher than in the E1 scenario, 109,000 m³ vs. 103,000 m³ (37,000 m³ vs. 35,000 m³). Also, no brine (at most 0.2 m³ in CCA) ultimately reaches the top of the Rustler.

A.2.3.1.2 Behavior in Formations Surrounding the Repository

A.2.3.1.2.1 Two-Phase Flow

Gas flow into the interbeds are presented in Figures A.2.3-16 [GVAR_106] to A.2.3-22 [GVAR_112]. In general, gas flows into the interbeds tend to be larger in the PAVT as compared to the CCA. As in the E1 scenario, fewer realizations (as compared to the Undisturbed Scenario) result in gas flow from the DRZ into the marker beds. This behavior is is similar to that predicted in the CCA. In MB138, the largest of the realizations shows 55,000 m³ (5,800 m³) flowing to the north (Figure A.2.3-16 [GVAR_106]) and 58,000 m³ (11,500 m³) flowing to the south (Figure A.2.3-19 [GVAR_109]). In Anhydrite a and b (Figures A.2.3-17 [GVAR_107] and A.2.3-20 [GVAR_110]), the maximum flows are 570,000 m³ (85,000 m³) to the north and 84,000 m³ (43,000 m³) to the south. In MB139, a maximum of 580,000 m³ (13,200 m³) flows to the north (Figure A.2.3-18 [GVAR_108]); to the south, the maximim gas flow is 105,000 m³ (3,300 m³) (Figure A.2.3-21 [GVAR_111]). In all marker beds, a total maximum of 1.45 × 106 m³ (1.58 × 105 m³) flows from the DRZ into the marker beds (Figure A.2.3 -22 [GVAR_112]).

After the second intrusion at 1000 years, large volumes of gas (up to $15.5 \times 10^6 \,\mathrm{m}^3$) (up to $8.0 \times 10^6 \,\mathrm{m}^3$ in the CCA) are quickly vented up the borehole (Figure A.2.3-23 [GVAR_101]). Gas continues to flow up the borehole in several vectors for the remainder of the 10,000 years, with a maximum of $23.0 \times 10^6 \,\mathrm{m}^3$. This behavior is different than was predicted in the CCA where gas flow from the panel generally occurred only over a short period of time, about 1000 years. However, in both the PAVT and the CCA, larger amounts continue to flow from the DRZ for as long as gas is generated (Figure A.2.3-24 [GVAR_102]). The total amount of gas vented up the borehole ranges from about $0.0 \,\mathrm{m}^3$ up to $38 \times 10^6 \,\mathrm{m}^3$ ($1.0 \times 10^6 \,\mathrm{m}^3$ up to $36 \times 10^6 \,\mathrm{m}^3$). The maximum total amount of gas generated is $43 \times 10^6 \,\mathrm{m}^3$ ($39 \times 10^6 \,\mathrm{m}^3$) (Figure A.2.3-3 [GVAR_022]). Thus, a large fraction of the gas generated eventually flows up the borehole. Very little gas flows up the shaft. Figure A.2.3-25 [GVAR_100] shows that a maximum of $23 \,\mathrm{m}^3$ ($22 \,\mathrm{m}^3$) flows up the shaft at the interface between the Salado and Rustler formations. A

detailed examination of gas flows at different locations in the shaft shows that this gas came exclusively from the asphalt shaft seal immediately below this interface. None of this gas originates from lower elevations in the shaft, including the repository. Thus, the shaft seals are very effective in keeping gas from flowing up the shaft.

Brine flow out of the marker beds and into the DRZ (Figures A.2.3-26 [GVAR_079] to A.2.3-46 [GVAR_099]) ranges up to 31,000 m³ (63,500 m³) (A.2.3-32 [GVAR_085]). Brine flow out of the DRZ into MB138 and Anhydrite a and b is essentially zero, nearly identical to E1 scenario, in which a maximum of 40 m³ (4 m³) flows out Marker Bed 138 to the north. Flows out of the DRZ surrounding the repository and into MB139 are also nearly identical to the E1 scenario. The interbed flows are summarized in Table A.2.3-2.

The maximum amount of brine that flows in from the marker beds is about 75% (equal) smaller than the maximum that flows up the borehole from the Castile, 31,000 m³ vs. 120,000 m³ (63,500 m³ vs. 66,000 m³) up from the Castile. Relatively small amounts of brine flow out of the DRZ and into the marker beds, primarily into Marker Bed 139, into which a maximum of about 2800 m³ (200 m³) flows, or less than 10% (1%) of the amount that flows into the DRZ from the marker beds.

Table A.2.3-2. Cur	mulative Net Interbed Brine Flows for E2E1 Intra	usion Scenario (S6).
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Marker Bed	Max. Net Brine Flow from MB into DRZ, m ³	Max. Net Brine Flow from DRZ into MB, m ³
MB138 North	55 (300)	70 (0)
MB138 South	1000 (3650)	0 (0)
Anhydrite a & b North	3800 (8700)	0 (0)
Anhydrite a & b South	4650 (9800)	0 (0)
MB139 North	10,000 (20,000)	1200 (100)
MB139 South	11,500 (21,100)	1600 (100)
All Marker Beds	31,000 (63,500)	2870 (200)

As shown in Table A.2.3-3 larger quantities of brine flow out across the land withdrawal boundary in the PAVT, whereas in the CCA only very small amounts of brine crossed the land withdrawal boundary. These increased releases occur, as in S3, in vector #38. The maximum in all marker beds is 3203 m³ (1.66 m³). As noted previously in the S3 scenario, the sampled parameter values for vector #38 indicate that this vector had the highest sampled MB139 permeability in combination with the 7th highest sampled DRZ permeability and the 17th lowest borehole permeability. However, this brine does not come from the repository since at most 1380 m³ (180 m³) flows to the north into MB139 from the DRZ (Figure A.2.3-35 [GVAR_088]), which is far less than the pore volume of MB139 which is 155,500 m³ between the repository and

land withdrawal boundary. This conclusion is verified by the Salado transport calculations described in Section 3.0.

Table A.2.3-3. Cumulative Interbed Brine Flows Across Land Withdrawal Boundary for E2E1 Intrusion Scenario (S6).

Marker Bed	Maximum Brine Outflow across Land Withdrawal Boundary, m ³
MB138 North	142 (0.22)
MB138 South	149 (0.0)
Anhydrite a & b North	604 (0.34)
Anhydrite a & b South	149 (0.0)
MB139 North	1492 (1.1)
MB139 South	669 (0.0)
All Marker Beds	3203 (1.66)

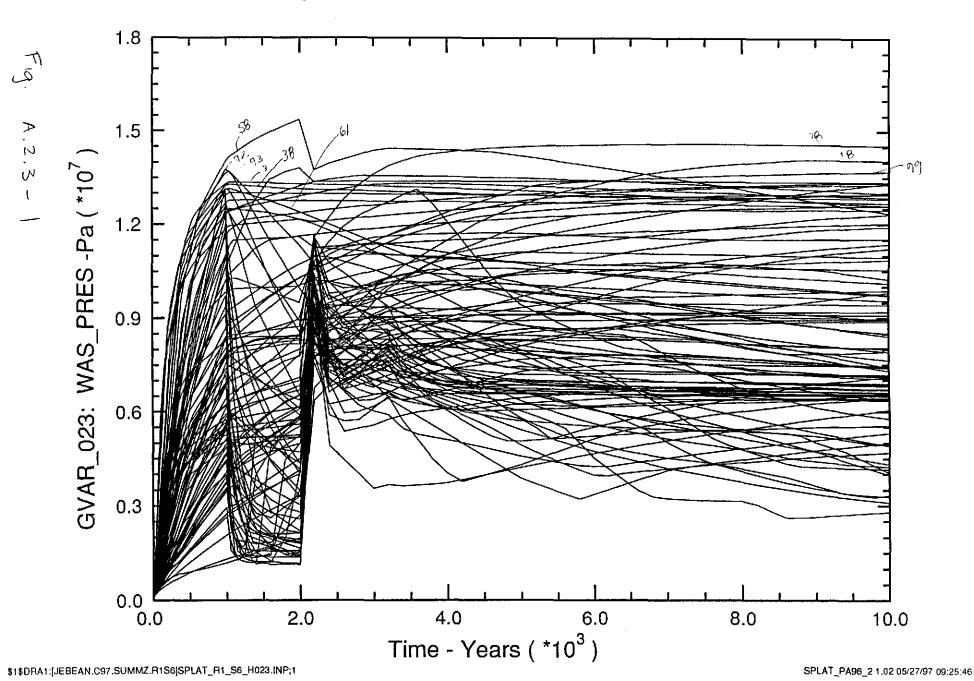
A.2.3.1.2.2 Mechanical Response

In most realizations, gas is not generated at sufficiently high rates to reach fracture pressures prior to the first intrusion at 1000 years. After the intrusion, the borehole prevents pressures from building up in all but a few realizations to the point where fracturing could again take place. As a consequence, fracturing in the interbeds occurs in only a few realizations (A.2.3-47 [GVAR_113] to A.2.3-52 [GVAR_118]). The most extensive fracturing occurs to the north in Anhydrite a and b and Marker Bed 139, the maximum fracture length is 1000 m and 400 m, respectively. These fracture lengths decreases at later times. In the CCA, most of the fracturing occurs to the north in Marker Bed 138 and Anhydrite a and b, up to 100m.

As in the S3 scenario, DRZ fracturing occurs in about 20 vectors and in most vectors DRZ fractures close in less than 500 years after the borehole intrusion. Significant fracturing in the DRZ occurs in only about 5 realizations, as indicated by increasing DRZ permeability (Figure A.2.3-53 [EX_H033]). Vector #78 exhibits the largest DRZ permeability increase (vector with highest permeability after 4000 years). This vector had a low borehole permeability (rank of 5), a low marker bed permeability (rank of 8), and a relatively high initial DRZ porosity (rank of 61). DRZ porosity increases, indicative of DRZ fracturing are also evident in several realizations (Figure A.2.3-54 [EX_H022]). Only one realization (#78) results in a long-term DRZ permeability greater than 1x10⁻¹² m² and porosity greater than 0.03. Mean, median, and maximum values for DRZ permeability and porosity are shown in Table A.1-3.

SNL WIPP C97: BRAGFLO SIMULATIONS (C97 R1 S6)

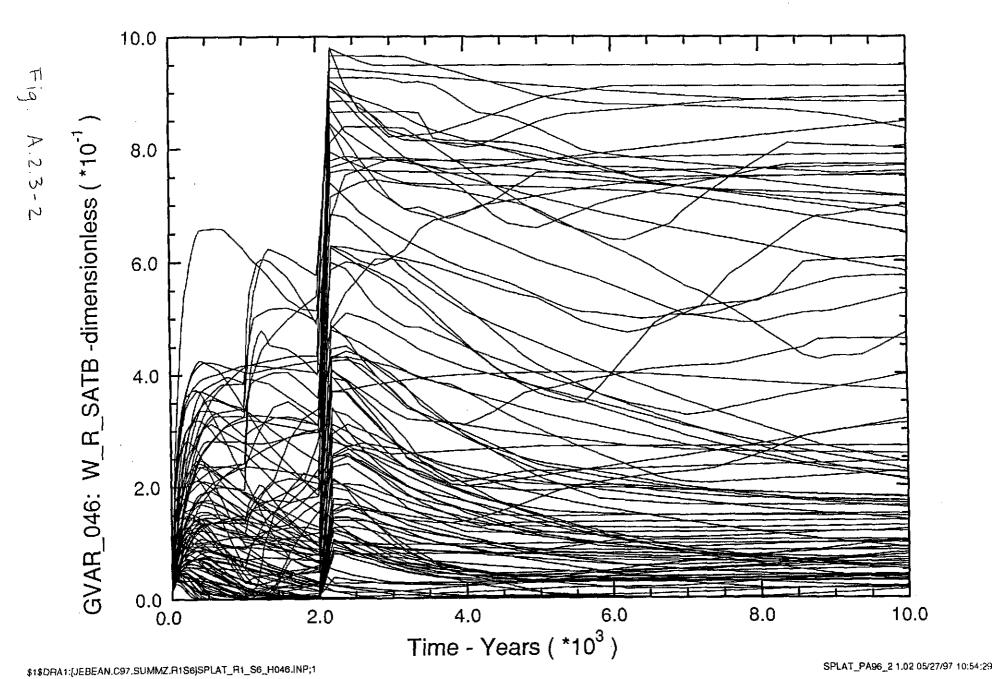
Volume-Averaged Pressure in Waste Panel

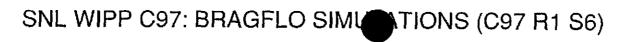




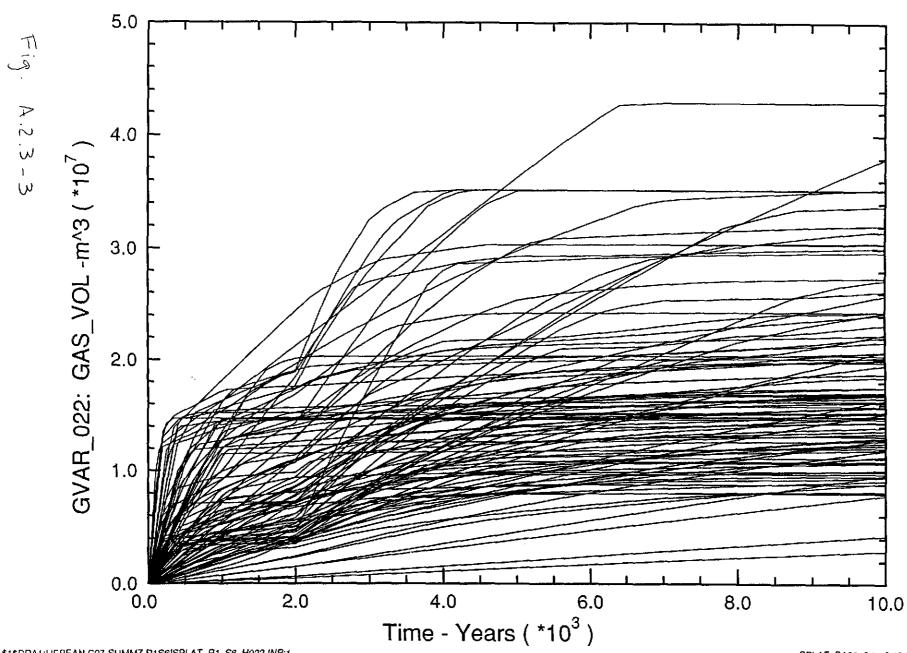


Volume-Averaged Brine Saturation in Waste Panel plus Rest of Repository



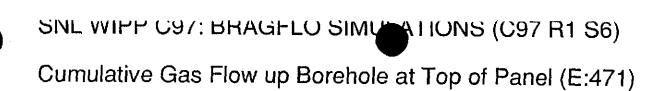


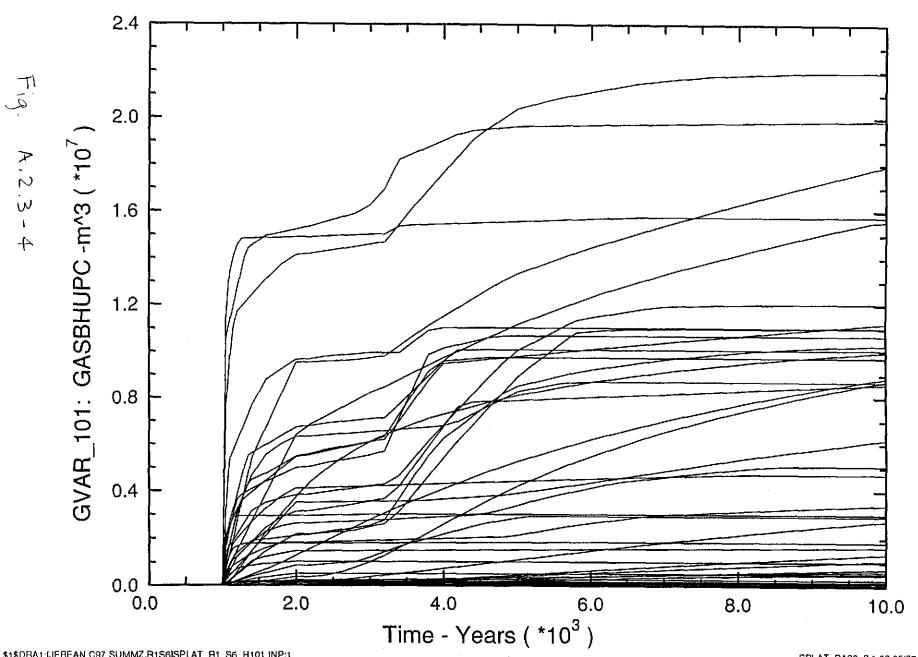




\$1\$DRA1:[JEBEAN.C97.SUMMZ.R1S6]SPLAT_R1_S6_H022.fNP;1

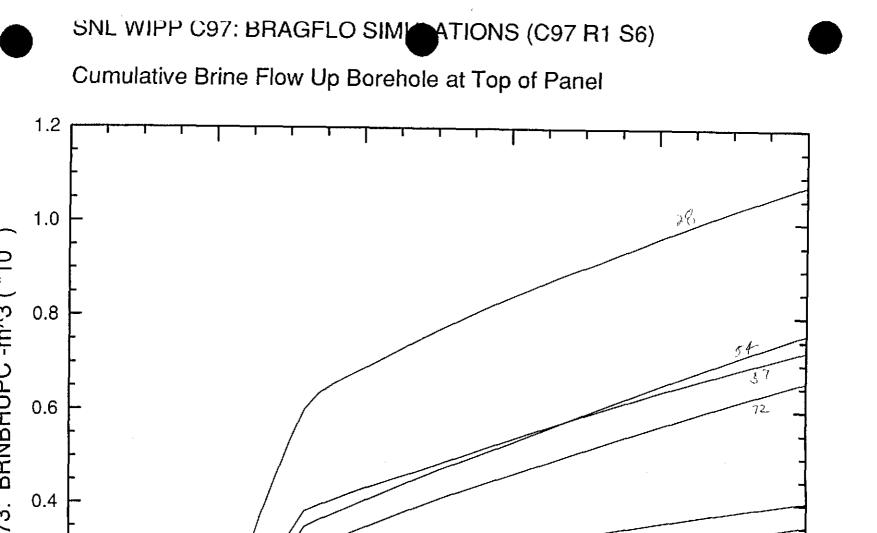
SPLAT_PA96_2 1.02 05/27/97 09:21:45

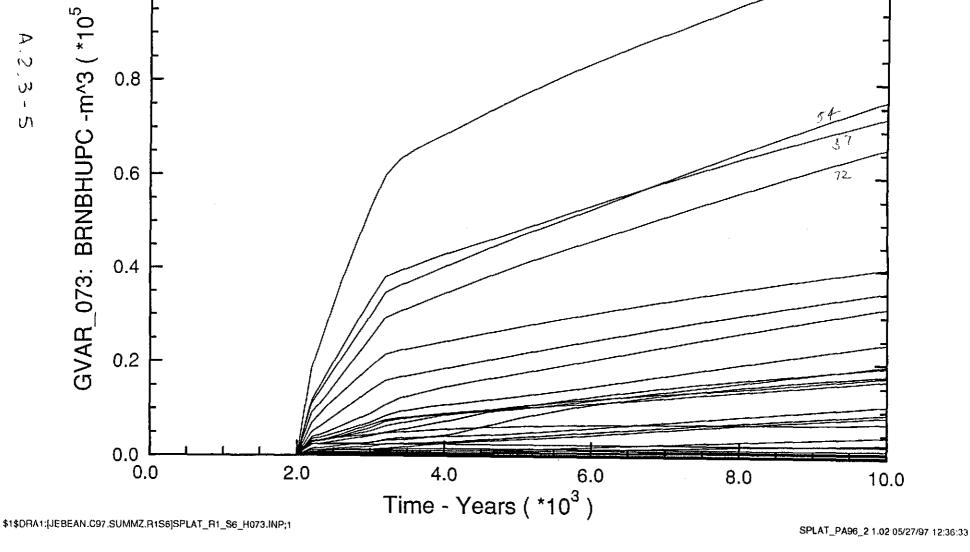


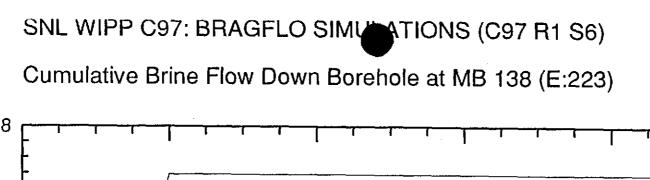


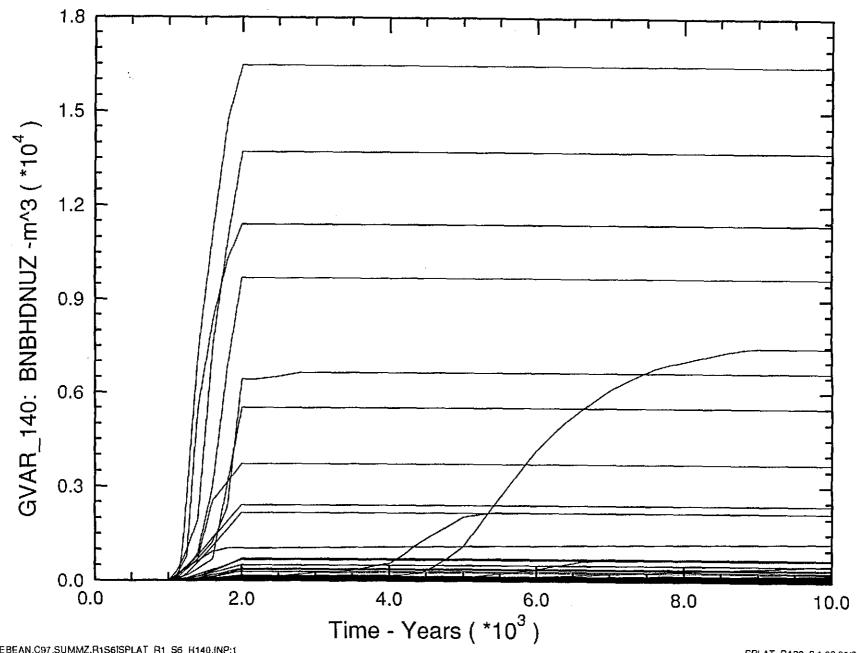
\$1\$DRA1;[JEBEAN.C97.SUMMZ.R1S6]SPLAT_R1_S6_H101.INP;1

SPLAT_PA96_2 1.02 05/27/97 14:16:41



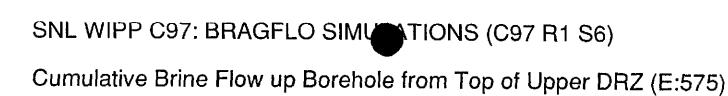


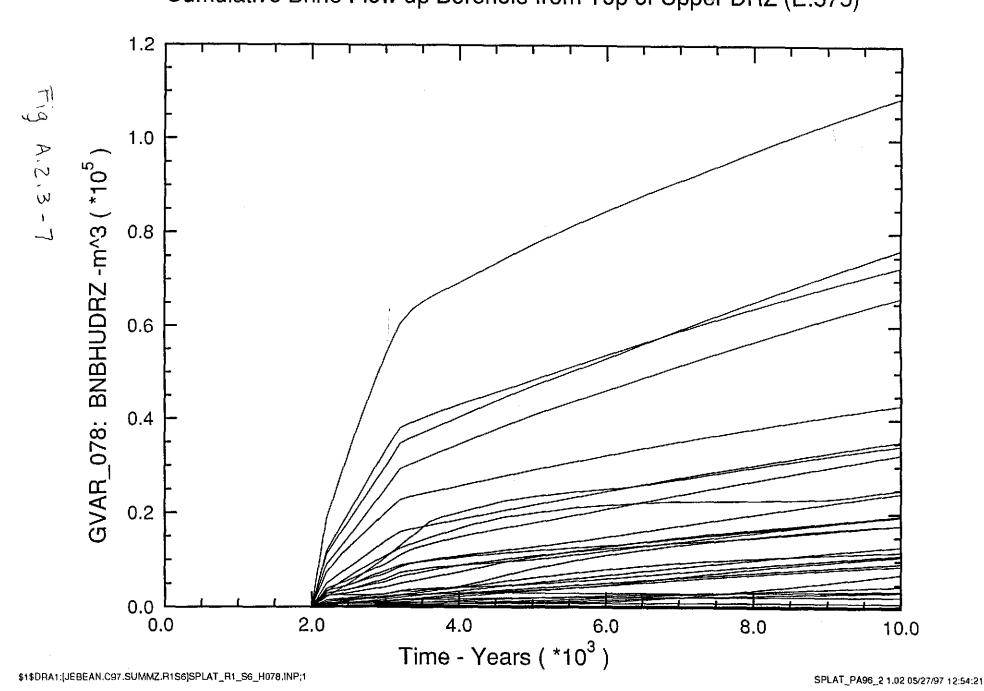


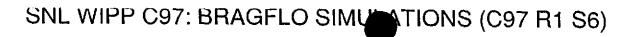


\$1\$DRA1:[JEBEAN.C97.SUMMZ.R1S6]SPLAT_R1_S6_H140.fNP;1

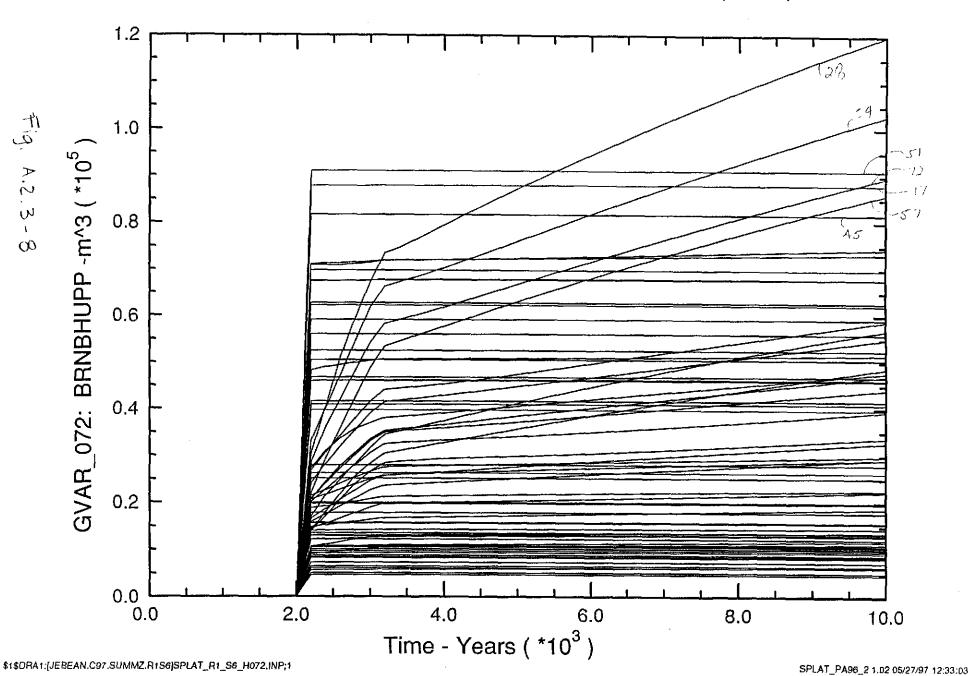
SPLAT_PA96_2 1.02 05/28/97 10:17:39







Cumulative Brine Flow up Borehole at Bottom of Panel (E:599)



Figures corresponding to the following CCA Figures were not used.

CCA Fig. 7.2.3-9

-10

-11

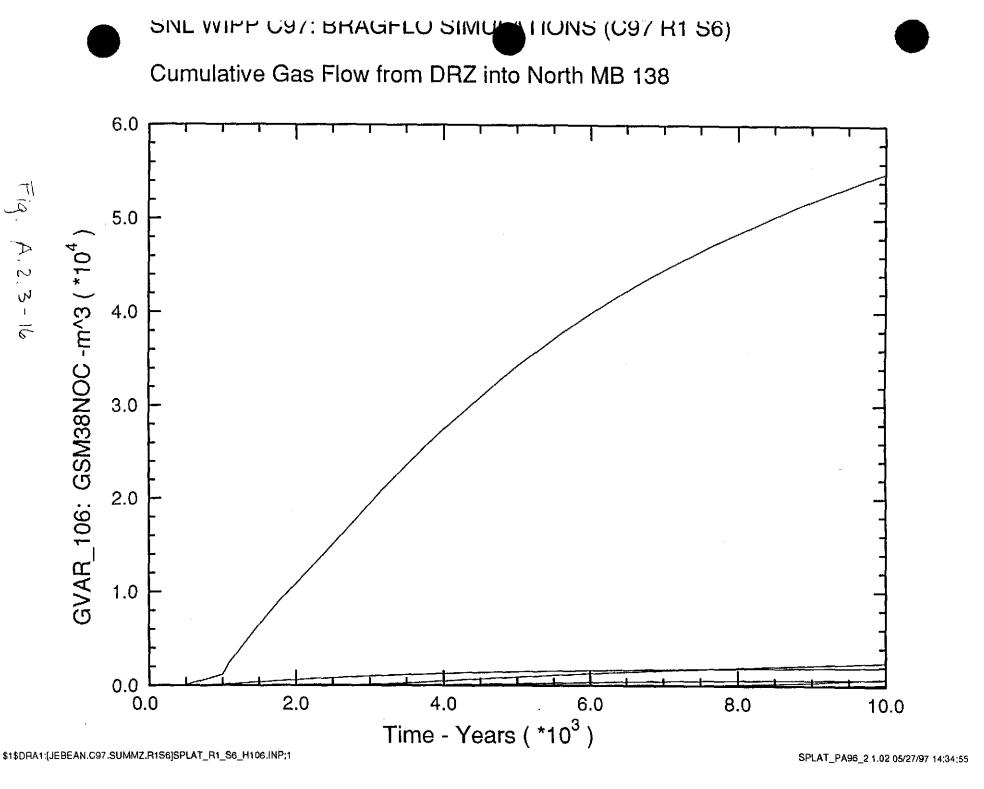
-12

- 13

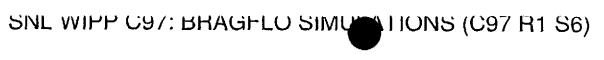
- 14

- 15

Information Only



Information Only



Cumulative Gas Flow from DRZ into North Anhydrite A/B

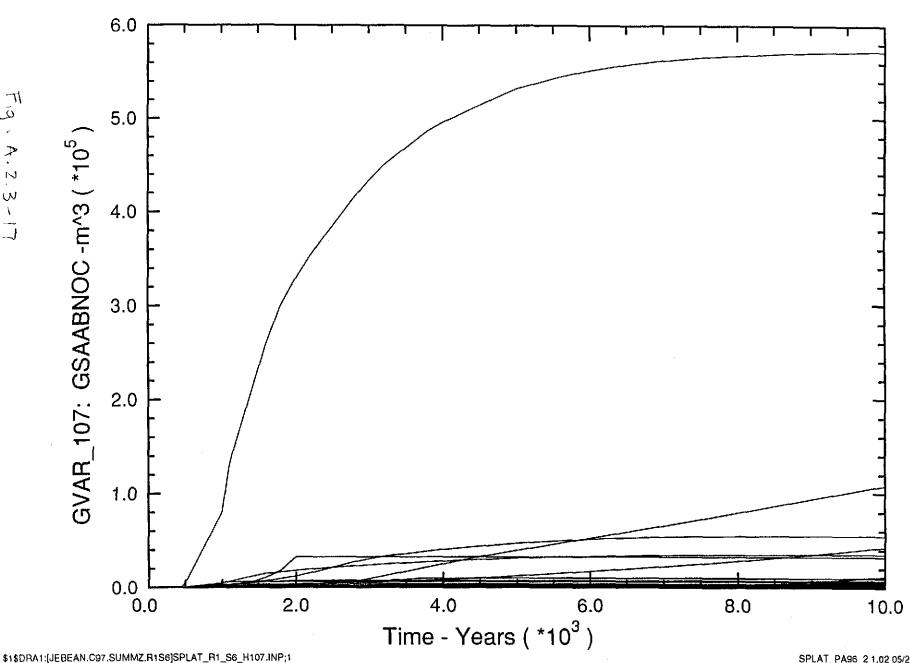
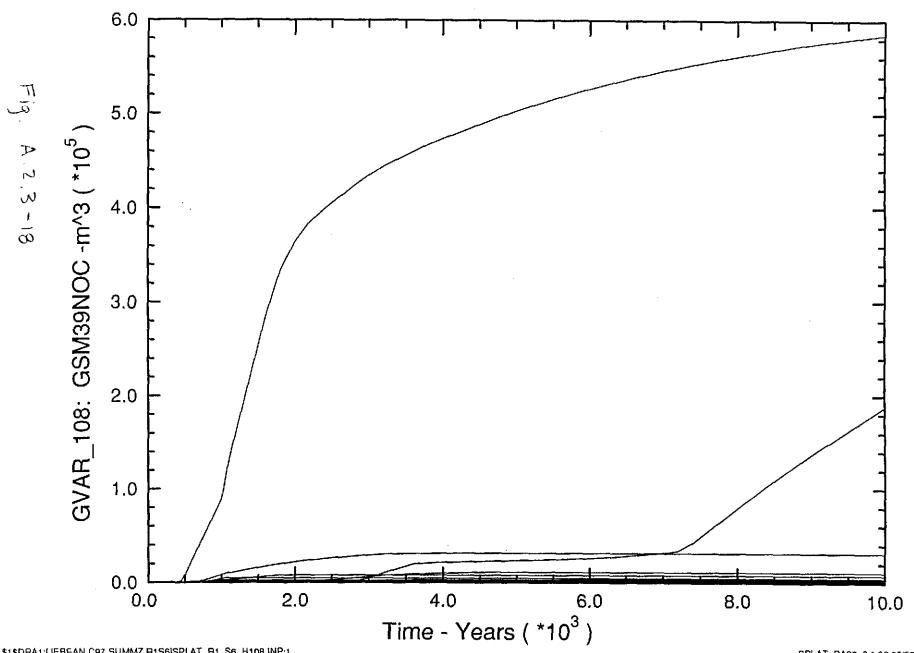


Fig. A. 2.3-17

SPLAT_PA96_2 1.02 05/27/97 14:38:26

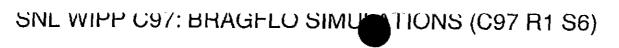


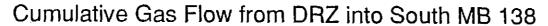


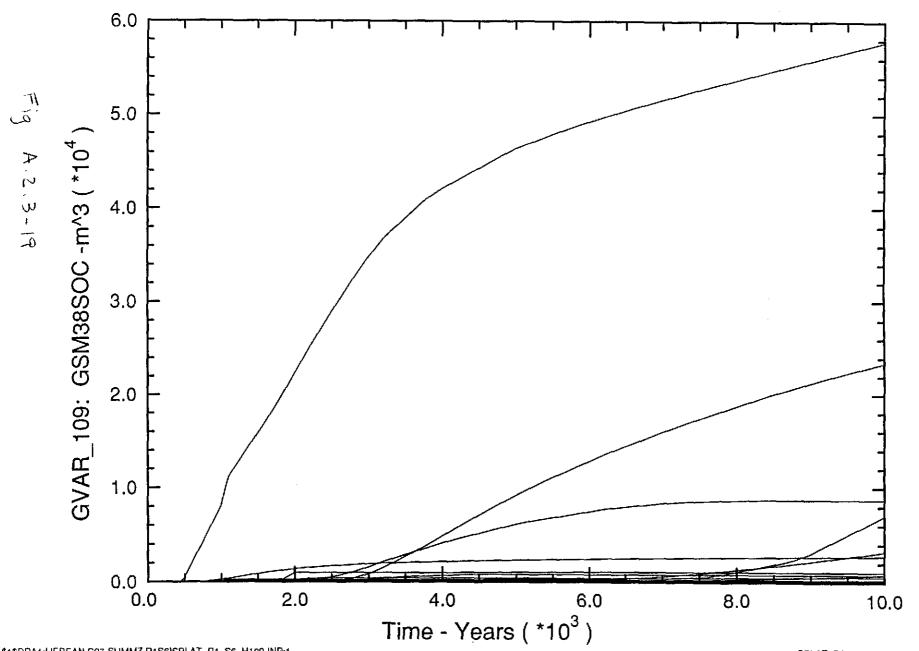


\$1\$DRA1;[JEBEAN.C97.SUMMZ.R1S6]SPLAT_R1_S6_H108.INP;1

SPLAT_PA96_2 1.02 05/27/97 14;41:58

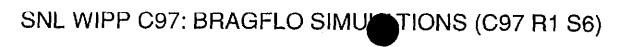




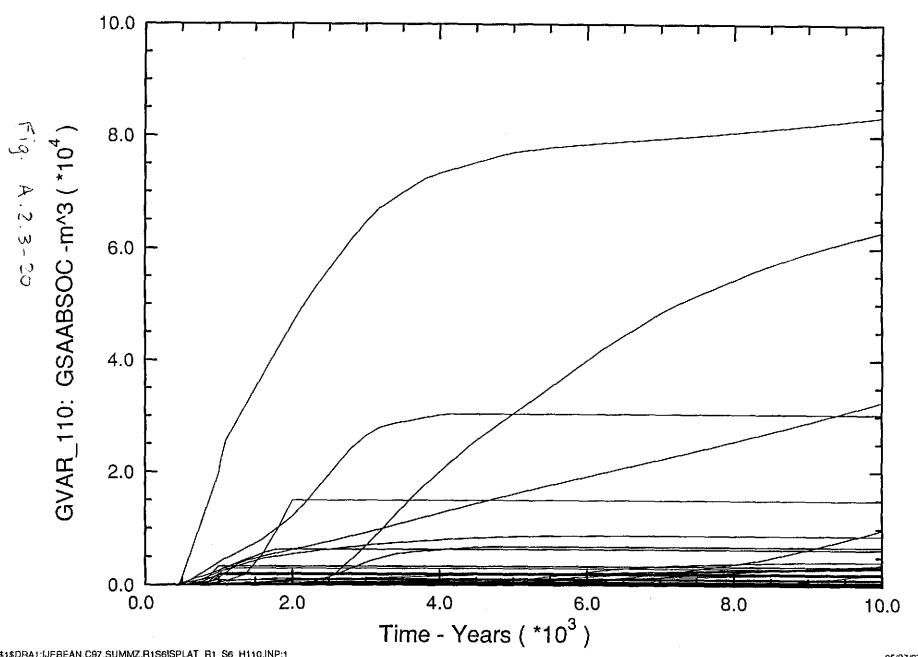


\$1\$DRA1:[JEBEAN.C97.SUMMZ.R1S6]SPLAT_R1_S6_H109.INP;1

SPLAT_PA96_2 1.02 05/27/97 14:45:29



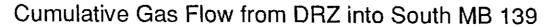
Cumulative Gas Flow from DRZ into South Anhydrite A/B

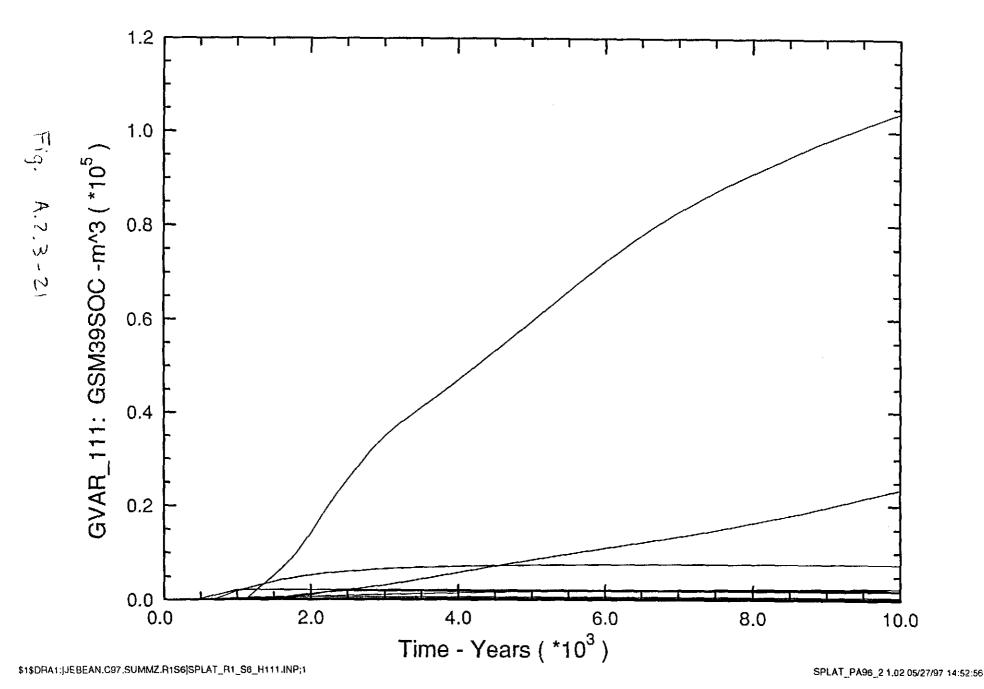


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05/27/97 14:49:00



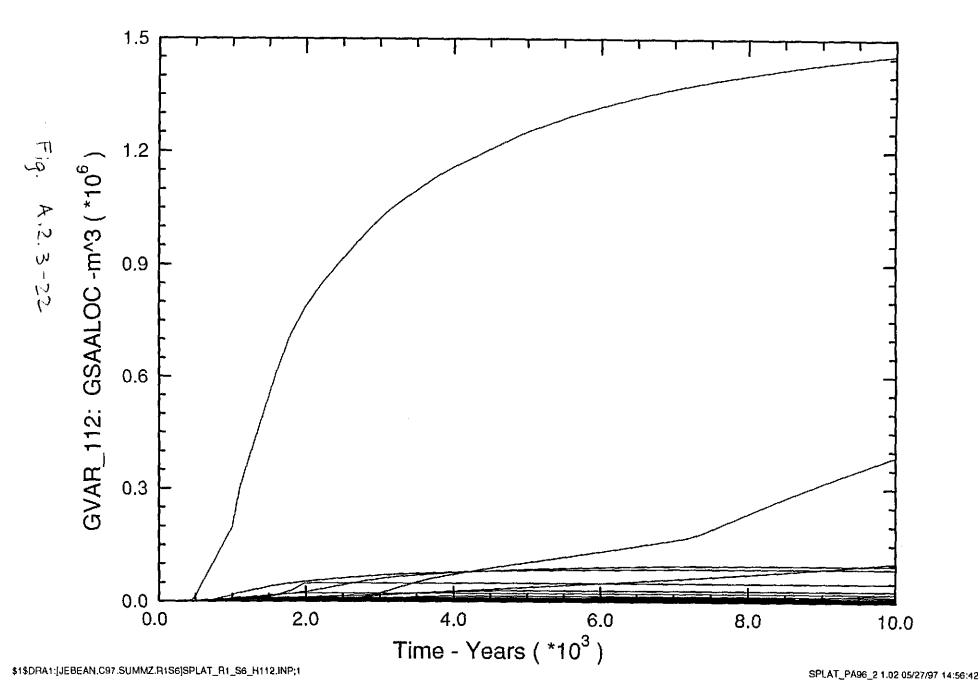




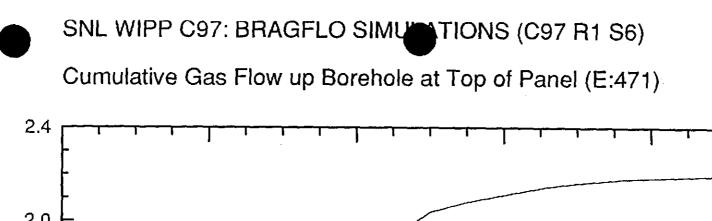
Information Only

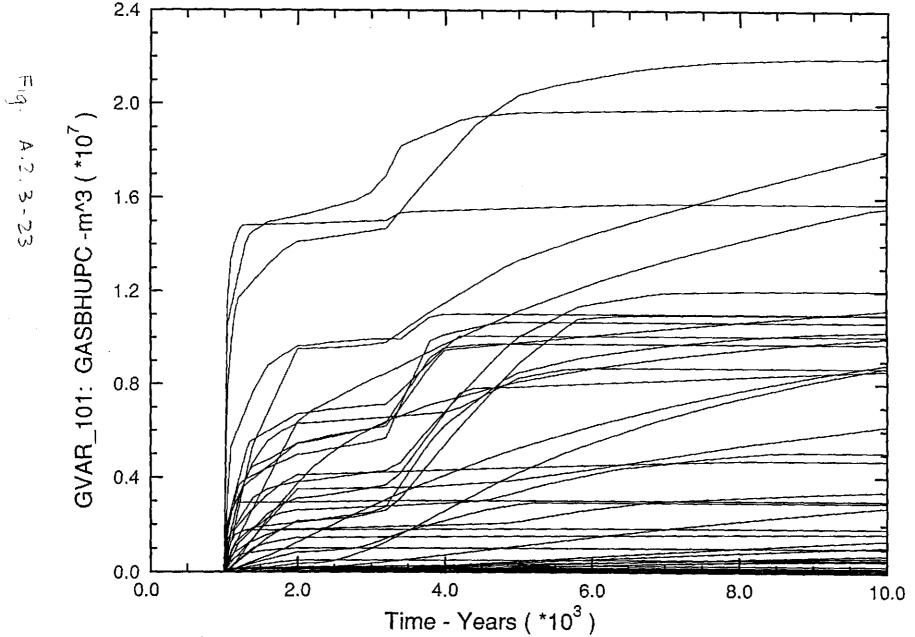






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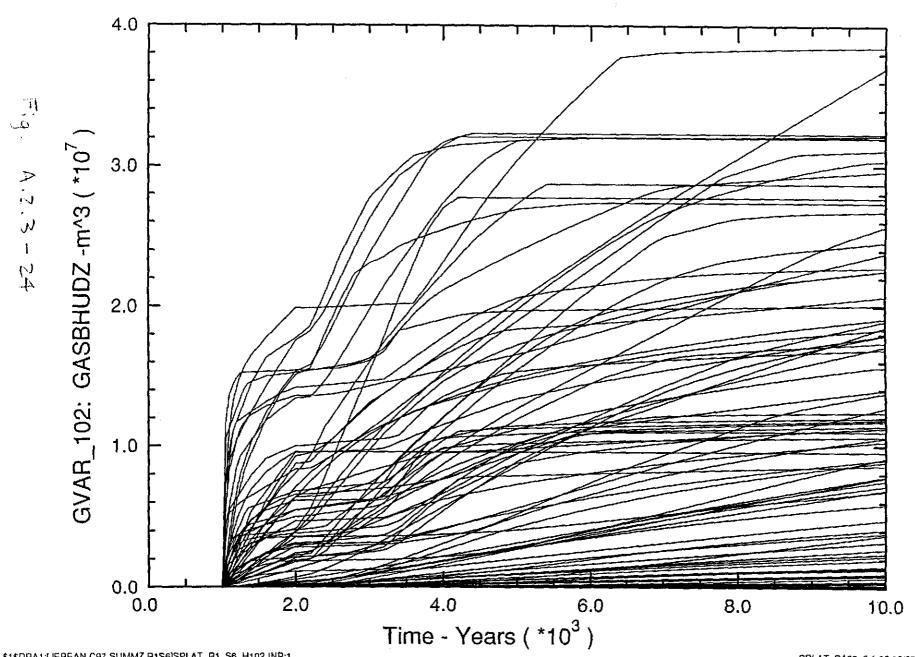


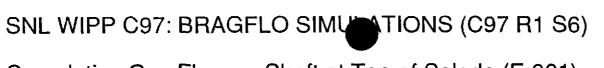
\$1\$DRA1:[JEBEAN.C97.SUMMZ.R1S6]SPLAT_R1_S6_H101.INP;1

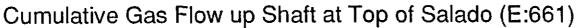
SPLAT_PA96_2 1.02 05/27/97 14:16:41

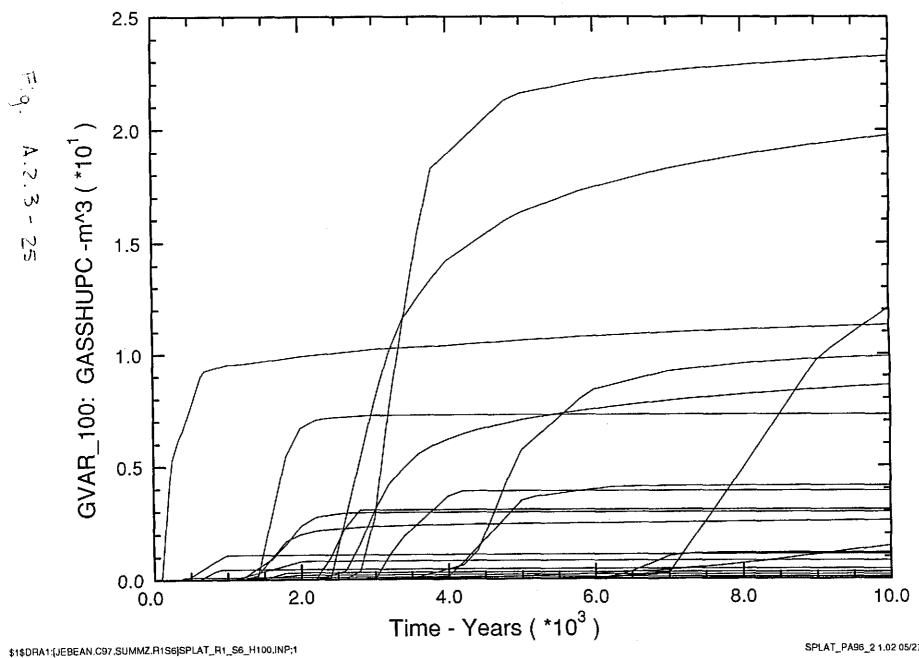


Cumulative Gas Flow Out of Upper DRZ at Borehole (E:575)





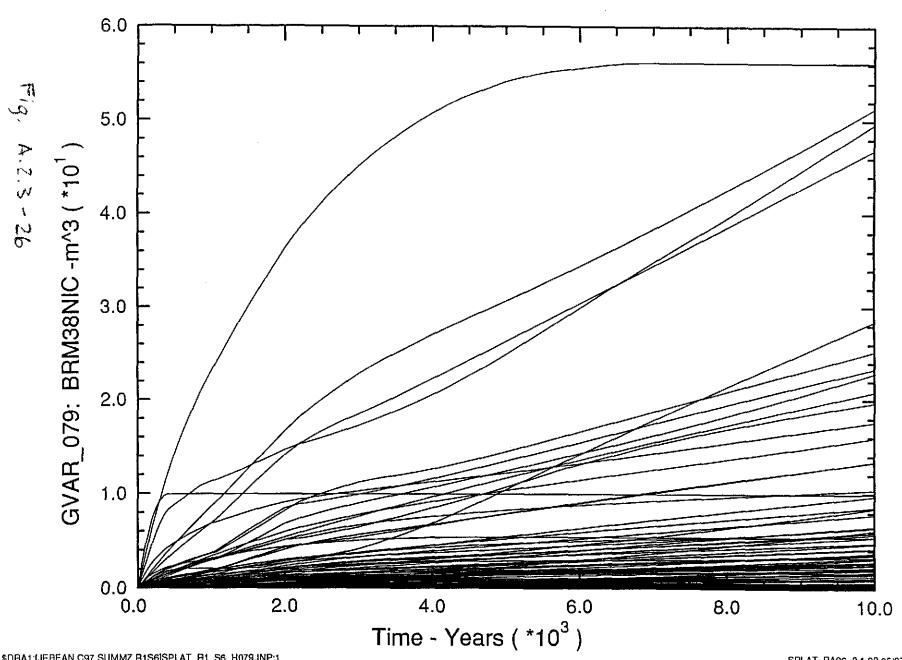




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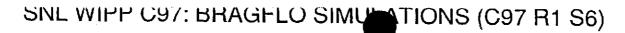
SNL WIPP C97: BRAGFLO SIMULIONS (C97 R1 S6)

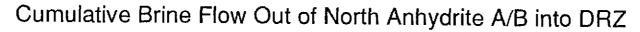
Cumulative Brine Flow Out of North MB 138 into DRZ

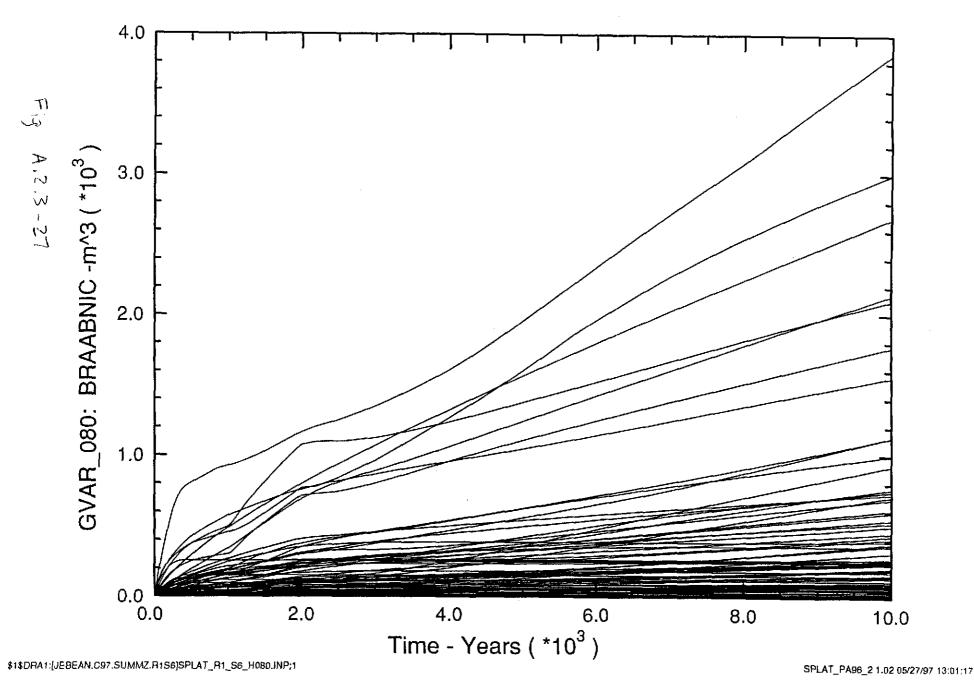


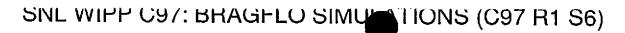
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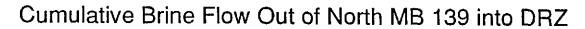
SPLAT_PA96_2 1.02 05/27/97 12:57:47

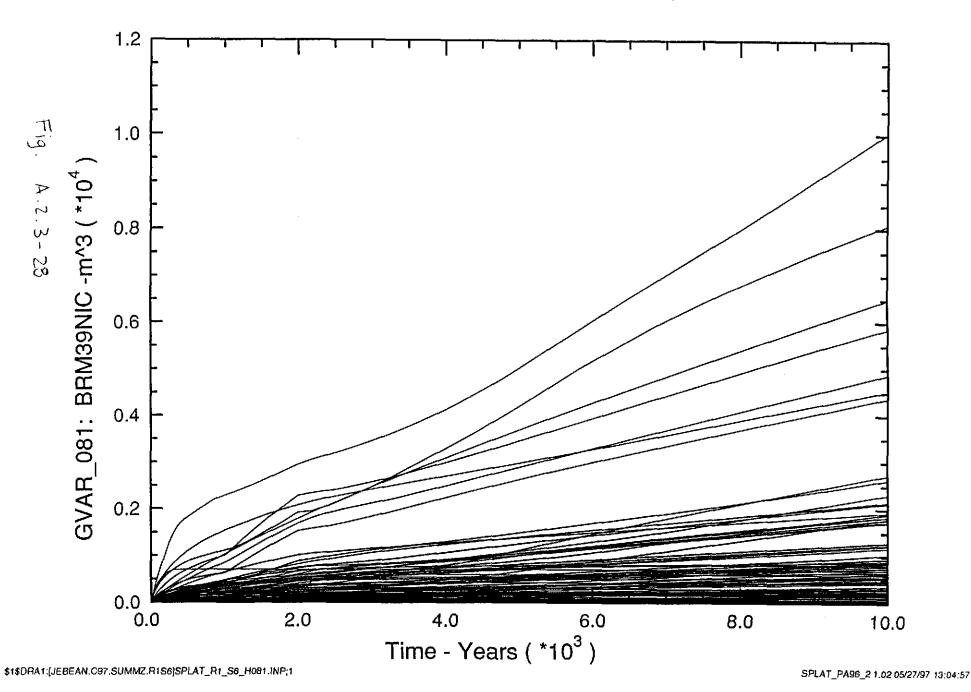


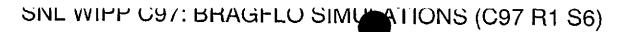


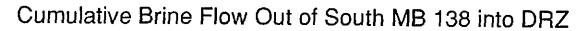


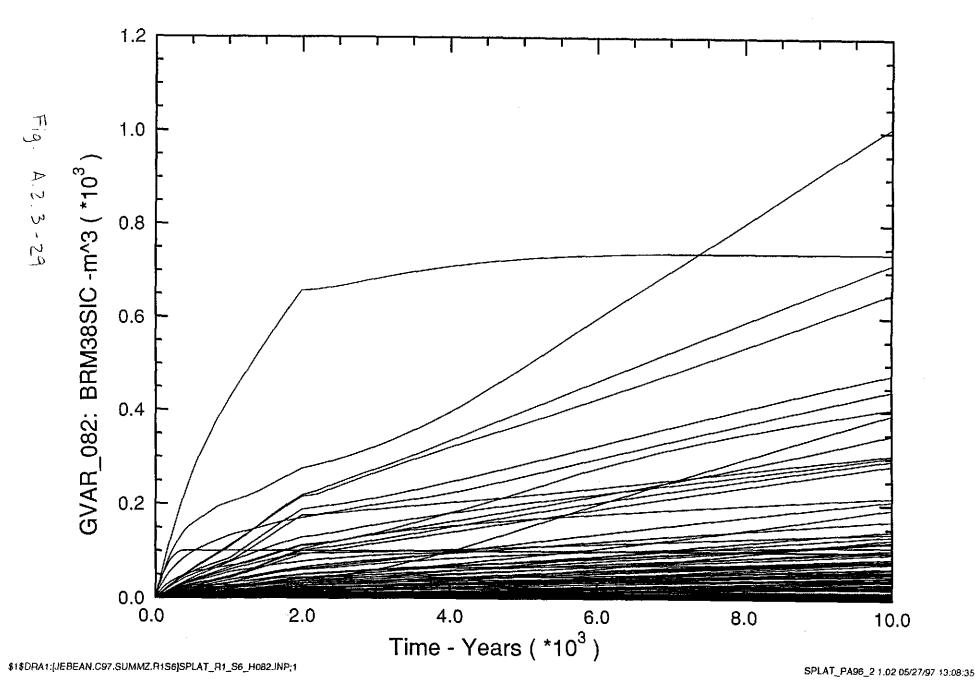


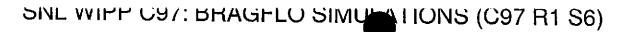




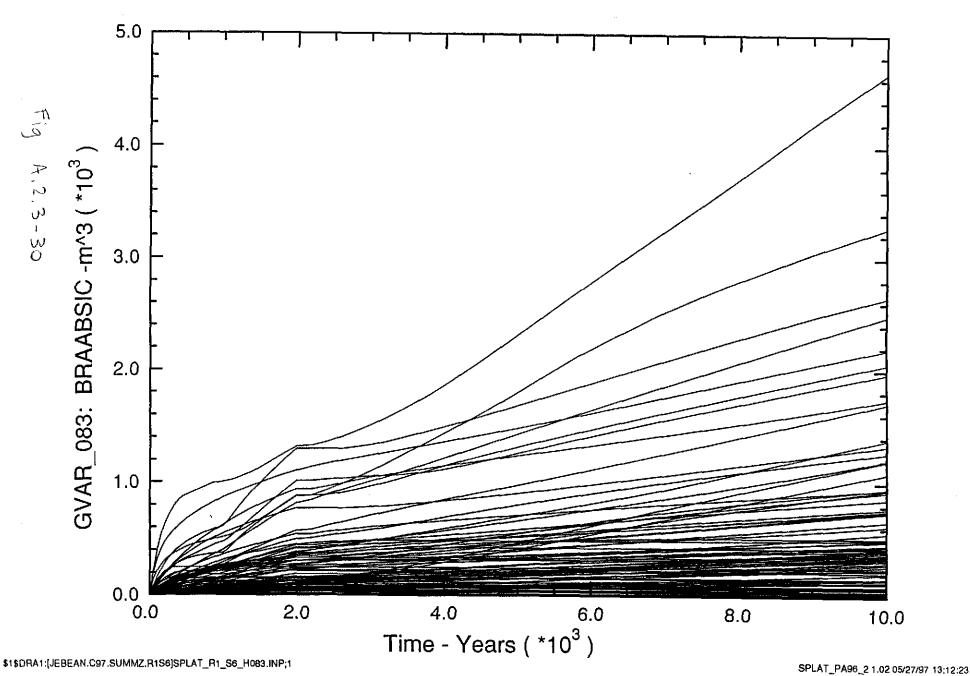




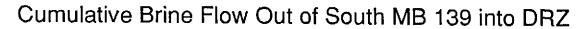


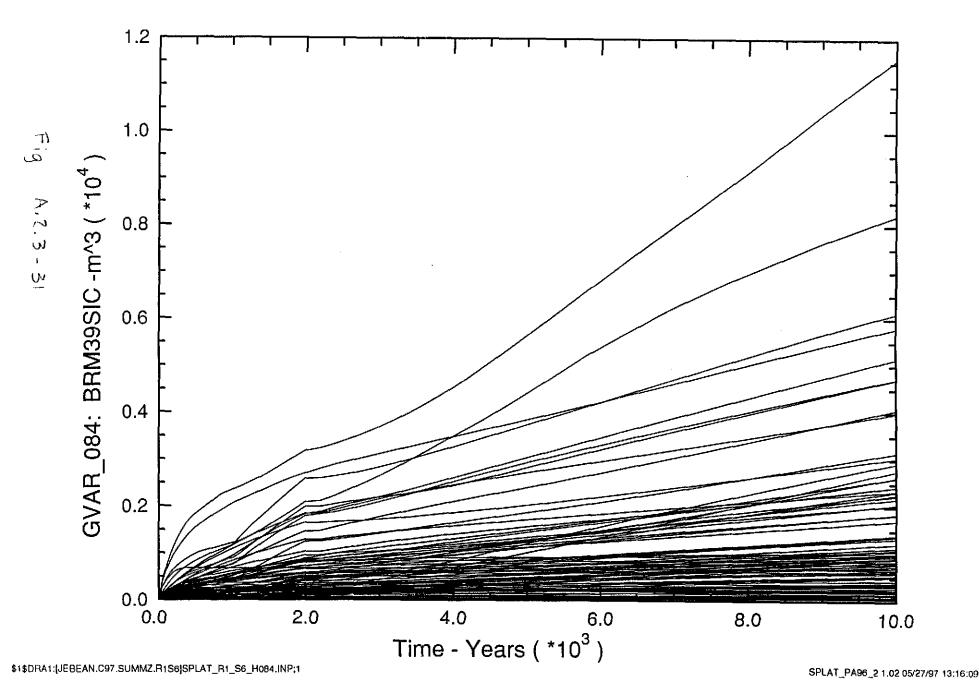


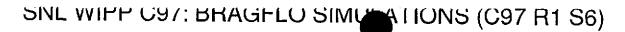




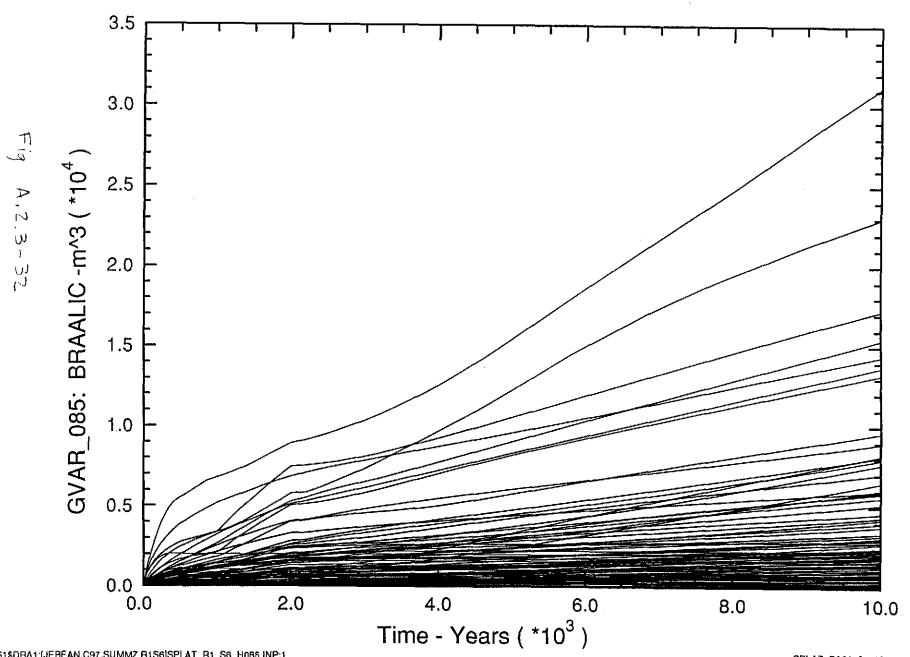








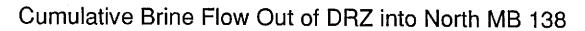
Cumulative Brine Flow into DRZ from All Marker Beds

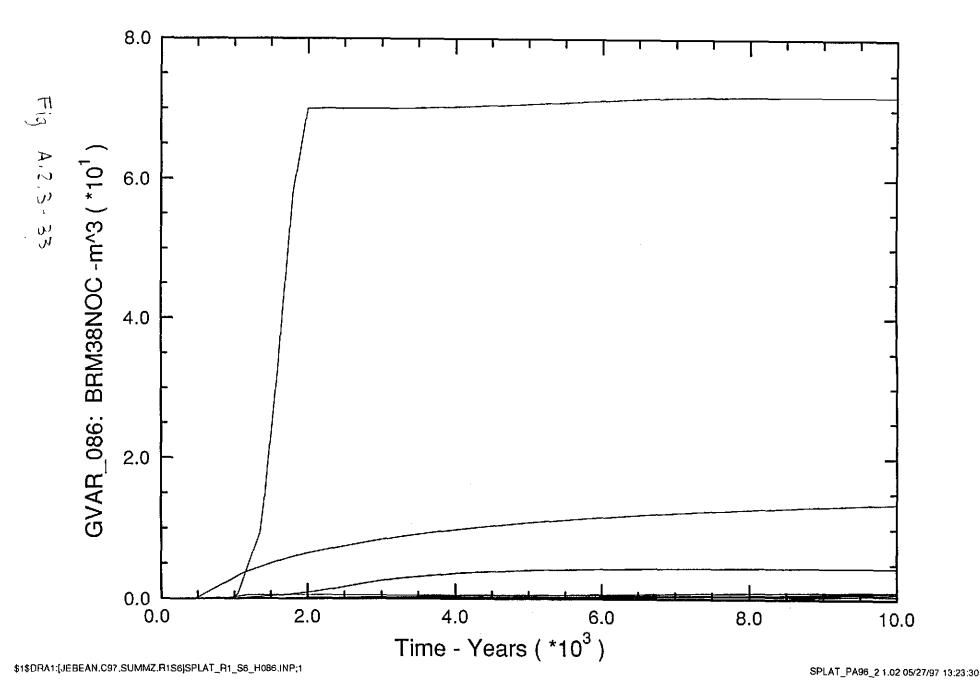


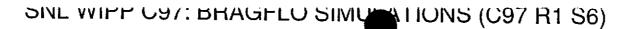
\$1\$DRA1:[JEBEAN.C97.SUMMZ.R1S6]SPLAT_R1_S6_H085.INP;1

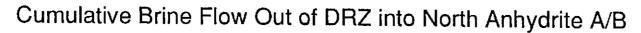
SPLAT_PA96_2 1.02 05/27/97 13:19:51

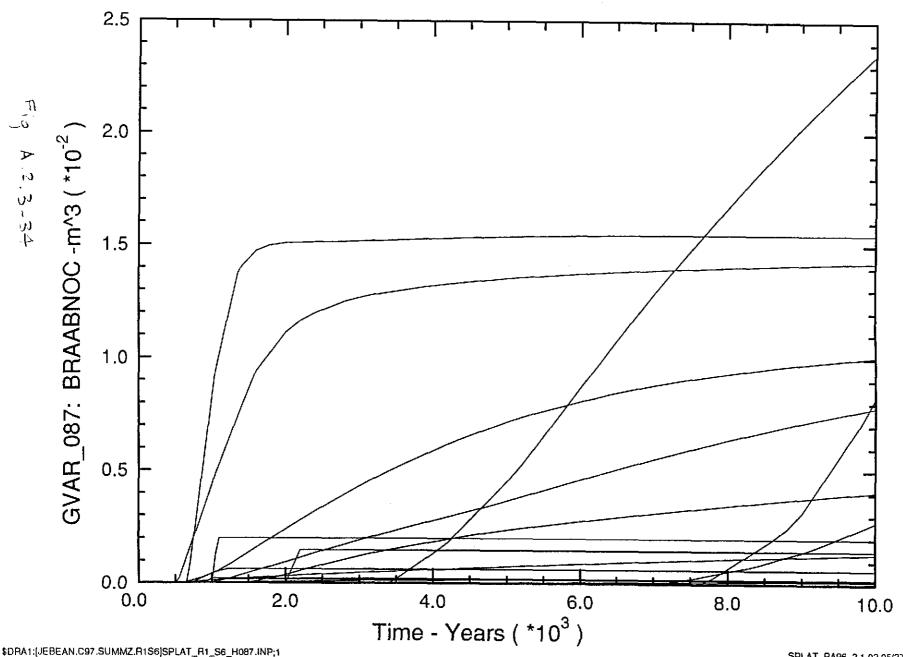








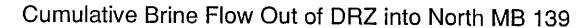


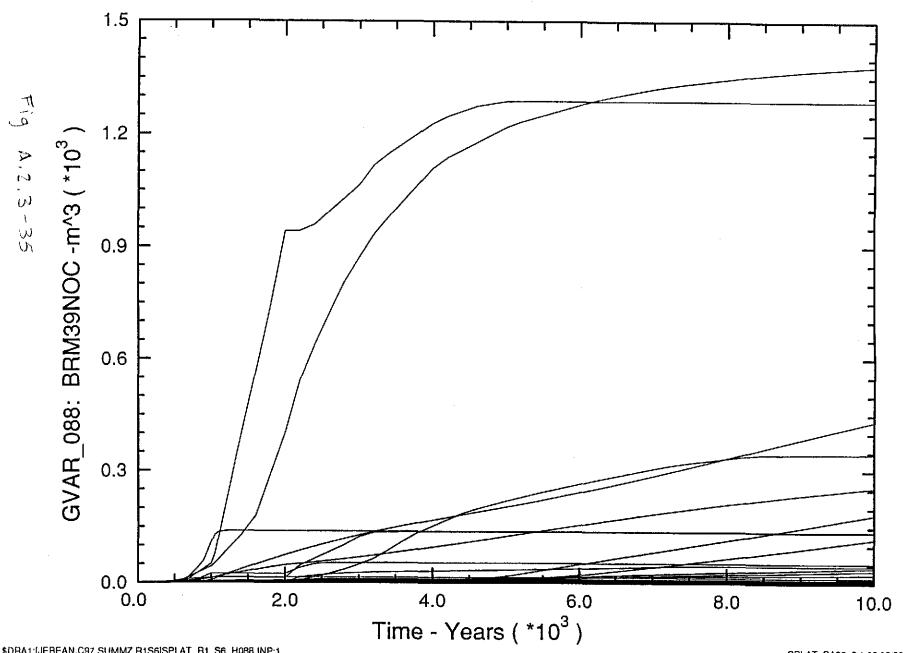


\$1\$DRA1:[JEBEAN.C97.SUMMZ.R1S6]SPLAT_R1_S6_H087.INP;1

SPLAT_PA96_2 1.02 05/27/97 13:26:48

SNL WIPP C97: BRAGFLO SIMULTIONS (C97 R1 S6)



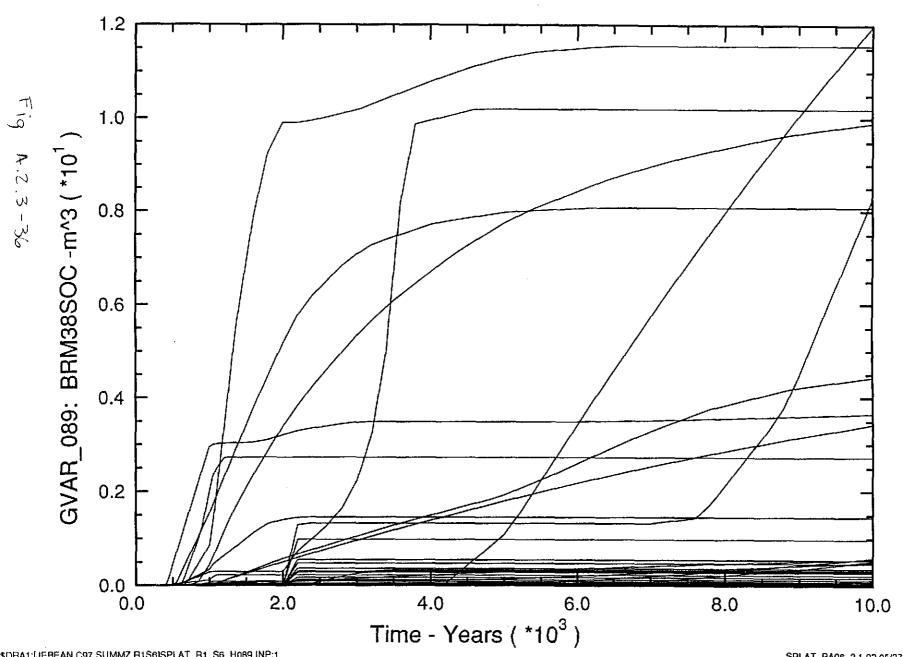


\$1\$DRA1:[JEBEAN.C97.SUMMZ.R1S6]SPLAT_R1_S6_H088.INP;1

SPLAT_PA96_2 1.02 05/27/97 13:30:23

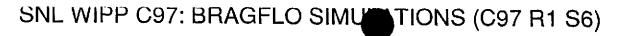


Cumulative Brine Flow Out of DRZ into South MB 138

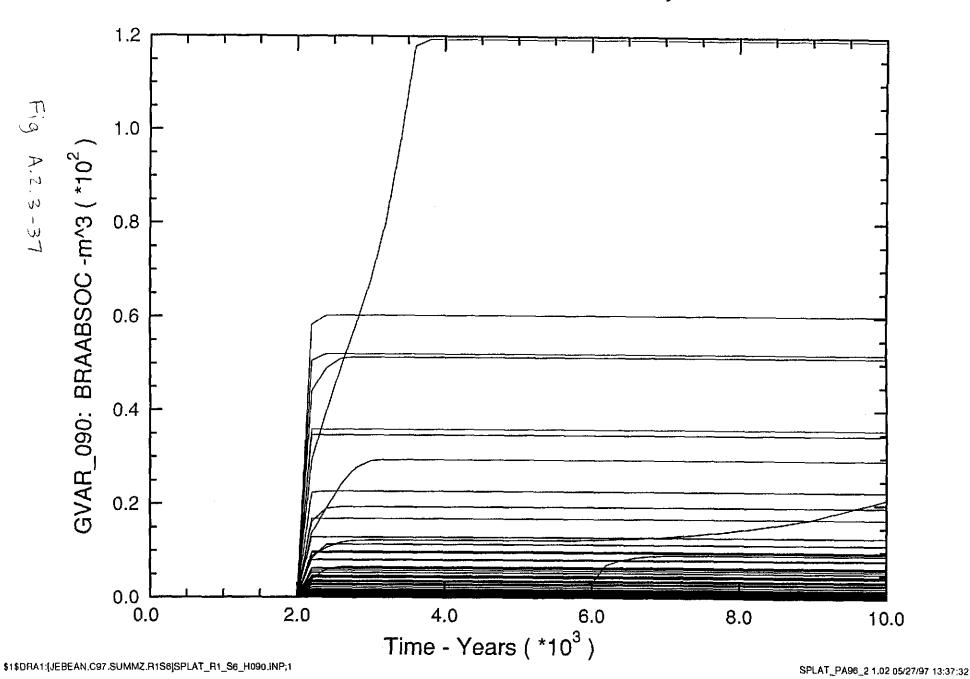


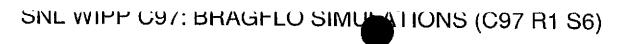
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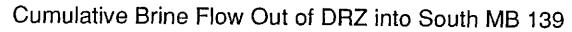
SPLAT_PA96_2 1.02 05/27/97 13:33:52

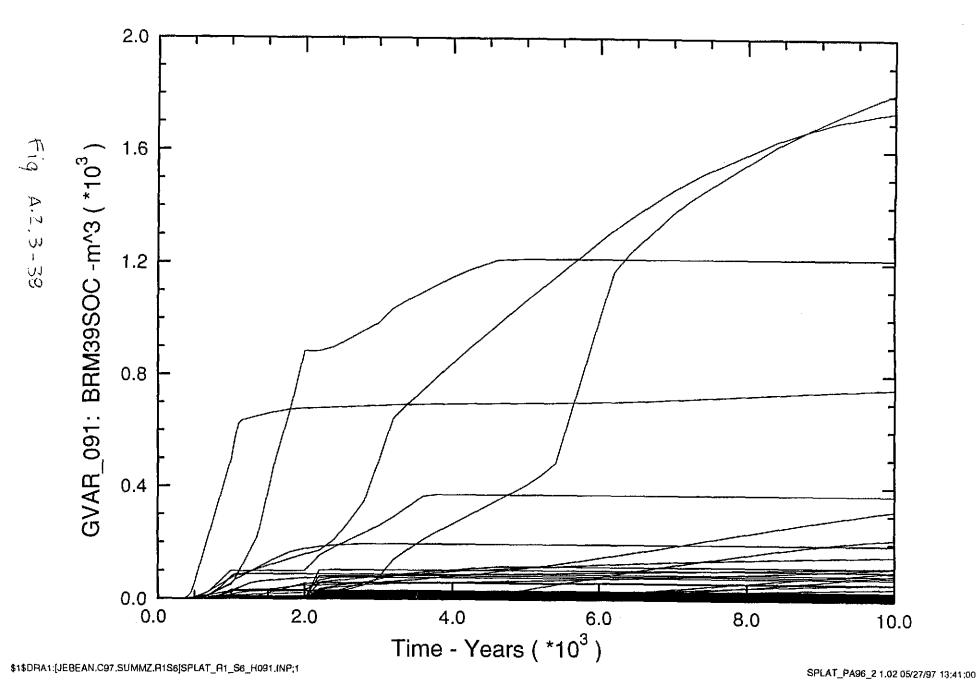


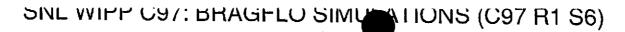
Cumulative Brine Flow Out of DRZ into South Anhydrite A/B



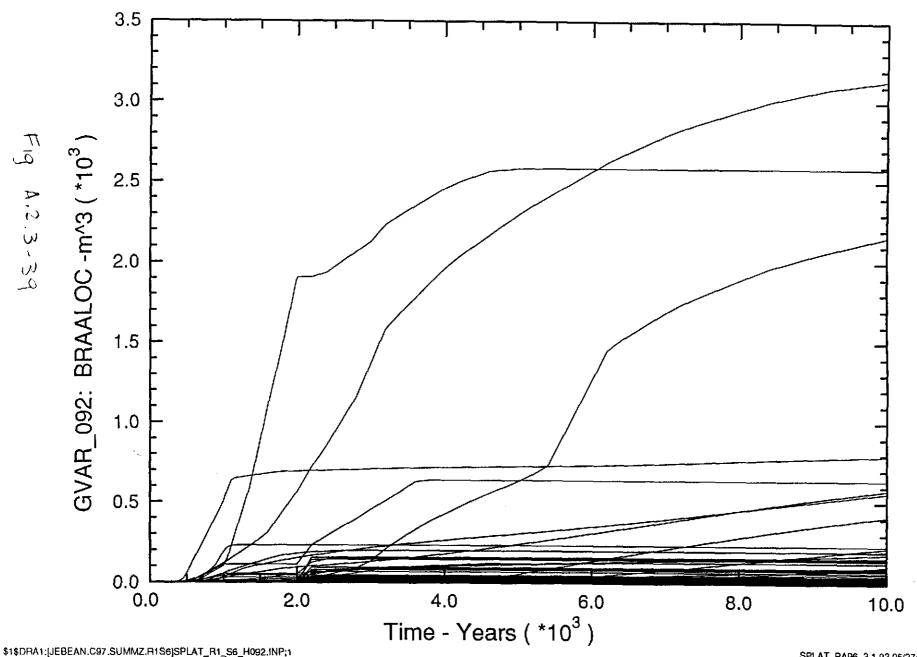






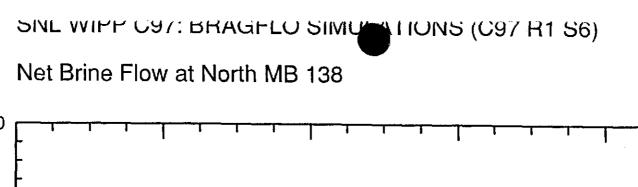


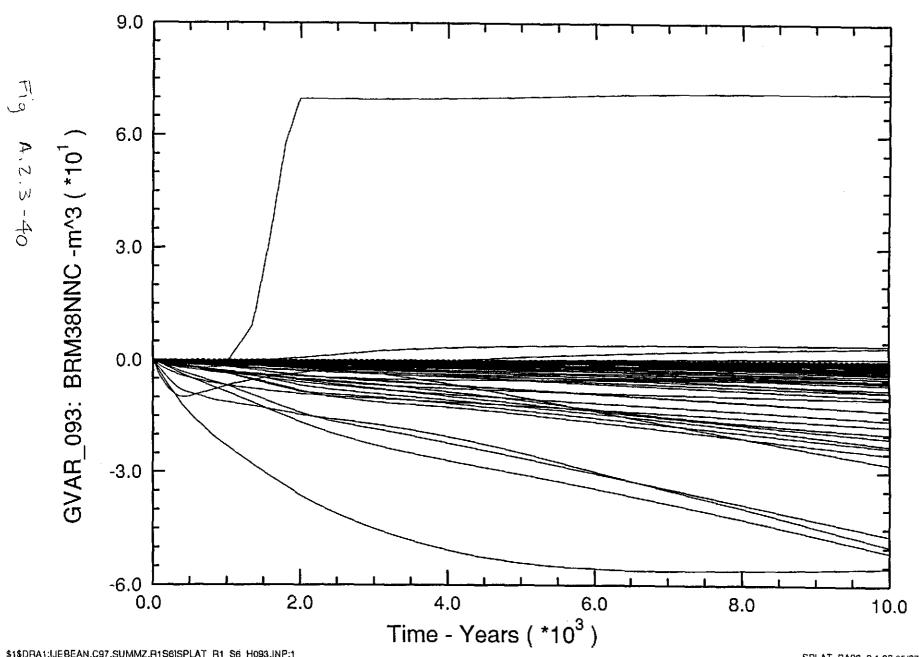
Cumulative Brine Flow Out of DRZ into All Marker Beds



Information Only

SPLAT_PA96_2 1.02 05/27/97 13:44:35



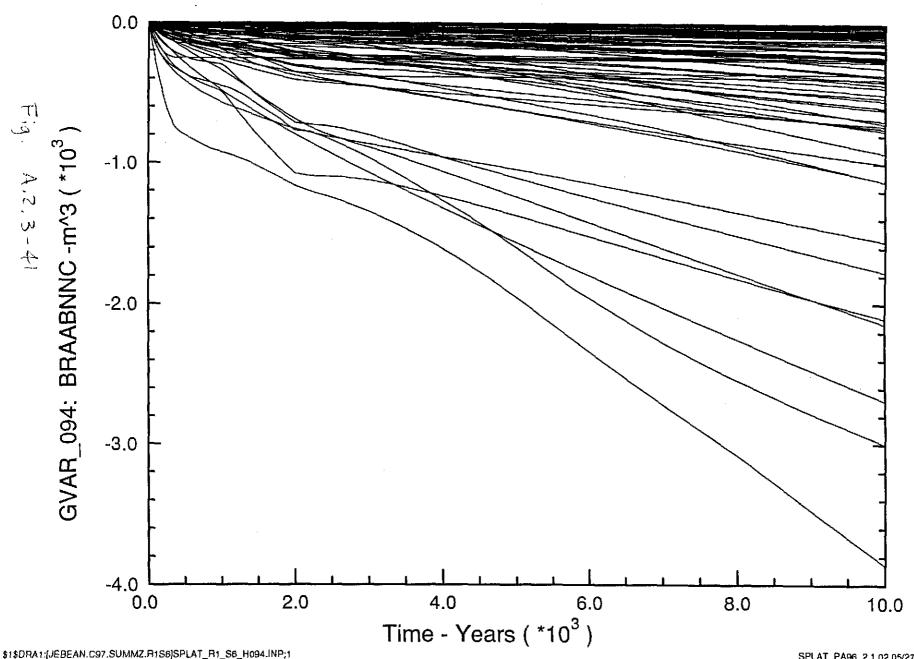


\$1\$DRA1:[JEBEAN.C97.SUMMZ.R1S6]SPLAT_R1_S6_H093.INP;1

SPLAT_PA96_2 1.02 05/27/97 13:48:26

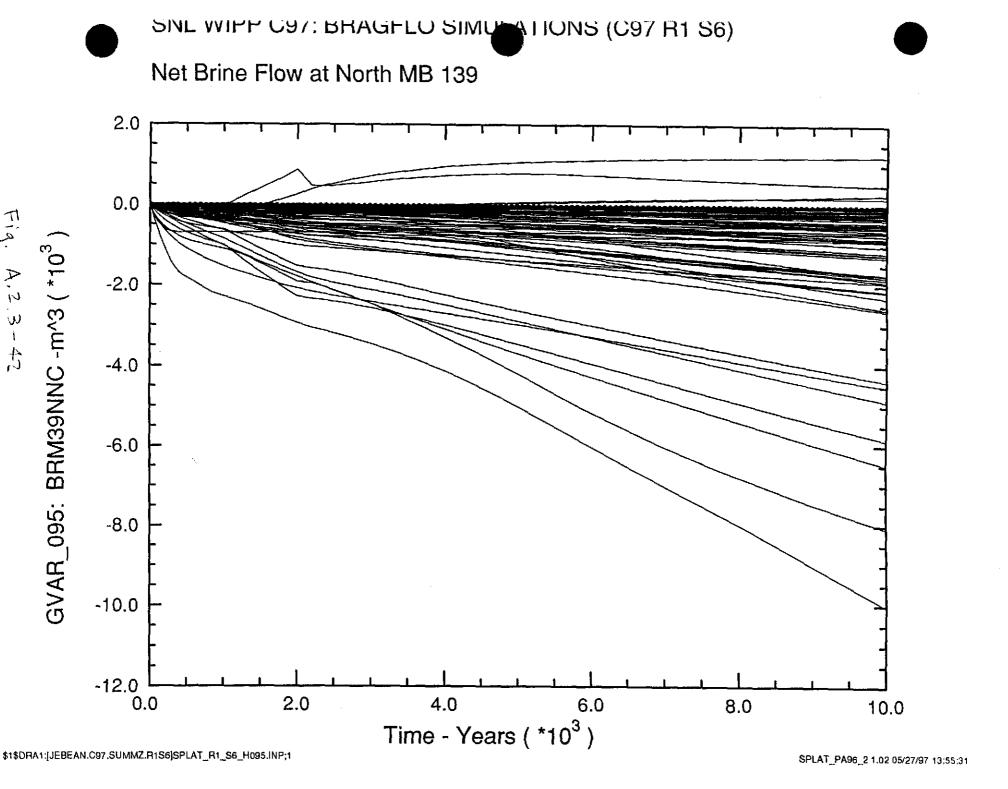
SNL WIPP C97: BRAGFLO SIMUM HONS (C97 R1 S6)

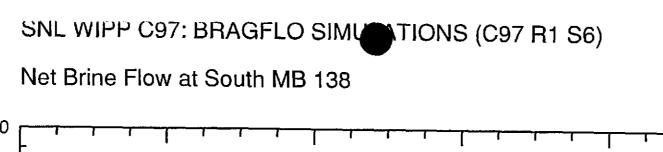
Net Brine Flow at North Anhydrite A/B

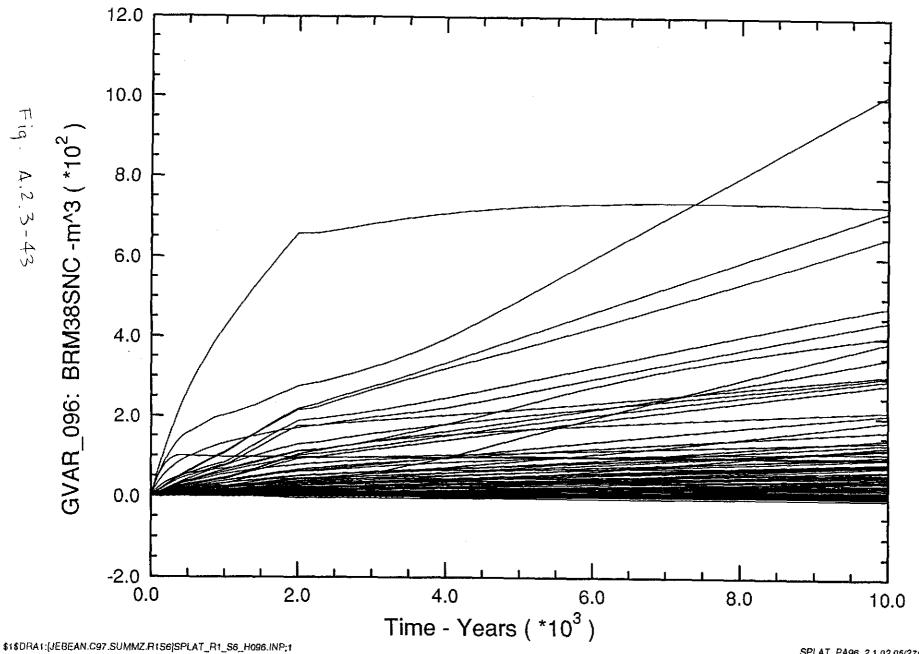


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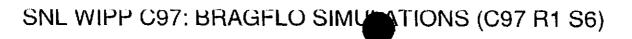
SPLAT_PA96_2 1.02 05/27/97 13:51:55



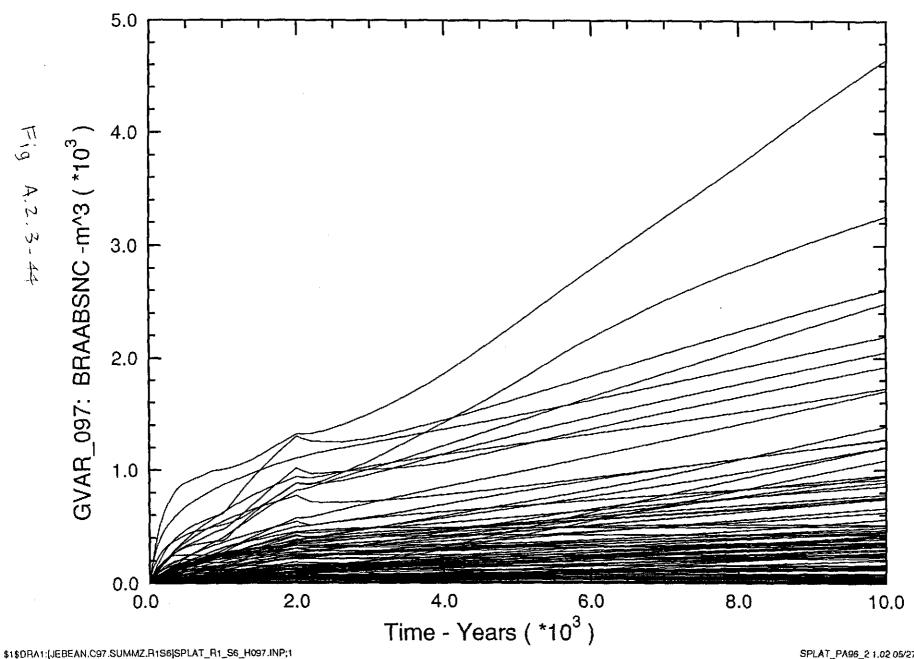




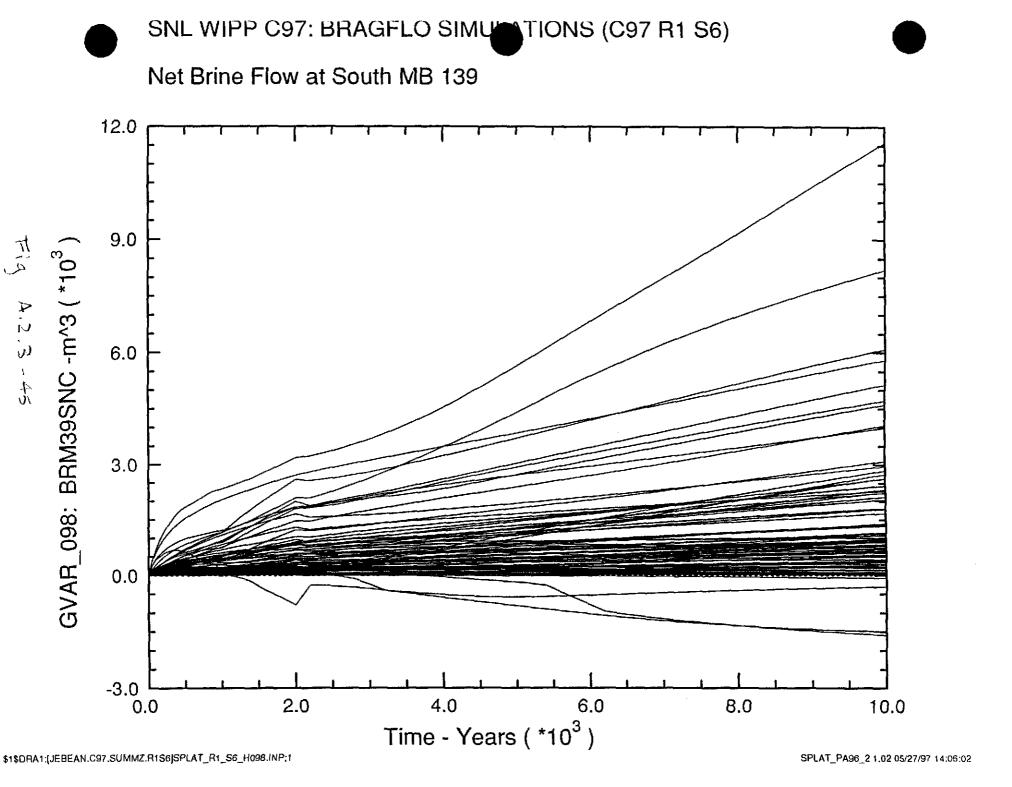
SPLAT_PA96_2 1.02 05/27/97 13:59:02

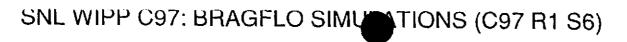




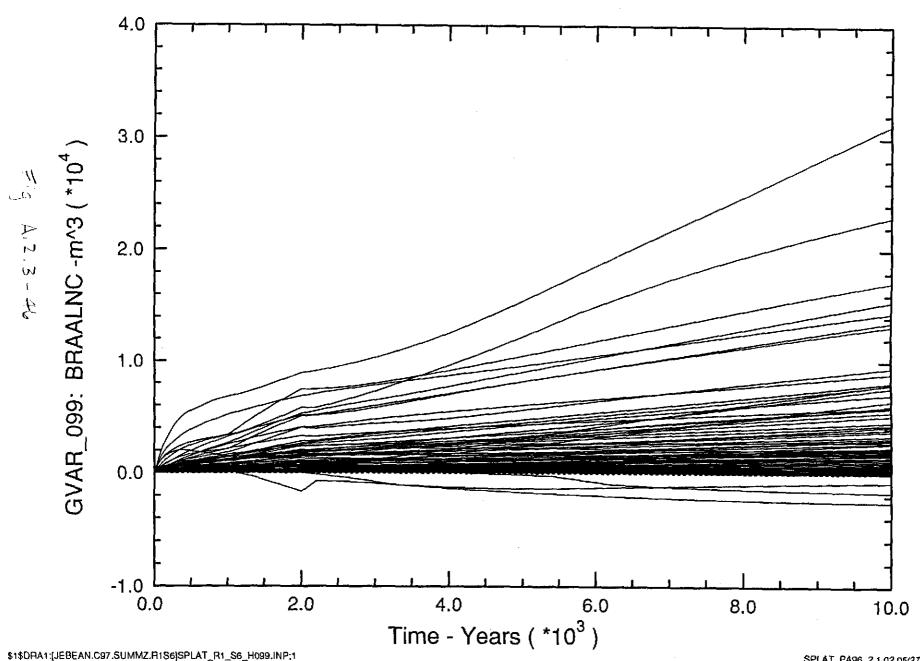


SPLAT_PA96_2 1.02 05/27/97 14:02:32

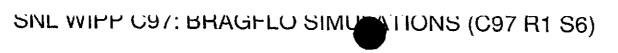




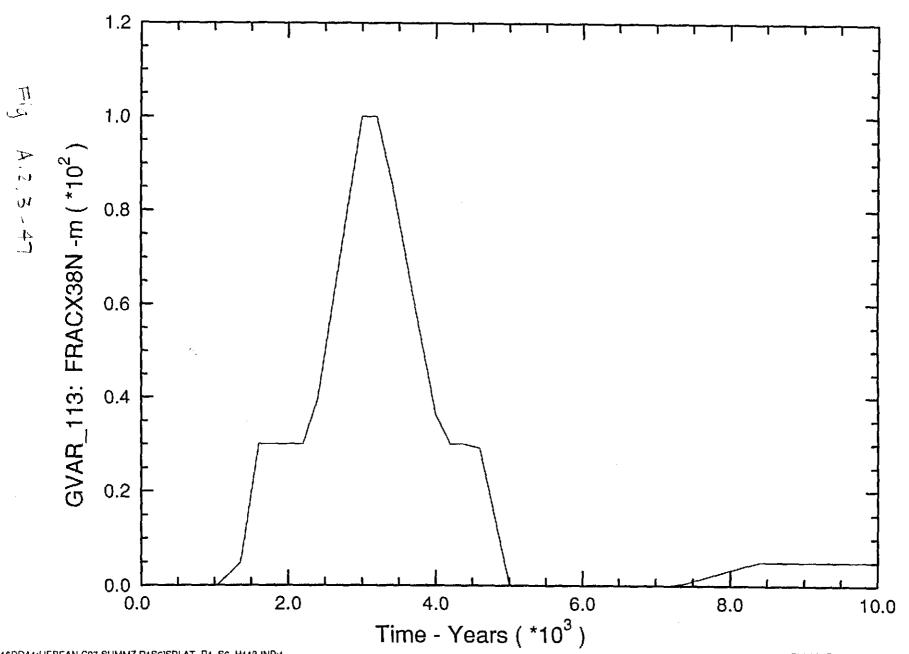




SPLAT_PA96_2 1.02 05/27/97 14:09:37

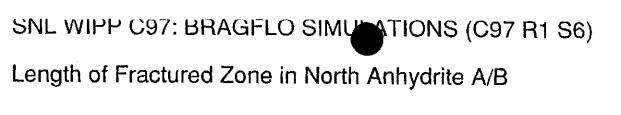


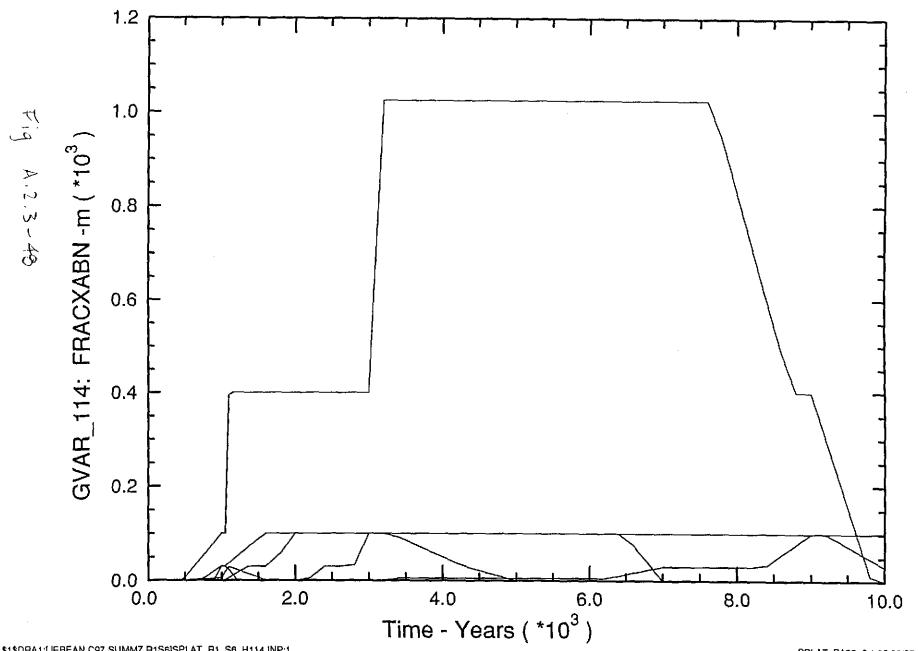
Length of Fractured Zone in North MB 138



\$1\$DRA1:[JE8EAN.C97.SUMMZ.R1S6]SPLAT_R1_S6_H113.INP;1

SPLAT_PA96_2 1.02 05/27/97 14:59:56



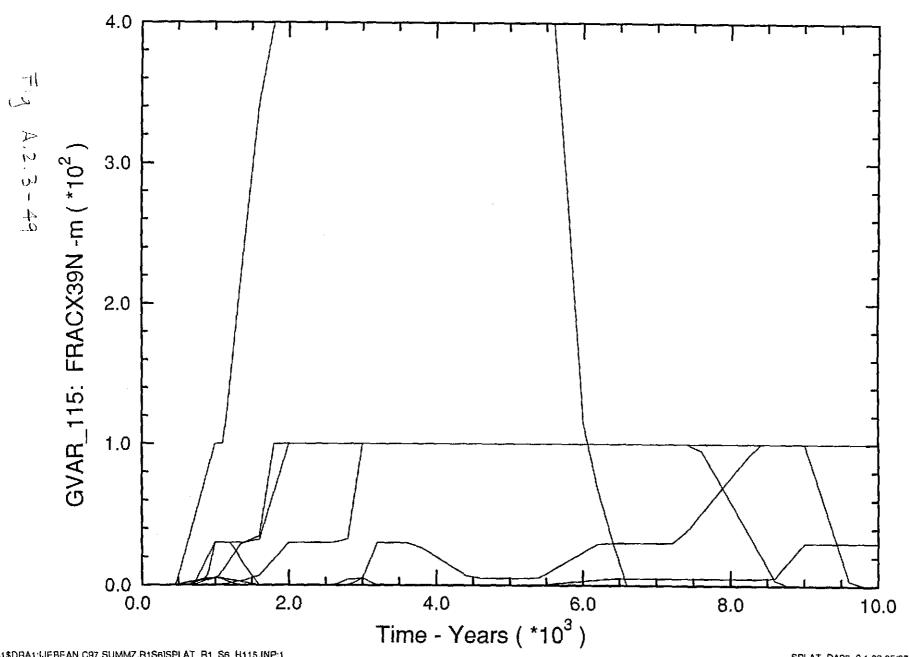


\$1\$DRA1:[JEBEAN.C97.SUMMZ.R1S6]SPLAT_R1_S6_H114.INP;1

SPLAT_PA96_2 1.02 05/27/97 15:03:14

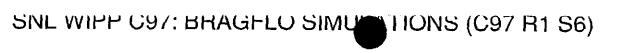


Length of Fractured Zone in North MB 139

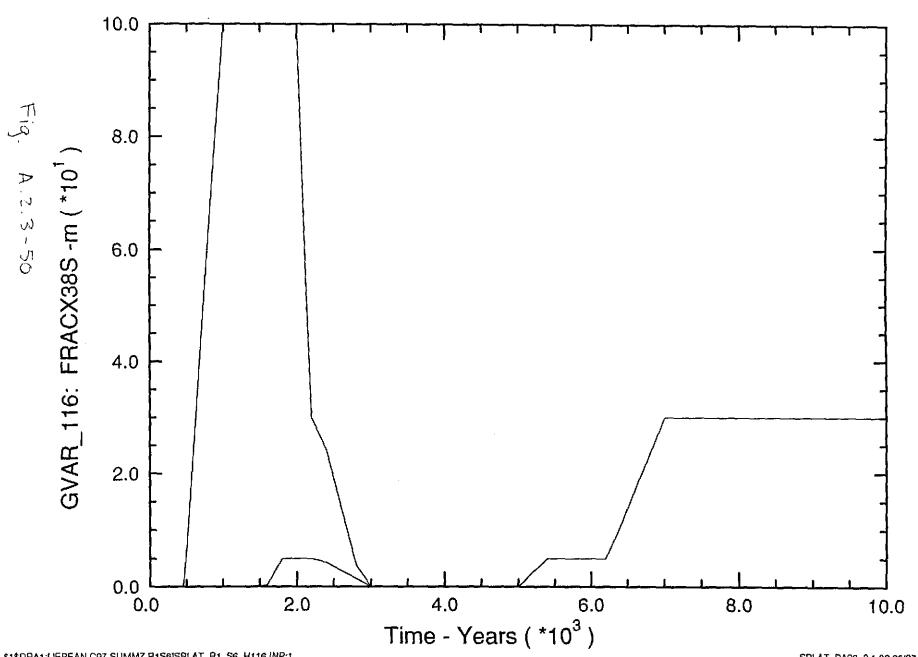


\$1\$DRA1:[JEBEAN.C97.SUMMZ.R1S6]SPLAT_R1_S6_H115.INP;1

SPLAT_PA96_2 1.02 05/27/97 15:06:45

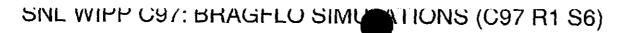


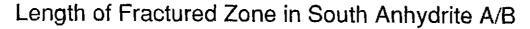
Length of Fractured Zone in South MB 138

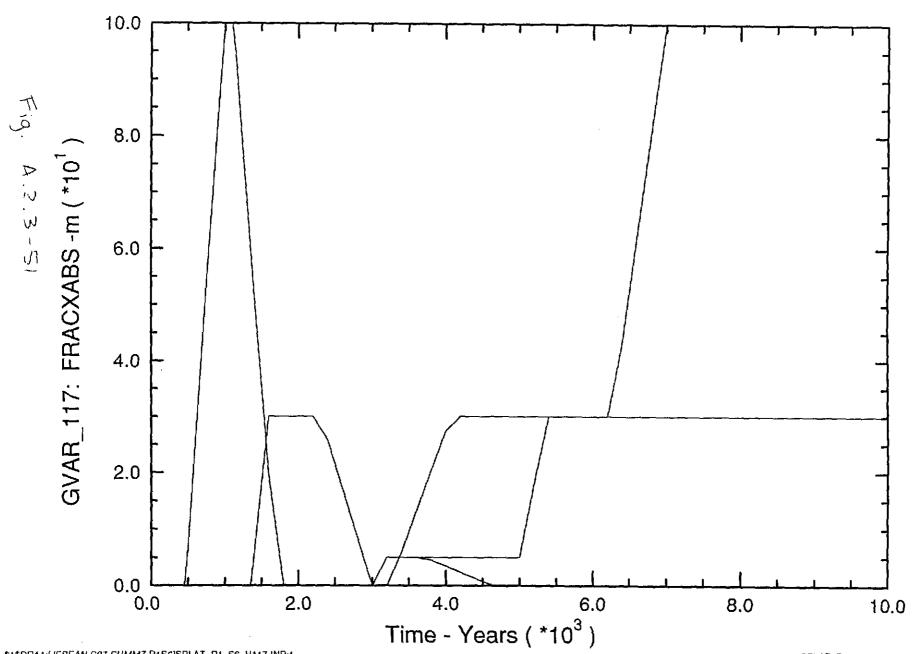


\$1\$DRA1:[JEBEAN.C97.SUMMZ.R1S6]SPLAT_R1_S6_H116.INP;1

SPLAT_PA96_2 1.02 05/27/97 15:10:16

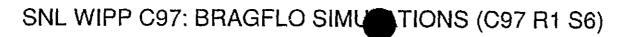




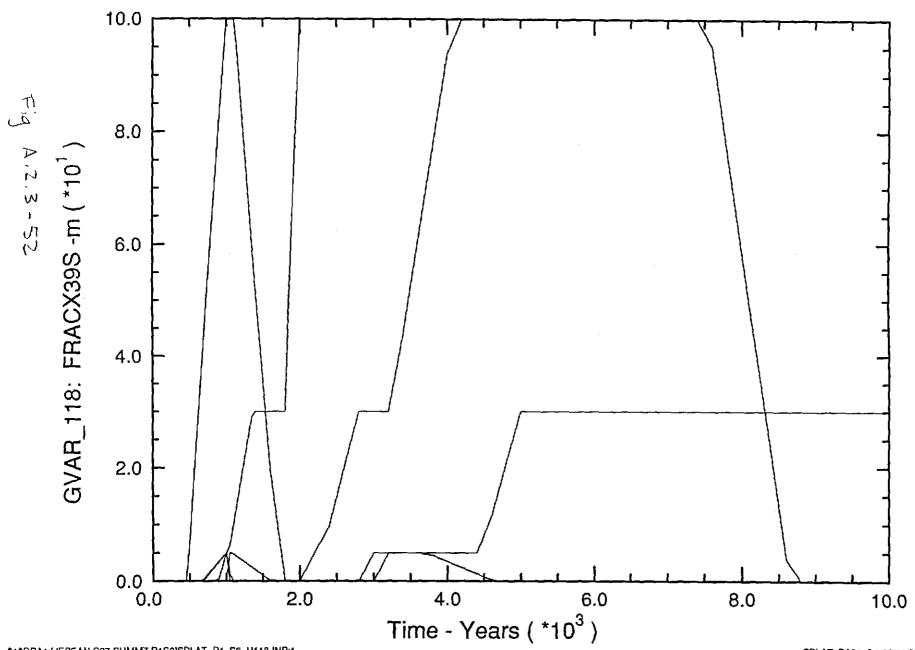


\$1\$DRA1:[JEBEAN.C97.SUMMZ.R156]SPLAT_R1_S6_H117.INP;1

SPLAT_PA96_2 1.02 05/27/97 15:13:46

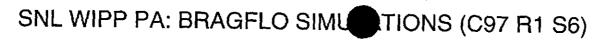


Length of Fractured Zone in South MB 139

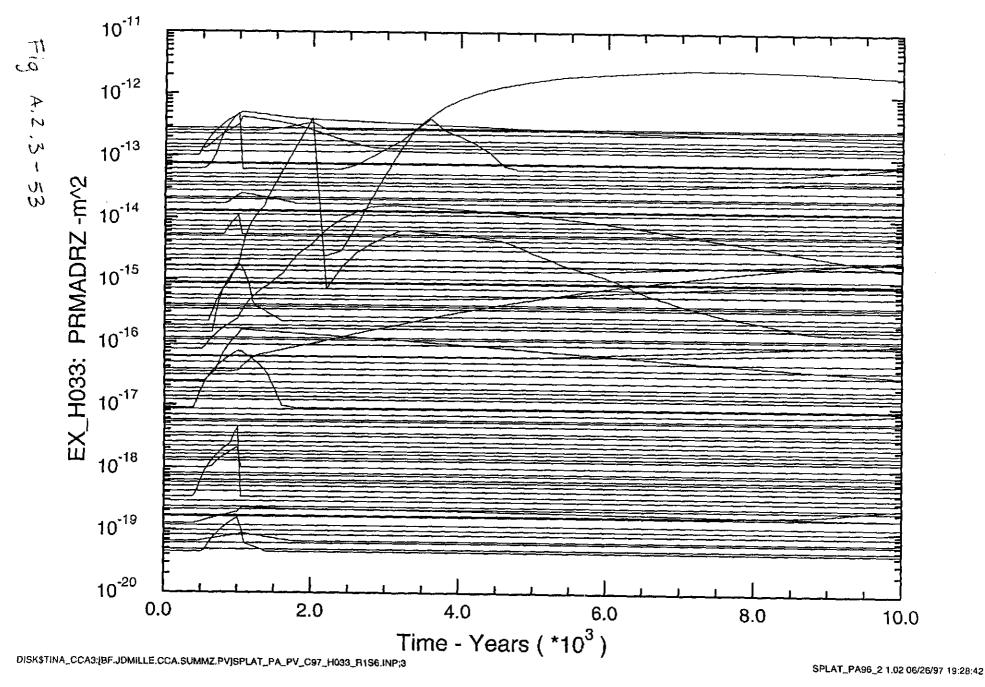


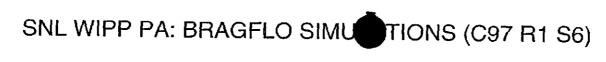
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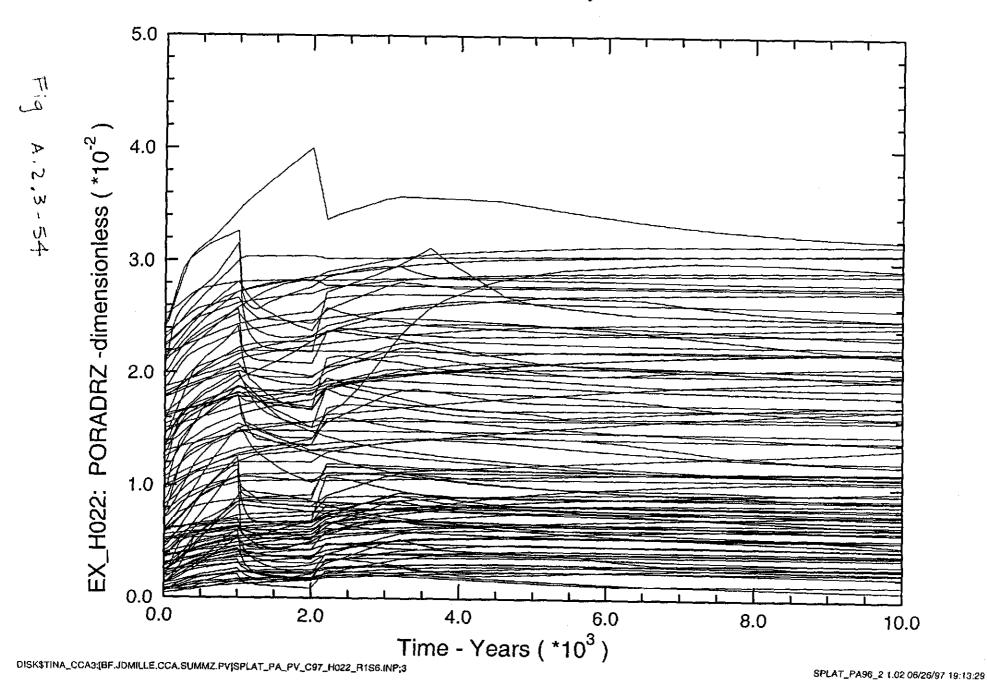


Volume-Averaged Permeability in All DRZ Layers





Volume-Averaged Porosity in All DRZ Layers



APPENDIX B

DIFFERENCES BETWEEN BRAGFLO RESULTS FROM PAVT AND CCA SIMULATIONS

B.1 SI SCENARIO

The following discussion outlines, in bullet form, the major differences in the PAVT results relative to the CCA results.

Repository Behavior

- Pressure in the waste panel plus rest of repository is higher during first 2000 years due to larger gas volume generated by higher corrosion rates. By 10,000 years pressures are slightly lower.
- Brine saturation in the waste panel plus rest of repository is lower at all times. This
 condition is due to more brine consumption at early time and lower brine inflow
 from the DRZ in realizations with low DRZ permeabilities.

Gas Generation

- More gas is generated by corrosion at early time, a similar volume is generated over 10,000 years. Steel remaining in the repository is similar but there is less steel remaining in waste panel. Gas generated by corrosion is limited both by brine and waste panel steel inventories being depleted.
- Brine consumption due to corrosion is higher at early time. By 10,000 years there are a few more high consumption vectors and a few less low consumption vectors, but the median and mean values are slightly lower.
- Gas generated by microbial is slightly less because gas generation is shut off by lack of brine in several realizations.

Halite Creep

Creep closure is not noticeably different despite higher early time pressures.

Fluid Flow

- Brine inflow to the repository is similar, a little higher at 90th percentile, a little lower at 10th percentile. These differences are due to the range in DRZ permeability, high permeability enhances inflow relative to the CCA, low permeability reduces inflow.
- Brine flow up the shaft is negligible, as in the CCA.

Two-Phase Flow

- Brine flow out of the repository is similar but has greater spread consistent with the variation in DRZ permeability. Three vectors (#24,#44,#22) have rapid (within 200 years) outflow. These vectors have high DRZ permeability, high brine saturation, and low residual brine saturation. Additionally, there are a few more vectors with greater than 10,000 m³ outflow at 10,000 years and a few more vectors with zero outflow.
- Brine flow into the DRZ from the marker beds is similar but the maximums are not as high because of the higher repository pressures at early time. Note that one CCA vector is much higher than all others.
- Brine flow out of the DRZ to the marker beds is also similar with 2 vectors higher than the CCA maximum. These two vectors have flow increases at 2000 years (#58) and 4000 years (#51), respectively, coincident with significant fracturing in the DRZ and marker beds.
- Brine flow to the Land-Withdrawal Boundary is slightly less (only 3 vectors with greater than 5 m³), although 1 vector (#38) is much larger (3300 m³) than the CCA maximum. The high flow to the LWB in vector #38 is due to the combination of very high DRZ and marker bed permeabilities, a high pressure at 1000 years, a very low DRZ porosity, and a low far-field pressure.
- Gas flow from DRZ into the marker beds is lower.

Mechanical Response

- Significant DRZ fracturing in about 20% of the realizations. Three realizations (#51, #58, #28) result in DRZ permeabilities greater than 1x10⁻¹¹ m² and porosities greater than 0.03.
- Marker Bed fracture lengths are shorter.

B.2 S3 SCENARIO

The following discussion outlines, in bullet form, the major differences in the PAVT results relative to the CCA results.

Repository Behavior

- Pressure in the waste panel plus rest of repository is higher during first 1200 years due to larger gas volume generated by higher corrosion rates. After intrusion there are more realizations with intermediate (7-10 MPa) and higher (12-14 MPa) pressures. These realizations correspond to low borehole permeabilities. There are more high pressure realizations because the low end of the log permeability range was changed from -14 to -16.3.
- Brine saturation in the waste panel and waste panel plus rest of repository tends to be lower at all times. This condition is due to more brine consumption at early time and lower brine inflow from the DRZ in realizations with low DRZ permeabilities and lower downward flow from overlying formations in realizations with low borehole permeabilities.

Gas Generation

- More gas is generated at early time (due to higher corrosion rate), a similar volume (15 % more) is generated over 10,000 years. Steel remaining in the repository is lower, 2 % vs 17%.
- Gas generated by microbial is nearly identical, nine realizations have cellulose remaining at 10,000 years.

Halite Creep

• Slightly higher 10,000 year porosities corresponding to vectors that had high post-intrusion repository pressures (> 13 MPa) due to low borehole permeabilities.

Fluid Flow

• Brine inflow to the repository is similar prior to intrusion, a little higher at 90th percentile, a little lower at 10th percentile. These differences are due to the range in DRZ permeability, high permeability enhances inflow relative to the CCA, low permeability reduces inflow. The inflow following intrusion is lower because of i) reduced inflow down the borehole due to lower borehole permeabilities, and ii) reduced inflow from DRZ and marker beds due to higher pressures in the repository.

- Brine flow up the shaft is similar and negligible.
- Brine flows and in particular maximum brine flows up the borehole are higher. The maximums are higher because they have high borehole permeabilities and high initial Castile pressures. Overall, brine flows tend to be higher because the brine reservoir is significantly larger.

Two-Phase Flow

- Brine flow out of the repository prior to intrusion is similar but has greater spread consistent with the variation in DRZ permeability. Three vectors (#24,#44,#22) have rapid (within 200 years) outflow. These vectors have high DRZ permeability, high brine saturation, and low residual brine saturation. Brine outflow following intrusion is lower due to lower borehole permeabilities and lower brine saturations.
- Brine flow into the DRZ from the marker beds is lower due to higher repository pressures.
- Brine flow out of the DRZ to the marker beds is higher due to higher repository pressures.
- Only one vector (#38) showed significant flow to the Land Withdrawal Boundary. The flow (2630 m³) was much larger than the CCA maximum (1.3 m³). The high flow to the LWB in vector #38 is due to the combination of very high DRZ and marker bed permeabilities, low borehole permeability, a very low DRZ porosity, and a low far-field pressure.
- Gas flow volumes up the borehole are similar but several maximums are larger.
- Gas flow volumes from the DRZ into the marker beds are higher.

Mechanical Response

- Significant DRZ fracturing in only about 20 realizations. Only three realizations (#28, #51, #58) had a DRZ permeability greater than 1x10⁻¹¹ m² and a porosity greater than 0.03.
- Marker Bed fracturing occurs in about the same number of realizations but in two realizations fracture lengths to the north in marker beds 139 and a and b are much longer (#58, #61).

B.3 S5 SCENARIO

The following discussion outlines, in bullet form, the major differences in the PAVT results relative to the CCA results.

Repository Behavior

- Pressure in the waste panel plus rest of repository is higher during first 1200 years due to larger gas volume generated by higher corrosion rates. After intrusion there are more realizations with intermediate (7-10 MPa) and high (12-14 MPa) pressures. These realizations correspond to low borehole permeabilities. There are more realizations because the low end of the log permeability range was changed from -14 to -16.3.
- Brine saturation in the waste panel plus rest of repository is lower at all times. This condition is due to more brine consumption at early time and lower brine inflow from the DRZ in realizations with low DRZ permeabilities. Brine inflow is also lower due to higher repository pressures.

Gas Generation

- More gas is generated at early time (due to higher corrosion rate), a similar volume (slightly lower) is generated over 10,000 years. Steel remaining in the repository is similar except for one realization (#28) that has only 3% remaining.
- Maximum brine consumption at 10,000 years is slightly higher. By 10,000 years there are a few more high-consumption and a few less low-consumption vectors.
- Gas generated by microbial is slightly less, nine realizations have cellulose remaining at 10,000 years.

Halite Creep

• Slightly higher 10,000 year porosities corresponding to vectors that had high postintrusion repository pressures (> 13 MPa) due to low borehole permeabilities.

Fluid Flow

Brine inflow to the repository is similar prior to intrusion, a little higher at 90th percentile, a little lower at 10th percentile. These differences are due to the range in DRZ permeability, high permeability enhances inflow relative to the CCA, low permeability reduces inflow. The inflow following intrusion is lower because of i) reduced inflow down the borehole due to lower borehole permeabilities, and ii) reduced inflow from DRZ and marker beds due to higher pressures in the

repository.

- Brine flow up the shaft is similar and negligible.
- The maximum brine flows up the borehole are lower but more realizations have non-zero flow. The maximums are lower because of the changes to the DRZ permeability. In the CCA most of the brine flow out of the repository flowed up the borehole. Additional brine flowed into the borehole from the DRZ. In the PAVT there is no additional brine contribution from DRZ to the borehole (maximums occur in realizations with high borehole permeability and low DRZ permeability). In cases where the DRZ permeability is high, the repository pressures tend to be lower and there is not as much of a driving force for brine up the borehole.

Two-Phase Flow

- Brine flow out of the repository prior to intrusion is similar but has greater spread consistent with the variation in DRZ permeability. Three vectors (#24,#44,#22) have rapid (within 200 years) outflow. These vectors have high DRZ permeability, high brine saturation, and low residual brine saturation. Brine outflow following intrusion is lower due to lower borehole permeabilities and lower brine saturations.
- Brine flow into the DRZ from the marker beds is lower due to higher repository pressures.
- Brine flow out of the DRZ to the marker beds is higher due to higher repository pressures.
- Only one vector (#38) showed significant flow to the Land Withdrawal Boundary. The flow (2735 m³) was much larger than the CCA maximum (1.3 m³). The high flow to the LWB in vector #38 is due to the combination of very high DRZ and marker bed permeabilities, a high pressure at 1000 years (caused in part by low borehole permeability), a very low DRZ porosity, and a low far-field pressure.
- Gas flow up borehole has similar maximums but lower minimums. Lower minimums are due to lower borehole permeabilities at low end of range.
- Gas flow from the DRZ into the marker beds is higher.

Mechanical Response

- Significant DRZ fracturing in only about 3 realizations. Only one realization (#58) had a DRZ permeability greater than 1x10⁻¹² m² and a porosity greater than 0.03.
- Marker Bed fracture lengths are longer and occur in a few more realizations.

B.4 S6 SCENARIO

The following discussion outlines, in bullet form, the major differences in the PAVT results relative to the CCA results.

Repository Behavior

- Pressure in the waste panel plus rest of repository is higher during first 1000 years due to larger gas volume generated by higher corrosion rates. After the second intrusion there are more realizations with intermediate (7-10 MPa) and higher (12-14 MPa) pressures. These realizations correspond to low borehole permeabilities. There are more high pressure realizations because the low end of the log permeability range was changed from -14 to -16.3. Also, pressure in the brine reservoir remains higher because of the much larger brine reservoir volume.
- Brine saturation in the waste panel plus rest of repository tends to be lower for all times, especially prior to the second intrusion. This condition is due to more brine consumption at early time and lower brine inflow from the DRZ in realizations with low DRZ permeabilities and lower downward flow from overlying formations in realizations with low borehole permeabilities.

Gas Generation

- More gas is generated at early time (due to higher corrosion rate), a similar volume (10 % more) is generated over 10,000 years. Steel remaining in the repository is lower, 0 % vs 4%.
- Gas generated by microbial is nearly identical, nine realizations have cellulose remaining at 10,000 years.

Halite Creep

• Slightly higher 10,000 year porosities corresponding to vectors that had high postintrusion repository pressures (> 13 MPa) due to low borehole permeabilities.

Fluid Flow

Brine inflow to the repository is similar prior to the first intrusion, a little higher at 90th percentile, a little lower at 10th percentile. These differences are due to the range in DRZ permeability, high permeability enhances inflow relative to the CCA, low permeability reduces inflow. The inflow following the first intrusion is lower because of i) reduced inflow down the borehole due to lower borehole permeabilities, and ii) reduced inflow from DRZ and marker beds due to higher

pressures in the repository. Brine inflow after the second intrusion, however, is much larger due to the larger brine reservoir that doesn't deplete as readily.

- Brine flow up the shaft is similar and negligible.
- Brine flows and in particular maximum brine flows up the borehole are higher. The maximums are higher because they have high borehole permeabilities and high initial Castile pressures. Overall, brine flows tend to be higher because the brine reservoir is significantly larger.

Two-Phase Flow

- Brine flow out of the repository prior to the first intrusion is similar but has greater spread consistent with the variation in DRZ permeability. Three vectors (#24,#44,#22) have rapid (within 200 years) outflow. These vectors have high DRZ permeability, high brine saturation, and low residual brine saturation. Brine outflow after the second intrusion is higher due to brine from the larger brine reservoir.
- Brine flow into the DRZ from the marker beds is lower due to higher repository pressures.
- Brine flow out of the DRZ to the marker beds is higher due to higher repository pressures.
- Only one vector (#38) showed significant flow to the Land Withdrawal Boundary. The flow (3203 m³) was much larger than the CCA maximum (1.7 m³). The high flow to the LWB in vector #38 is due to the combination of very high DRZ and marker bed permeabilities, low borehole permeability, a very low DRZ porosity, and a low far-field pressure.
- Gas flow volumes up the borehole are similar but several maximums are larger.
- Gas flow volumes from the DRZ into the marker beds are larger.

Mechanical Response

- Significant DRZ fracturing in only about 20 realizations. Only three realizations (#28, #51, #58) had a DRZ permeability greater than 1x10⁻¹¹ m² and a porosity greater than 0.03.
- Marker Bed fracturing occurs in about the same number of realizations but in two realizations fracture lengths to the north in marker beds 139 and a and b are much longer (#58, #61).

B.5 INPUT FOR S2 SCENARIO VECTOR 78

invoked.

IJACSWITCH =

IJACRESET =

The following outlines changes to BRAGFLO input reflecting tolerance changes required to run S2 vector #78 in PAVT replicate 1 (C97 R1 S2 V078).

<u>PARAMETER</u>	<u>ORIGINAL</u>	FINAL
EPSNORM(2)	1.0E-2	1.0E-3
EPSLOOSE(1)	3.0	2.0
EPSLOOSE(2)	1.0E-2	1.0E-3
FTOLLOOSE(1)	1.0E-2	1.0
IJACSWITCH	41	0
IJACRESET	5	10
Where		
EPSNORM(2) =	Maximum relative change in brine pressure allowed over a time step.	
EPSLOOSE(1) =	Number of digits of accuracy to the right of the decimal in the change in gas saturation required for convergence when looser tolerances are invoked.	
EPSLOOSE(2) =	Same as EPSNORM(2) but used when looser tolerances are invoked.
FTOLLOOSE(1) =	Value of normalized r	residual for gas conservation equation required for oser tolerances have been invoked.

Following a non-converged step in BRAGFLO, looser tolerances are invoked for the next 10 steps. After these 10 steps the tolerances are returned to their original values.

Number of time step reductions allowed before looser tolerances are

Number of timesteps during which looser tolerances are in effect.

APPENDIX C

NUTS AND PANEL RESULTS FOR SALADO TRANSPORT

Appendix C includes the following Figures and Tables which contain results from Salado transport calculations performed using NUTS (for S1 through S5) and PANEL (for S6).

Figures

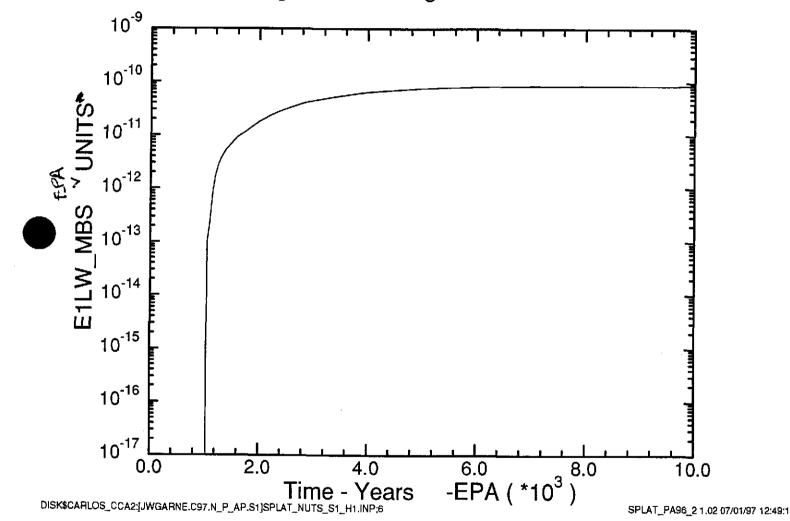
C.1 - C.7 S1 Integrated Discharge at LWB
C.8 - C.19 S2 Integrated Discharge up Borehole (t=100, 350 yrs)
C.20 - C.49 S3 Integrated Discharge up Borehole (t=1000, 3000, 5000, 7000, 9000 yrs)
C.50 - C.61 S4 Integrated Discharge up Borehole (t=100, 350 yrs)
C.62 - C.91 S5 Integrated Discharge up Borehole (t=1000, 3000, 5000, 7000, 9000 yrs)
C.92 - C.133 S6 Integrated Discharge up Borehole
(t=100,350,1000,2000,4000,6000,9000 yrs)

Tables

	-	
C.1		S1 Integrated Discharge at LWB
C.2	- C.3	S2 Integrated Discharge up Borehole (t=100, 350 yrs)
C.4	- C.8	S3 Integrated Discharge up Borehole (t=1000, 3000, 5000, 7000, 9000 yrs)
C.9		S4 Integrated Discharge up Borehole (t=100, 350 yrs)
C.11		S5 Integrated Discharge up Borehole (t=1000, 3000, 5000, 7000, 9000 yrs)
C.16	-C.22	S6 Integrated Discharge up Borehole (t=100,350,1000,2000,4000,6000,9000 yrs)

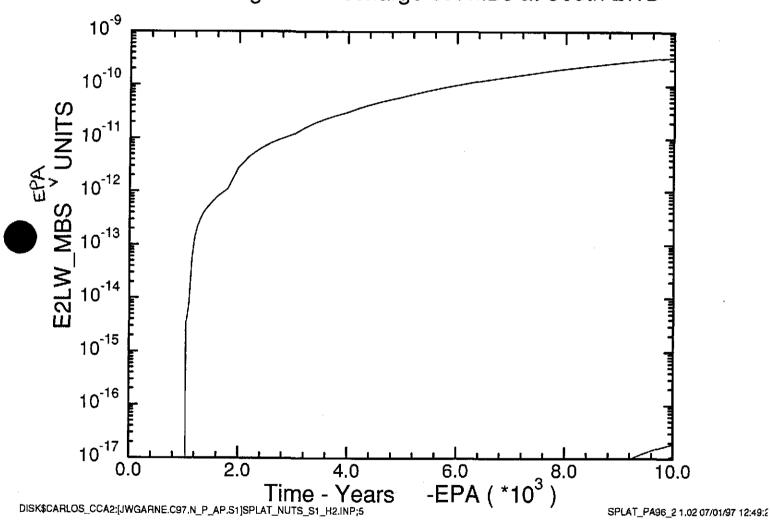
Note: Tables contain discharges for screened in vectors only.

SNL WIPP PA96: NUTS SIMULATIONS (C97 S1)
Am-241 Integrated Discharge out MBs at South LWB



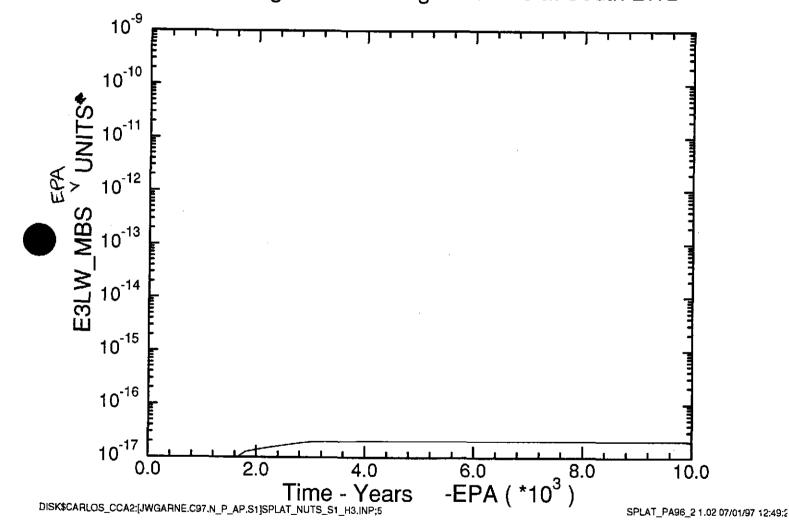
CI

SNL WIPP PA96: NUTS SIMULATIONS (C97 S1)
Pu-239 Integrated Discharge out MBs at South LWB



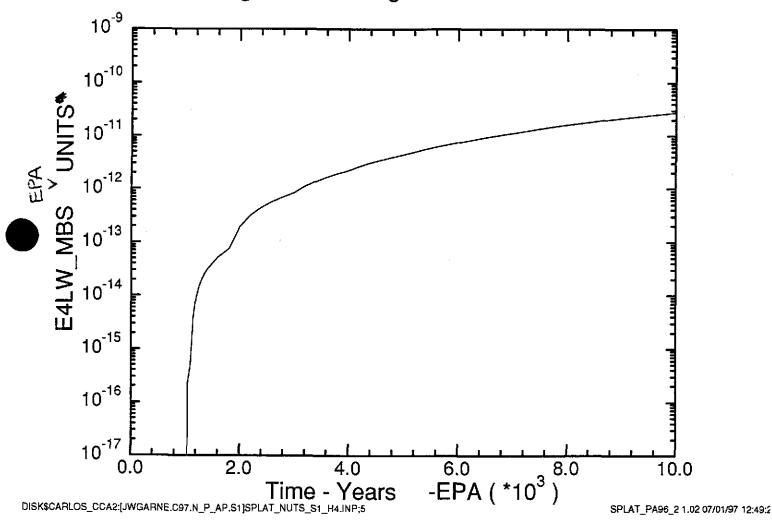
CZ

SNL WIPP PA96: NUTS SIMULATIONS (C97 S1)
Pu-238 Integrated Discharge out MBs at South LWB



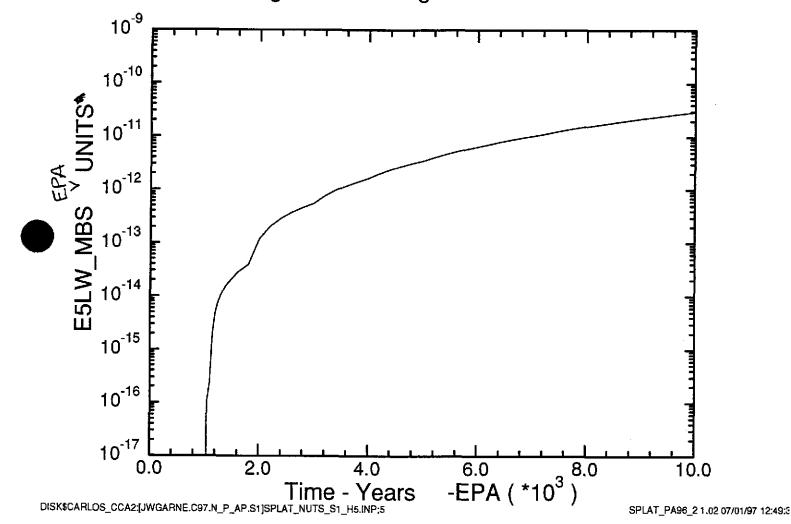
03

SNL WIPP PA96: NUTS SIMULATIONS (C97 S1) U-234 Integrated Discharge out MBs at South LWB



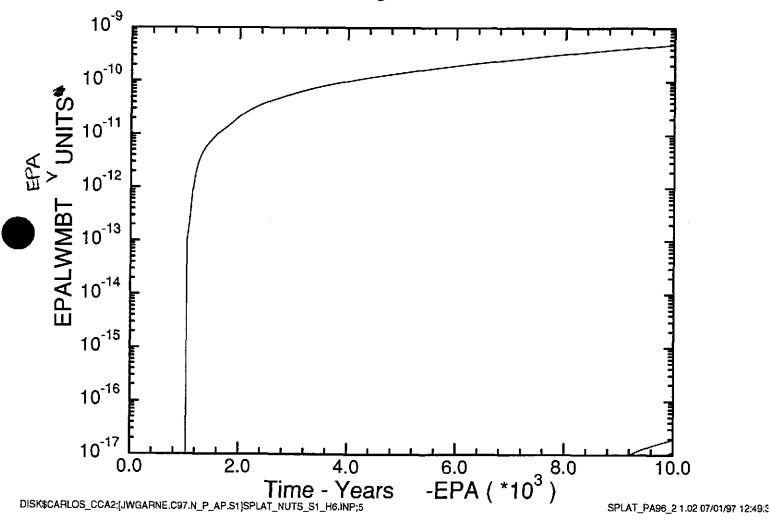
CA

SNL WIPP PA96: NUTS SIMULATIONS (C97 S1)
Th-230 Integrated Discharge out MBs at South LWB



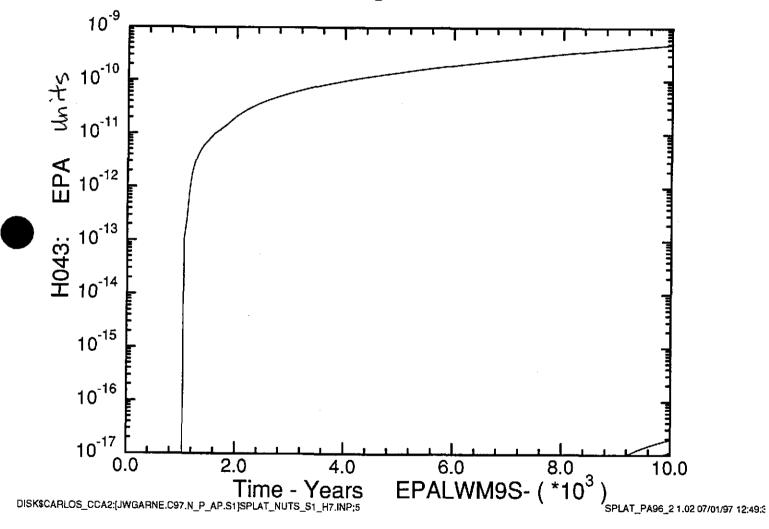
65

SNL WIPP PA96: NUTS SIMULATIONS (C97 S1) Total Integrated Discharge out MBs at South LWB



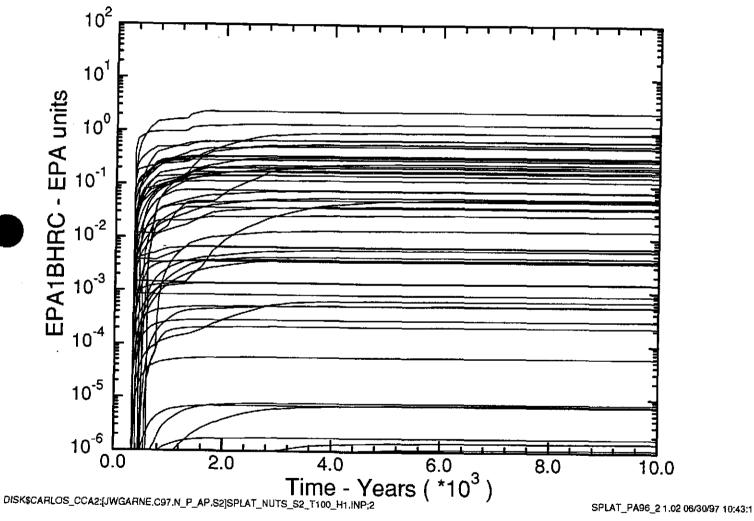
06

SNL WIPP PA96: NUTS SIMULATIONS (C97 S1)
Total Integrated Discharge out MB139 at South LWB



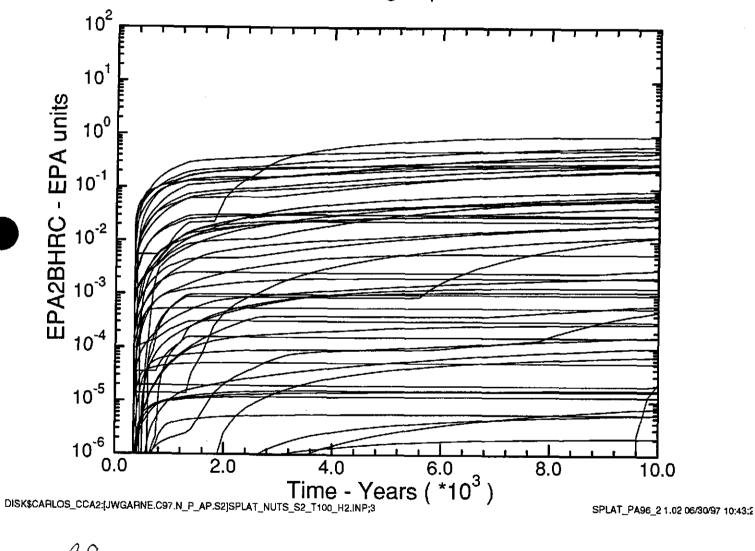
07

SNL WIPP PA96: NUTS SIMULATIONS (C97 S2 T100) Am-241 Integrated Discharge up Borehole at MB138



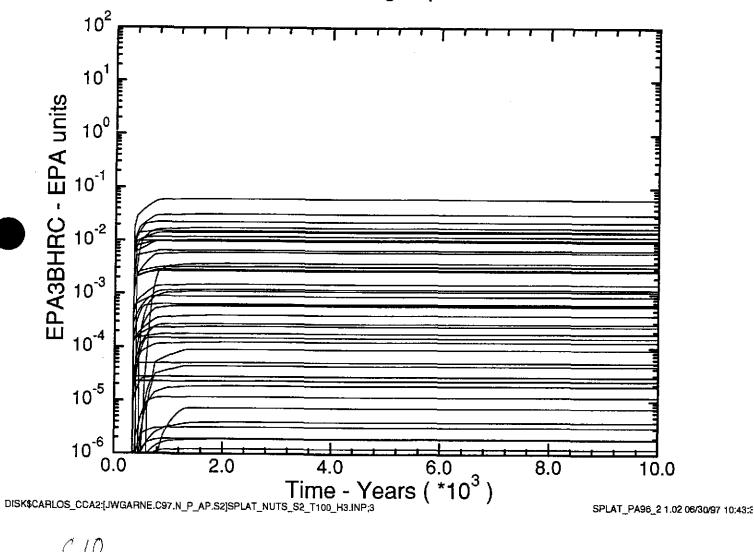
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SNL WIPP PA96: NUTS SIMULATIONS (C97 S2 T100)
Pu-239 Integrated Discharge up Borehole at MB138



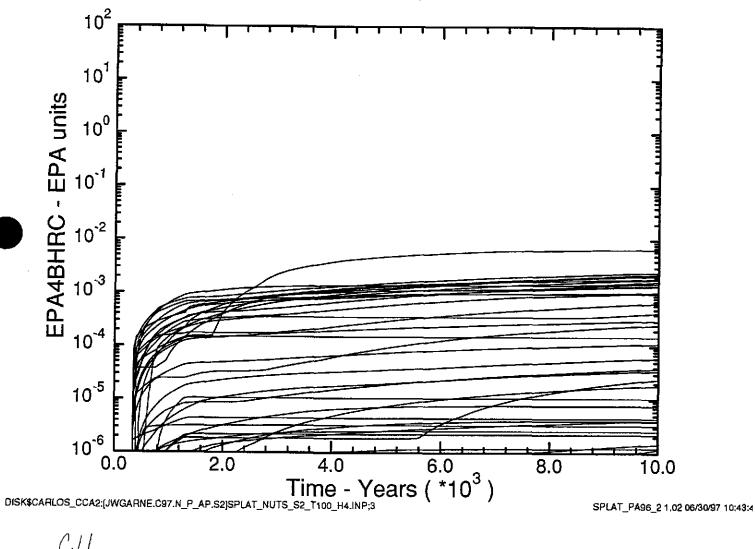
09

SNL WIPP PA96: NUTS SIMULATIONS (C97 S2 T100) Pu-238 Integrated Discharge up Borehole at MB138



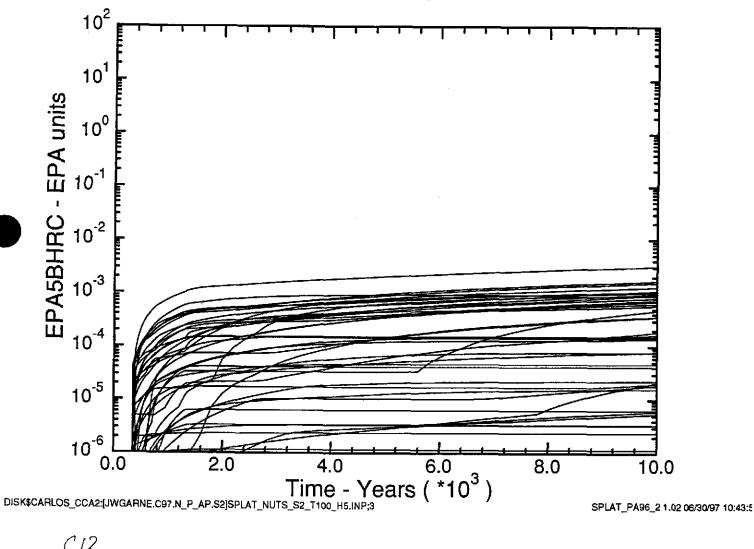
C10

SNL WIPP PA96: NUTS SIMULATIONS (C97 S2 T100) U-234 Integrated Discharge up Borehole at MB138



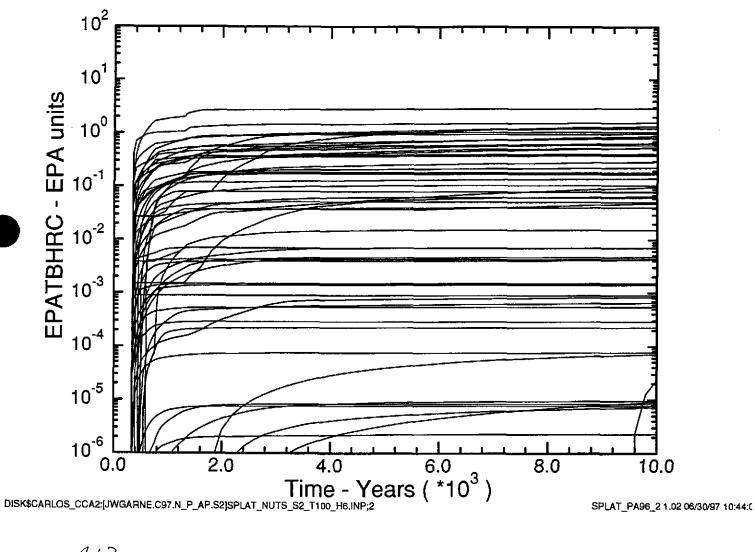
CII

SNL WIPP PA96: NUTS SIMULATIONS (C97 S2 T100) Th-230 Integrated Discharge up Borehole at MB138



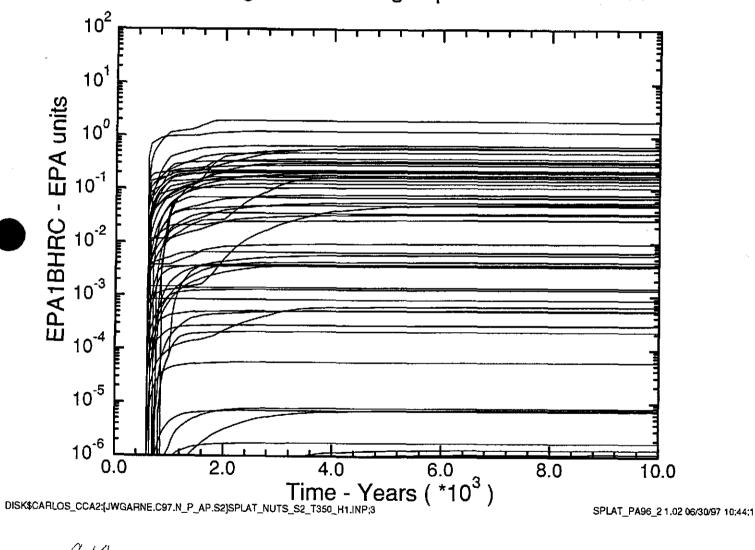
CIZ

SNL WIPP PA96: NUTS SIMULATIONS (C97 S2 T100)
Total Integrated Discharge up Borehole at MB138



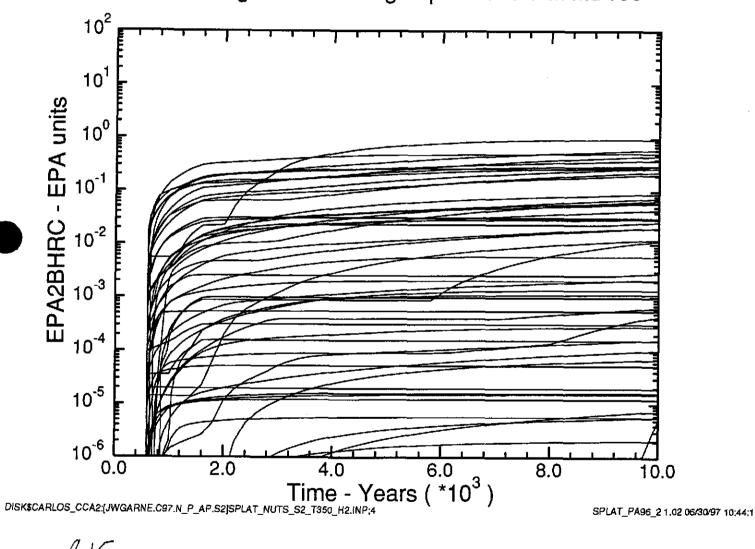
013

SNL WIPP PA96: NUTS SIMULATIONS (C97 S2 T350) Am-241 Integrated Discharge up Borehole at MB138



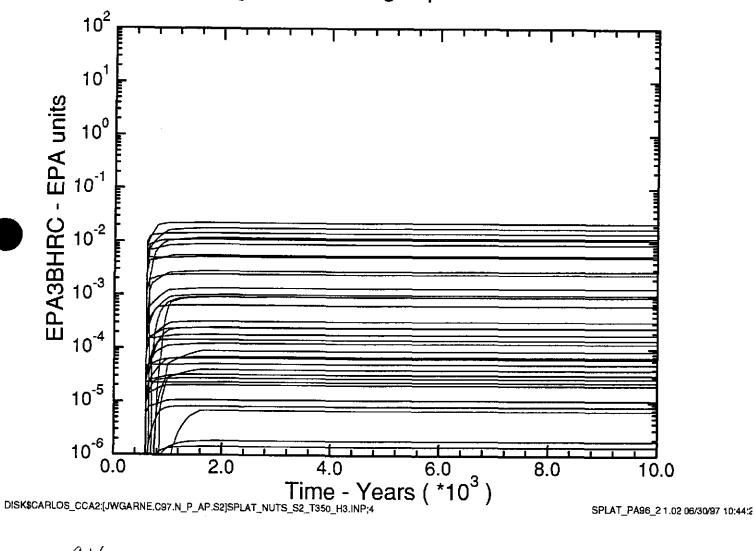
CK

SNL WIPP PA96: NUTS SIMULATIONS (C97 S2 T350) Pu-239 Integrated Discharge up Borehole at MB138



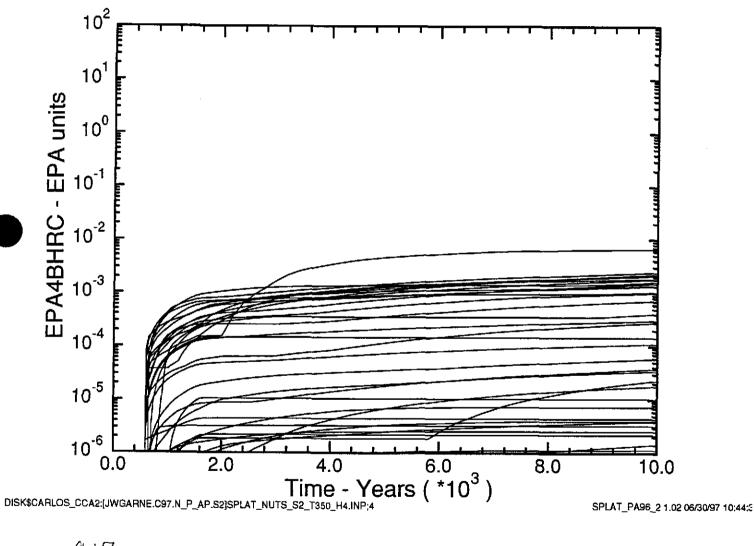
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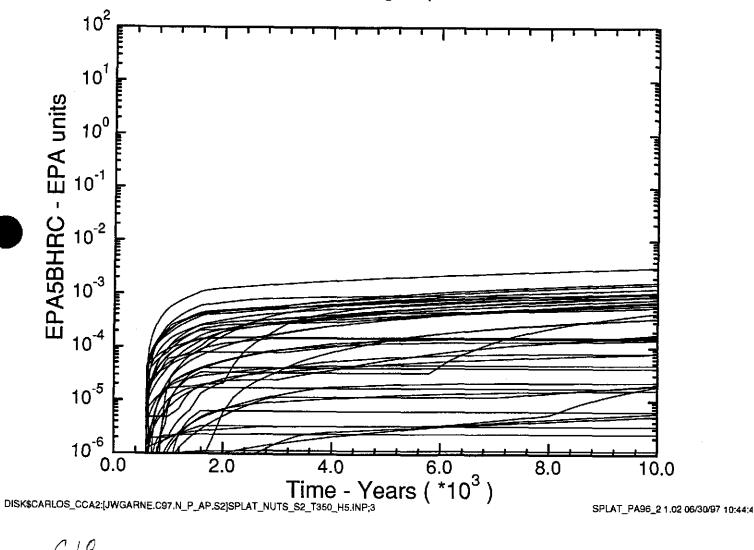
C16

SNL WIPP PA96: NUTS SIMULATIONS (C97 S2 T350) U-234 Integrated Discharge up Borehole at MB138



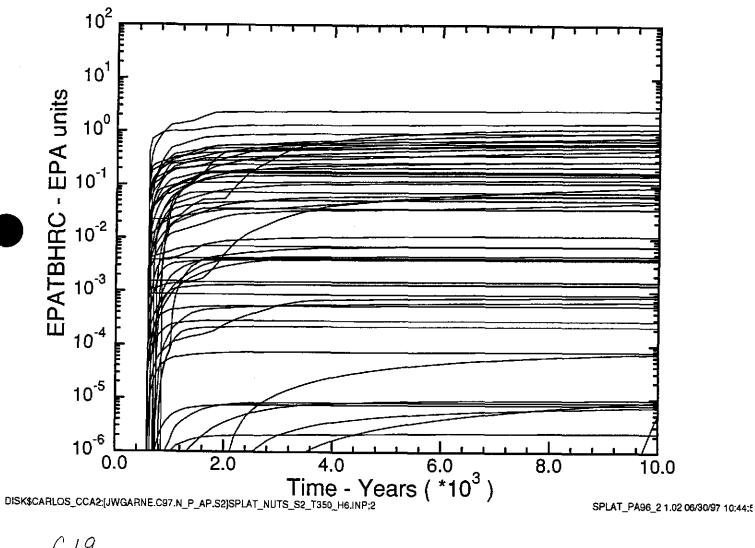
C17

SNL WIPP PA96: NUTS SIMULATIONS (C97 S2 T350) Th-230 Integrated Discharge up Borehole at MB138



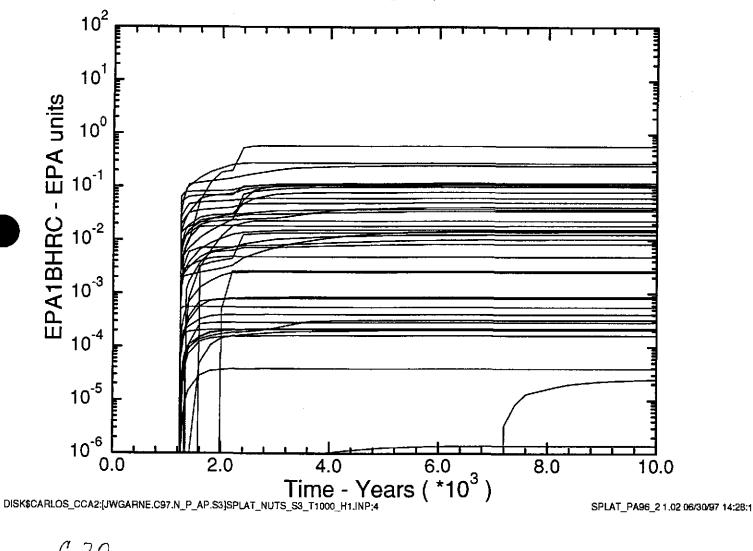
C18

SNL WIPP PA96: NUTS SIMULATIONS (C97 S2 T350) Total Integrated Discharge up Borehole at MB138



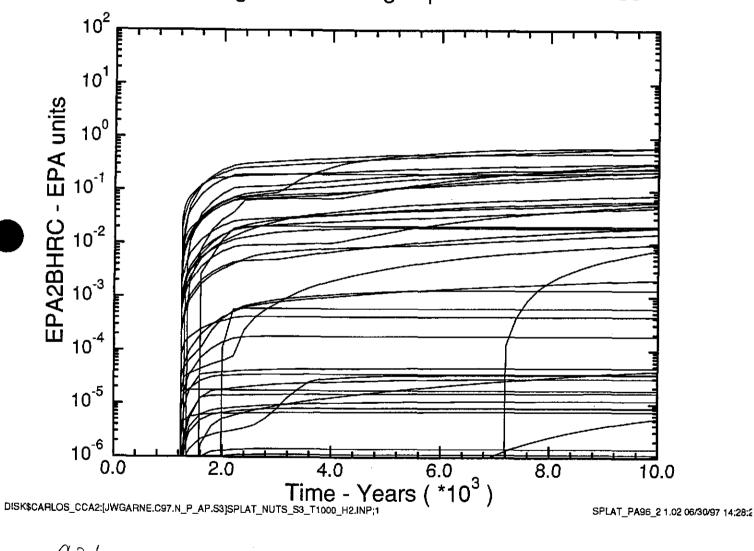
C19

SNL WIPP PA96: NUTS SIMULATIONS (C97 S3 T1000) Am-241 Integrated Discharge up Borehole at MB138



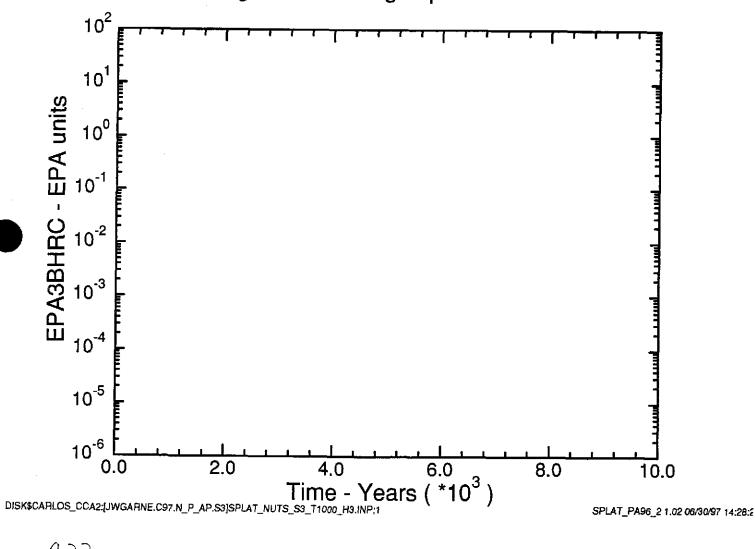
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SNL WIPP PA96: NUTS SIMULATIONS (C97 S3 T1000) Pu-239 Integrated Discharge up Borehole at MB138



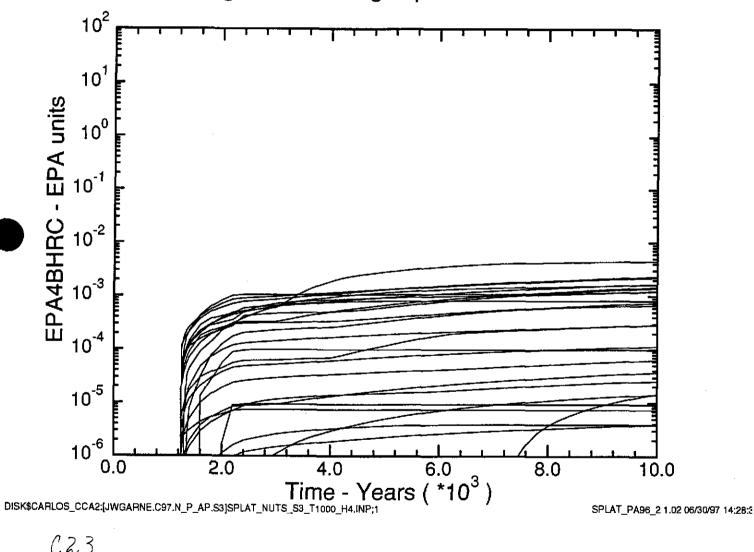
C2/

SNL WIPP PA96: NUTS SIMULATIONS (C97 S3 T1000) Pu-238 Integrated Discharge up Borehole at MB138



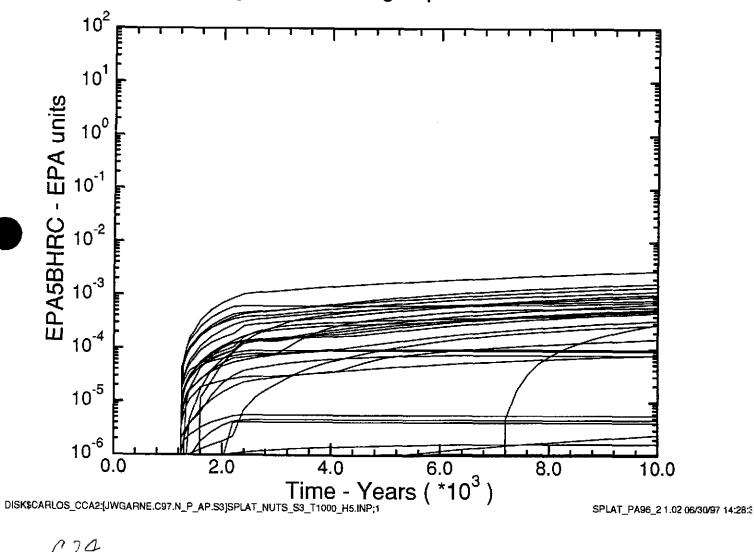
CZZ

SNL WIPP PA96: NUTS SIMULATIONS (C97 S3 T1000) U-234 Integrated Discharge up Borehole at MB138



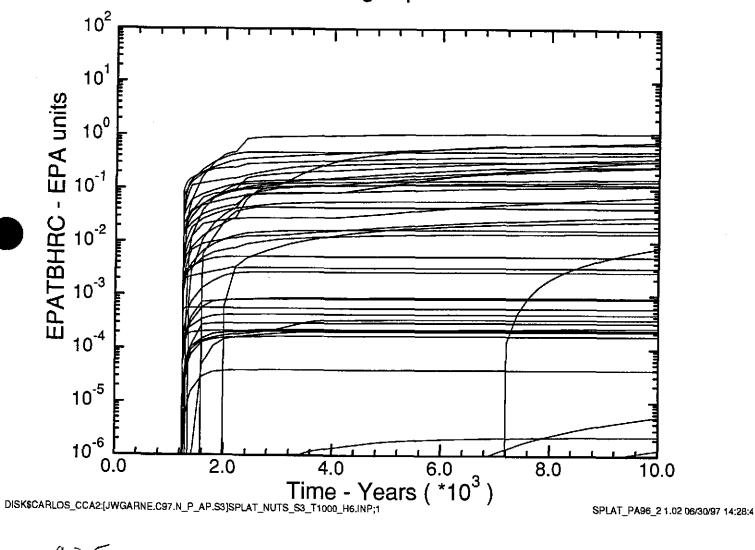
C23

SNL WIPP PA96: NUTS SIMULATIONS (C97 S3 T1000) Th-230 Integrated Discharge up Borehole at MB138



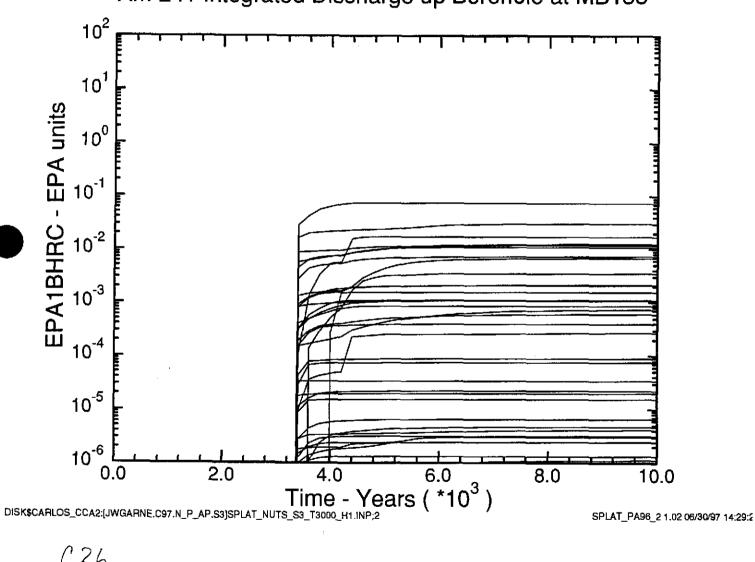
C24

SNL WIPP PA96: NUTS SIMULATIONS (C97 S3 T1000) Total Integrated Discharge up Borehole at MB138



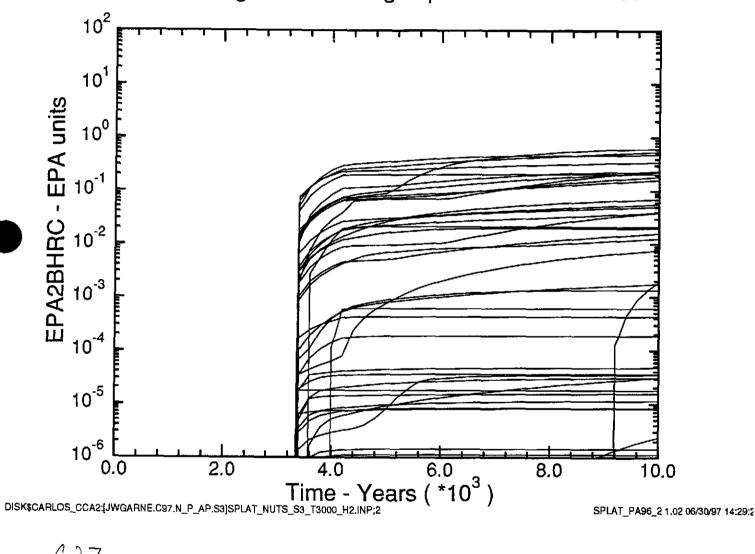
C 25

SNL WIPP PA96: NUTS SIMULATIONS (C97 S3 T3000) Am-241 Integrated Discharge up Borehole at MB138



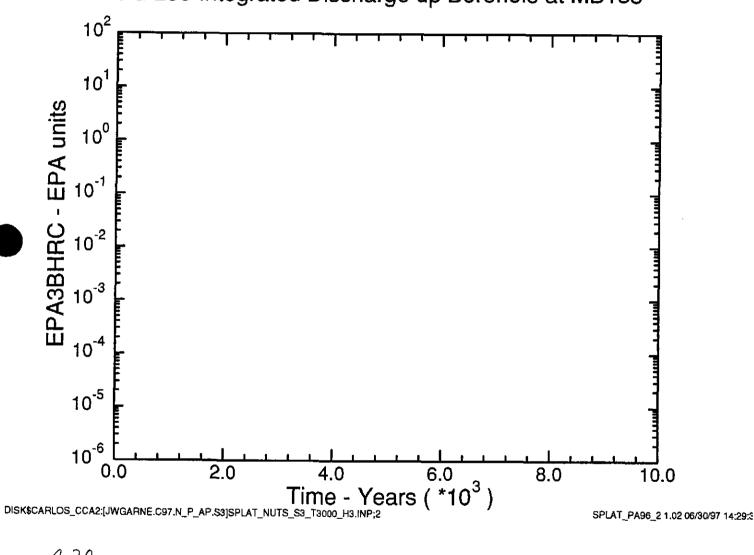
C26

SNL WIPP PA96: NUTS SIMULATIONS (C97 S3 T3000) Pu-239 Integrated Discharge up Borehole at MB138



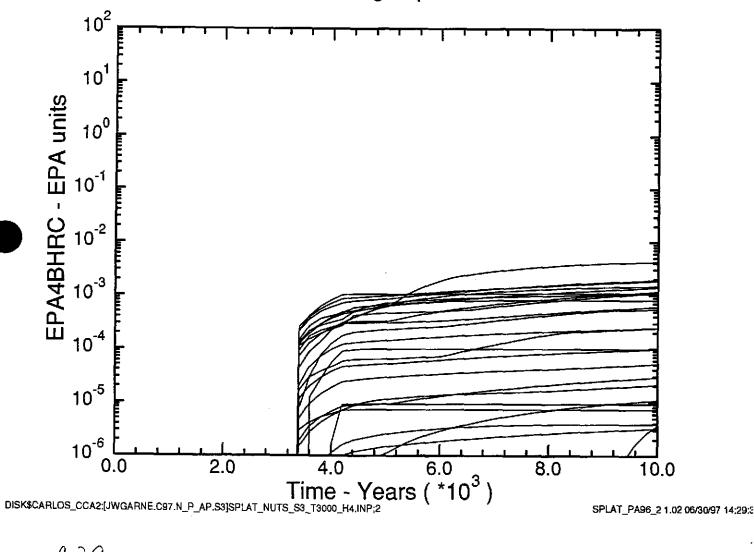
C27

SNL WIPP PA96: NUTS SIMULATIONS (C97 S3 T3000) Pu-238 Integrated Discharge up Borehole at MB138

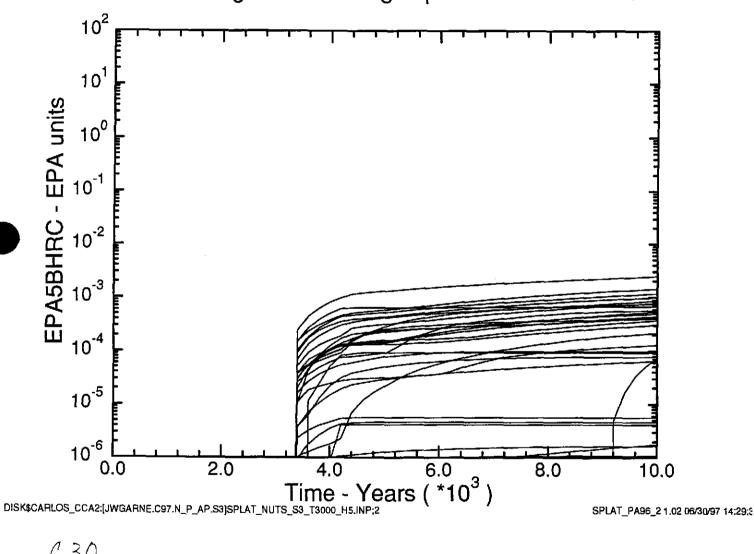


C28

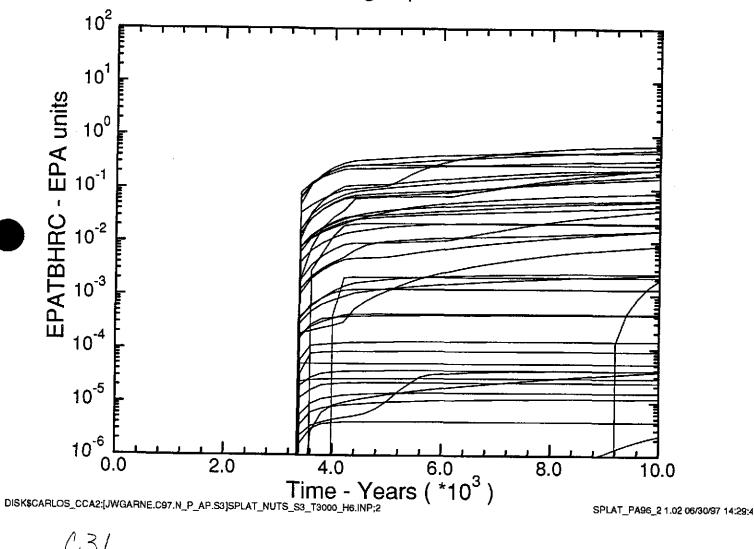
SNL WIPP PA96: NUTS SIMULATIONS (C97 S3 T3000) U-234 Integrated Discharge up Borehole at MB138



SNL WIPP PA96: NUTS SIMULATIONS (C97 S3 T3000) Th-230 Integrated Discharge up Borehole at MB138

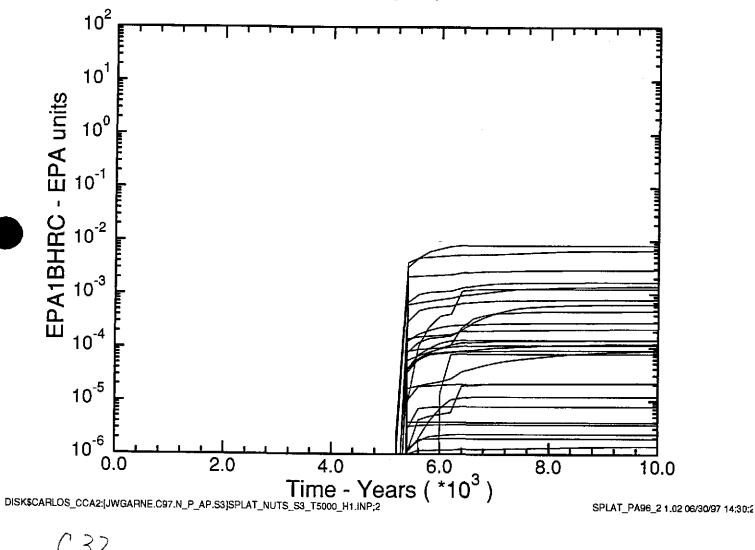


SNL WIPP PA96: NUTS SIMULATIONS (C97 S3 T3000) Total Integrated Discharge up Borehole at MB138

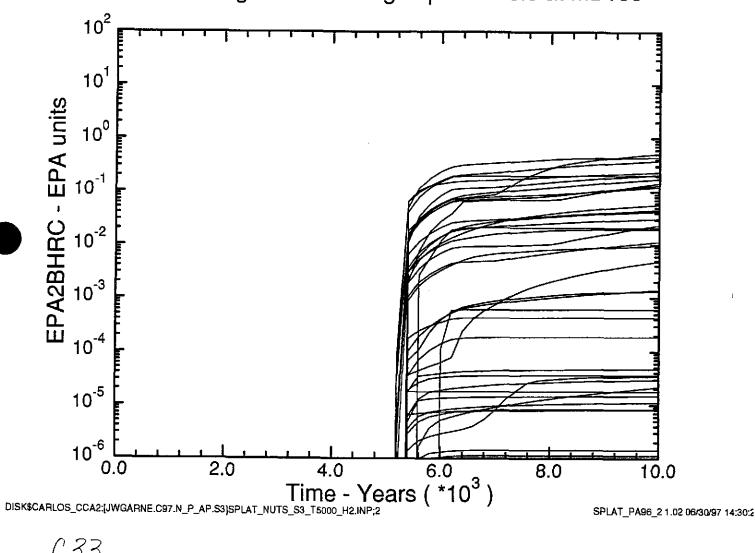


031

SNL WIPP PA96: NUTS SIMULATIONS (C97 S3 T5000) Am-241 Integrated Discharge up Borehole at MB138



SNL WIPP PA96: NUTS SIMULATIONS (C97 S3 T5000) Pu-239 Integrated Discharge up Borehole at MB138



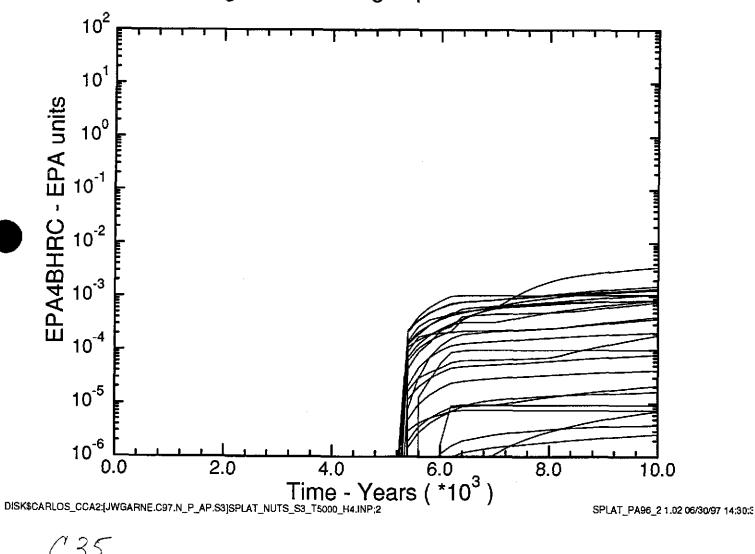
C33

SNL WIPP PA96: NUTS SIMULATIONS (C97 S3 T5000) Pu-238 Integrated Discharge up Borehole at MB138 10² 10¹ **EPA3BHRC** - **EPA** units 10⁰ 10⁻¹ 10⁻² 10⁻⁵ 10⁻⁶ 0.0 2.0 4.0 6.0 8.0 10.0 Time - Years (*10³)

SPLAT_PA96_2 1.02 06/30/97 14:30:2

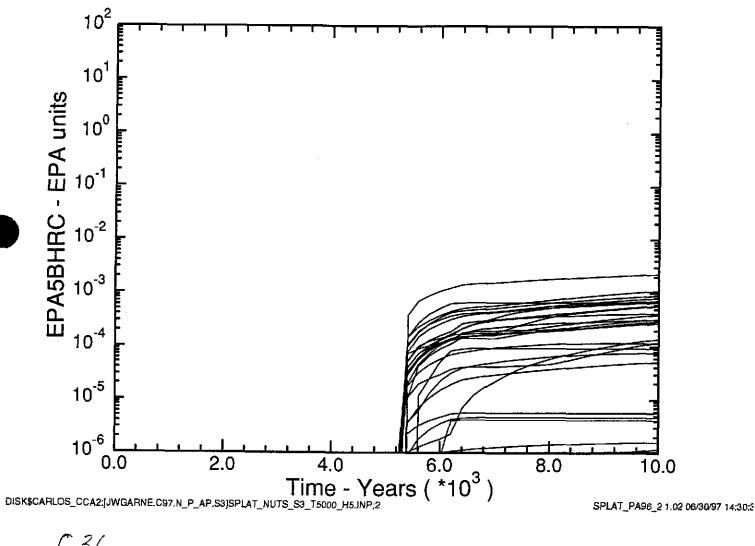
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SNL WIPP PA96: NUTS SIMULATIONS (C97 S3 T5000) U-234 Integrated Discharge up Borehole at MB138

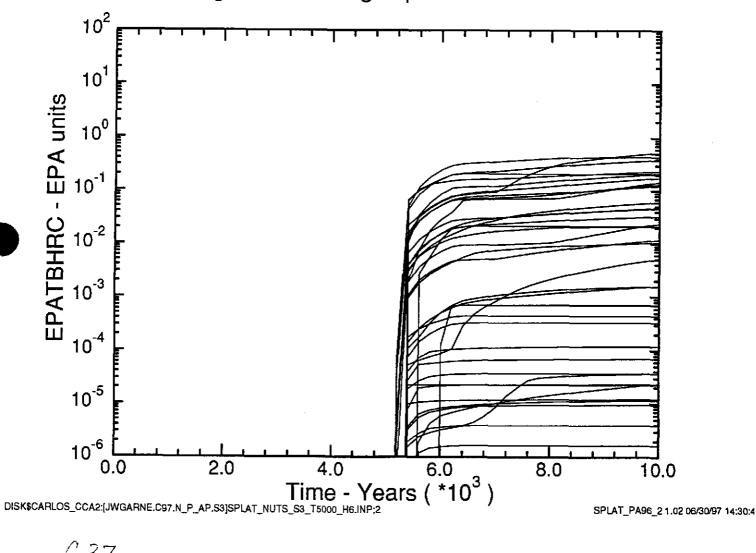


C35

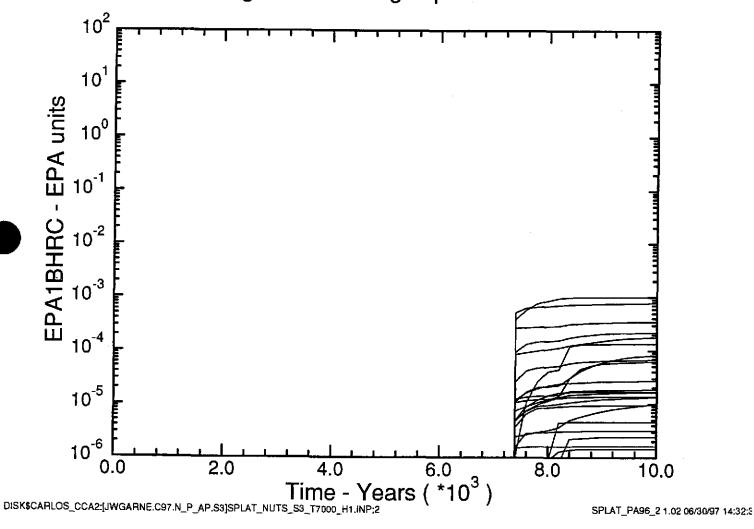
SNL WIPP PA96: NUTS SIMULATIONS (C97 S3 T5000) Th-230 Integrated Discharge up Borehole at MB138



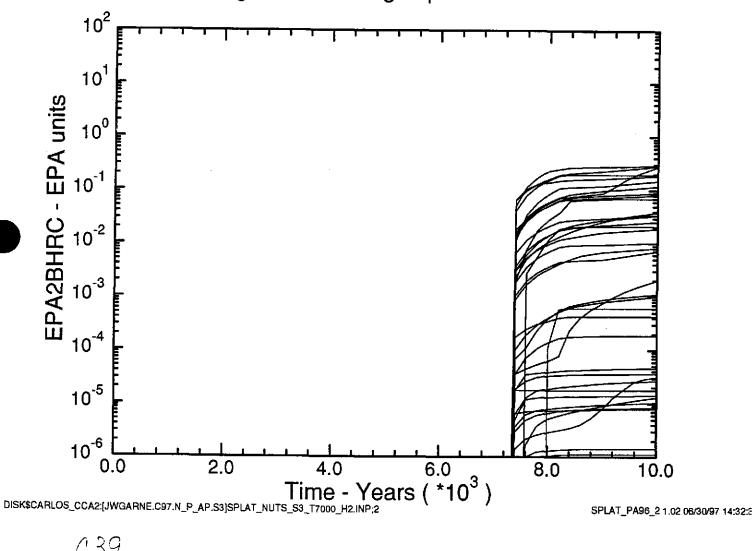
SNL WIPP PA96: NUTS SIMULATIONS (C97 S3 T5000) Total Integrated Discharge up Borehole at MB138



SNL WIPP PA96: NUTS SIMULATIONS (C97 S3 T7000) Am-241 Integrated Discharge up Borehole at MB138

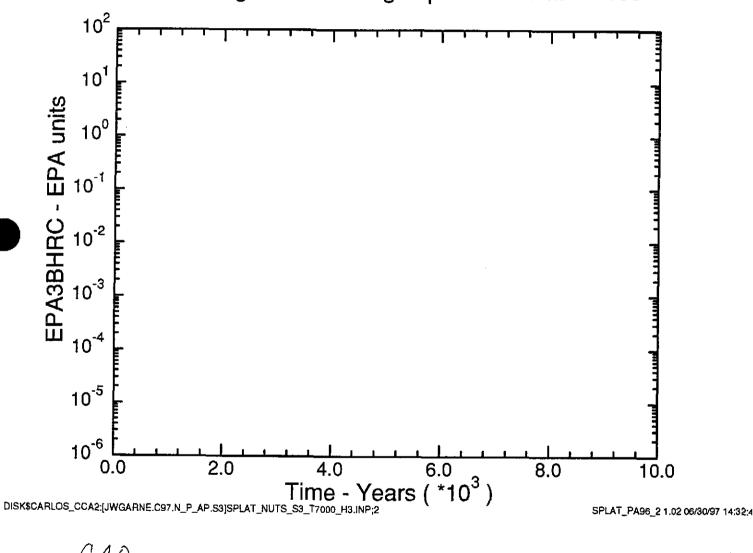


SNL WIPP PA96: NUTS SIMULATIONS (C97 S3 T7000) Pu-239 Integrated Discharge up Borehole at MB138



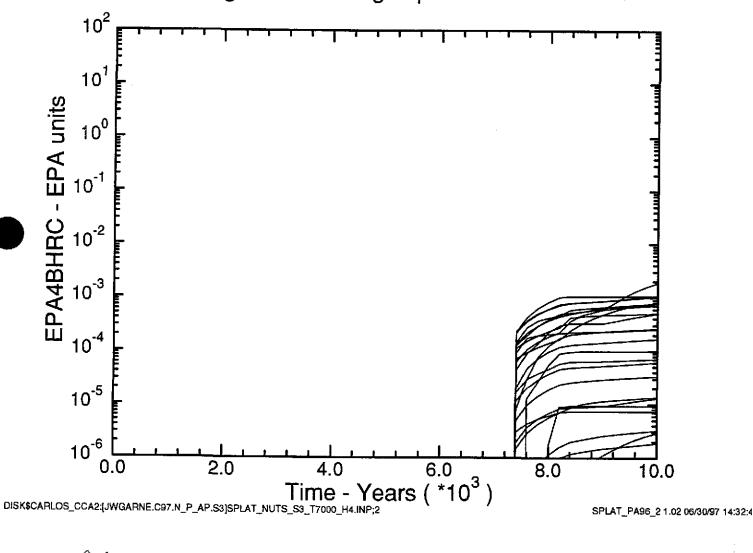
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SNL WIPP PA96: NUTS SIMULATIONS (C97 S3 T7000) Pu-238 Integrated Discharge up Borehole at MB138



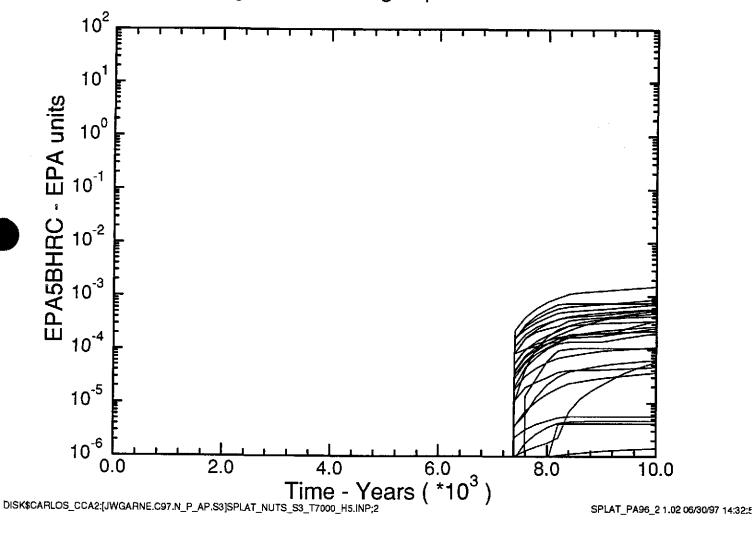
C40

SNL WIPP PA96: NUTS SIMULATIONS (C97 S3 T7000) U-234 Integrated Discharge up Borehole at MB138



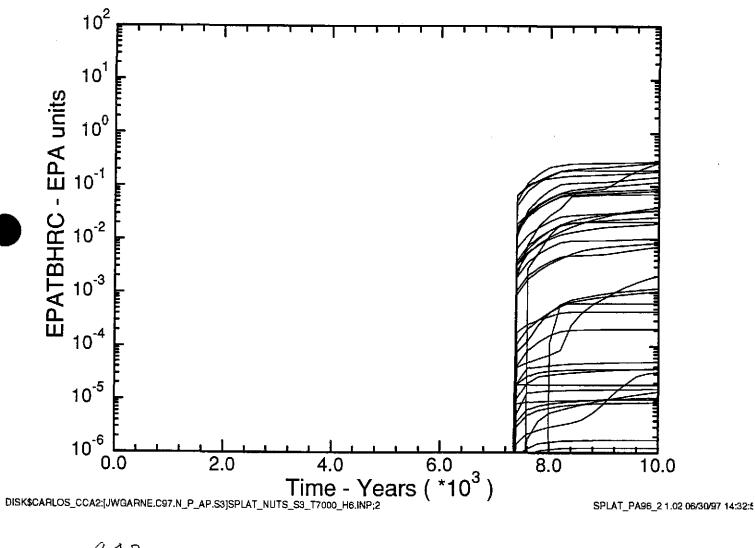
C41

SNL WIPP PA96: NUTS SIMULATIONS (C97 S3 T7000)
Th-230 Integrated Discharge up Borehole at MB138



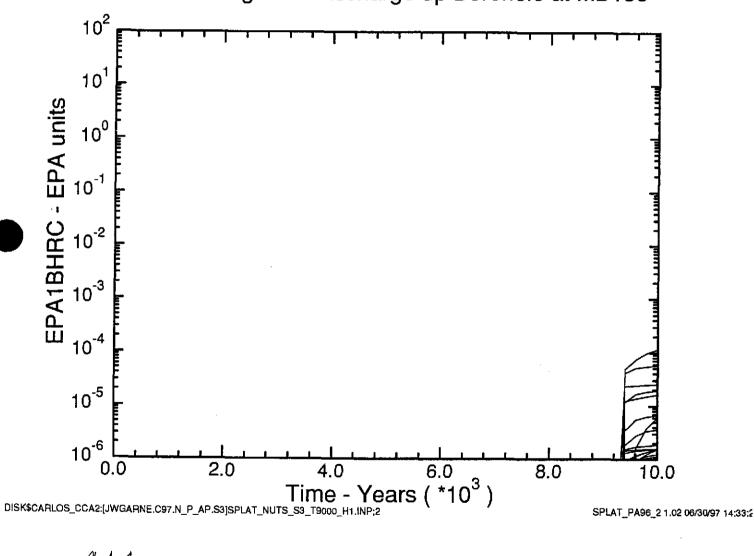
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SNL WIPP PA96: NUTS SIMULATIONS (C97 S3 T7000) Total Integrated Discharge up Borehole at MB138



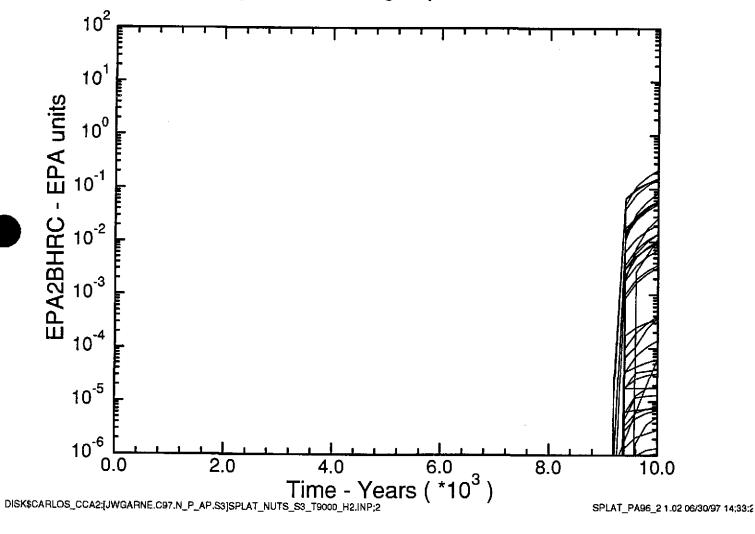
C43

SNL WIPP PA96: NUTS SIMULATIONS (C97 S3 T9000) Am-241 Integrated Discharge up Borehole at MB138



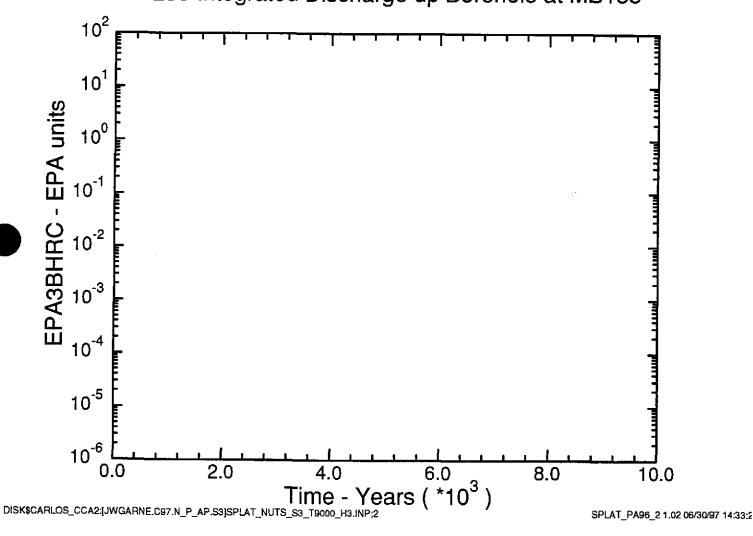
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SNL WIPP PA96: NUTS SIMULATIONS (C97 S3 T9000) Pu-239 Integrated Discharge up Borehole at MB138



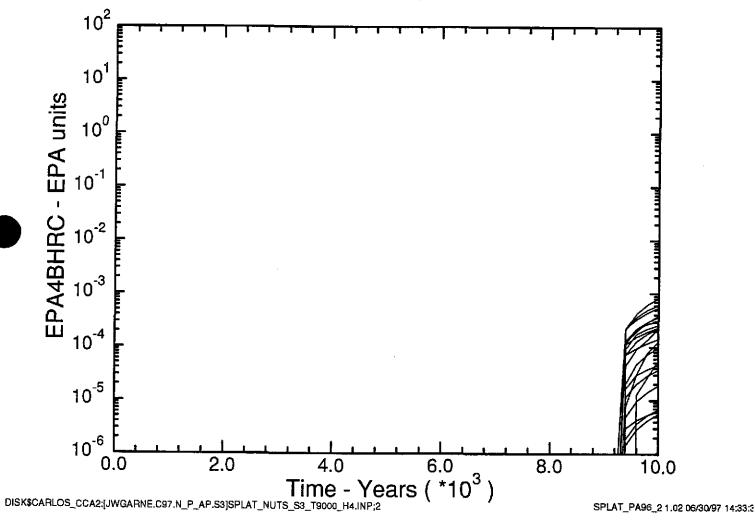
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SNL WIPP PA96: NUTS SIMULATIONS (C97 S3 T9000)
Pu-238 Integrated Discharge up Borehole at MB138



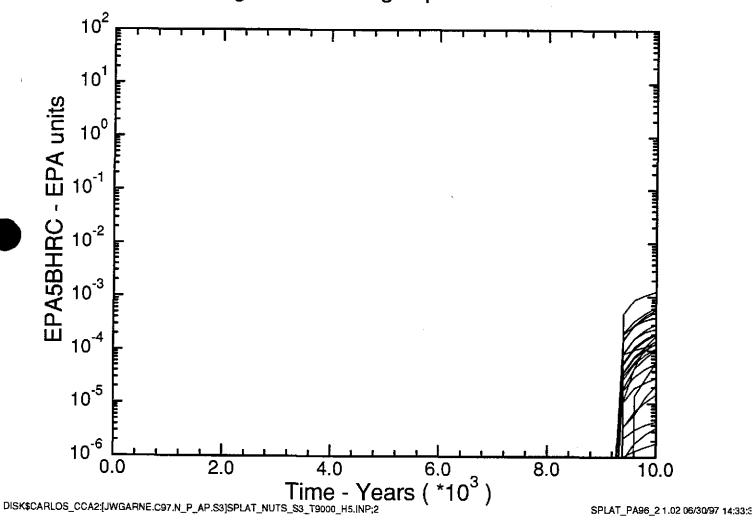
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SNL WIPP PA96: NUTS SIMULATIONS (C97 S3 T9000) U-234 Integrated Discharge up Borehole at MB138



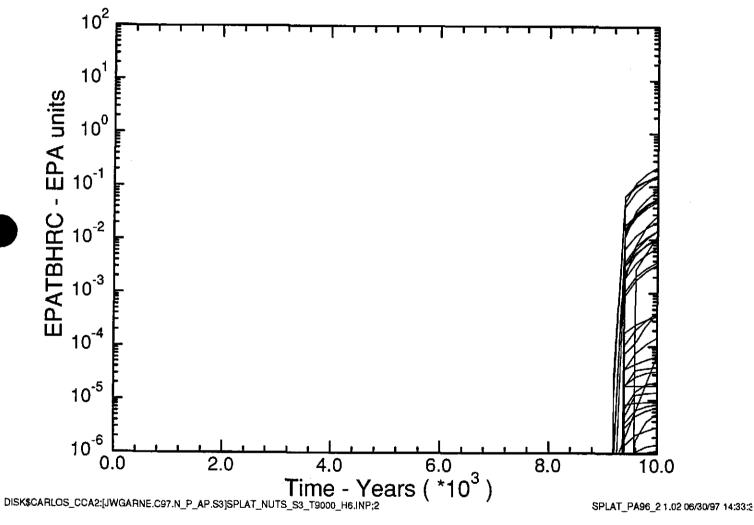
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SNL WIPP PA96: NUTS SIMULATIONS (C97 S3 T9000) Th-230 Integrated Discharge up Borehole at MB138



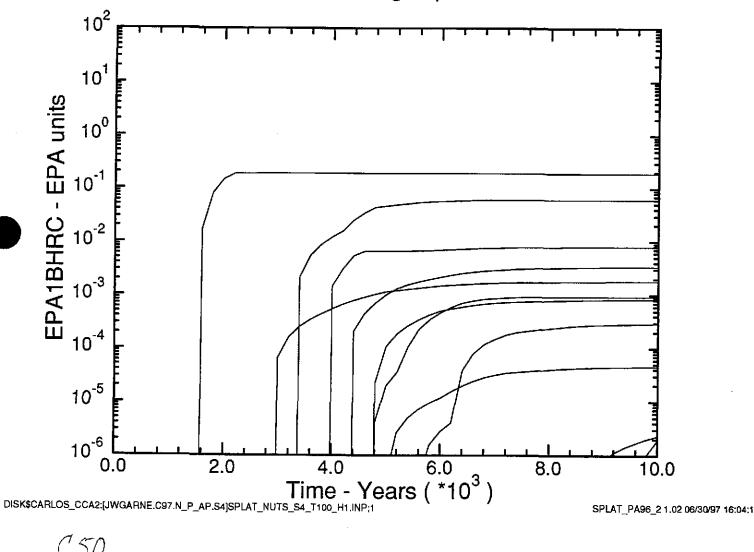
C48

SNL WIPP PA96: NUTS SIMULATIONS (C97 S3 T9000) Total Integrated Discharge up Borehole at MB138



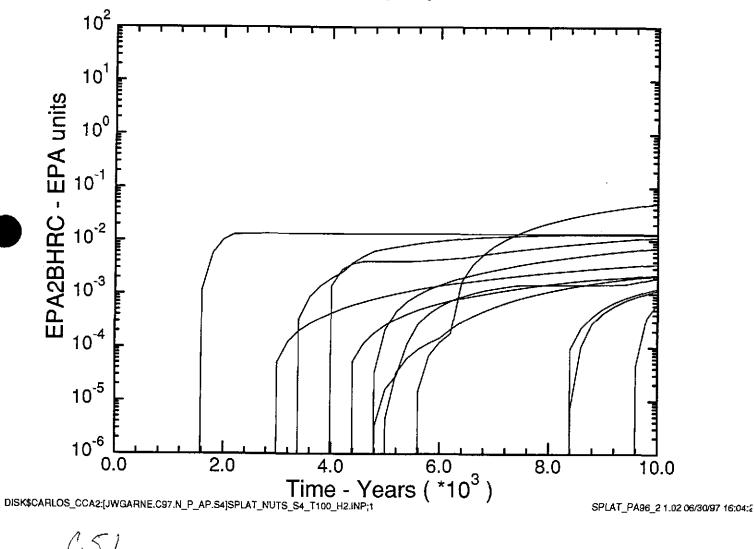
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SNL WIPP PA96: NUTS SIMULATIONS (C97 S4 T100) Am-241 Integrated Discharge up Borehole at MB138



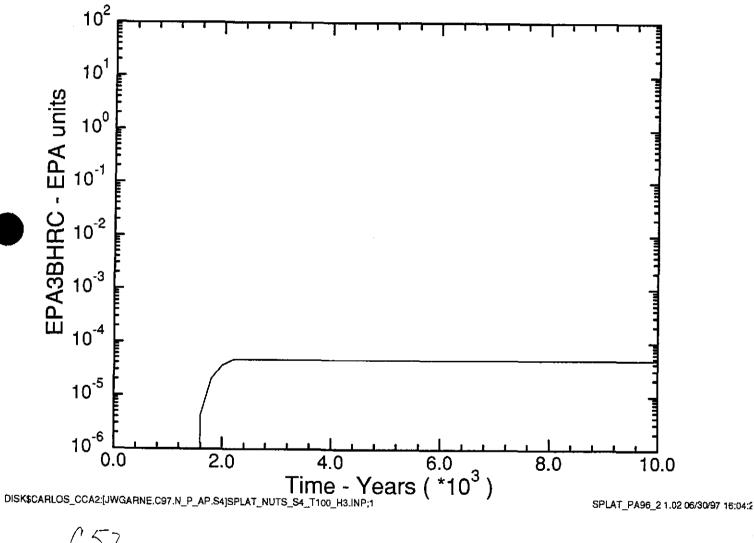
C50

SNL WIPP PA96: NUTS SIMULATIONS (C97 S4 T100) Pu-239 Integrated Discharge up Borehole at MB138



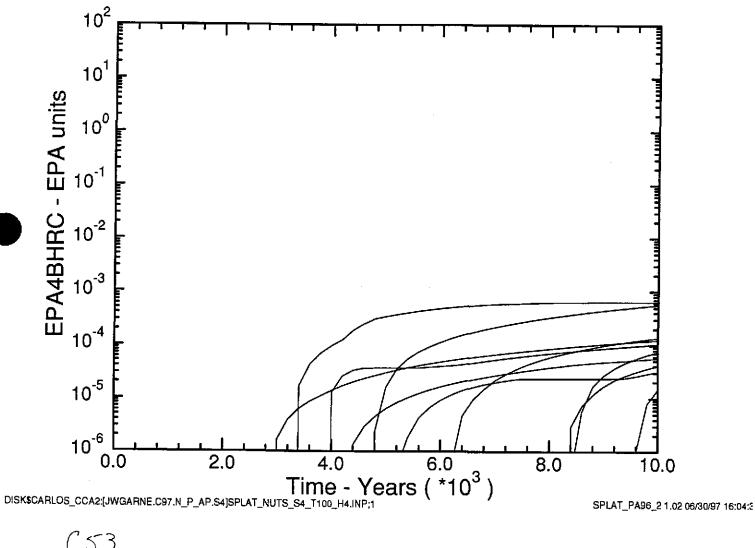
C51

SNL WIPP PA96: NUTS SIMULATIONS (C97 S4 T100) Pu-238 Integrated Discharge up Borehole at MB138



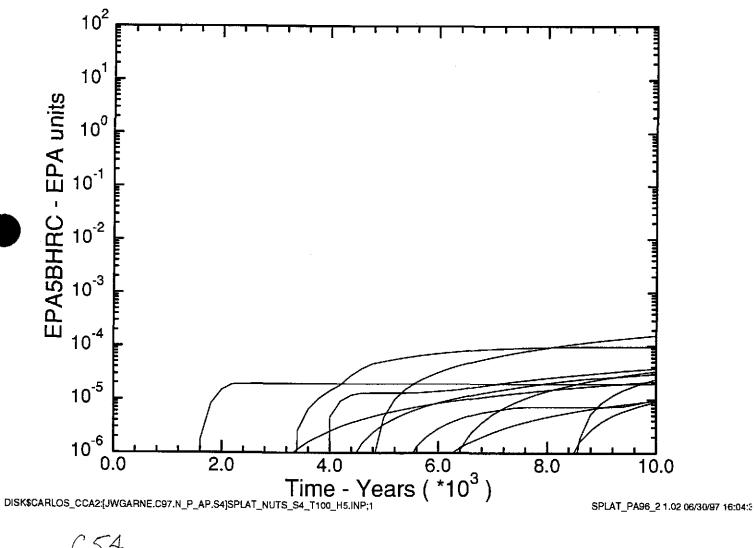
C52

SNL WIPP PA96: NUTS SIMULATIONS (C97 S4 T100) U-234 Integrated Discharge up Borehole at MB138



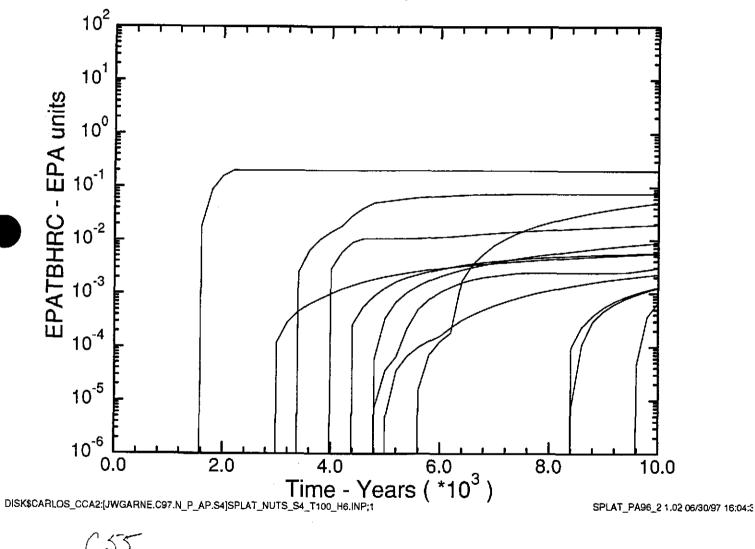
(53

SNL WIPP PA96: NUTS SIMULATIONS (C97 S4 T100) Th-230 Integrated Discharge up Borehole at MB138



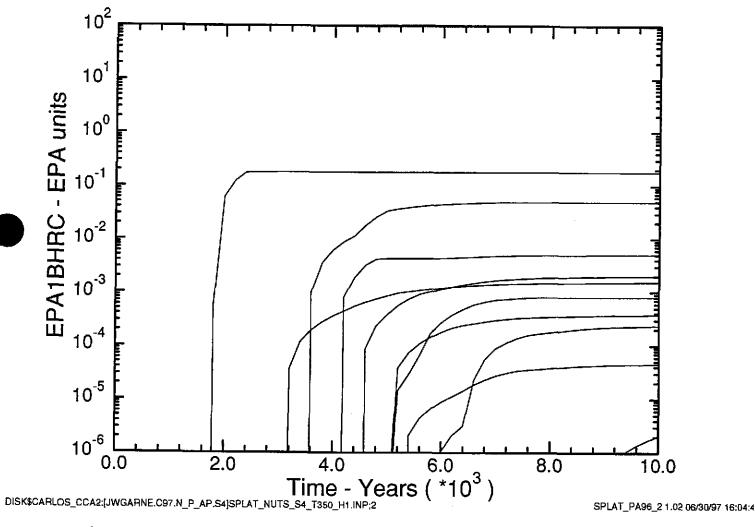
C54

SNL WIPP PA96: NUTS SIMULATIONS (C97 S4 T100) Total Integrated Discharge up Borehole at MB138

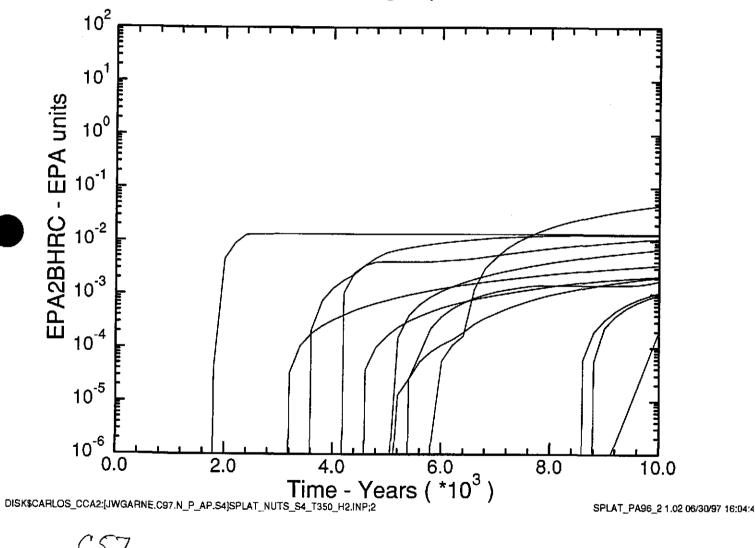


C55

SNL WIPP PA96: NUTS SIMULATIONS (C97 S4 T350) Am-241 Integrated Discharge up Borehole at MB138

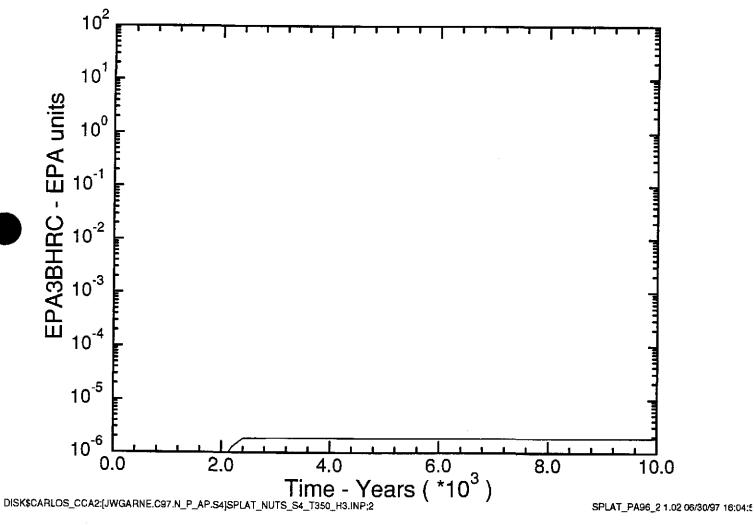


SNL WIPP PA96: NUTS SIMULATIONS (C97 S4 T350) Pu-239 Integrated Discharge up Borehole at MB138



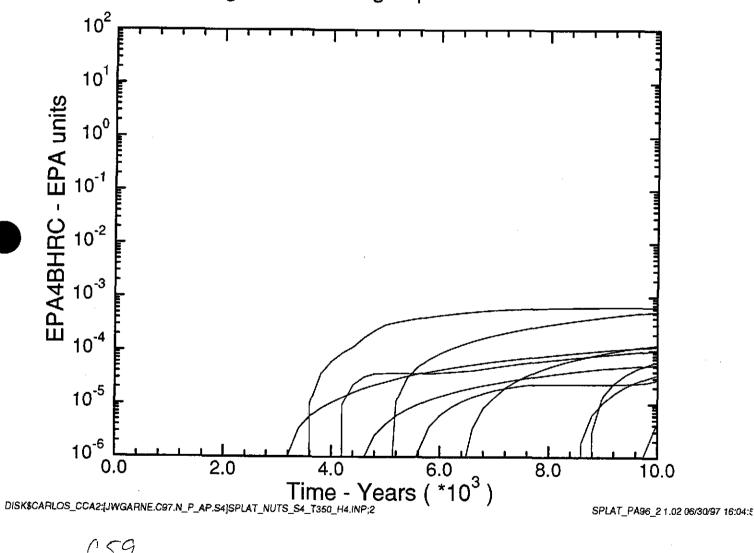
C57

SNL WIPP PA96: NUTS SIMULATIONS (C97 S4 T350) Pu-238 Integrated Discharge up Borehole at MB138



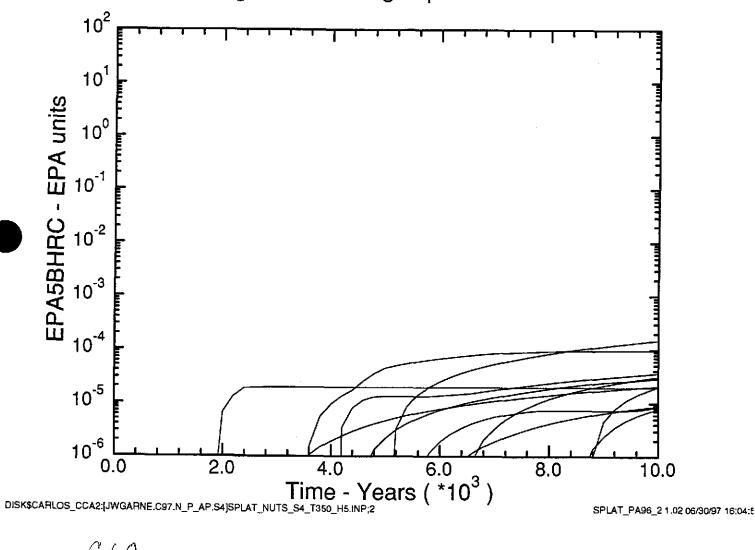
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SNL WIPP PA96: NUTS SIMULATIONS (C97 S4 T350) U-234 Integrated Discharge up Borehole at MB138



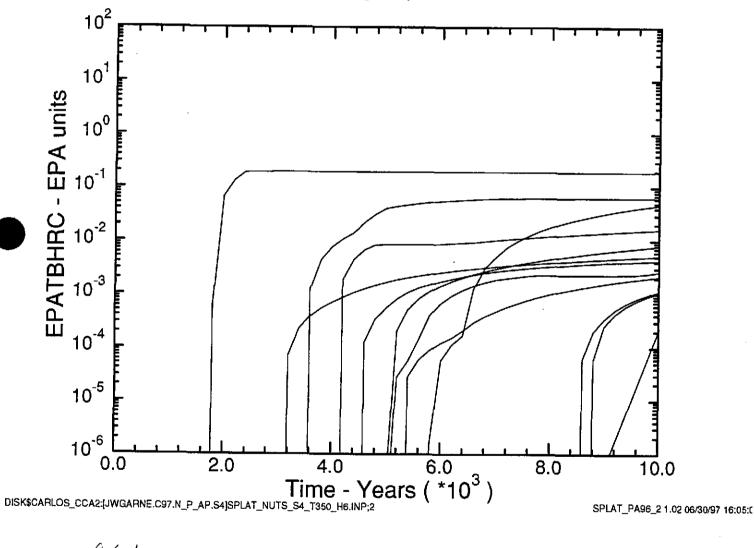
C59

SNL WIPP PA96: NUTS SIMULATIONS (C97 S4 T350) Th-230 Integrated Discharge up Borehole at MB138



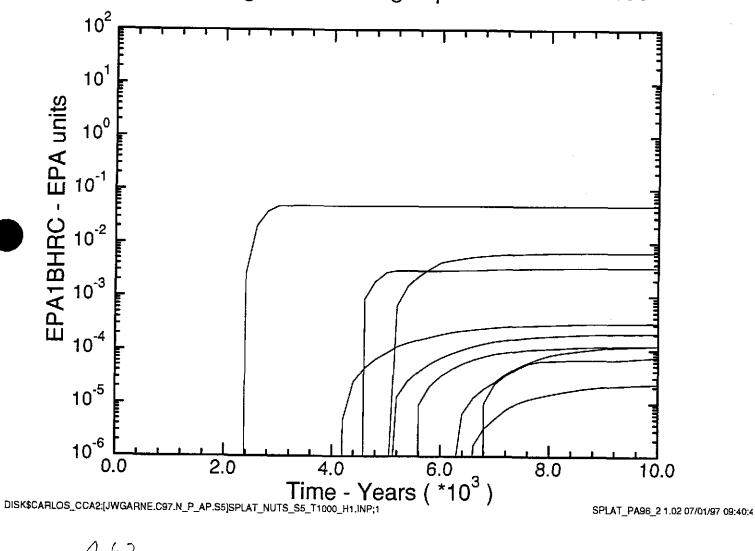
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SNL WIPP PA96: NUTS SIMULATIONS (C97 S4 T350) Total Integrated Discharge up Borehole at MB138



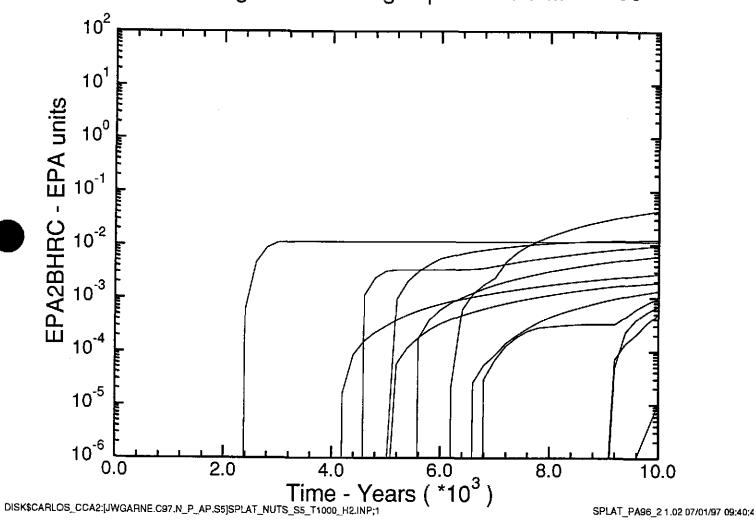
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SNL WIPP PA96: NUTS SIMULATIONS (C97 S5 T1000) Am-241 Integrated Discharge up Borehole at MB138



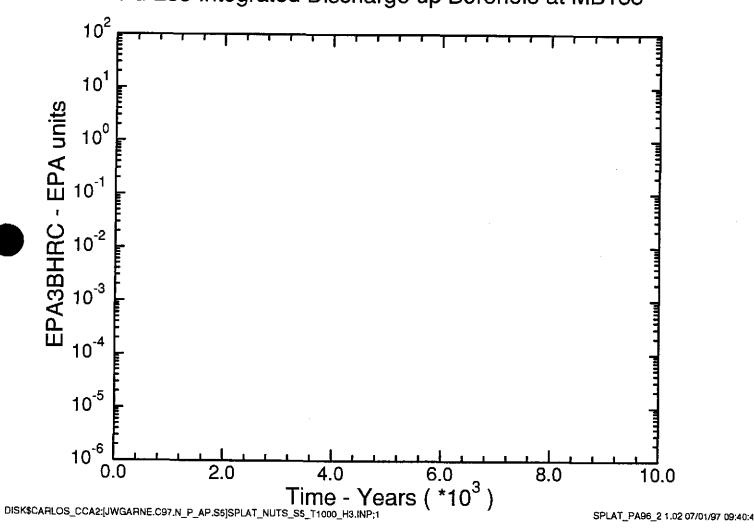
062

SNL WIPP PA96: NUTS SIMULATIONS (C97 S5 T1000) Pu-239 Integrated Discharge up Borehole at MB138



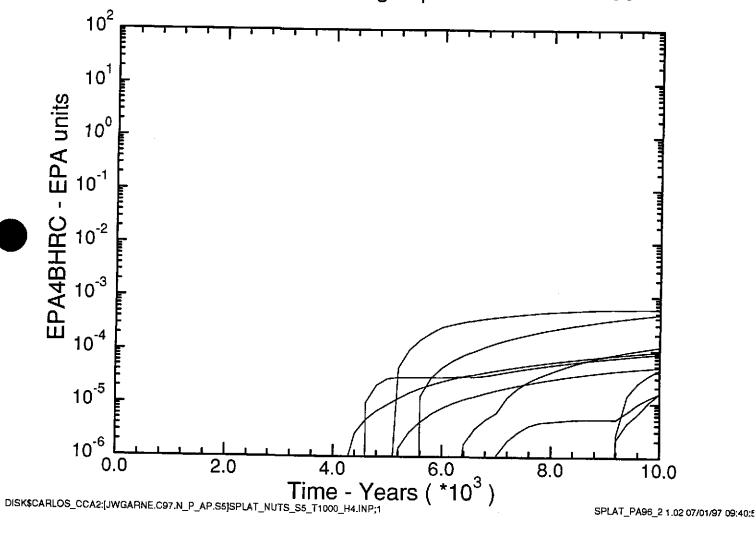
C 63

SNL WIPP PA96: NUTS SIMULATIONS (C97 S5 T1000) Pu-238 Integrated Discharge up Borehole at MB138



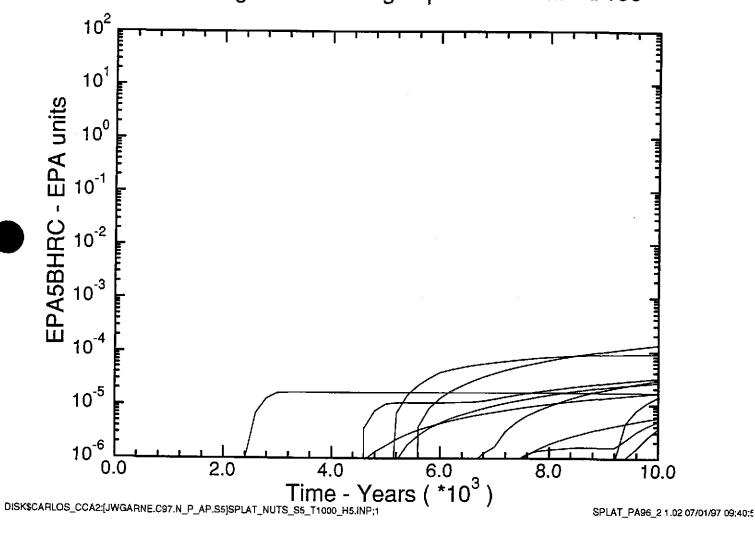
664

SNL WIPP PA96: NUTS SIMULATIONS (C97 S5 T1000) U-234 Integrated Discharge up Borehole at MB138



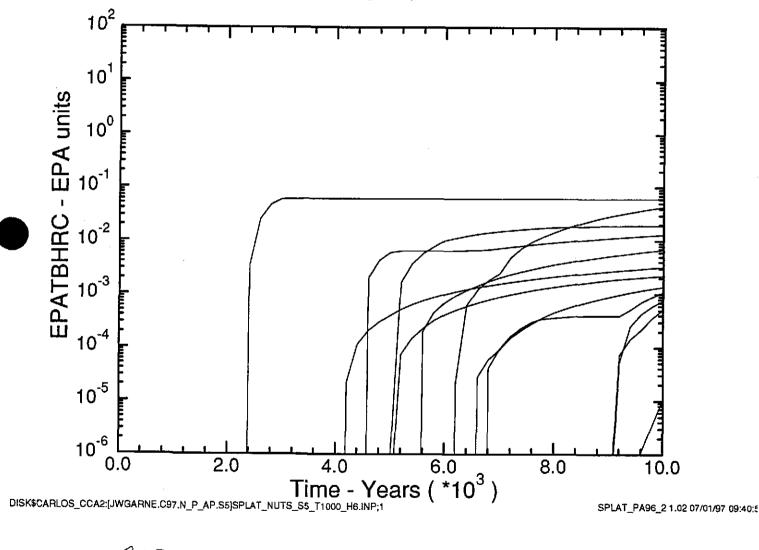
065

SNL WIPP PA96: NUTS SIMULATIONS (C97 S5 T1000) Th-230 Integrated Discharge up Borehole at MB138



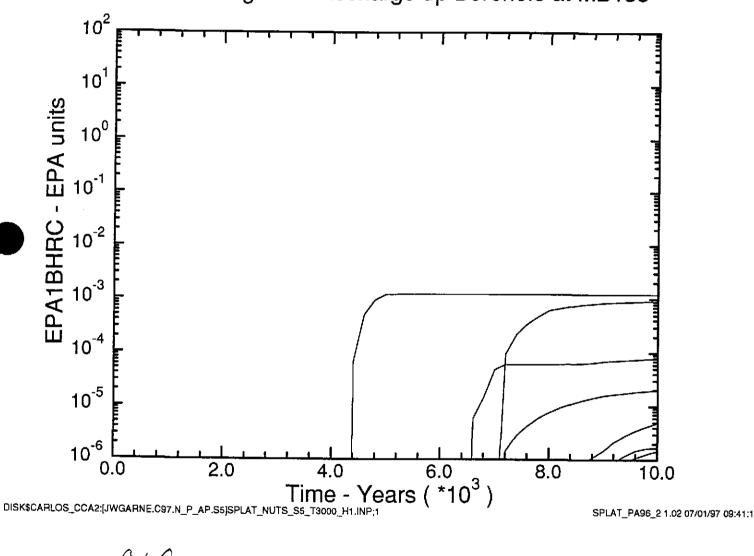
C66

SNL WIPP PA96: NUTS SIMULATIONS (C97 S5 T1000) Total Integrated Discharge up Borehole at MB138



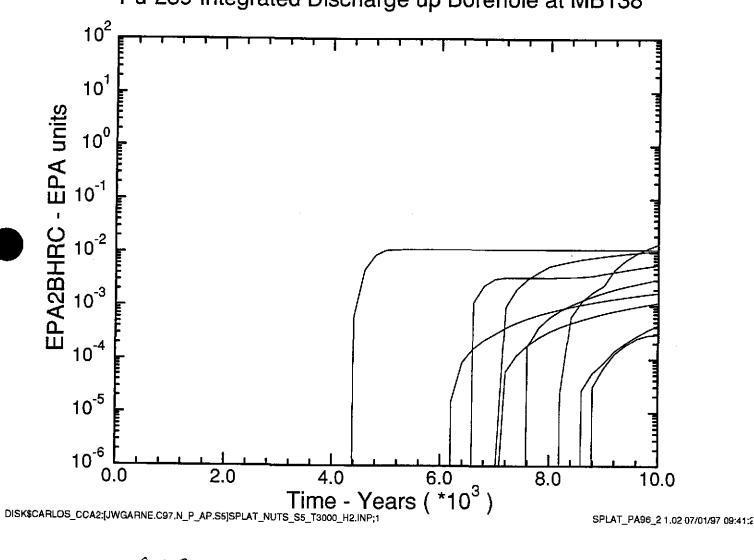
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SNL WIPP PA96: NUTS SIMULATIONS (C97 S5 T3000) Am-241 Integrated Discharge up Borehole at MB138



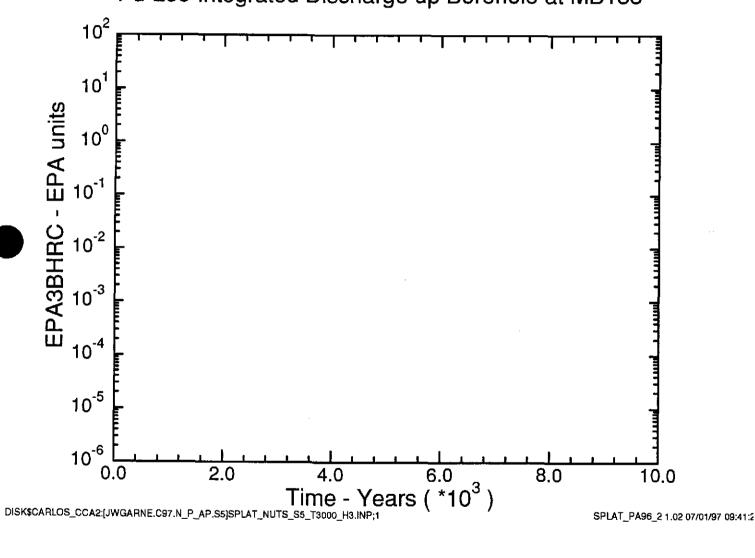
C68

SNL WIPP PA96: NUTS SIMULATIONS (C97 S5 T3000) Pu-239 Integrated Discharge up Borehole at MB138



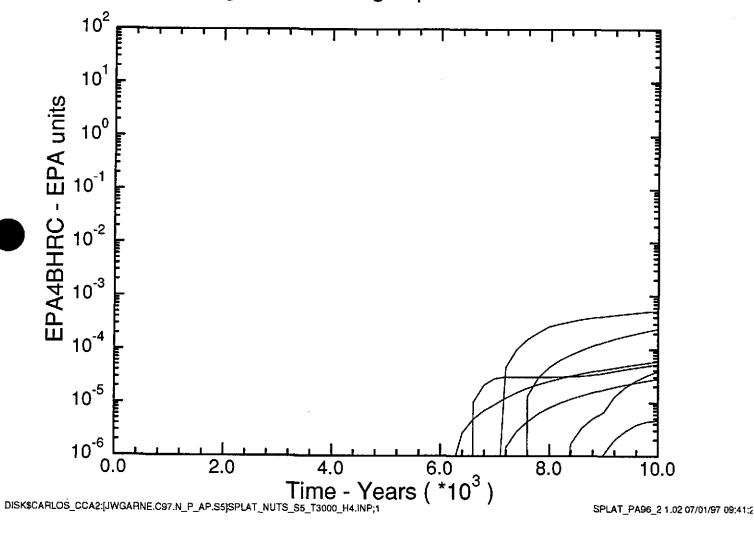
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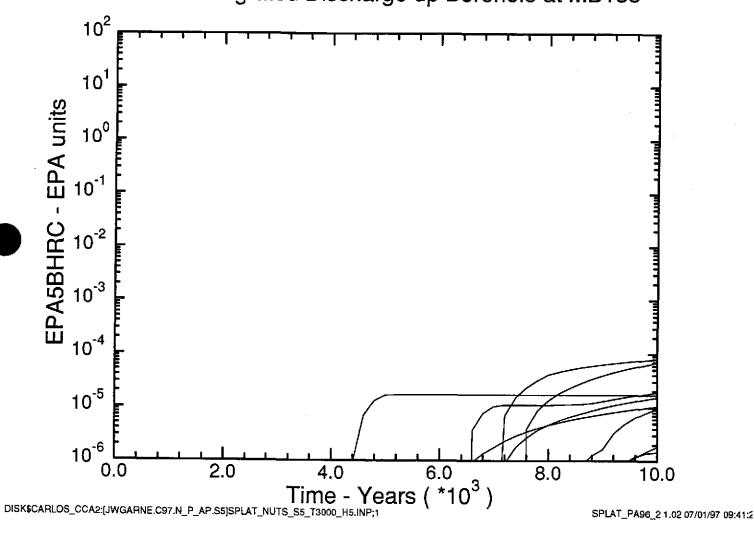
670

SNL WIPP PA96: NUTS SIMULATIONS (C97 S5 T3000) U-234 Integrated Discharge up Borehole at MB138



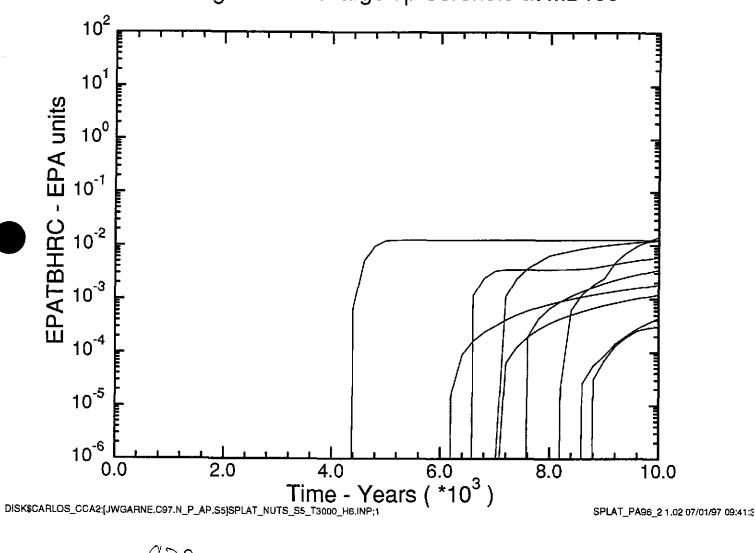
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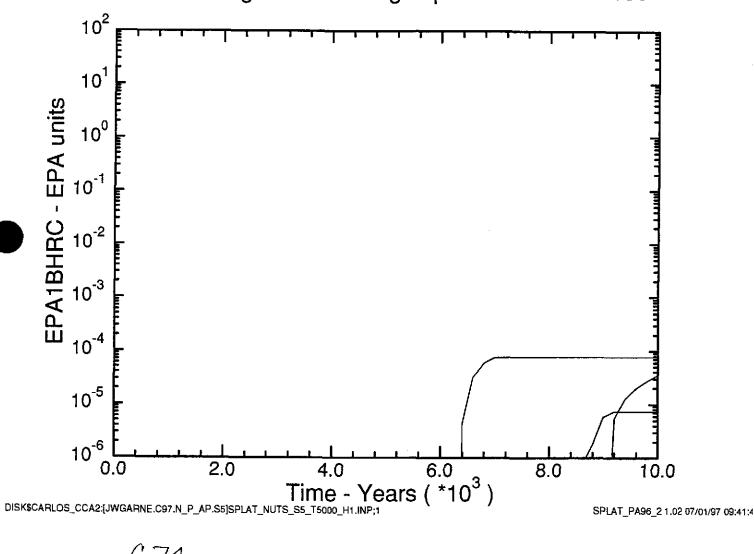
C72

SNL WIPP PA96: NUTS SIMULATIONS (C97 S5 T3000) Total Integrated Discharge up Borehole at MB138



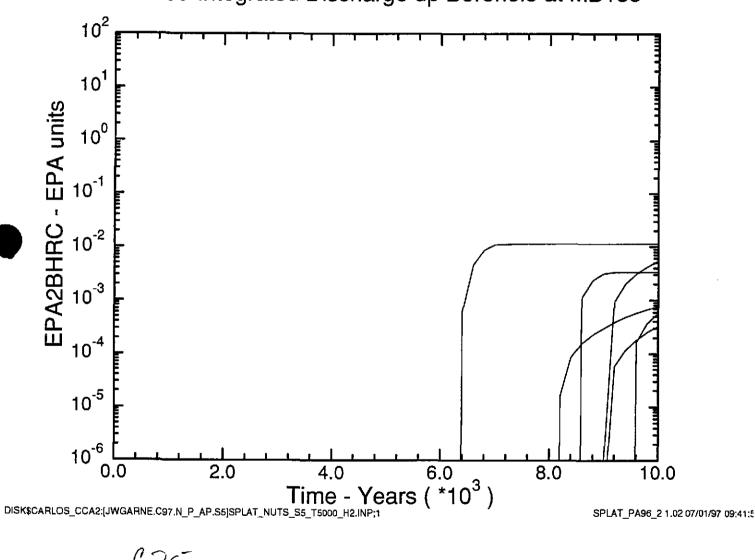
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SNL WIPP PA96: NUTS SIMULATIONS (C97 S5 T5000) Am-241 Integrated Discharge up Borehole at MB138



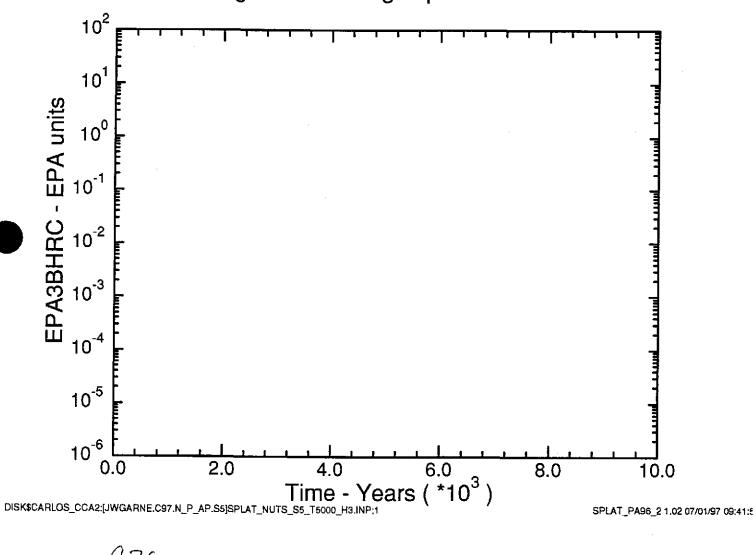
C74

SNL WIPP PA96: NUTS SIMULATIONS (C97 S5 T5000) Pu-239 Integrated Discharge up Borehole at MB138



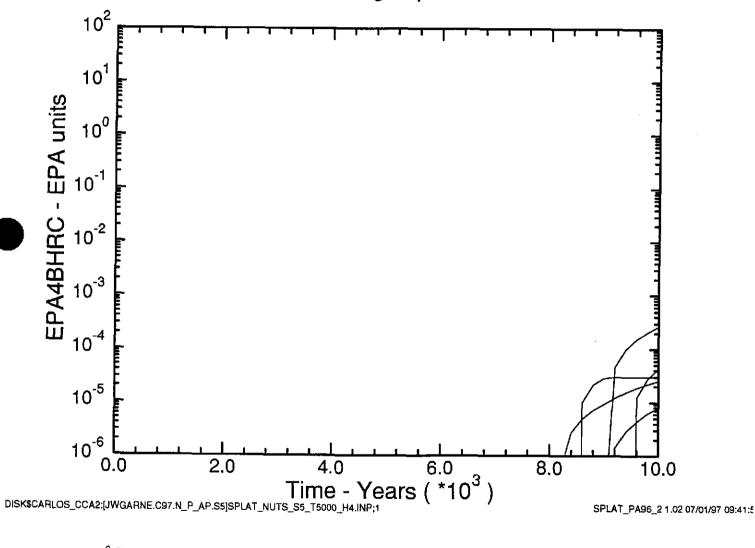
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SNL WIPP PA96: NUTS SIMULATIONS (C97 S5 T5000) Pu-238 Integrated Discharge up Borehole at MB138



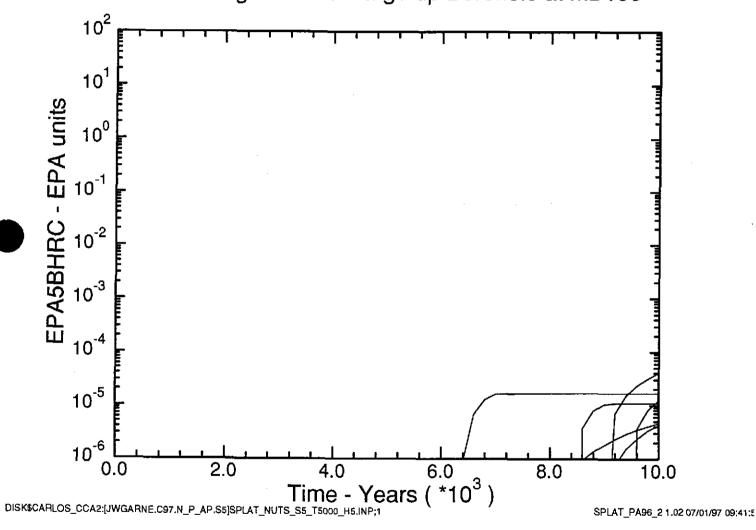
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SNL WIPP PA96: NUTS SIMULATIONS (C97 S5 T5000) U-234 Integrated Discharge up Borehole at MB138



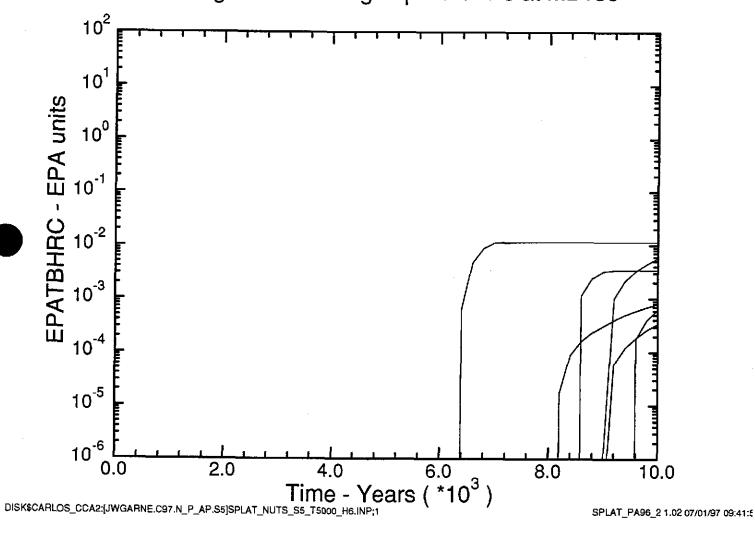
677

SNL WIPP PA96: NUTS SIMULATIONS (C97 S5 T5000) Th-230 Integrated Discharge up Borehole at MB138



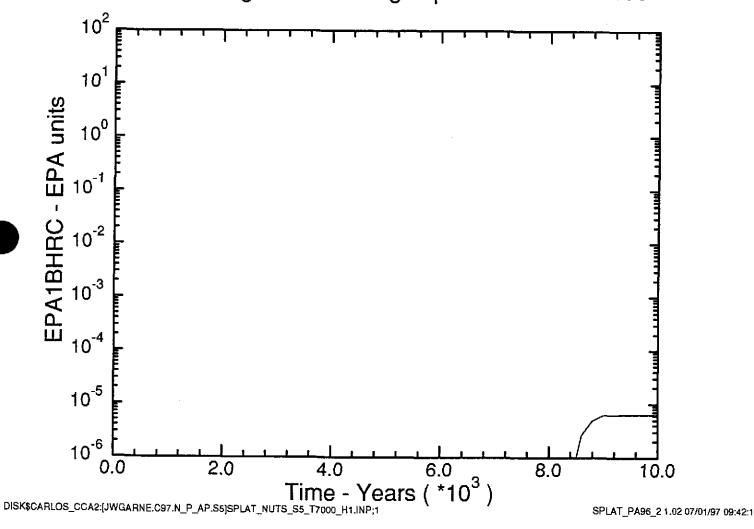
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SNL WIPP PA96: NUTS SIMULATIONS (C97 S5 T5000) Total Integrated Discharge up Borehole at MB138



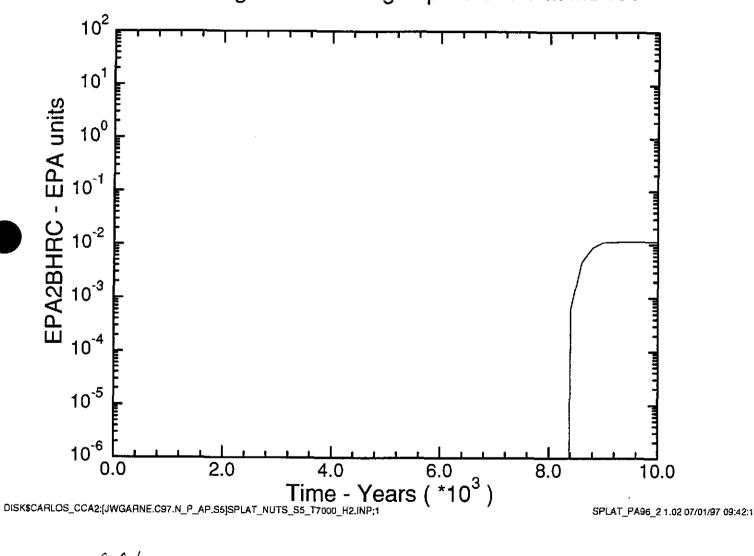
C79

SNL WIPP PA96: NUTS SIMULATIONS (C97 S5 T7000) Am-241 Integrated Discharge up Borehole at MB138



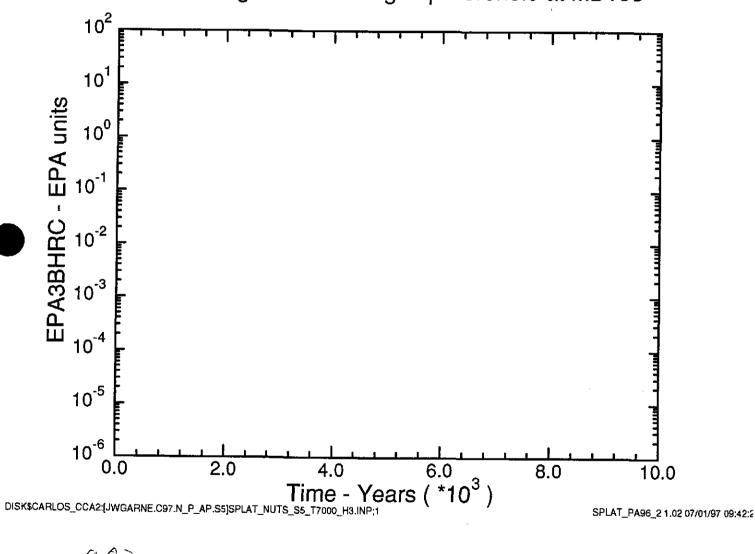
080

SNL WIPP PA96: NUTS SIMULATIONS (C97 S5 T7000) Pu-239 Integrated Discharge up Borehole at MB138



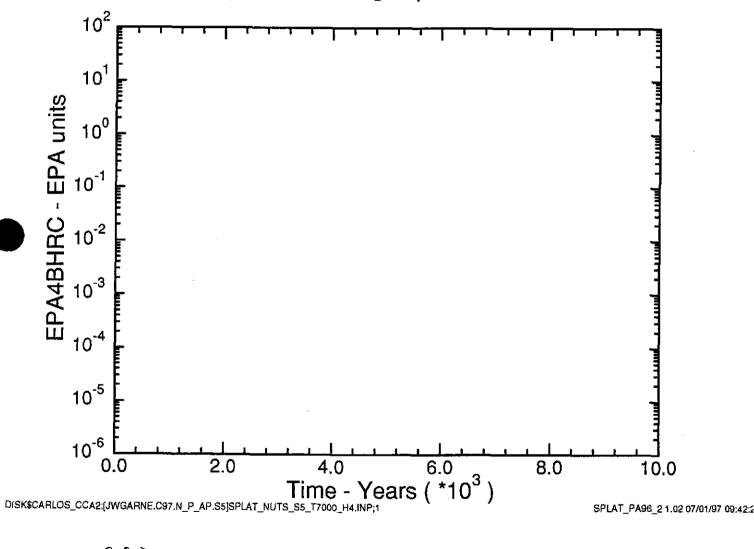
C81

SNL WIPP PA96: NUTS SIMULATIONS (C97 S5 T7000)
Pu-238 Integrated Discharge up Borehole at MB138



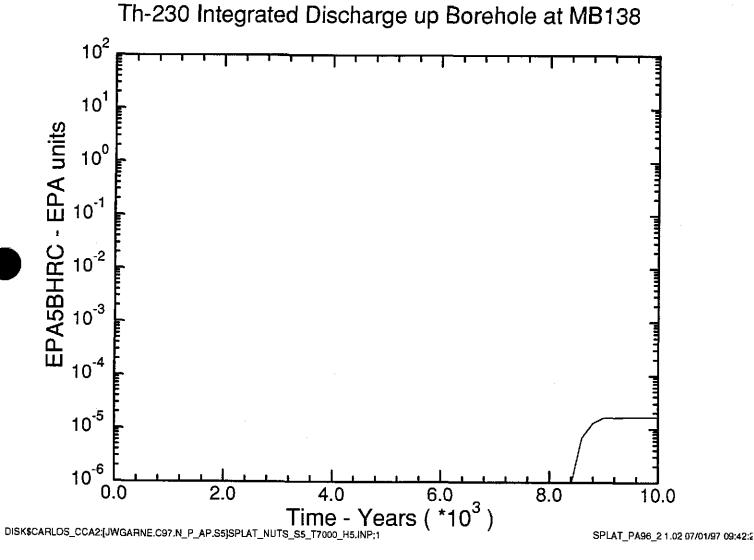
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SNL WIPP PA96: NUTS SIMULATIONS (C97 S5 T7000) U-234 Integrated Discharge up Borehole at MB138



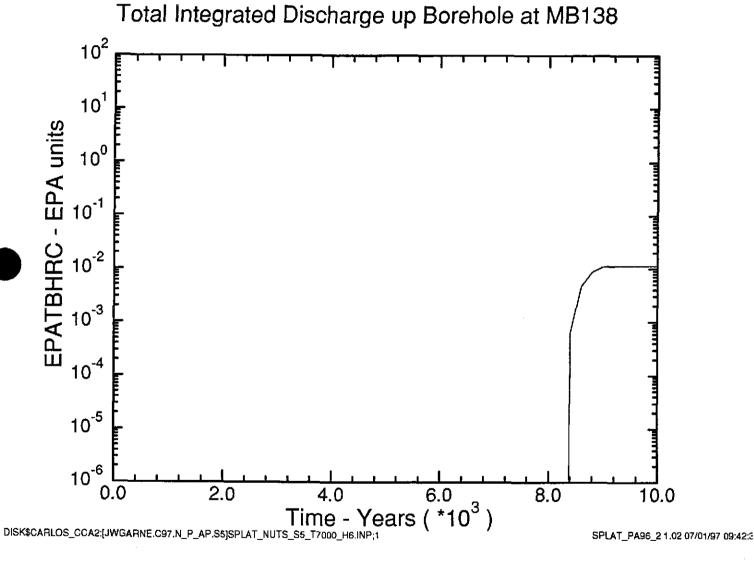
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SNL WIPP PA96: NUTS SIMULATIONS (C97 S5 T7000)



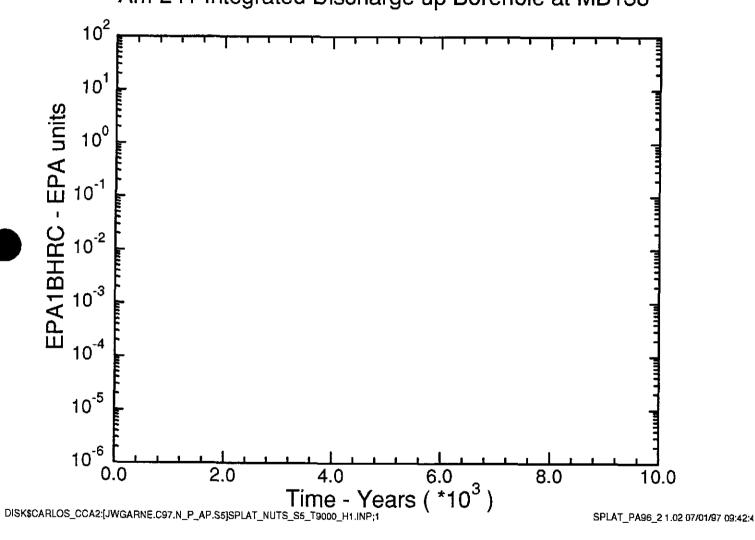
084

SNL WIPP PA96: NUTS SIMULATIONS (C97 S5 T7000)



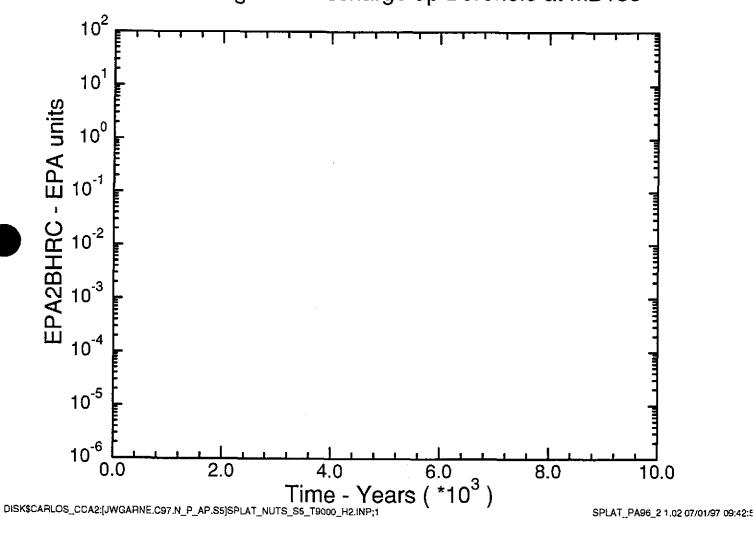
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SNL WIPP PA96: NUTS SIMULATIONS (C97 S5 T9000) Am-241 Integrated Discharge up Borehole at MB138



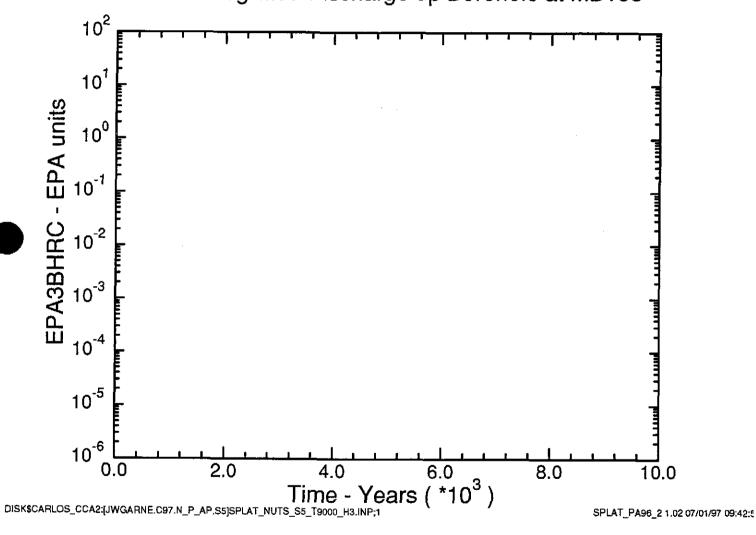
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SNL WIPP PA96: NUTS SIMULATIONS (C97 S5 T9000) Pu-239 Integrated Discharge up Borehole at MB138



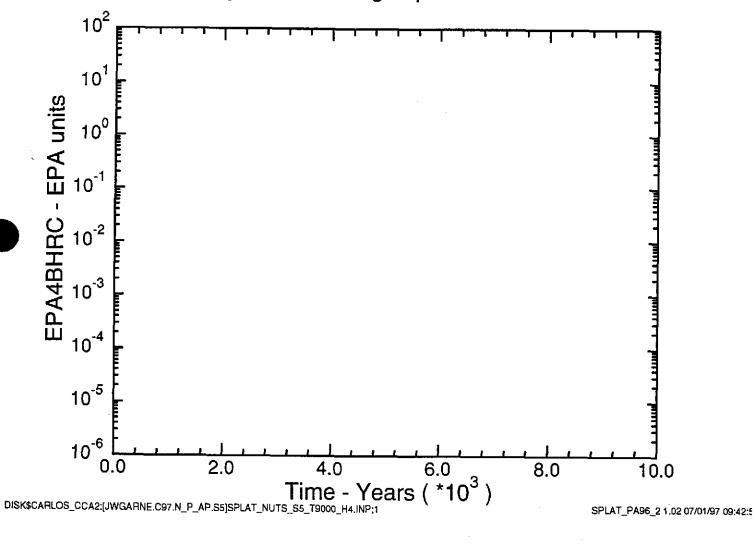
C87

SNL WIPP PA96: NUTS SIMULATIONS (C97 S5 T9000) Pu-238 Integrated Discharge up Borehole at MB138



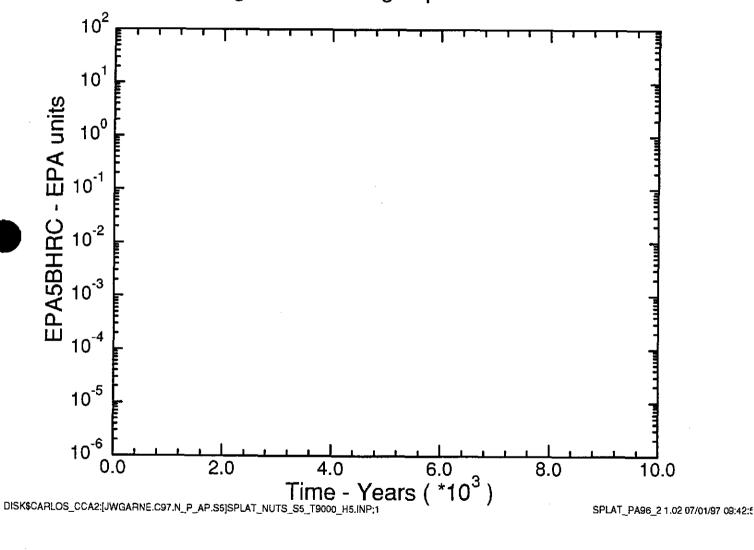
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SNL WIPP PA96: NUTS SIMULATIONS (C97 S5 T9000) U-234 Integrated Discharge up Borehole at MB138



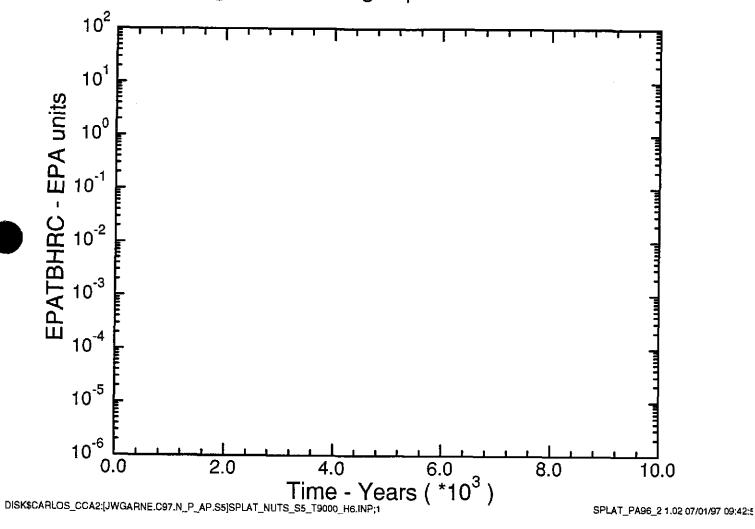
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SNL WIPP PA96: NUTS SIMULATIONS (C97 S5 T9000) Th-230 Integrated Discharge up Borehole at MB138



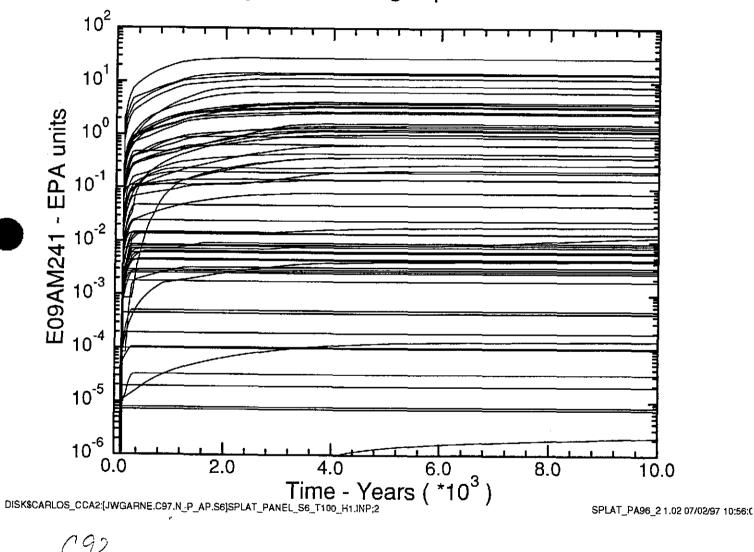
C90

SNL WIPP PA96: NUTS SIMULATIONS (C97 S5 T9000) Total Integrated Discharge up Borehole at MB138



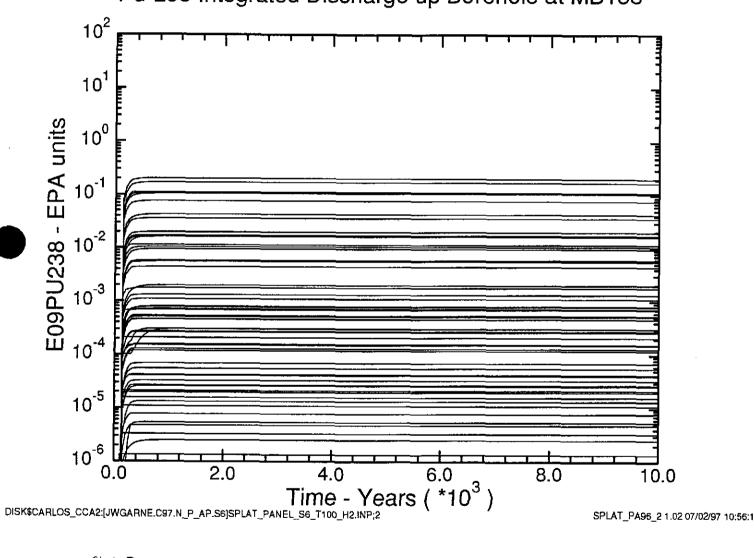
09/

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T100) Am-241 Integrated Discharge up Borehole at MB138



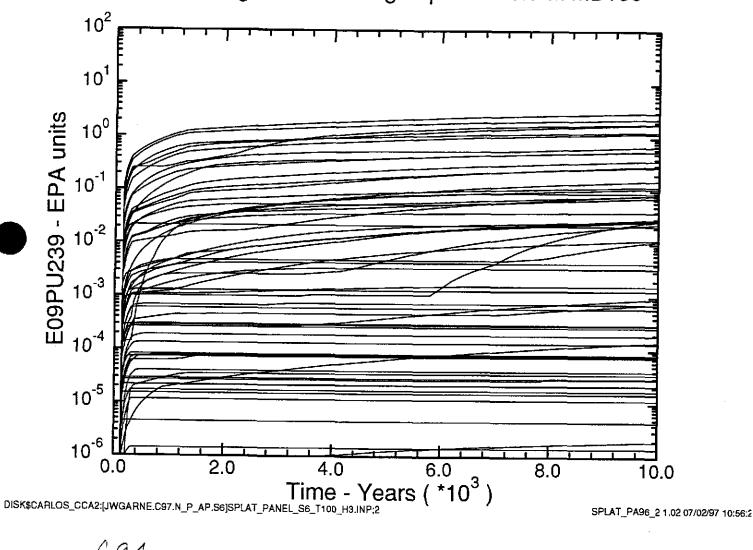
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SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T100) Pu-238 Integrated Discharge up Borehole at MB138



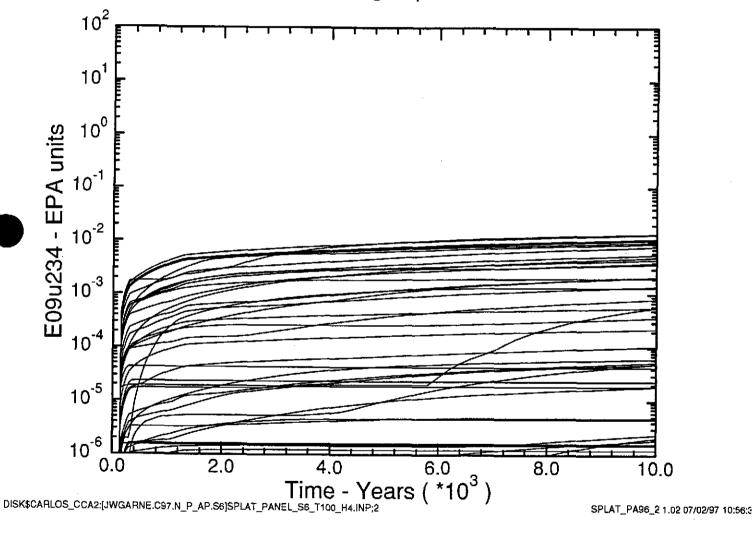
C93

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T100) Pu-239 Integrated Discharge up Borehole at MB138



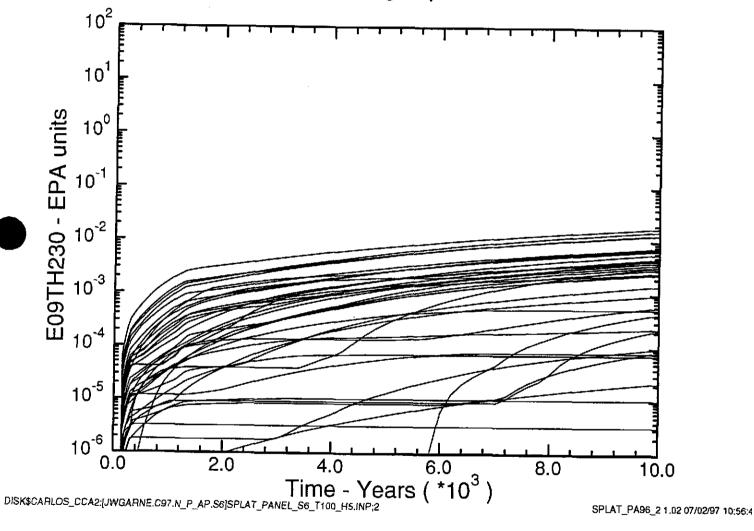
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SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T100) U-234 Integrated Discharge up Borehole at MB138



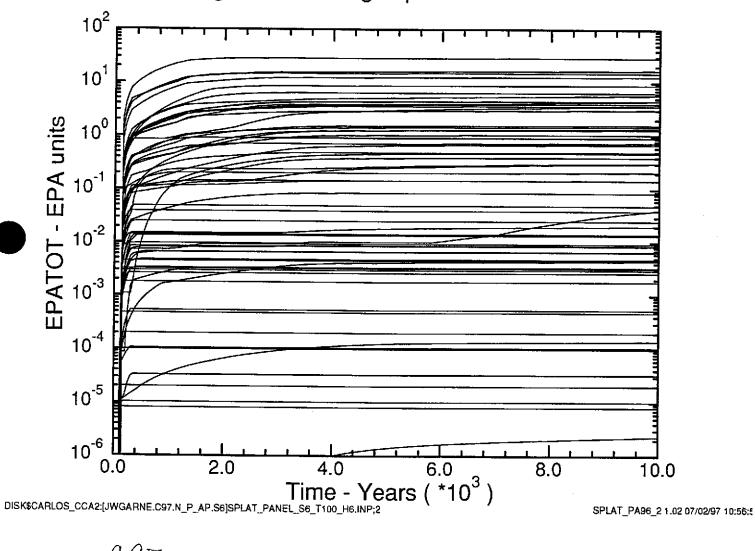
095

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T100) Th-230 Integrated Discharge up Borehole at MB138



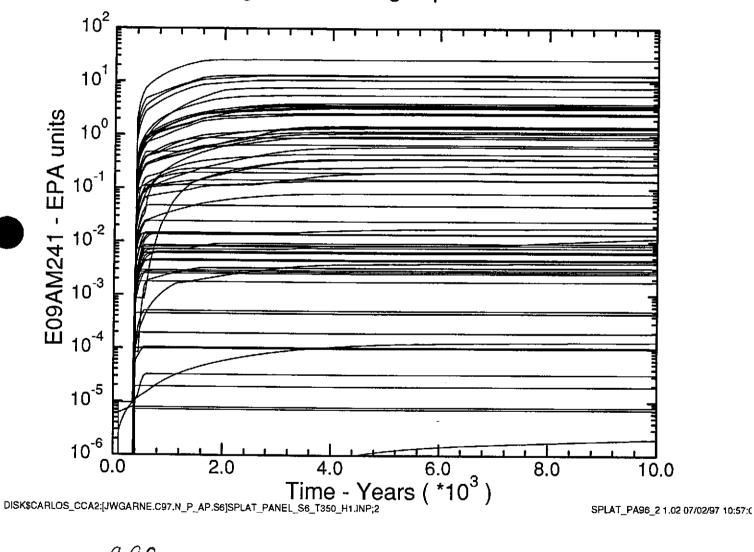
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SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T100) Total Integrated Discharge up Borehole at MB138



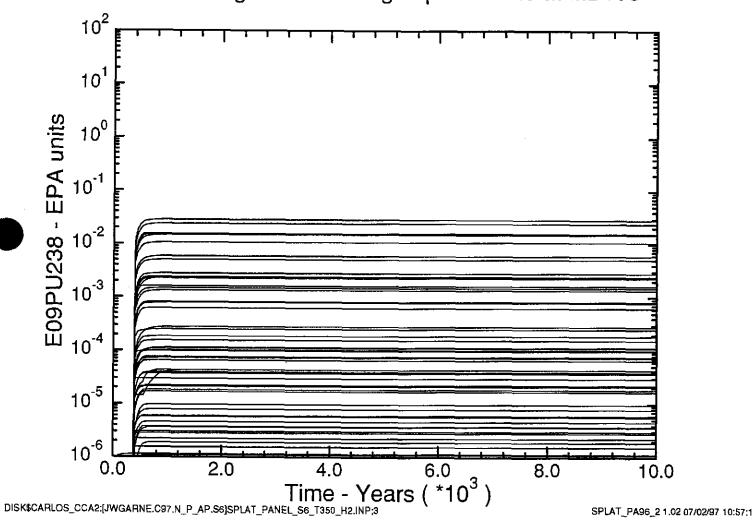
097

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T350) Am-241 Integrated Discharge up Borehole at MB138



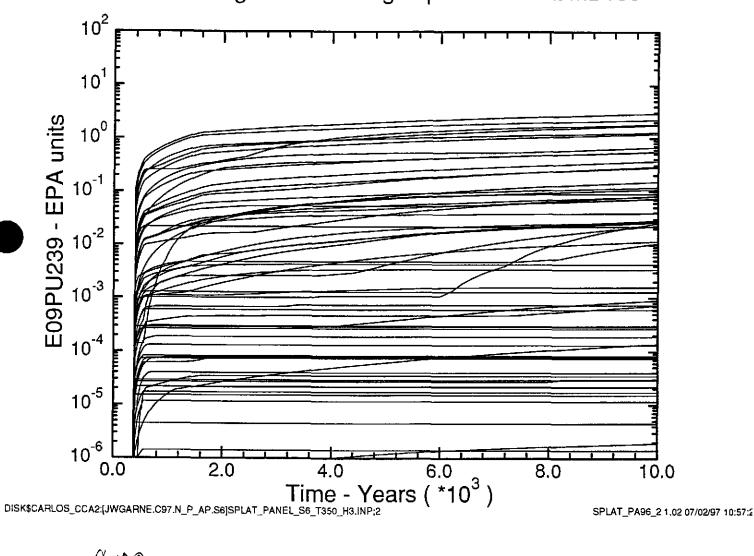
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SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T350) Pu-238 Integrated Discharge up Borehole at MB138



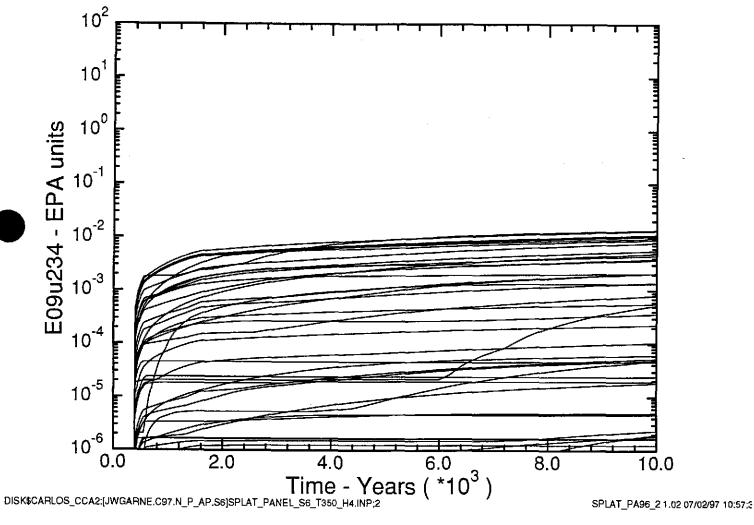
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SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T350)
Pu-239 Integrated Discharge up Borehole at MB138



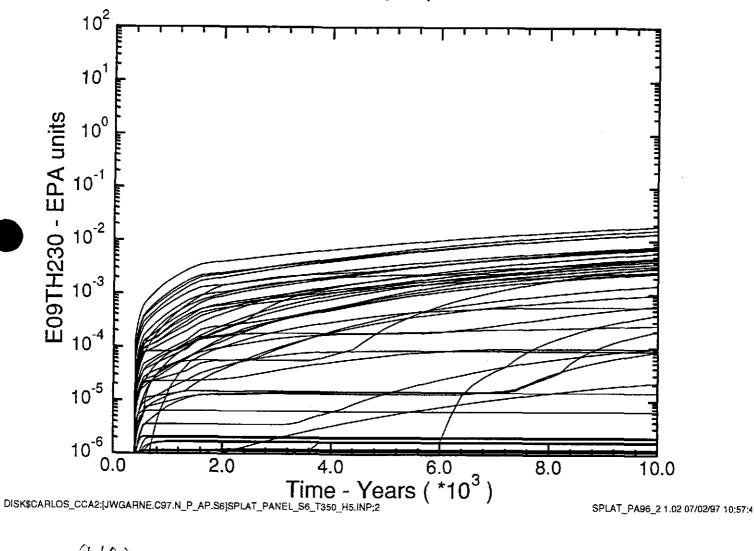
0100

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T350) U-234 Integrated Discharge up Borehole at MB138



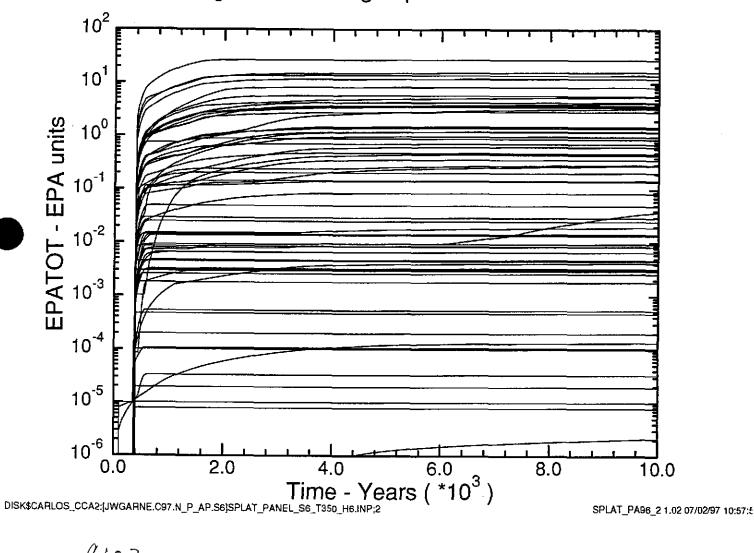
C101

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T350) Th-230 Integrated Discharge up Borehole at MB138



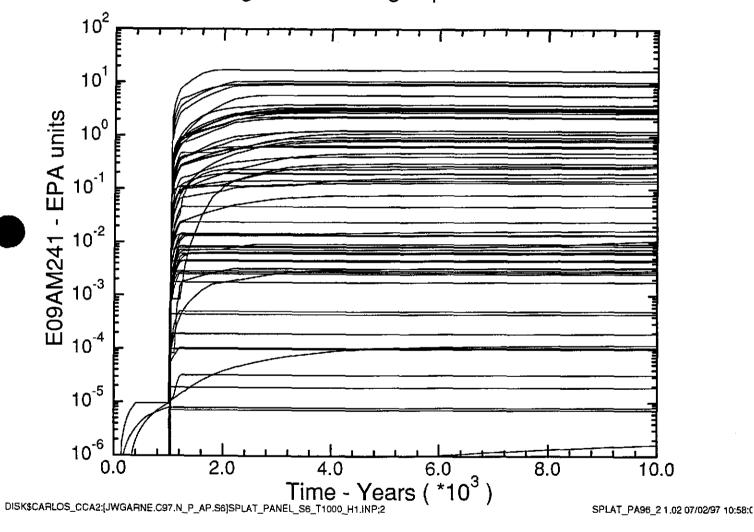
C102

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T350) Total Integrated Discharge up Borehole at MB138



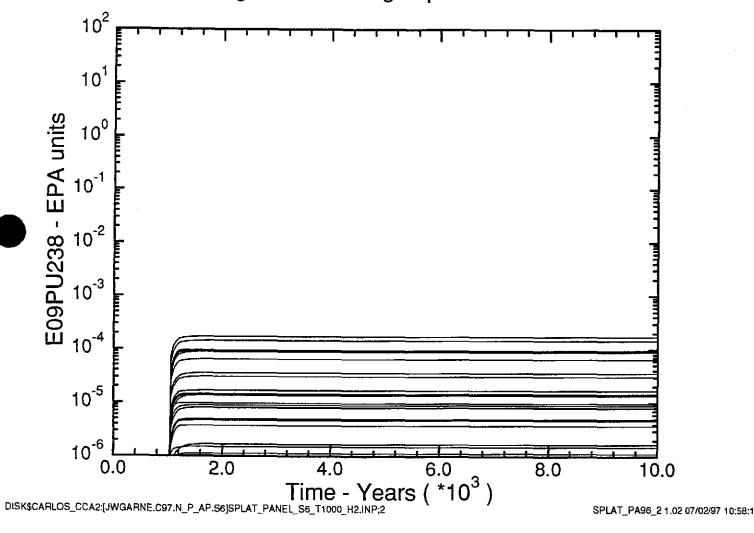
C/03

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T1000) Am-241 Integrated Discharge up Borehole at MB138



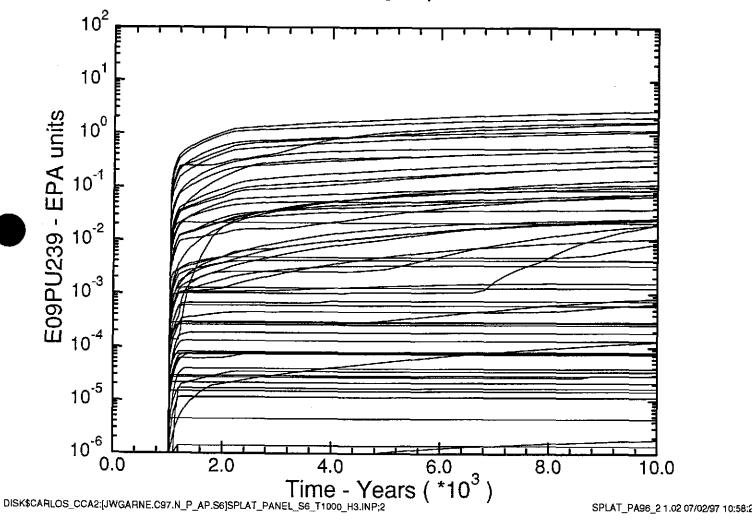
6104

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T1000) Pu-238 Integrated Discharge up Borehole at MB138



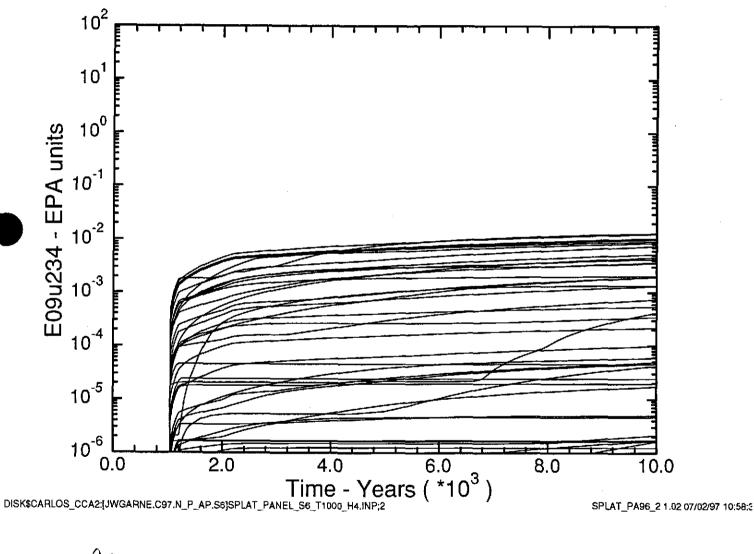
C105

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T1000) Pu-239 Integrated Discharge up Borehole at MB138



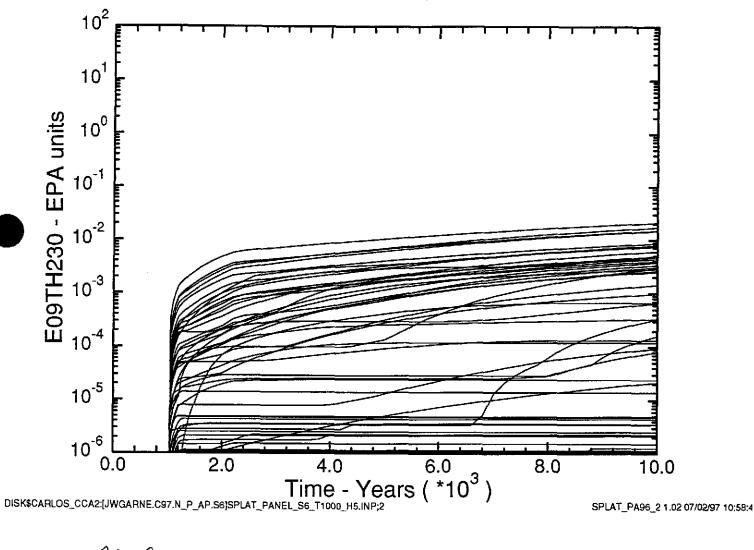
C106

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T1000) U-234 Integrated Discharge up Borehole at MB138



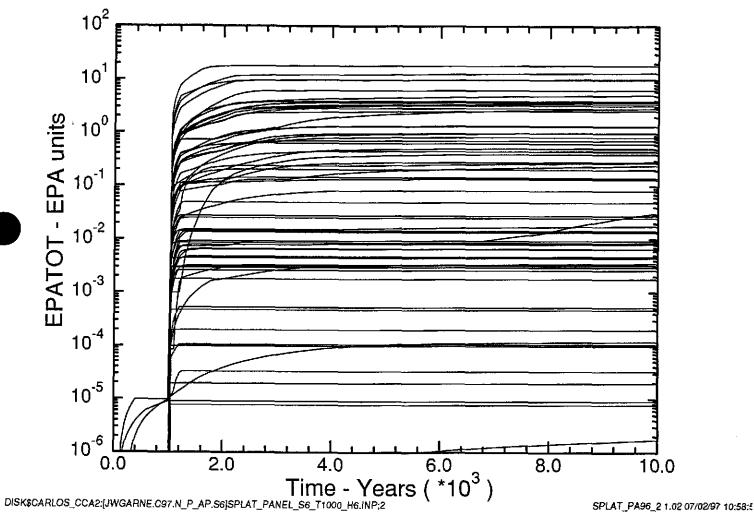
C107

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T1000) Th-230 Integrated Discharge up Borehole at MB138



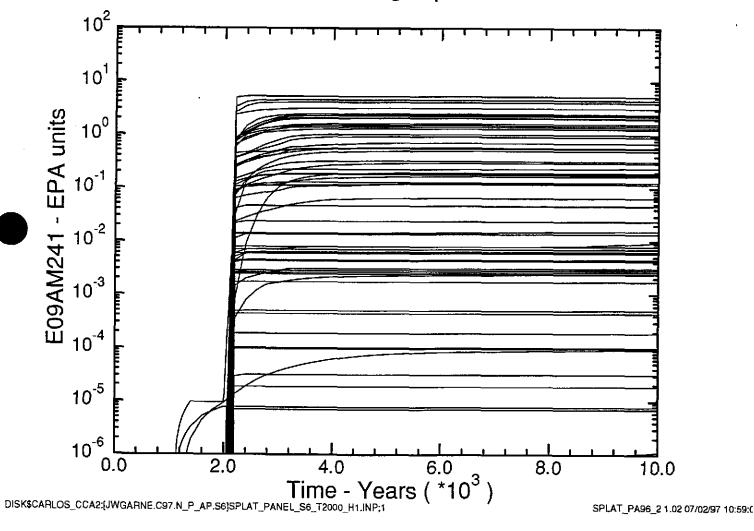
C108

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T1000) Total Integrated Discharge up Borehole at MB138



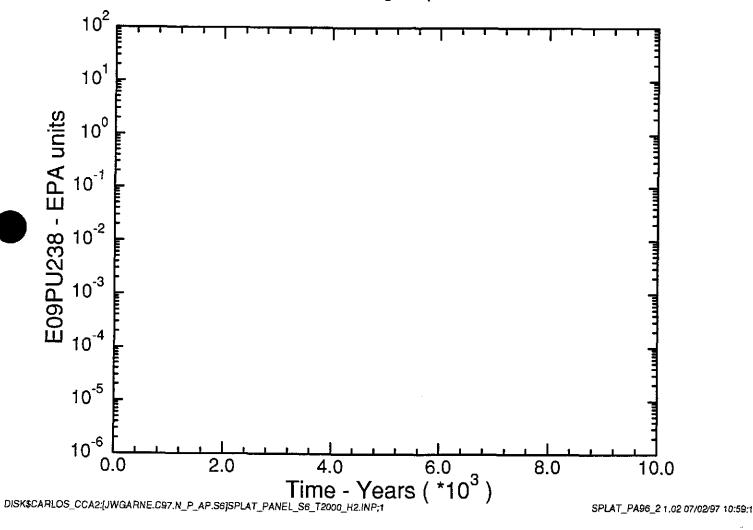
C109

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T2000) Am-241 Integrated Discharge up Borehole at MB138



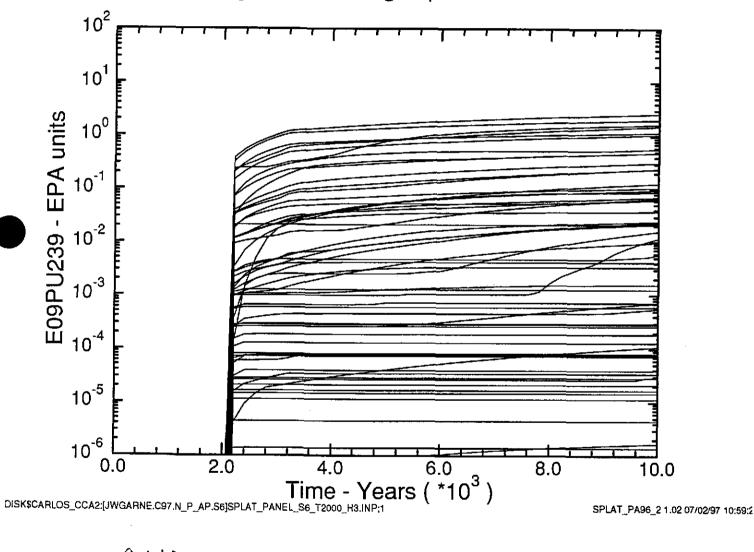
0110

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T2000) Pu-238 Integrated Discharge up Borehole at MB138



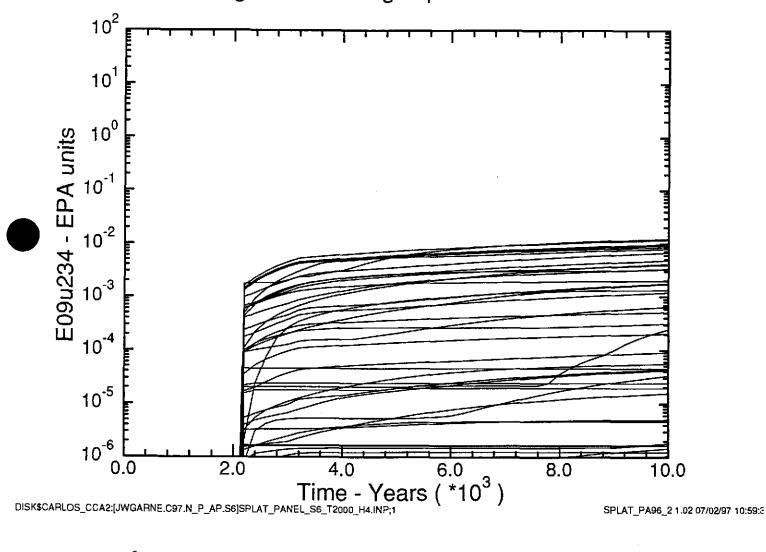
0111

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T2000) Pu-239 Integrated Discharge up Borehole at MB138



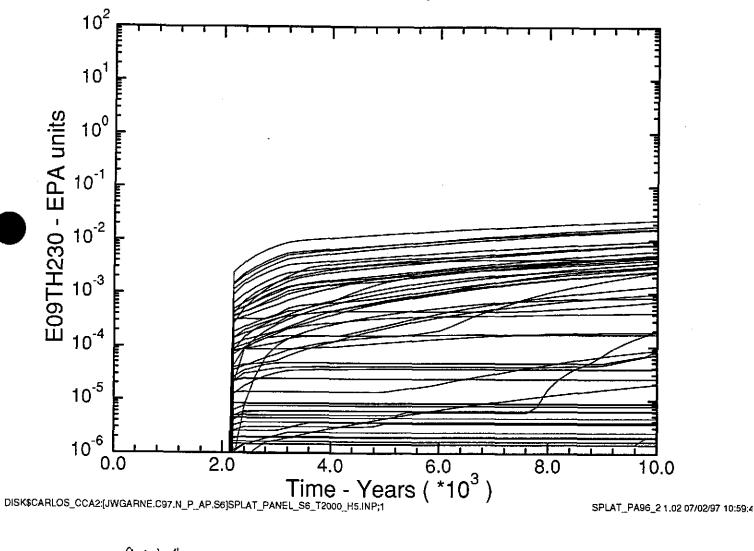
C112

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T2000) U-234 Integrated Discharge up Borehole at MB138



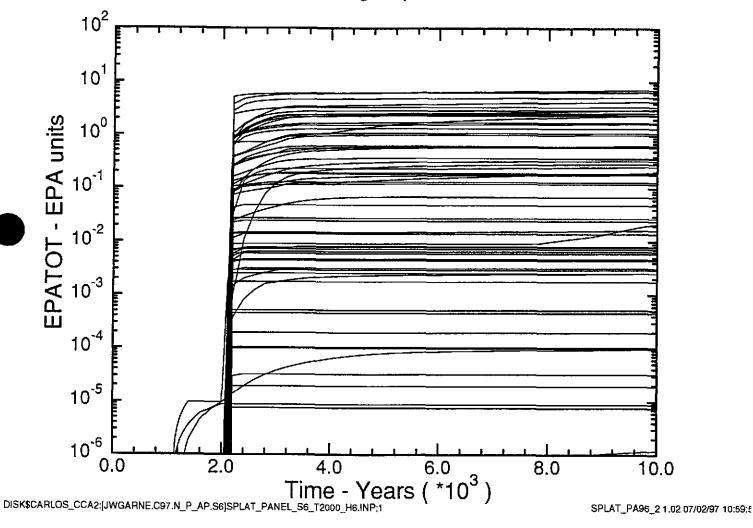
0113

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T2000) Th-230 Integrated Discharge up Borehole at MB138



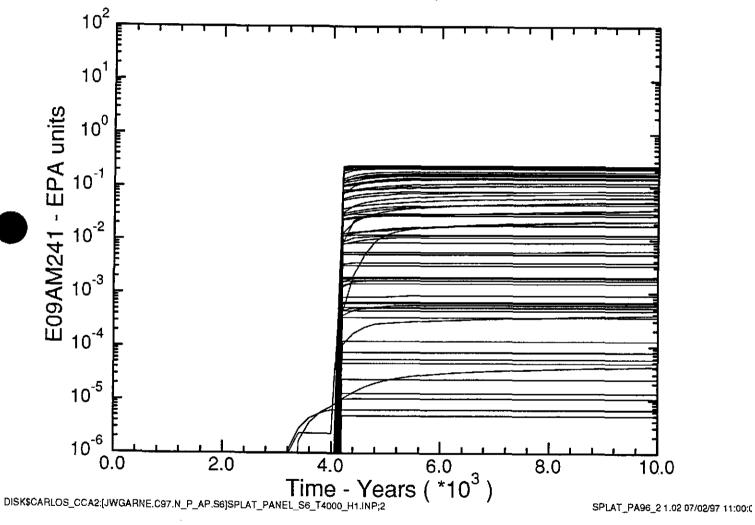
C114

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T2000) Total Integrated Discharge up Borehole at MB138



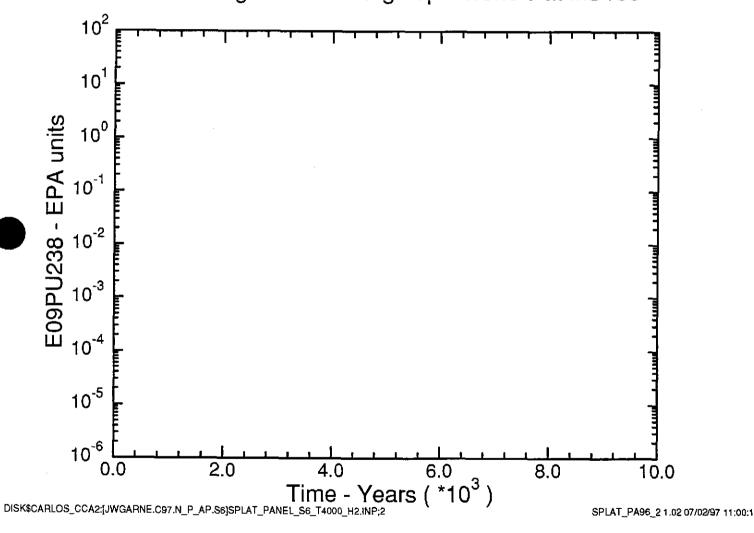
0115

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T4000) Am-241 Integrated Discharge up Borehole at MB138



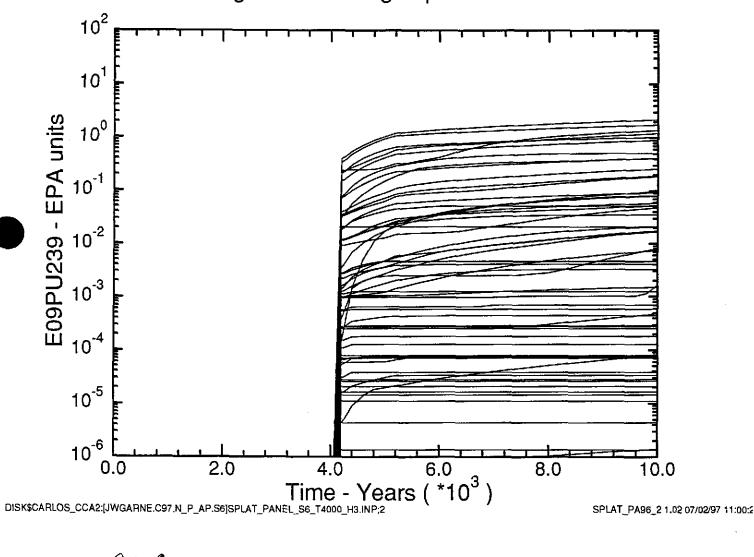
C116

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T4000) Pu-238 Integrated Discharge up Borehole at MB138



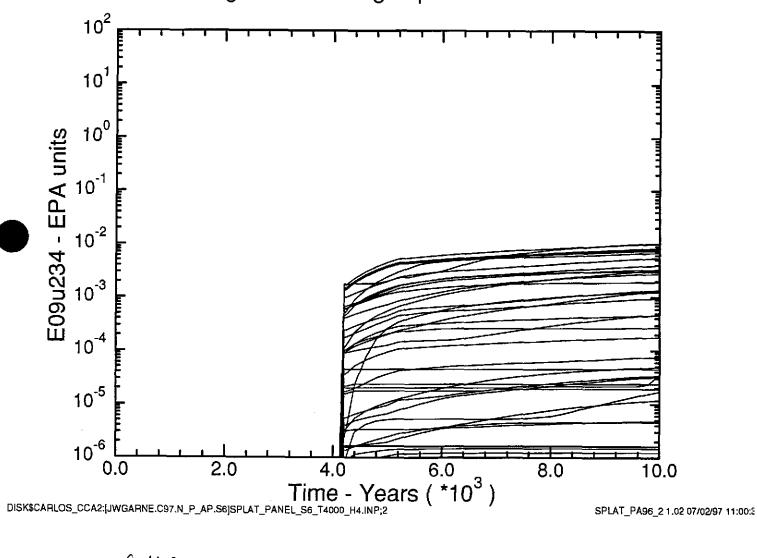
C117

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T4000) Pu-239 Integrated Discharge up Borehole at MB138



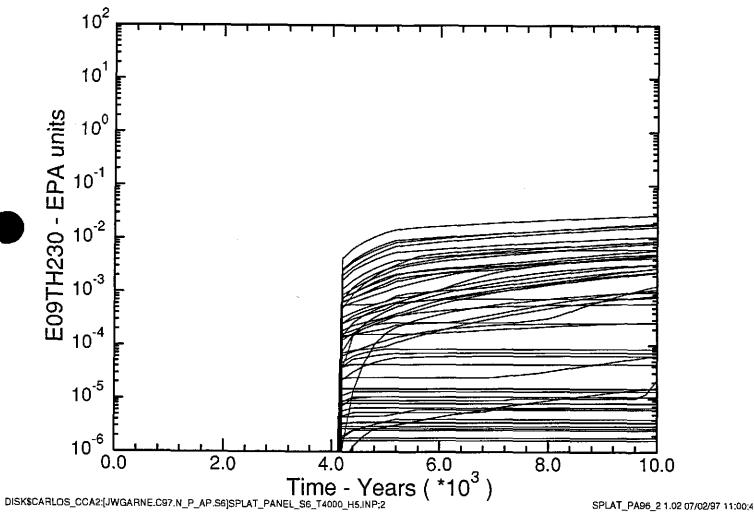
CIIB

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T4000) U-234 Integrated Discharge up Borehole at MB138



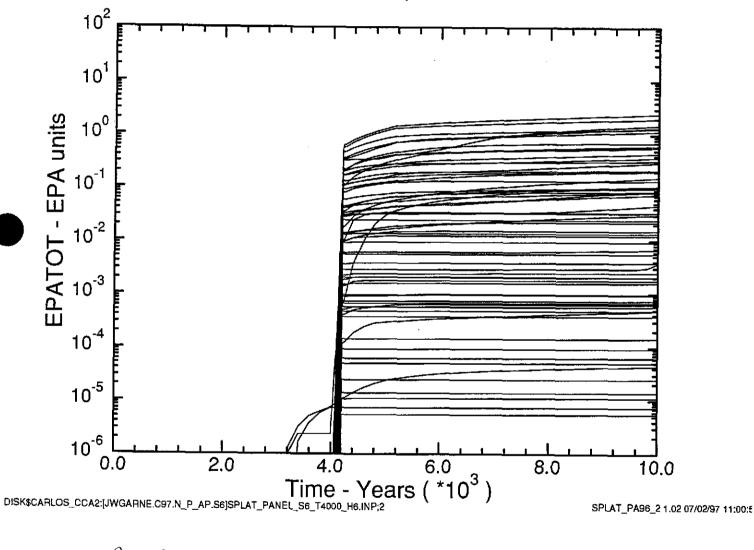
C119

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T4000) Th-230 Integrated Discharge up Borehole at MB138



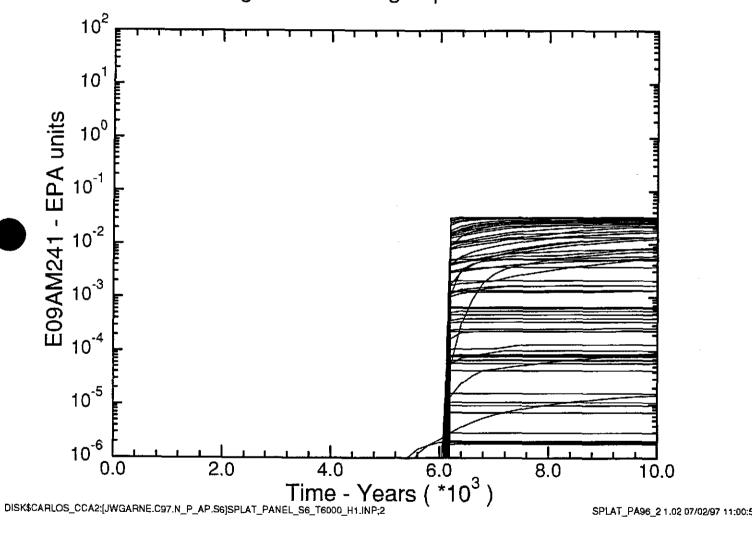
C/20

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T4000)
Total Integrated Discharge up Borehole at MB138



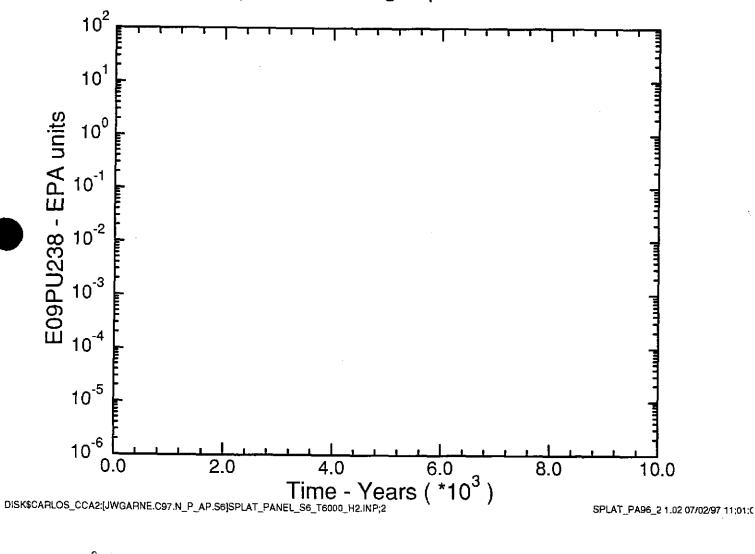
C/21

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T6000) Am-241 Integrated Discharge up Borehole at MB138



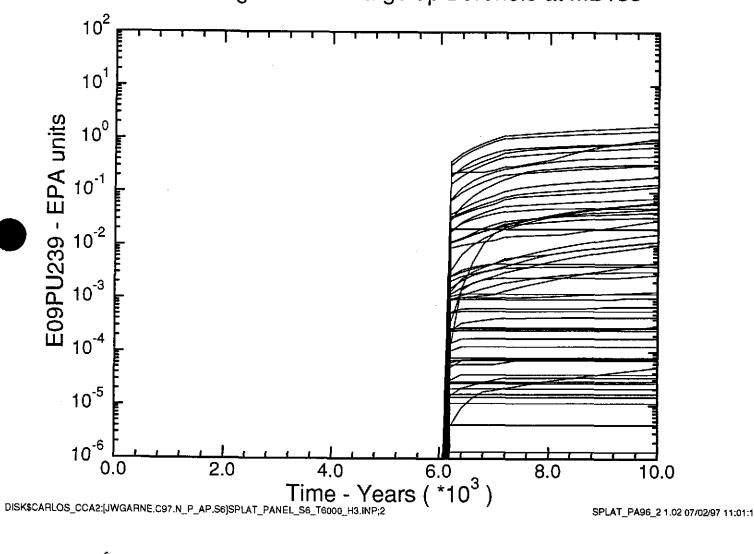
0/22

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T6000) Pu-238 Integrated Discharge up Borehole at MB138



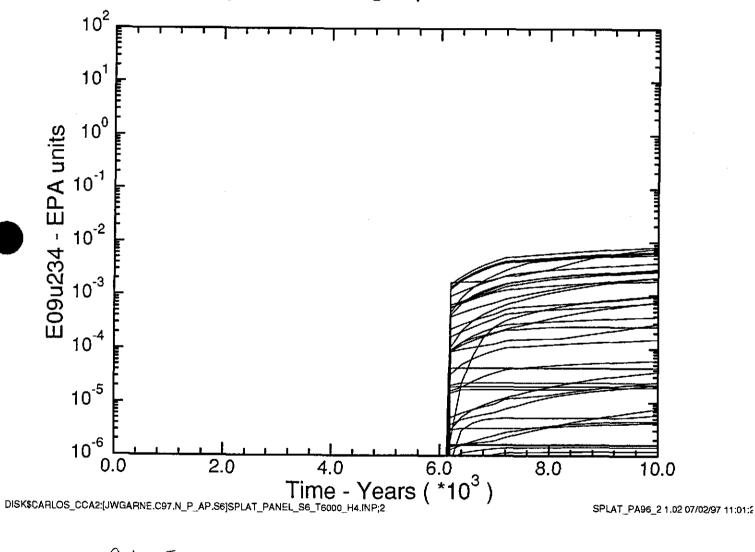
0123

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T6000) Pu-239 Integrated Discharge up Borehole at MB138



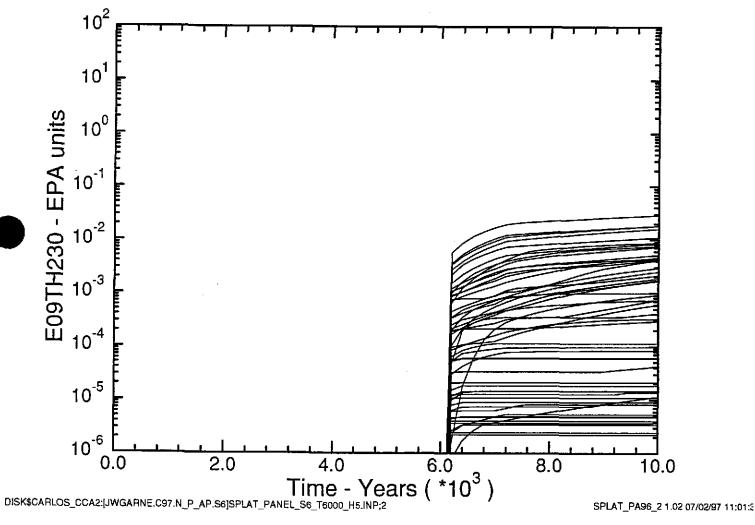
C124

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T6000)
U-234 Integrated Discharge up Borehole at MB138



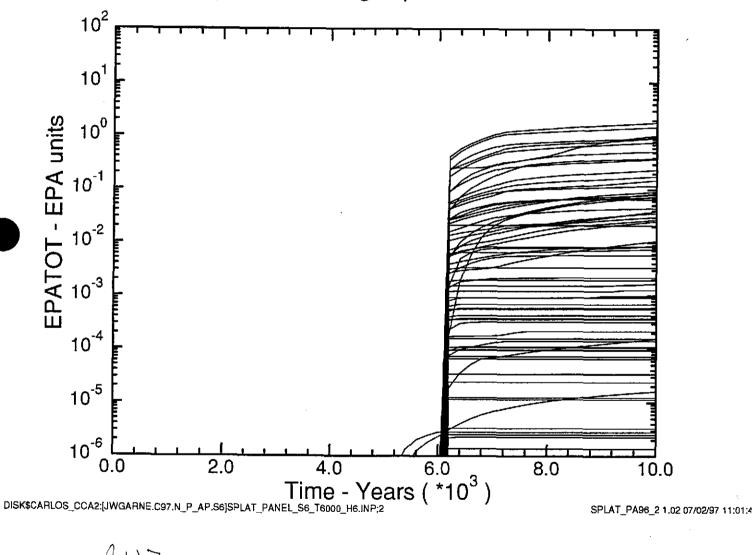
0125

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T6000) Th-230 Integrated Discharge up Borehole at MB138



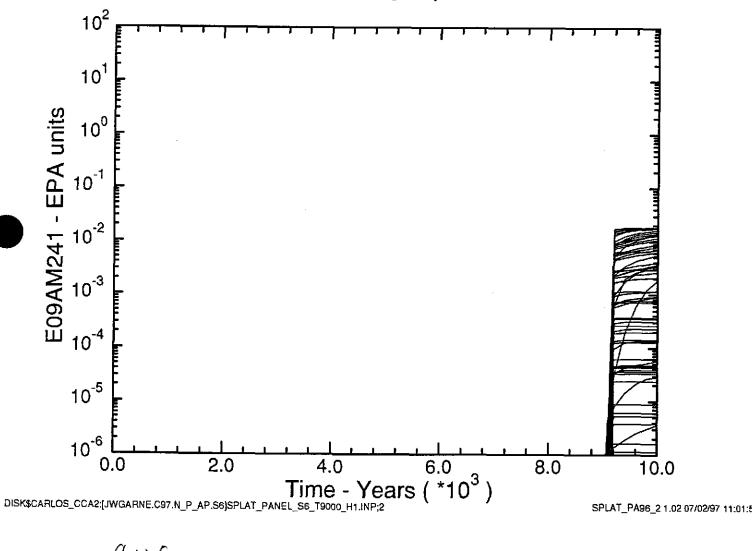
C126

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T6000) Total Integrated Discharge up Borehole at MB138



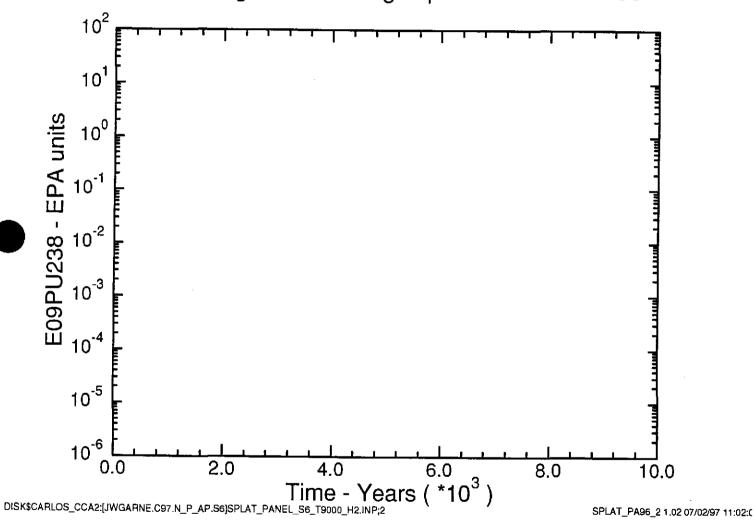
0127

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T9000) Am-241 Integrated Discharge up Borehole at MB138



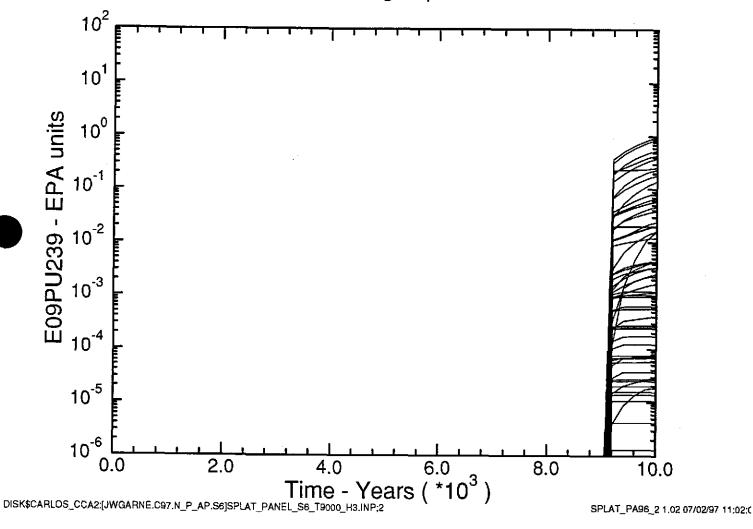
C128

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T9000) Pu-238 Integrated Discharge up Borehole at MB138



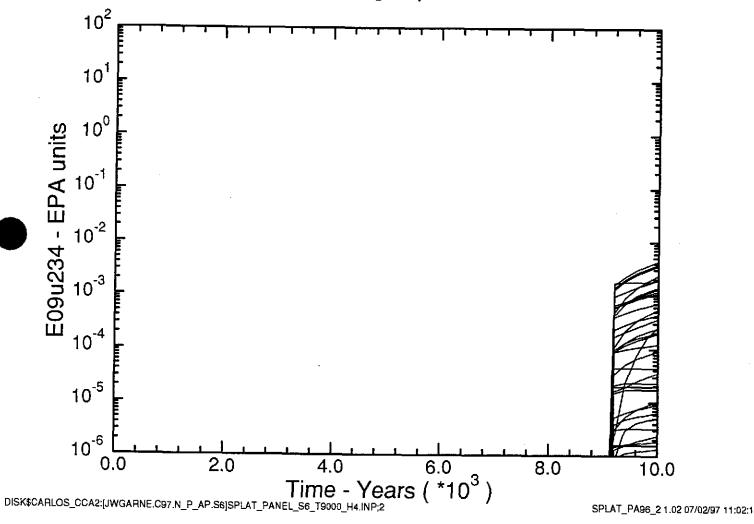
0129

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T9000) Pu-239 Integrated Discharge up Borehole at MB138



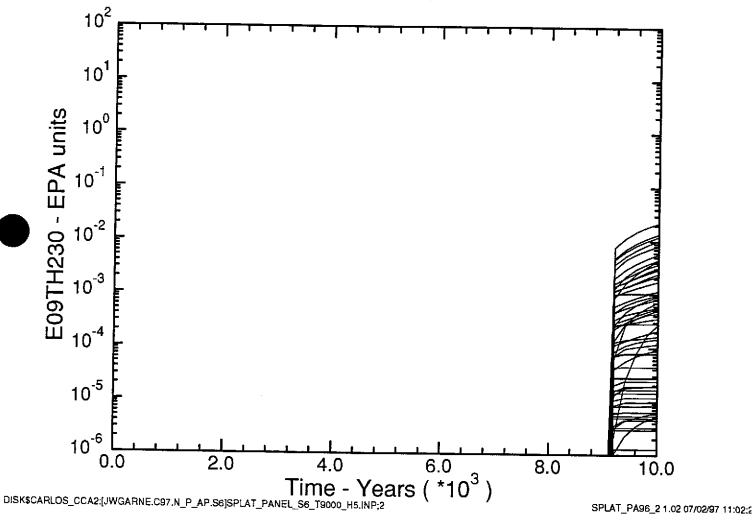
C130

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T9000) U-234 Integrated Discharge up Borehole at MB138



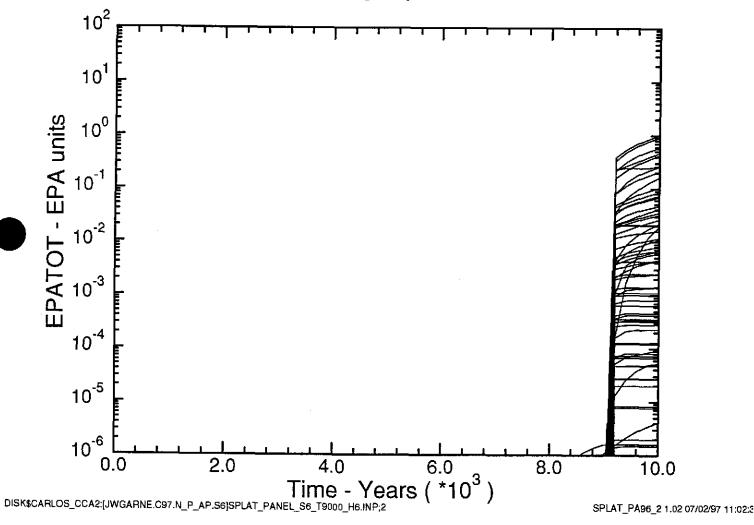
0131

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T9000) Th-230 Integrated Discharge up Borehole at MB138



C132

SNL WIPP PA96: PANEL SIMULATIONS (C97 S6 T9000) Total Integrated Discharge up Borehole at MB138



C133

Table C.1. S1.

vector	time	EILW_MBS	E2LW_MBS	E3LW_MBS	E4LW_MBS	E5LW_MBS	EPALWMBT	EPALWM9S
_		²⁴¹ Am	²³⁹ Pu	²³⁸ Pu	²³⁴ U	²³⁰ Th	Total - All MB	Total - MB139S
38	10000	8.67E-11	3.40E-10	2.05E-17	2.74E-11	2.96E-11	4.84E-10	4.84E-10
58	10000	3.15E-20	1.87E-17	3.52E-30	1.38E-19	3.80E-19	1,93E-17	1.93E-17
26	10000	8.94E-23	1.12E-17	0.00E+00	2.82E-21	2.35E-20	1.13E-17	1.13E-17
_ 8	10000	1.46E-21	3.59E-19	0.00E+00	2.56E-20	2.80E-20	4.14E-19	4.14E-19

Table C.2. s2 at 100.

vector	time	EPA1BHRC		EPA3BHRC	EPA4BHRC	EPA5BHRC	EPATBHRC
		²⁴¹ Am	²³⁹ Pu_	²³⁸ Pu	²³⁴ U	²³⁰ Th	Total - All MB
28	10000	2.33E+00	5.36E-01	3.15E-02	3.06E-04	3.15E-03	2.90E+00
80	10000	1.34E+00	2.19E-01	1.20E-02	1.83E-03	6.34E-04	1.58E+00
54	10000	6.83E-01	6.44E-01	1.53E-02	2.14E-03	1.56E-03	1.35E+00
83	10000	2.50E-01	9.66E-01	1.01E-02	6.59E-03	8.86E-04	1.23E+00
53	10000	9.59E-01	9.13E-02	3.24E-03	1.86E-03	1.02E-03	1.06E+00
55	10000	6.69E-01	3.09E-01	1.75E-02	1.65E-03	1.11E-03	9.99E-01
81	10000	3.42E-01	4.80E-01	6.07E-02	1.01E-03	9.13E-04	8.84E-01
5	10000	5.21E-01	2.79E-01	1.04E-02	1.54E-03	9.62E-04	8.14E-01
72	10000	3.46E-01	3.01E-01	6.60E-03	2.48E-03	1.30E-03	6.58E-01
57	10000	2.27E-01	3.94E-01	2.28E-02	1.36E-03	1.08E-03	6.46E-01
60	10000	5.75E-01	2.09E-02	2.48E-04	3.50E-05	6.89E-04	5.97E-01
66	10000	2.97E-01	2.33E-01	9.77E-03	6.49E-04	3.52E-04	5.41E-01
74	10000	2.09E-01	3.06E-01	1.44E-02	2.16E-03	8.05E-04	5.32E-01
88	10000	3.47E-01	6.36E-02	9.05E-04	1.12E-04	1.68E-03	4.13E-01
29	10000	3.22E-01	6.11E-02	2.69E-03	1.40E-03	5.75E-04	3.88E-01
30	10000	2.11E-01	7.56E-02	3.75E-03	2.29E-03	6.97E-04	2.94E-01
64	10000	1.83E-01	4.51E-02	1.52E-03	5.97E-05	1.08E-03	2.31E-01
82	10000	1.4 8 E-01	3.11E-02	5.98E-03	1.49E-04	1.53E-04	1.86E-01
51	10000	1.48E-01	2.80E-02	1.12E-03	4.32E-04	1.87E-04	1.78E-01
49	10000	1.70E-01	9.89E-04	9.07E-05	2.16E-06	4.10E-05	1.72E-01
50	10000	1.21E-01	2.10E-02	6.47E-04	3.87E-05	7.39E-04	1.43E-01
97	10000	7.52E-02	3.00E-02	1.21E-03	1.04E-03	1.39E-04	1.08E-01
43	10000	2.72E-02	6.88E-02	2.85E-03	2.53E-04	1.65E-04	9.93E-02
33	10000	7.69E-02	2.94E-03	5.98E-04	5.33E-07	1.99E-05	8.05E-02
	10000	5.35E-02	1.25E-02	2.32E-05	1.83E-05	3.59E-04	6.64E-02
	10000	5.70E-02	5.76E-03	3.98E-04	7.63E-06	1.46E-04	6.33E-02
	10000	4.98E-02	2.02E-03	2.76E-04	2.54E-06	4.68E-05	5.22E-02
i i	10000	3.67E-02	1.22E-02	4.44E-05	2.41E-05	4.68E-04	4.95E-02
	10000	3.89E-02	2.14E-03	1.25E-04	3.99E-06	7.83E-05	4.12E-02
	10000	1.40E-02	1.34E-03	5.13E-05	3.94E-06	7.70E-05	1.54E-02
	10000	6.60E-03	3.13E-04	1.80E-04	4.42E-06	3.36E-06	7.11E-03
	10000	5.92E-03	1.13E-03	1. 88E- 05	1.22E-06	2.24E-05	7.08E-03
7	10000	6.85E-03	1.58E-04	7.23E-06	1.04E-05	6.25E-06	7.04E-03

1	100	10000	4.40E-03	2.84E-04	3.93E-06	8.75E-07	1.58E-05	4.71E-03	I
	52	10000	3.86E-03	4.83E-04	1.16E-05	1.17E-06	2.04E-05	4.38E-03	1
	2	10000	3.58E-03	5.52E-04	1.51E-04	3.26E-06	2.38E-06	4.29E-03	١
	24	10000	3.60E-03	6.32E-04	1.87E-06	1.46E-06	1.83E-05	4.25E-03	
İ	34	10000	1.44E-03	5.19E-05	2.81E-05	7.55E-08	1.15E-06	1.52E-03	
1	46	10000	1.40E-03	1.22E-05	1.23E-06	1.98E-08	3.01E-07	1.42E-03	İ
ľ	1	10000	6.67E-04	1.65E-04	2.37E-07	3.18E-07	5.36E-06	8.38E-04	1
	45	10000	5.42E-04	1.03E-04	2.28E-07	3.79E-07	5.97E-06	6.52E-04	İ
1	16	10000	5.26E-04	1.53E-05	3.14E-06	3.33E-08	5.40E-07	5.45E-04	
	90	10000	2.89E-04	7.36E-07	2.32E-07	2.69E-09	4.35E-08	2.90E-04	
l	7	10000	2.18E-04	5.73E-06	1.63E-07	1.38E-08	2.29E-07	2.24E-04	1
ĺ	31	10000	5.78E-05	1.62E-05	1.93E-06	1.28E-08	7.05E-08	7.60E-05	l
	27	10000	1.10E-06	6.97E-05	1.59E-11	7.02E-08	9.93E-08	7.09E-05	
ł	22	10000	8.57E-09	2.23E-05	1.47E-18	4.64E-07	1.97E-07	2.30E-05	
	98	10000	7.32E-06	2.06E-06	3.85E-10	5.72E-09	7.80E-08	9.47E-06	
	9	10000	4.92E-07	7.61E-06	1.68E-13	8.30E-07	2.06E-07	9.13E-06	
ĺ	96	10000	7.85E-06	4.87E-07	7.40E-09	1.28E-09	1.92E-08	8.37E-06	l
l	73	10000	7.08E-06	5.26E-07	1.24E-08	1.34E-09	1.79E-08	7.64E-06	
	67	10000	1.46E-06	5.69E-06	6.69E-12	6.84E-09	4.33E-08	7.20E-06	
	56	10000	1.78E-06	4.71E-07	3.67E-09	1.98E-09	6.55E-09	2.26E-06	l
	14	10000	1.36E-08	5.48E-07	1.88E-15	8.53E-10	8.15E-09	5.70E-07	l
	20	10000	6.56E-10	1.62E-07	3.08E-18	5.13E-09	7.96E-09	1.76E-07	l
	84	10000	5. 96E- 11	1.18E-07	2.07E-19	4.44E-09	4.56E-09	1.27E-07	
	23	10000	6.34E-13	3.41E-08	6.91E-21	8.78E-12	6.87E-11	3.41E-08	
7	70	10000	1.50E-11	2.45E-10	6.75E-17	4.18E-13	5.35E-12	2.66E-10	l
l	95	10000	5.28E-19	7.30E-11	0.00E+00	7.39E-14	6.48E-14	7.32E-11	
ĺ	99	10000	9.85E-14	5.57E-11	4.09E-22	1.20E-13	1.72E-12	5.77E-11	
	77	10000	2.64E-13	2.78E-11	3.93E-20	6.41E-13	6.89E-13	2.94E-11	ĺ
	78	10000	2.64E-13	2.78E-11	3.93E-20	6.41E-13	6.89E-13	2.94E-11	
	68	10000	4.65E-17	1.39E-12	1.58E-26	6.41E-14	8.24E-14	1.54E-12	
	44	10000	3.00E-17	8.05E-13	5.71E-28	9.03E-16	1.24E - 14	8.18E-13	
	42	10000	1.86E-20	6.39E-18	4.50E-24	3.13E-20	2.29E-20	6.47E-18	
	13	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	
	38	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	ĺ
	48	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	
L	58	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	

Table C.3. s2 at 350 years.

vector	time	EPA1BHRC	EPA2BHRC	EPA3BHRC	EPA4BHRC	EPA5BHRC	EPATBHRC
		²⁴¹ Am	²³⁹ Pu	²³⁸ Pu	234 U	²³⁰ T h	Total - All MB
28	10000	1.96E+00	5.32E-01	1.79E-02	3.02E-04	3.15E-03	2.51E+00
80	10000	1.23E+00	2.08E-01	1. 09E-02	1.79E-03	6.22E-04	1.45E+00
83	10000	1.82E-01	9.62E-01	5.14E-03	6.57E-03	8.82E-04	1.16E+00
54	10000	3.81E-01	6.10E-01	1.44E-02	2.10E-03	1.53E-03	1.01E+00
55	10000	6.64E-01	2.99E-01	1.17E-02	1.60E-03	1.08E-03	9.78E-01
81	10000	3.38E-01	4.69E-01	3.18E-04	9.92E-04	9.19E-04	8.09E-01

1 -								
5	10000		2.76E-01	8.95E-03	1.49E-03	9.39E-04	7.79E-01	
53	10000	6.08E-01	8.98E-02	3.21E-05	1.84E-03	1.01E-03	7.01E-01	
57	10000	2.25E-01	3.87E-01	2.23E-02	1.34E-03	1.07E-03	6.37E-01	
60	10000	5.78E-01	2.05E-02	2.48E-04	3.43E-05	6.76E-04	6.00E-01	
72	10000	2.88E-01	2.97E-01	5.54E-03	2.43E-03	1.27E-03	5.94E-01	۱
74	10000	2.07E-01	3.04E-01	2.79E-03	2.13E-03	7.89E-04	5.17E-01	ļ
66	10000	2.32E-01	2.32E-01	6.46E-05	7.14E-04	3.50E-04	4.65E-01	ĺ
29	10000	3.15E-01	5.98E-02	2.43E-03	1.37E-03	5.64E-04	3.80E-01	
30	10000	2.11E-01	7.38E-02	9.14E-04	2.23E-03	6.80E-04	2.89E-01	
88	10000	2.20E-01	6.27E-02	2.03E-05	1.10E-04	1.66E-03	2.85E-01	ļ
64	10000	1.84E-01	4.41E-02	1.34E-03	5.84E-05	1.05E-03	2.30E-01	i
82	10000	1.48E-01	3.11E-02	6.91E-05	1.46E-04	1.54E-04	1.79E-01	
49	10000	1.68E-01	9.89E-04	8.95E-05	2.16E-06	4.10E-05	1.69E-01	
51	10000	1.28E-01	2.66E-02	9.25E-04	4.09E-04	1.76E-04	1.56E-01	ł
50	10000	1.09E-01	2.04E-02	6.40E-04	3.77E-05	7.20E-04	1.31E-01	Ì
97	10000	7.93E-02	2.98E-02	1.01E-03	1.01E-03	1.37E-04	1.11E-01	١
43	10000	2.70E-02	6.69E-02	1.07E-05	2.76E-04	1.63E-04	9.44E-02	
33	10000	7.05E-02	2.82E-03	6.89E-07	4.85E-07	1.90E-05	7.33E-02	l
86	10000	5.27E-02	1.22E-02	2.31E-05	1.79E-05	3.50E-04	6.53E-02	
39	10000	5.70E-02	5.76E-03	8.02E-07	7.38E-06	1.45E-04	6.29E-02	
35	10000	4.98E-02	2.02E-03	2.41E-04	2.54E-06	4.68E-05	5.21E-02	
26	10000	3.54E-02	1.15E-02	3.95E-05	2.28E-05	4.42E-04	4.74E-02	l
75	10000	3.38E-02	2.11E-03	1.24E-04	3.93E-06	7.72E-05	3.61E-02	
32	10000	9.66E-03	1.34E-03	5.08E-05	3.94E-06	7.73E-05	1.11E-02	
21	10000	6.61E-03	3.13E-04	1.79E-04	4.43E-06	3.36E-06	7.11E-03	İ
69	10000	5.92E-03	1.12E-03	6.50E-08	1.14E-06	2.22E-05	7.06E-03	l
100	10000	4.40E-03	2.82E-04	1.53E-07	8.12E-07	1.57E-05	4.70E-03	l
52	10000	3.86E-03	4.38E-04	8.07E-06	1.05E-06	1. 86E-0 5	4.33E-03	l
24	10000	3.65E-03	6.34E-04	1. 84E-0 6	1.45E-06	1.98E-05	4.30E-03	l
2	10000	3.58E-03	5.52E-04	1.44E-04	3.24E-06	2.38E-06	4.29E-03	ľ
17	10000	3.83E-03	1.56E-04	6.72E-06	1.04E-05	6.25E-06	4.01E-03	l
34	10000	1.44E-03	5.19E-05	2.74E-05	7.52E-08	1.15E-06	1.52E-03	l
46	10000	1.32E-03	1.22E-05	2.50E-08	1.55E-08	3.01E-07	1.34E-03	l
13	[10000]	8.55E-04	1.95E-05	2.62E-07	2.86E-08	5.61E-07	8.76E-04	ĺ
1	10000	6.41E-04	1.60E-04	1.06E-08	2.6 8E -07	5.18E-06	8.07E-04	ı
45	10000	5.42E-04	1.01E-04	2.27E-07	3.68E-07	5.81E-06	6.49E-04	١
16	10000	5.26E-04	1.53E-05	1.32E-08	2.75E-08	5.39E-07	5.42E-04	l
90	10000	2.83E-04	7.07E-07	2.25E-07	2.59E-09	4.35E-08	2.84E-04	ĺ
7	10000	2.17E-04	5.69E-06	1.63E-07	1.38E-08	2.30E-07	2.23E-04	l
31	10000	5.78E-05	1.62E-05	1.42E-06	1.05E-08	7.07E-08	7.54E-05	l
27	10000	1.10E-06	6.86E-05	5.66E-13	4.92E-08	8.72E-08	6.99E-05	
98	10000	7.33E-06	2.05E-06	8.46E-13	3.95E-09	7.72E-08	9.46E-06	
9	10000	4.13E-07	7.37E-06	2.43E-15	8.01E-07	1.99E-07	8.78E-06	
96	10000	7.86E-06	4.85E-07	6.35E-09	1.24E-09	1.92E-08	8.37E-06	
73	10000	7.08E-06	4.73E-07	1.09E-08	1.20E-09	1.79E-08	7.58E-06	
67	10000	1.33E-06	5.62E-06	6.62E-12	6.64E-09	4.26E-08	7.00E-06	
22	10000	2.76E-09	5.19E-06	7.14E-19	1.08E-07	4.60E-08	5.34E-06	

56	10000	1.78E-06	4.71E-07	1.16E-10	1.66E-09	6.50E-09	2.26E-06
14	10000	1.19E-08	5.34E-07	8.50E-16	8.11E-10	7.92E-09	5.55E-07
20	10000	6.52E-10	1.11E-07	3.96E-20	4.74E-09	7.38E-09	1.24E-07
84	10000	5.91E-11	1.08E-07	1.94E-19	4.05E-09	4.12E-09	1.17E-07
23	10000	6.22E-13	3.05E-08	3.28E-21	7.38E-12	6.07E-11	3.05E-08
70	10000	1.50E-11	2.38E-10	3.78E-20	3.17E-13	5.12E-12	2.58E-10
99	10000	9.84E-14	5.09E-11	4.06E-22	1.10E-13	1.60E-12	5.27E-11
77	10000	2.62E-13	2.41E-11	2.56E-20	6.12E-13	6.55E-13	2.56E-11
78	10000	2.62E-13	2.41E-11	2.56E-20	6.12E-13	6.55E-13	2.56E-11
68	10000	4.39E-17	1.00E-12	1.80E-28	4.53E-14	5.72E-14	1.11E-12
44	10000	1.69E-17	3.27E-13	5.44E-29	3.64E-16	5.01E-15	3.32E-13
95	10000	3.72E-22	4.13E-19	0.00E+00	1.49E-21	2.49E-20	4.40E-19
38	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
42	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
48	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
58	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00

Table C.4. s3 at 1000 years.

vector	time	EPA1BHRC	EPA2BHRC			EPA5BHRC	EPATBHRC
		²⁴¹ Am	²³⁹ Pu	²³⁸ Pu	²³⁴ U	²³⁰ Th	Total - All MB
28	10000	5.83E-01	5.20E-01	2.95E-06	2.84E-04	2.82E-03	1.11E+00
54	10000	1.16E-01	6.46E-01	2.93E-05	2.21E-03	1.42E-03	7.66E-01
83	10000	4.11E-02	6.53E-01	5.00E-05	4.45E-03	5.94E-04	6.99E-01
55	10000	2.79E-01	2.31E-01	8.47E-05	1.21E-03	7.54E-04	5.12E-01
72	10000	1. 17E-01	3.39E-01	4.03E-08	2.32E-03	1.19E-03	4.60E-01
57	10000	3.08E-02	3.86E-01	7.08E-05	1.31E-03	9.92E-04	4.19E-01
5	10000	1.00E-01	2.76E-01	4.97E-06	1.69E-03	9.60E-04	3.79E-01
81	10000	1.44E-02	3.27E-01	3.36E-07	6.68E-04	5.15E-04	3.43E-01
53	10000	2.51E-01	8.20E-02	1.56E-06	1.63E-03	8.15E-04	3.36E-01
74	10000	8.47E-03	2.60E-01	3.58E-10	1.47E-03	5.46E-04	2.71E-01
66	10000	3.49E-02	2.33E-01	5.56E-07	7.44E-04	3.36E-04	2.69E-01
80	10000	6.14E-02	1.97E-01	7.57E-06	1.41E-03	4.72E-04	2.61E-01
64	10000	1.08E-01	4.77E-02	4.88E-06	6.29E-05	1.05E-03	1.57E-01
29	10000	7.89E-02	6.03E-02	4.91E-06	1.24E-03	4.71E-04	1.41E-01
60	10000	1.08E-01	1.52E-02	3.87E-07	2.55E-05	5.03E-04	1.24E-01
88	10000	5.04E-02	6.46E-02	5.62E-07	1.13E-04	1.66E-03	1.17E-01
43	10000	1.85E-02	5.41E-02	2.53E-07	2.89E-04	1.52E-04	7.30E-02
97	10000	3.75E-02	1.97E-02	5.60E-06	8.04E-04	9.73E-05	5.81E-02
82	10000	2.28E-02	2.11E-02	2.21E-07	9.86E-05	9.21E-05	4.41E-02
50	10000	1.04E-02	2.01E-02	3.76E-08	3.70E-05	6.94E-04	3.11E-02
86	10000	1.51E-02	9.69E-03	2.49E-07	1.41E-05	2.78E-04	2.51E-02
32	10000	1.57E-02	1.35E-03	3.99E-07	3.91E-06	7.67E-05	1.72E-02
75	10000	1.26E-02	2.09E-03	1.44E-07	3.87E-06	7.63E-05	1.48E-02
26	10000	2.45E-05	7.50E-03	1.33E-16	1.45E-05	2.86E-04	7.82E-03
21	10000	4.86E-03	4.29E-04	2.75E-07	7.39E-06	5.62E-06	5.31E-03
51	10000	2.66E-03	6.09E-04	7.95E-08	9.26E-06	4.13E-06	3.28E-03

39	10000	2.51E-03	1.84E-04	1.62E-08	2.34E-07	4.61E-06	2.70E-03
100	10000	8.71E-04	2.99E-05	3.53E-09	8.40E-08	1.65E-06	9.02E-04
69	10000	8.10E-04	4.75E-05	5.63E-09	4.61E-08	9.22E-07	8.58E-04
13	10000	5.52E-04	1.78E-05	1.28E-08	2.60E-08	5.10E-07	5.70E-04
34	10000	4.03E-04	3.60E-05	5.05E-09	4.09E-08	9.12E-07	4.40E-04
1	10000	3.15E-04	3.50E-05	7.71E-10	5.50E-08	1.07E-06	3.51E-04
24	10000	2.87E-04	1.59E-05	1.32E-08	2.51E-08	4.43E-07	3.03E-04
45	10000	2.04E-04	4.18E-05	9.71E-11	1.24E-07	2.42E-06	2.49E-04
46	10000	2.19E-04	8.38E-06	4.57E-10	1.06E-08	2.06E-07	2.28E-04
52	10000	2.11E-04	7.14E-06	2.40E-08	1.47E-08	2.57E-07	2.18E-04
90	10000	2.08E-04	1.43E-06	8.54E-10	4.51E-09	8.83E-08	2.10E-04
16	10000	1.62E-04	1.13E-05	1.58E-10	2.03E-08	3.99E-07	1.74E-04
35	10000	3.87E-05	1.12E-06	6.21E-10	1.31E-09	2.57E-08	3.99E-05
27	10000	6.05E-10	5.35E-06	1.43E-19	4.02E-09	8.26E-09	5.37E-06
98	10000	1.40E-06	8.55E-07	8.88E-17	1.66E-09	3.26E-08	2.29E-06
9	10000	8.64E-10	1.09E-06	6.45E-21	1.07E-07	6.91E-08	1.27E-06
67	10000	5.27E-11	2.41E-07	1.56E-22	2.22E-10	2.08E-09	2.43E-07
84	10000	1.28E-11	3.48E-08	5.01E-24	1.24E-09	1.23E-09	3.73E-08
14	10000	6.12E-13	5.90E-09	8.39E-26	4.91E-12	9.40E-11	5.99E-09
23	10000	3.59E-14	3.11E-09	1.98E-24	4.26E-13	5.87E-12	3.12E-09
70	10000	5.17E-13	3.05E-11	1.21E-23	4.05E-14	7.83E-13	3.19E-11
68	10000	5.14E-17	1.12E-12	0.00E+00	4.92E-14	6.11 E -14	1.23E-12
41	10000	1.20E-16	1.62E-13	8.81E-29	3.97E-16	7.50E-15	1.70E-13
38	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00

Table C.5. s3 at 3000 years.

vector	time	EPA1BHRC	EPA2BHRC	EPA3BHRC	EPA4BHRC	EPA5BHRC	EPATBHRC
		241Am	²³⁹ Pu	²³⁸ Pu	²³⁴ U	²³⁰ Th	Total - All MB
83	10000	3.03E-02	6.15E-01	2.03E-08	4.20E-03	5.69E-04	6.50E-01
54	10000	1.18E-02	5.42E-01	2.94E-08	1.87E-03	1.17E-03	5.57E-01
28	10000	1.72E-02	4.78E-01	2.29E-08	2.48E-04	2.46E-03	4.98E-01
57	10000	1.29E-02	3.38E-01	1.36E-06	1.13E-03	8.44E-04	3.53E-01
72	10000	2.43E-06	3.46E-01	2.28E-10	1.93E-03	9.91E-04	3.49E-01
55	10000	7.29E-02	2.08E-01	2.14E-07	1.09E-03	6.76E-04	2.82E-01
81	10000	2.69E-04	2.37E-01	1.29E-10	5.47E-04	4.94E-04	2.39E-01
5	10000	6.69E-03	2.25E-01	4.12E-08	1.40E-03	7.79E-04	2.34E-01
74	10000	4.77E-08	2.31E-01	1.14E-12	1.17E-03	4.41E-04	2.32E-01
66	10000	1.10E-06	1. 84E -01	9.36E-11	6.06E-04	3.05E-04	1.85E-01
80	10000	1.07E-03	1.60E-01	2.51E-08	1.11E-03	3.70E-04	1.63E-01
53	10000	1.24E-02	7.03E-02	2.21E-08	1.48E-03	7.49E-04	8.49E-02
29	10000	1.09E-02	5.05E-02	1.51E-07	1.06E-03	3.97E-04	6.28E-02
88	10000	2.13E-03	5.59E-02	1.21E-08	9.82E-05	1.43E-03	5.96E-02
64	10000	7.24E-03	3.93E-02	5.55E-08	5.18E-05	8.59E-04	4.74E-02
43	10000	1.54E-05	3.90E-02	5.51E-10	2.44E-04	1.29E-04	3.93E-02
97	10000	2.08E-03	1.97E-02	1.66E-08	8.04E-04	9.70E-05	2.27E-02
82	10000	8.59E-04	2.11E-02	4.55E-10	9.86E-05	9.20E-05	2.21E-02

60	10000	3.47E-03	1.26E-02	5.34E-09	2.11E-05	4.15E-04	1.65E-02
50	10000	4.09E-06	1.58E-02	1.32E-10	2.91E-05	5.38E-04	1.64E-02
86	10000	7.34E-04	7.50E-03	2.27E-09	1.09E-05	2.16E-04	8.46E-03
32	10000	1.10E-03	1.35E-03	1.57E-08	3.91E-06	7.67E-05	2.53E-03
75	10000	5.99E-04	1.76E-03	2.40E-09	3.26E-06	6.43E-05	2.43E-03
51	10000	1.56E-03	6.09E-04	5.06E-11	9.25E-06	4.13E-06	2.18E-03
26	10000	2.39E-07	1.89E-03	7.17E-19	3.65E-06	7.20E-05	1.97E-03
39	10000	1.10E-03	1.84E-04	2.80E-11	2.41E-07	4.62E-06	1.29E-03
21	10000	1.31E-06	4.29E-04	5.01E-10	7.39E-06	5.63E-06	4.44E-04
100	10000	3.96E-04	3.06E-05	3.66E-10	8.57E-08	1.64E-06	4.28E-04
69	10000	8.81E-05	4.77E-05	3.27E-11	4.62E-08	9.01E-07	1.37E-04
24	10000	7.40E-05	1.55E-05	2.54E-11	2.53E-08	4.27E-07	8.99E-05
13	10000	3.38E-05	1.78E-05	1.30E-09	2.60E-08	5.10E-07	5.21E-05
34	10000	2.42E-06	3.60E-05	2.19E-10	4.11E-08	8.17E-07	3.93E-05
1	10000	3.04E-06	3.49E-05	2.68E-12	5.49E-08	1.08E-06	3.91E-05
45	10000	4.68E-06	3.13E-05	1.23E-13	9.03E-08	1. 76E-06	3.78E-05
52	10000	1.98E-05	8.16E-06	1.66E-08	1.68E-08	2.87E-07	2.82E-05
90	10000	2.20E-05	1.43E-06	1.56E-11	4.51E-09	8.84E-08	2.35E-05
46	10000	6.51E-06	8.41E-06	3.74E-12	1.13E-08	2.07E-07	1.51E-05
16	10000	6.42E-08	1.13E-05	9.06E-13	2.03E-08	3.98E-07	1.18E-05
35	10000	3.15E-06	1.13E-06	1.17E-11	1.31E-09	2.57E-08	4.31E-06
27	10000	6.19E-11	2.35E-06	2.22E-23	1.72E-09	3.42E-09	2.35E-06
98	10000	6.16E-11	7.93E-07	1.15E-18	1.54E-09	3.01E-08	8.25E-07
9	10000	1.89E-12	4.56E-07	1.33E-23	4.40E-08	2.67E-08	5.27E-07
67	10000	3.30E-12	6.62E-08	1.15E-25	6.00E-11	5.58E-10	6.68E-08
84	10000	2.61E-14	1.05E-08	2.67E-27	3.65E-10	3.33E-10	1.12E-08
23	10000	3.25E-15	5.20E-10	2.34E-27	6.67E-14	9.48E-13	5.21E-10
14	10000	8.38E-15	1.81E-10	5.45E-25	1.62E-12	3.77E-12	1.86E-10
70	10000	5.27E-17	2.13E-11	5.43E-26	6.10E-13	8.56E-13	2.27E-11
68	10000	3.55E-22	5.1 8 E-14	0.00E+00	2.17E-15	2.36E-15	5.63E-14
41	10000	3.16E-19	2.33E-14	4.89E-30	5.51E-17	1.07E-15	2.44E-14
_ 38	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00

Table C.6. s3 at 5000 years.

vector	time	EPA1BHRC	EPA2BHRC	EPA3BHRC	EPA4BHRC	EPA5BHRC	EPATBHRC
		²⁴¹ Am	²³⁹ Рц	²³⁸ Pu	²³⁴ U	²³⁰ Th	Total - All MB
83	10000	6.60E-03	5.10E-01	1.53E-10	3.48E-03	5.64E-04	5.21E-01
28	10000	1.26E-03	4.38E-01	3.69E-12	2.09E-04	2.25E-03	4.42E-01
54	10000	2.86E-03	3.80E-01	1.46E-10	1.38E-03	8.95E-04	3.85E-01
57	10000	1.88E-03	2.86E-01	1.31E-06	1.10E-03	7.17E-04	2.90E-01
72	10000	3.59E-07	2.32E-01	2.88E-12	1.54E-03	8.02E-04	2.34E-01
55	10000	8.20E-03	2.02E-01	8.86E-10	1.08E-03	6.75E-04	2.12E-01
74	10000	1.17E-08	2.07E-01	1.44E-14	8.45E-04	3.25E-04	2.08E-01
5	10000	6.46E-04	1.73E-01	3.29E-11	1.09E-03	5.87E-04	1.75E-01
81	10000	2.19E-05	1.45E - 01	5.11E-13	4.12E-04	2.96E-04	1.46E-01
66	10000	1.50E-07	1.32E-01	7.81E-13	3.80E-04	2.74E-04	1.32E-01

				1	•		
80	10000	1	1.22E-01	2.36E-10	7.72E-04	2.97E-04	1.23E-01
53	10000		5.70E-02	1.19E-08	1.31E-03	7.20E-04	6.04E-02
88	10000	2.20E-04	4.60E-02	1.53E-10	8.07E-05	1.09E-03	4.74E-02
29	10000	1.68E-03	4.29E-02	1.91E-09	8.51E-04	4.16E-04	4.59E-02
64	10000	7.93E-04	3.12E-02	5.79E-11	4.12E-05	6.67E-04	3.27E-02
43	10000	1.97E-06	2.35E-02	3.26E-12	1.84E-04	1.19E-04	2.38E-02
82	10000	1.18E-05	2.11E-02	9.08E-13	9.86E-05	9.20E-05	2.13E-02
97	10000	2.90E-04	1.97E-02	1.52E-10	8.04E-04	1.15E-04	2.09E-02
50	10000	1.41E-06	1.14E-02	6.57E-13	2.10E-05	3.94E-04	I.18E-02
60	10000	4.76E-04	9.78E-03	4.58E-11	1.64E-05	3.22E-04	1.06E-02
86	10000	8.65E-05	4.84E-03	1.37E-11	7.05E-06	1.39E-04	5.07E-03
75	10000	1.16E-04	1.41E-03	2.99E-11	2.61E-06	5.14E-05	1.58E-03
32	10000	1.36E-04	1.33E-03	9.23E-11	3.85E-06	7.58E-05	1.54E-03
51	10000	7.55E-05	6.09E-04	5.90E-15	9.25E-06	4.13E-06	6.98E-04
21	10000	1.77E-07	4.29E-04	3.83E-12	7.39E-06	5.64E-06	4.43E-04
39	10000	1.38E-04	1.84E-04	1.42E-13	2.41E-07	4.62E-06	3.27E-04
100	10000	8.82E-05	2.96E-05	9.80E-13	8.28E-08	1.58E-06	1.20E-04
69	10000	2.07E-05	4.74E-05	2.77E-13	4.59E-08	8.95E-07	6.91E-05
34	10000	4.82E-08	3.60E-05	1.54E-12	4.11E-08	8.18E-07	3.69E-05
1	10000	4.24E-07	3.45E-05	2.82E-14	5.43E-08	1.07E-06	3.61E-05
45	10000	5.84E-07	2.16E-05	6.39E-16	6.06E-08	1.18E-06	2.34E-05
24	10000	7.79E-06	1.49E-05	4.04E-14	2.49E-08	4.20E-07	2.31E-05
13	10000	3.93E-06	1.78E-05	5.76E-12	2.60E-08	5.12E-07	2.22E-05
52	10000	3.58E-06	8.14E-06	1.65E-08	1.68E-08	2.88E-07	1.20E-05
16	10000	1.71E-08	1.11E-05	4.51E-15	2.03E-08	3.91E-07	1.15E-05
46	[10000]	8.17E-07	8.40E-06	2.12E-14	1.13E-08	2.09E-07	9.44E-06
90	10000	2.38E-06	1.43E-06	6.18E-14	4.51E-09	8.85E-08	3.91E-06
35	10000	5.03E-07	1.13E-06	9.45E-14	1.31E-09	2.57E-08	1.66E-06
98	10000	8.90E-12	6.50E-07	1.46E-20	1.25E-09	2.45E-08	6.76E-07
27	10000	2.23E-12	2.56E-07	8.80E-26	1.82E-10	3.46E-10	2.56E-07
9	[10000]	6.79E-14	6.13E-08	6.15E-26	5.82E-09	3.37E-09	7.05E-08
84	10000	1.63E-17	7.41E-10	2.25E-29	2.50E-11	2.10E-11	7.87E-10
67	10000	2.04E-14	7.33E-10	2.42E-28	6.38E-13	5.91E-12	7.39E-10
23	10000	8.25E-17	1.56E-11	1.11E-29	1.95E-15	2.74E-14	1.57E-11
70	10000	1.81E-17	1.13E-11	2.88E-28	3.17E-13	4.24E-13	1.20E-11
14	10000	2.50E-18	1.04E-13	3.83E-27	7.53E-14	3.65E-14	2.15E-13
68	10000	4.94E-24	8.52E-16	0.00E+00	3.39E-17	3.17E-17	9.17E-16
41	10000	9.03E-22	4.06E-17	2.05E-33	8.58E-20	1.64E-18	4.23E-17
26	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
38	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00

Table C.7. s3 at 7000 years.

vector	time	EPA1BHRC	EPA2BHRC	EPA3BHRC	EPA4BHRC	EPA5BHRC	EPATBHRC
		²⁴¹ Am	²³⁹ Pu	²³⁸ Pu	²³⁴ U	²³⁰ T h	Total - All MB
28	10000	1.34E-04	2.90E-01	8.41E-15	1.67E-04	1.51E-03	2.91E-01
54	10000	3.49E-04	2.79E-01	7.73E-13	1.04E-03	7.06E-04	2.82E-01

	83	10000	7.73E-04	2.73E-01	8.35E-13	1.86E-03	3.47E-04	2.76E-01	I
	57	10000	2.57E-04	2.34E-01	1.31E-06	9.14E-04	6.99E-04	2.36E-01	
	55	10000	9.96E-04	1.97E-01	2.66E-12	1.05E-03	7.39E-04	1.99E-01	
	72	10000	4.82E-08	1.86E-01	2.20E-14	1.08E-03	5.68E-04	1.88E-01	ļ
	74	10000	1.38E-09	1.49E-01	1.83E-16	5.00E-04	2.02E-04	1.50E-01	
	5	10000	8.18E-05	1.18E-01	3.57E-13	7.77E-04	4.77E-04	1.20E-01	
	80	10000	1.39E-05	8.87E-02	1.39E-12	5.00E-04	2.19E-04	8.94E-02	1
	66	10000	1.53E-08	8.28E-02	3.35E-15	2.53E-04	2.30E-04	8.33E-02	i
	81	10000	2.42E-06	7.03E-02	2.79E-15	2.61E-04	3.40E-04	7.10E-02	
	53	10000	1.80E-04	3.85E-02	1.18E-08	7.99E-04	5.36E-04	4.00E-02	İ
	88	10000	1.86E-05	3.48E-02	1.54E-09	6.10E-05	8.67E-04	3.57E-02	ŀ
1	29	10000	2.18E-04	3.36E-02	1.45E-11	7.13E-04	4.28E-04	3.50E-02	ļ
١	64	10000	6.74E-05	2.56E-02	6.94E-14	3.37E-05	5.80E-04	2.62E-02	
	82	10000	1.44E-06	2.11E-02	4.00E-15	9.86E-05	1.07E-04	2.02E-02 2.13E-02	
1	97	10000	2.74E-05	1.88E-02	6.20E-13	7.62E-04	1.07E-04 1.09E-04	1.97E-02	İ
	43	10000	2.40E-07	1.03E-02	1.64E-14	7.02E-04 7.13E-05	4.67E-05		١
	60	10000	6.25E-05	8.16E-03	5.06E-13	1.37E-05	i	1.04E-02	l
İ	50	10000	0.25E-07	7.03E-03	3.72E-15	1.37E-03 1.30E-05	2.69E-04	8.50E-03	ı
l	86	10000	1.01E-05	2.00E-03	1.10E-13	Į.	2.52E-04	7.29E-03	l
ļ	32	10000	1.65E-05	1.11E-03		2.91E-06	5.74E-05	2.07E-03	١
	75	10000	1.36E-05		4.64E-13	3.23E-06	6.35E-05	1.20E-03	l
١	73 51	10000		1.00E-03	2.80E-13	1.86E-06	3.67E-05	1.06E-03	
l		ł I	4.61E-06	6.09E-04	3.79E-19	9.25E-06	4.13E-06	6.27E-04	l
l	21	10000	2.22E-08	4.29E-04	2.09E-14	7.39E-06	5.64E-06	4.42E-04	l
	39	10000	1.70E-05	1.84E-04	7.36E-16	2.41E-07	4.62E-06	2.06E-04	l
Ī	69	10000	3.17E-06	4.62E-05	3.53E-15	4.47E-08	8.71E-07	5.03E-05	l
l	100	10000	9.56E-06	2.67E-05	3.32E-15	7.40E-08	1.41E-06	3.77E-05	l
l	34	10000	7.13E-09	3.60E-05	1.95E-14	4.11E-08	8.05E-07	3.69E-05	l
ĺ	I	10000	6.10E-08	3.13E-05	3.55E-16	4.91E-08	9.65E-07	3.24E-05	l
l	13	10000	4.38E-07	1.78E-05	1.92E-14	2.60E-08	5.12E-07	1.88E-05	l
	24	10000	7.98E-07	1.43E-05	6.63E-17	2.43E-08	4.12E-07	1.55E-05	l
ı	45	10000	7.10E-08	1.31E-05	3.19E-18	3.57E-08	7.00E-07	1.39E-05	
l	16	10000	2.16E-09	1.04E-05	2.55E-17	1.89E-08	3.65E-07	1.08 E-0 5	
l	52	10000	1.62E-06	7.94E-06	1.65E-08	1.63E-08	2.81E-07	9.87E-06	
	46	10000	1.13E-07	8.34E-06	1.76E-16	1.12E-08	2.08E-07	8.68E-06	
	90	10000	1.94E-07	1.43E-06	2.60E-16	4.51E-09	8.85E-08	1.72 E-06	
	35	10000	7.43E-08	1.13E-06	1.20E-15	1.31E-09	2.57E-08	1.23E-06	
	98	10000	1.06E-12	3.44E-07	1.82E-22	6.50E-10	1.28E-08	3.57E-07	
	27	10000	1.04E-15	3.08E-10	1.45E-29	2.15E-13	3.91E-13	3.09E-10	
	9	10000	5.40E-18	1.97E-11	1.19E-30	1.85E-12	1.09E-12	2.26E-11	
	70	10000	1.25E-18	2.67E-12	1.82E-30	7.33E-14	9.25E-14	2.84E-12	
	84	10000	6.34E-21	2.54E-13	0.00E+00	8.09E-15	5.18E-15	2.67E-13	
	67	10000	7.19E-19	4.16E-14	0.00E+00	3.47E-17	3.20E-16	4.19E-14	
	14	10000	1.33E-21	1. 50E- 15	4. 8 5E-29	3.25E-15	8.24E-16	5.58E-15	
	23	10000	3.00E-20	2.74E-15	0.00E+00	3.46E-19	4.45E-18	2.74E-15	
	41	10000	4.69E-24	1. 05E-17	0.00E+00	2.04E-20	3.75E-19	1.09E-17	
	68	10000	7.78E-27	1.93E-18	0.00E+00	7.40E-20	5.94E-20	2.06E-18	l
	26	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	

Table C.8. s3 at 9000 years.

vector	time	EPA1BHRC	EPA2BHRC	EPA3BHRC	EPA4BHRC	EPA5BHRC	EPATBHRC
		²⁴¹ Am	²³⁹ Pu	²³⁸ Pu	²³⁴ U	²³⁰ Th	Total - All MB
28	10000	6.01E-06	2.29E-01	5.98E-17	9.71E-05	1.26E-03	2.30E-01
54	10000	2.54E-05	1.61E-01	2.02E-07	5.53E-04	6.31E-04	1.62E-01
55	10000	1.13E-04	1.53E-01	1.56E-14	8.21E-04	5.76E-04	1.55E-01
57	10000	1.84E-05	1.45E-01	1.31E-06	5.80E-04	4.84E-04	1.46E-01
72	10000	4.85E-09	1.40E-01	1.19E-16	6.07E-04	4.19E-04	1.41E-01
74	10000	3.09E-11	8.46E-02	8.83E-19	2.25E-04	1.04E-04	8.50E-02
5	10000	3.61E-06	5.96E-02	4.20E-15	2.24E-04	2.51E-04	6.01E-02
83	10000	5.70E-05	5.74E-02	4.11E-15	3.91E-04	1.37E-04	5.79E-02
80	10000	1.57E-06	5.20E-02	6.92E-15	2.33E-04	1.30E-04	5.24E-02
66	10000	1.10E-09	5.15E-02	1.72E-17	2.56E-04	2.01E-04	5.19E-02
81	10000	1.04E-07	2.80E-02	1. 86E-17	1.25E-04	1.89E-04	2.83E-02
88	10000	1.85E-06	2.13E-02	1.51E-09	3.73E-05	5.28E-04	2.18E-02
29	10000	1.93E-05	1.42E-02	7.75E-14	3.10E-04	2.12E-04	1.47E-02
64	10000	6.69E-06	1.44E-02	4.60E-16	1.89E-05	3.14E-04	1.47E-02
82	10000	1.31E-07	1.19E-02	2.93E-17	5.55E-05	5.99E-05	1.20E-02
53	10000	1.63E-05	1. 08E-02	1.18E-08	1.41E-04	1.51E-04	1.11 E-0 2
97	10000	1.56E-06	9.74E-03	3.04E-15	3.70E-04	5.75E-05	1.02E-02
43	10000	2.92E-08	7.03E-03	8.32E-17	4.60E-05	3.00E-05	7.11E-03
50	10000	1.52E-07	3.66E-03	3.08E-17	6.76E-06	1.33E-04	3.80E-03
60	10000	1.58E-06	3.32E-03	2.31E-15	5.57E-06	1.10E-04	3.44E-03
75	10000	1.24E-06	4.07E-04	1.63E-15	7.54E-07	1.49E-05	4.24E-04
32	10000	1.55E-06	3.87E-04	2.26E-15	1.12E-06	2.19E-05	4.11E-04
21	10000	2.66E-09	3.49E-04	1.03E-16	6.09E-06	4.64E-06	3.60E-04
39	10000	1.13E-06	1.41E-04	3.52E-18	1.84E-07	3.51E-06	1.45E-04
51	10000	5.97E-08	6.56E-05	8.37E-23	9.93E-07	4.38E-07	6.70E-05
86	10000	3.78E-07	6.32E-05	2.64E-16	9.25E-08	1.80E-06	6.55E-05
69	10000	4.40E-07	3.96E-05	3.31E-17	3.82E-08	7.44E-07	4.08E-05
34	10000	1.02E-09	3.33E-05	2.47E-16	3.80E-08	7.44E-07	3.41E-05
100	10000	1.13E-06	1.92E-05	2.99E-17	5.28E-08	1.00E-06	2.14E-05
13	10000	5.70E-08	1.78E-05	1.34E-16	2.60E-08	5.12E-07	1. 84E-05
24	10000	9.94E-08	1.32E-05	3.75E-19	2.25E-08	3.86E-07	1.37E-05
52	10000	1.57E-06	7.42E-06	1.65E-08	1.52E-08	2.61E-07	9.28E-06
16	10000	2.75E-10	7.95E-06	2.11E-19	1.43E-08	2.77E-07	8.25E-06
46	10000	1.51E-08	6.89E-06	2.18E-18	9.24E-09	1.71E-07	7.08E-06
45	10000	6.48E-09	5.19E-06	1.73E-20	1.38E-08	2.71E-07	5.48E-06
1	10000	4.20E-09	2.95E-06	1.31E-18	4.44E-09	8.75E-08	3.04E-06
90	10000	2.32E-08	1.34E-06	1.51E-18	4.22E-09	8.29E-08	1.45E-06
35	10000	1.02E-08	1.08E-06	1.11E-17	1.25E-09	2.46E-08	1.11E-06
98	10000	5.9 8E -16	1.33E-09	8.44E-27	2.51E-12	4.94E-11	1.38E-09
14	10000	1.87E-22	3.62E-16	6.12E-31	8.14E-16	1.72E-17	1.19E-15
41	10000	2.97E-25	2.77E-18	0.00E+00	5.32E-21	1.00E-19	2.88E-18

	9	10000	2.50E-29	2.77E-20	0.00E+00	9.26E-24	1.98E-22	2.79E-20
	27	10000	7.99E-26	7.20E-21	0.00E+00	4.65E-24	7.34E-24	7.21E-21
7	23	10000	4.30E-26	5.31E-22	0.00E+00	1.47E-21	2.45E-22	2.24E-21
	67	10000	4.08E-31	3.39E-25	0.00E÷00	1.81E-25	2.93E-25	8.14E-25
	68	10000	0.00E+00	4.31E-29	0.00E÷00	0.00E+00	6.87E-29	1.12E-28
	26	10000	0.00E+00	0.00E+00	0.00E÷00	0.00E+00	0.00E+00	0.00E+00
	38	10000	0.00E+00	0.00E+00	0.00E÷00	0.00E+00	0.00E+00	0.00E+00
	70	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
L	84	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00

Table C.9. s4 at 100 years.

vector	time	EPAIBHRC	EPA2BHRC	EPA3BHRC	EPA4BHRC	EPA5BHRC	EPATBHRC
		²⁴¹ Am	²³⁹ Pu	²³⁸ Pu	²³⁴ U	²³⁰ Th	Total - All MB
28	10000	1.90E-01	1.34E-02	4.66E-05	9.52E-07	1.95E-05	2.03E-01
83	10000	6.12E-02	1.29E-02	2.61E-10	6.32E-04	9.59E-05	7.48E-02
5	10000	2.91E-04	5.00E-02	9.88E-14	1.36E-04	3.33E-05	5.04E-02
54	10000	8.00E-03	1.15E-02	6.11E-12	1.03E-04	3.75E-05	1.96E-02
72	10000	8.38E-04	7.22E-03	5.52E-15	5.58E-04	1.57E-04	8.78E-03
57	10000	3.37E-03	2.26E-03	1.95E-12	5.64E-05	2.99E-05	5.72E-03
74	10000	1.81E-03	3.59E-03	7.97E-12	1.23E-04	2.15E-05	5.55E-03
53	10000	9.33E-04	2.00E-03	1.68E-12	3.16E-05	9.79E-06	2.97E-03
86	10000	4.55E-05	2.21E-03	7.79E-12	7.02E-07	9.42E-06	2.27E-03
80	10000	2.28E-06	1.25E-03	1.55E-18	4.06E-05	9.04E-06	1.30E-03
81	10000	3.09E-07	1.16E-03	1.87E-18	7.41E-05	2.37E-05	1.26E-03
29	10000	1.90E-06	6.62E-04	2.67E-18	1.47E-05	1.03E-06	6.80E-04
26	10000	3.21E-12	2.18E-07	3.59E-25	5.17E-11	3.77E-10	2.18E-07
38	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
58	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00

Table C.10. s4 at 350 years.

4	time	EPA1BHRC	EPA2BHRC	EPA3BHRC	EPA4BHRC	EPA5BHRC	EPATBHRC
]	²⁴¹ Am	²³⁹ Pu	²³⁸ Pu	$^{234}\mathrm{U}$	²³⁰ Th	Total - All MB
28	10000	1.79E-01	1.34E-02	1.84E-06	9.50E-07	1.95E-05	1.92E-01
83	10000	4.96E-02	1.29E-02	2.57E-10	6.32E-04	9.59E-05	6.33E-02
5	10000	2.33E-04	4.64E-02	9.88E-14	1.27E-04	3.10E-05	4.68E-02
54	10000	5.07E-03	1.10E-02	5.50E-12	9.91E-05	3.59E-05	1.62E-02
72	[10000]	3.76E-04	6.85E-03	5.52E-15	5.29E-04	1.48E-04	7.90E-03
74	10000	1.54E-03	3.45E-03	7.93E-12	1.18E-04	2.06E-05	5.13E-03
57	10000	2.01E-03	2.17E-03	1.95E-12	5.39E-05	2.86E-05	4.26E-03
53	10000	8.12E-04	1.78E-03	1.32E-13	2.81E-05	8.71E-06	2.62E-03
86	10000	4.53E-05	2.0 8 E-03	7.79E-12	6.59E-07	8.85E-06	2.13E-03
80	10000	2.03E-06	1.07E-03	1.52E-18	3.48E-05	7.76E-06	1.12E-03
81	10000	5.65E-07	9.84E-04	1.41E-19	6.25E-05	2.00E-05	1.07E-03
29	10000	5.03E-07	2.02E-04	1.37E-18	4.49E-06	3.13E-07	2.08E-04

26	10000	7.71E-13	2.84E-08	1.58E-25	7.07E-12	4.94E-11	2.85E-08	
38	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	
58	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	

Table C.11. s5 at 1000 years.

vector	time	EPA1BHRC	EPA2BHRC	EPA3BHRC	EPA4BHRC	EPA5BHRC	EPATBHRC
,		²⁴¹ Am	²³⁹ Pu	²³⁸ Pu	²³⁴ U	²³⁰ Th	Total - All MB
28	10000	4.91E-02	1.13E-02	2.02E-08	8.06E-07	1.70E-05	6.05E-02
5	10000	1.20E-04	4.28E-02	3.70E-14	1.17E-04	2.86E-05	4.31E-02
83	10000	6.61E-03	1.21E-02	9.76E-13	5.92E-04	8.98E-05	1.94E-02
54	10000	3.46E-03	9.57E-03	5.83E-13	8.65E-05	3.13E-05	1.31E-02
72	[10000]	1.21E-04	6.08E-03	3.70E-17	4.71E-04	1.32E-04	6.81E-03
74	10000	3.17E-04	2.79E-03	9.40E-16	9.53E-05	1.66E-05	3.22E-03
57	10000	2.06E-04	1.94E-03	1.50E-13	4.82E-05	2.60E-05	2.22E-03
86	10000	2.28E-05	1.35E-03	9.33E-14	4.27E-07	5.75E-06	1.38E-03
53	10000	7.34E-05	9.97E-04	7.67E-16	1.58E-05	4.98E-06	1.09E-03
81	10000	1.82E-07	6.99E-04	1.27E-20	4.41E-05	1.42E-05	7.57E-04
80	10000	5.29E-08	4.98E-04	4.54E-20	1.58E-05	3.63E-06	5.17E-04
29	10000	1.69E-08	1.05E-05	2.90E-20	2.33E-07	1.68E-08	1.08E-05
38	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
58	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00

Table C.12. s5 at 3000 years.

vector	time	EPA1BHRC	EPA2BHRC	EPA3BHRC	EPA4BHRC	EPA5BHRC	EPATBHRC
		²⁴¹ Am	²³⁹ Pu	²³⁸ Pu	$^{234}{ m U}$	²³⁰ Th	Total - All MB
5	10000	4.90E-06	1.43E-02	1.17E-16	3.90E-05	9.56E-06	1.43E-02
28	10000	1.22E-03	1.13E-02	1.06E-10	8.06E-07	1.70E-05	1.26E-02
83	10000	9.23E-04	1.07E-02	1.23E-14	5.20E-04	7.87E-05	1.22E-02
54	10000	7.83E-05	5.80E-03	2.95E-15	5.24E-05	1.90E-05	5.95E-03
72	10000	2.24E-09	3.14E-03	3.93E-19	2.43E-04	6.87E-05	3.45E-03
74	10000	2.44E-09	1.75E-03	7.36E-18	5.93E-05	1.05E-05	1.82E-03
57	10000	2.00E-05	1.13E-03	9.82E-16	2.82E-05	1.54E-05	1.20E-03
86	10000	1.45E-06	4.31E-04	2.29E-16	1.36E-07	1.84E-06	4.34E-04
53	10000	1.69E-06	2.91E-04	6.03E-18	4.61E-06	1.45E-06	2.98E-04
29	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
38	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
58	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
80	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
81	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00

Table C.13. s5 at 5000 years.

ector	time	EPA1BHRC	EPA2BHRC	EPA3BHRC	EPA4BHRC	EPA5BHRC	EPATBHRC
		²⁴¹ Am	²³⁹ Pu	²³⁸ Pu	²³⁴ U	²³⁰ Th	Total - All MB

28	10000	7.66E-05	1.13E-02	1.52E-14	8.06E-07	1.66E-05	l 1.14E-02 i
83	10000	3.52E-05	5.48E-03	5.09E-17	2.67E-04	4.04E-05	5.82E-03
54	10000	7.35E-06	3.35E-03	1.46E-17	3.02E-05	1.09E-05	3.40E-03
74	10000	2.51E-10	7.64E-04	8.90E-20	2.52E-05	4.59E-06	7.94E-04
72	10000	1.29E-10	5.65E-04	3.35E-21	4.30E-05	1.24E-05	6.20E-04
57	10000	1.08E-06	3.25E-04	4.12E-18	7.96E-06	4.30E-06	3.39E-04
86	10000	3.89E-25	3.77E-24	0.00E+00	1.23E-27	1.66E-26	4.18E-24
5	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
29	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
38	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
53	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
58	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
80	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
81	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00

Table C.14. s5 at 7000 years.

vector	time	EPA1BHRC	EPA2BHRC	EPA3BHRC	EPA4BHRC	EPA5BHRC	EPATBHRC
		²⁴¹ Am	²³⁹ Pu	²³⁸ Pu	$^{234}\mathrm{U}$	²³⁰ Th	Total - All MB
28	10000	6.29E-06	1.13E-02	3.27E-17	8.06E-07	1.66E-05	1.14E-02
5	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
29	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
38	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
53	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
54	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
57	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
58	[10000]	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
72	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
74	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
80	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
81	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
83	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
86	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00

Table C.15. s5 at 9000 years.

vector	time	EPA1BHRC	EPA2BHRC	EPA3BHRC	EPA4BHRC	EPA5BHRC	EPATBHRC
		²⁴¹ Am	²³⁹ Pu	²³⁸ Pu	²³⁴ U	²³⁰ Th	Total - All MB
5	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
28	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
29	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
38	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
53	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
54	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
57	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
58	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00

72	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00 [
74	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
80	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
81	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
83	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
86	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00

Table C.16. s6 at 100 years.

	1	Г 	r	r	<u></u>		
vector	time	EPA1BHRC		EPA3BHRC	EPA4BHRC	EPA5BHRC	EPATBHRC
		²⁴¹ Am	²³⁹ Pu	²³⁸ Pu	²³⁴ U	²³⁰ T h	Total - All MB
28	10000	2.75E+01	1.29E+00	1.05E-01	5.64E-04	1.77E-02	2.89E+01
54	10000	1.37E+01	2.99E+00	2.02E-01	1.11E-02	1.55E-02	1.69E+01
80	10000	1.46E+01	2. 8 3E-01	1.74E-02	7.89E-03	5.83E-03	1.49E+01
72	10000	1.14E+01	1.22E+00	7.62E-02	1.33E-02	1.33E-02	1.27E+01
51	10000	8.27E+00	5.54E-01	1.68E-02	8.97E-03	6.72E-03	8.86E+00
49	10000	6.40E+00	2.71E-02	8.08E-04	6.16E-05	2.55E-03	6.43E+00
57	10000	3.32E+00	2.27E+00	1.70E-01	9.51E-03	1.30E-02	5.78E+00
55	10000	3.83E+00	6.79E-01	4.24E-02	3.92E-03	4.59E-03	4.56E+00
5	10000	4.14E+00	3.71E-01	2.00E-02	5.60E-03	7.57E-03	4.55E+00
81	10000	2.56E+00	1.81E+00	1.09E-01	1.42E-03	4.78E-03	4.49E+00
74	10000	3.42E+00	5.61E-01	3.62E-02	1.04E-02	7.11E-03	4.04E+00
53	10000	3.86E+00	1.10E-01	5.84E-03	3.74E-03	4.38E-03	3.98E+00
88	10000	3.50E+00	1.19E-01	9.56E-03	2.25E-04	7.51E-03	3.63E+00
83	10000	1.65E+00	1.85E+00	1.12E-01	1.36E-02	4.05E-03	3.62E+00
66	10000	2.74E+00	2.95E-01	1.62E-02	2.14E-03	3.05E-03	3.05E+00
29	10000	1.49E+00	8.09E-02	5.84E-03	4.52E-03	3.67E-03	1.58E+00
64	10000	1.39E+00	7.38E-02	5.88E-03	1.05E-04	4.08E-03	1.48E+00
30	10000	1.19E+00	1.54E-01	1.99E-03	4.97E-03	3.70E-03	1.36E+00
60	10000	1.26E+00	2.71E-02	1.11E-03	4.93E-05	2.45E-03	1.29E+00
50	10000	1.02E+00	2.66E-02	1.33E-03	5.33E-05	2.61E-03	1.06E+00
87	10000	9.13E - 01	4.27E-03	7.85E-04	1.23E-06	1.04E-05	9.18E-01
	10000	6.61E-01	7.31E-02	1.06E-02	3.64E-04	5.86E-04	7.45E-01
ŀ	10000	6.56E-01	2.90E-02	7.19E-04	2.15E-03	3.41E-03	6.91E-01
97	10000	4.48E-01	3.94E-02	5.57E-03	2.06E-03	2.28E-04	4.96E-01
	10000	3.85E-01	8.88E-02	3.08E-04	1.35E-03	5.23E-04	4.76E-01
	10000	3.85E-01	1.18E-02	4.58E-04	1.86E-05	9.74E-04	3.99E-01
1	10000	2.82E-01	2.36E-02	3.07E-04	4.96E-05	3.34E-03	3.09E-01
1	10000	2.18E-01	8.40E-02	4.43E-03	8.18E-04	1.47E-03	3.09E-01
33	10000	1.98E-01	1.12E-02	1.78E-03	2.06E-06	2.17E-04	2.11E-01
40	10000	1.46E-01	7.38E-04	1.58E-04	2.35E-06	8.44E-05	1.47E-01
	10000	1.44E-01	1.59E-03	4.63E-04	4.82E-06	8.01E-05	1.46E-01
I	10000	8.10E-02	3.41E-03	5.17E-04	4.57E-06	7.17E-05	8.50E-02
	10000	4.75E-02	1.29E-03	5.40E-04	2.33E-05	3.26E-06	4.93E-02
	10000	1.20E-02	2.70E-02	6.90E-04	5.65E-04	4.34E-04	4.07E-02
	10000	6.06E-03	2.16E-02	1.15E-02	4.30E-05	1.00E-06	3.92E-02
13	10000	2.44E-02	6.04E-04	2.63E-04	9.04E-07	3.24E-06	2.52E-02

	_								
	75	10000		9.28E-04	1.19E-04	1.85E-06	9.74E-05	2.03E-02	ı
	35	10000	1	2.64E-04	1.50E-04	3.08E-07	9.38E-07	1.45E-02	
	52	10000	1.40E-02	1.32E-04	5.52E-05	2.77E-07	1.04E-06	1.42E-02	
7	46	10000		3.99E-05	1.33E-05	5.18E-08	2.11E-07	1.36E-02	-
١	1	10000	9.32E-03	7.86E-05	2.68E-05	1.21E-07	8.26E-07	9.42E-03	
	61	10000		7.33E-04	2.76E-04	1.88E-05	7.54E-07	8.75E-03	İ
	90	10000	F .	1.16E-05	4.74E-06	3.71E-08	1.34E-07	8.58E-03	
-	34	10000	j .	1.88E-04	6.88E-05	2.19E-07	8.78E-07	6.68E-03	
-	100	10000]	7.86E-05	2.59E-05	2.21E-07	9.84E-07	6.65E-03	
	16	10000		7.57E-05	3.25E-05	1.36E-07	4.97E-07	4.75E-03	1
-	96	10000	4.41E-03	8.21E-05	4.25E-05	1.64E-07	5.30E-07	4.54E-03	
ĺ	15	10000	4.48E-03	2.90E-05	2.12E-05	7.15E-07	3.59E-08	4.53E-03	
	45	10000	4.28E-03	1.42E-04	2.50E-06	4.05E-07	2.22E-05	4.44E-03	ı
	31	10000	2.91E-03	3.01E-04	1.30E-04	7.33E-08	2.65E-07	3.34E-03	
j	8	10000	3.24E-03	3.49E-05	5.40E-06	8.08E-08	6.02E-07	3.28E-03	1
ł	2	10000	2.72E-03	2.87E-04	2.10E-04	1.51E-06	1.52E-07	3.22E-03	
ĺ	7	10000	2.94E-03	2.95E-05	1.98E-05	5.93E-08	5.64E-07	2.99E-03	ŀ
	69	10000	2.54E-03	7.35E-05	4.02E-05	7.10E-08	2.20E-07	2.65E-03	ı
	24	10000	1.78E-03	2.16E-05	1.58E-05	3.25E-08	8.25E-08	1.81E-03	ļ
ł	9	10000	5.08E-04	1.71E-05	7.80E-06	1.61E-06	2.17E-08	5.34E-04	
ı	44	10000	4.50E-04	1.50E-05	1.09E-05	8.58E-09	2.18E-08	4.76E-04	ļ
ł	48	10000	1.93E-04	4.50E-06	3.29E-06	1.94E-09	4.92E-09	2.01E-04	
	89	10000	1.38E-04	1.94E-06	1.37E-07	5.68E-09	2.55E-07	1.40E-04	
	98	10000	1.04E-04	1.40E-06	7.80E-07	2.52E-09	7.90E-09	1.06E-04	
7	18	10000	9.94E-05	3.28E-07	2.39E-07	4.50E-10	1.14E-09	9.99E-05	1
l	41	10000	3.24E-05	4.02E-07	1.74E-07	7.72E-10	2.79E-09	3.29E-05	
1	14	10000	1.91E-05	4.58E-07	3.34E-07	2.87E-10	7.30E-10	1.99E-05	Į
İ	92	10000	7.89E-06	8.73E-07	1.33E-06	4.66E-09	2.21E-10	1.01E-05	
	84	10000	7.14E-06	4.96E-07	3.62E-07	1.45E-08	3.09E-10	8.02E-06	
ĺ	4	10000	2.16E-06	1.07E-07	5.62E-12	2.90E-10	1.86E-08	2.29E-06	l
	70	10000	9.32E-07	2.08E-08	1.52E-08	2.30E-11	5.85E-11	9.69E-07	l
	36	10000	3.99E-07	1.95E-08	2.13E-08	8.97E-12	1.93E-11	4.39E-07	
ĺ	76	10000	2.25E-08	1.44E-09	1.06E-09	1.69E-11	1.31E-12	2.51E-08	l
	68	10000	7.07E-09	3.70E-10	2.86E-10	1.18E-11	3.13E-13	7.74E-09	
	62	10000	3.53E-09	1.02E-09	1.64E-09	2.62E-12	8.43E-14	6.20E-09	
	11	10000	5.40E-09	1.54E-11	2.47E-11	3.00E-14	3.74E-14	5.44E-09	
	58	10000	4.63E-09	1.01E-10	1.62E-10	4.99E-12	1.56E-13	4.90E-09	
	67	10000	3.37E-09	1.37E-10	2.19E-10	8.91E-14	5.10E-14	3.72E-09	
	3	10000	3.38E-09	I.37E-11	2.19E-11	1.97E-14	2.45E-14	3.41E-09	ĺ
	85	10000	2.99E-09	2.16E-11	3.47E-11	1.99E-12	7.15E-14	3.05E-09	
	42	10000	1.71E-09	3.89E-10	6.22E-10	1.19E-12	9.19E-14	2.72E-09	
	37	10000	1.72E-09	7.74E-12	1.24E-11	1.61E-14	2.00E-14	1.74E-09	ĺ
	25	10000	1.15E-09	6.25E-12	1.00E-11	1.57E-14	1.96E-14	1.17E-09	
	27	10000	4.14E-10	1.40E-10	2.24E-10	7.52E-14	6.46E-15	7.78E-10	
		10000	3.93E-10	8.58E-12	1.37E-11	2.63E-13	1.41E-14	4.16E-10	
	78	10000	2.18E-10	1.29E-10	4.69E-27	2.54E-13	1.92E-11	3.67E-10	
	79	10000	9.82E-11	3.22E-12	5.15E-12	6.93E-15	3.58E-16	1.07E-10	

1	1			i	•		
23	10000	2.54E-11	1.30E-11	2.07E-11	1.11E-15	1.03E-15	5.92E-11
95	10000	4.75E-11	3.24E-13	5.19E-13	6.27E-16	7.81E-16	4. 84 E-11
94	10000	1.59E-11	5.36E-12	8.59E-12	2.71E-14	1.15E-15	2.99E-11
19	10000	1.56E-11	1.21E-13	1.93E-13	2.58E-16	3.22E-16	1.59E-11
38	10000	2.94E-12	2.62E-13	4.20E-13	2.72E-15	2.02E-16	3.63E-12
93	10000	2.97E-12	9.47E-14	1.52E-13	1.18E-15	7.36E-17	3.22E-12
10	10000	1.64E-12	5.31E-14	8.51E-14	3.86E-15	3.73E-17	1.78E-12
56	10000	1.09E-12	5.68E-14	9.10E-14	1.69E-16	4.08E-17	1.23E-12
59	10000	3.29E-14	5.14E-15	8.23E-15	3.01E-17	1.01E-18	4.63E-14
12	10000	3.72E-14	1.35E-15	2.16E-15	1. 84E-18	2.29E-18	4.07E-14
6	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
47	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
65	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
71	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
73	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
77	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
99	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00

Table C.17. s6 at 350 years.

	vector	time	EPA1BHRC	EPA2BHRC	EPA3BHRC	EPA4BHRC	EPA5BHRC	EPATBHRC
			²⁴¹ Am	²³⁹ Pu	²³⁸ Pu	²³⁴ U	²³⁰ Th	Total - All MB
_	28	10000	2.58E+01	1.28E+00	1.47E-02	5.61E-04	1.86E-02	2.71E+01
	54	10000	1.30E+01	2.94E+00	2.84E-02	1.09E-02	1.59E-02	1.60E+01
	80	10000	1.35E+01	2.77E-01	2.44E-03	7.77E-03	5.92E-03	1.38E+01
	72	10000	1.09E+01	1.20E+00	1.07E-02	1.32E-02	1.37E-02	1.21E+01
	51	10000	7.79E+00	5.45E-01	2.36E-03	8.86E-03	6.95E-03	8.36E+00
ı	49	10000	5.67E+00	2.67E-02	1.13E-04	6.09E-05	2.64E-03	5.70E+00
1	57	10000	3.22E+00	2.23E+00	2.39E-02	9.44E-03	1.36E-02	5.50E+00
	55	10000	3.71E+00	6.65E-01	5.94E-03	3.86E-03	4.72E-03	4.39E+00
	5	10000	3.96E+00	3.64E-01	2.80E-03	5.51E-03	7.71E-03	4.34E+00
	81	10000	2.47E+00	1.77E+00	1.52E-02	1.39E-03	4.84E-03	4.26E+00
	74	10000	3.30E+00	5.51E-01	5.07E-03	1.03E-02	7.33E-03	3.87E+00
1	53	10000	3.55E+00	1.08E-01	8.19E-04	3.70E-03	4.49E-03	3.67E+00
	88	10000	3.40E+00	1.17E-01	1.34E-03	2.23E-04	7.84E-03	3.52E+00
1	83	10000	1.50E+00	1. 82E+00	1.57E-02	1.35E-02	4.16E-03	3.35E+00
1	66	10000	2.62E+00	2.88E-01	2.28E-03	2.10E-03	3.07E-03	2.91E+00
1	29	10000	1.43E+00	7.94E-02	8.18E-04	4.47E-03	3.77E-03	1.52E+00
1	64	10000	1.36E+00	7.24E-02	8.24E-04	1.04E-04	4.18E-03	1.43E+00
ĺ	30	10000	1.10E+00	1.50E-01	2.79E-04	4.87E-03	3.73E-03	1.26E+00
1	60	10000	1.18E+00	2.65E-02	1.55E-04	4.85E-05	2.47E-03	1.21E+00
	50	10000	9.63E-01	2.60E-02	1.86E-04	5.23E-05	2.62E-03	9.92E-01
1	87	10000	8.83E-01	4.26E-03	1.10E-04	1.25E-06	1.44E-05	8.87E-01
		10000	6.59E-01	7.17E-02	1.48E-03	3.62E-04	6.07E-04	7.33E-01
┙	17	10000	6.07E-01	2.82E-02	1.01E-04	2.10E-03	3.41E-03	6.41E-01
	97	10000	4.40E-01	3.92E-02	7.81E-04	2.08E-03	2.57E-04	4. 8 2E-01
T	63	10000	3.64E-01	8.86E-02	4.31E-05	1.34E-03	5.65E-04	4.55E-01

	86	10000	3.53E-01	1.15E-02	6.43E-05	1.83E-05	9.78E-04	3.66E-01	١
	26	10000	2.71E-01	2.26E-02	4.30E-05	4.75E-05	3.23E-03	2.97E-01	
	43	10000	2.03E-01	8.17E-02	6.21E-04	7.99E-04	1.46E-03	2.87E-01	l
	33	10000	1.97E-01	1.05E-02	2.49E-04	1.95E-06	2.02E-04	2.08E-01	
	40	10000	1.46E-01	7.14E-04	2.21E-05	2.32E-06	8.35E-05	1.46E-01	
	32	10000	1.40E-01	1.59E-03	6.49E-05	4.94E-06	9.50E-05	1.42E-01	
	39	10000	8.02E-02	3.40E-03	7.25E-05	4.63E-06	8.56E-05	8.38E-02	
	21	10000	4.74E-02	1.29E-03	7.57E-05	2.42E-05	6.29E-06	4.88E-02	İ
	22	10000	1.16E-02	2.50E-02	9.68E-05	5.24E-04	4.05E-04	3.76E-02	ĺ
	91	10000	6.06E-03	2.15E-02	1.62E-03	4.51E-05	2.10E-06	2.93E-02	l
	13	10000	2.44E-02	6.03E-04	3.69E-05	9.40E-07	6.32E-06	2.50E-02	Į
	75	10000	1.83E-02	8.99E-04	1.67E-05	1.81E-06	9.65E-05	1.94E-02	l
	35	10000	1.40E-02	2.64E-04	2.10E-05	3.25E-07	2.01E-06	1.43E-02	l
1	52	10000	1.40E-02	1.32E-04	7.74E-06	2.87E-07	1.98E-06	1.41E-02	l
.	46	10000	1.35E-02	3.99E-05	1.86E-06	5.34E-08	3.86E-07	1.35E-02	
	1	10000	9.31E-03	7.85E-05	3.75E-06	1.25E-07	1.23E-06	9.39E-03	
1	90	10000	8.56E-03	1.15E-05	6.65E-07	3.85E-08	2.60E-07	8.57E-03	l
	61	10000	7.59E-03	7.32E-04	3.86E-05	1.95E-05	1.16E-06	8.38E-03	
1	00	10000	6.54E-03	7.85E-05	3.63E-06	2.27E-07	1.72E-06	6.62E-03	
[:	34	10000	6.41E-03	1.88E-04	9.64E-06	2.27E-07	1.62E-06	6.61E-03	l
	16	10000	4.64E-03	7.56E-05	4.56E-06	1.41E-07	9.60E-07	4.72E-03	
	15	10000	4.48E-03	2.90E-05	2.97E-06	7.66E-07	8.60E-08	4.51E-03	
9	96	10000	4.41E-03	8.20E-05	5.96E-06	1.72E-07	1.10E-06	4.50E-03	ĺ
4	45	10000	4.01E-03	1.38E-04	3.50E-07	3.94E-07	2.20E-05	4.17E-03	
7	8	10000	3.24E-03	3.49E-05	7.57E-07	8.18E-08	8.63E-07	3.27E-03	l
1	31	10000	2.91E-03	3.00E-04	1.82E-05	7.61E-08	5.15E-07	3.23E-03	
	2	10000	2.72E-03	2.87E-04	2.94E-05	1.62E-06	3.65E-07	. 3.03E-03	
l	7	10000	2.94E-03	2.95E-05	2.77E-06	6.30E-08	7.64E-07	2.97E-03	
6	59	10000	2.53E-03	7.34E-05	5.64E-06	7.47E-08	4.66E-07	2.61E-03	
	24	10000	1.78E-03	2.16E-05	2.22E-06	3.48E-08	1.98E-07	1.80E-03	
1	9	10000	5.07E-04	1.70E-05	1.09E-06	1.68E-06	4.33E-08	5.27E-04	
1	14	10000	4.49E-04	1.50E-05	1.54E-06	9.18E-09	5.22E-08	4.66E-04	ļ
	18	10000	1.93E-04	4.50E-06	4.61E-07	2.07E-09	1.18E-08	1.98E-04	
	39	10000	1.32E-04	1.91E-06	5.94E-08	5.60E-09	2.59E-07	1.34E-04	
1	8	10000	1.04E-04	1.40E-06	1.09E-07	2.65E-09	1.66E-08	1.06E-04	į
	18	10000	9.93E-05	3.28E-07	3.36E-08	4.82E-10	2.74E-09	9.97E-05	ĺ
l	11	10000	3.23E-05	4.01E-07	2.44E-08	8.03E-10	5.42E-09	3.28E-05	
	4	10000	1.91E-05	4.58E-07	4.69E-08	3.08E-10	1.75E-09	1.96E-05	
1)2	10000	7.89E-06	8.74E-07	1. 14E-06	4.79E-09	3.22E-10	9.91E-06	
	34	10000	7.14E-06	4.96E-07	5.08E-08	1.55E-08	7.41E-10	7.70E-06	
l l	4	10000	2.00E-06	1.03E-07	5.62E-12	2.80E-10	1.83E-08	2.12E-06	
ſ	70	10000	9.32E-07	2.08E-08	2.13E-09	2.46E-11	1.40E-10	9.55E-07	
	6	10000	3.98E-07	1.95E-08	7.02E-09	9.75E-12	4.36E-11	4.25E-07	
	76	10000	2.25E-08	1.44E-09	1.57E-10	1.80E-11	3.13E-12	2.42E-08	
L	58	10000	7.07E-09	3.70E-10	6.48E-11	1.25E-11	7.39E-13	7.52E-09	
	$\begin{bmatrix} 52 \\ 1 \end{bmatrix}$	10000	3.53E-09	1.02E-09	1.64E-09	2.62E-12	8.43E-14	6.20E-09	
1	1	10000	5.40E-09	1.54E-11	2.47E-11	3.00E-14	3.74E-14	5.44E-09	

58	10000	4.63E-09	1.01E-10	1.62E-10	4.99E-12	1.56E-13	4.90E-09	ı
67	10000	3.37E-09	1.37E-10	2.19E-10	8.91E-14	5.10E-14	3.72E-09	
3	10000	3.38E-09	1.37E-11	2.19E-11	1.97E-14	2.45E-14	3.41E-09	١
85	10000	2.99E-09	2.16E-11	3.47E-11	1.99E-12	7.15E-14	3.05E-09	
42	10000	1.71E-09	3.89E-10	6.22E-10	1.19E-12	9.19E-14	2.72E-09	
37	10000	1.72E-09	7.74E-12	1.24E-11	1.61E-14	2.00E-14	1.74E-09	
25	10000	1.15E-09	6.25E-12	1.00E-11	1.57E-14	1.96E-14	1.17E-09	ļ
27	10000	4.14E-10	1.40E-10	2.24E-10	7.52E-14	6.46E-15	7.78E-10	İ
20	10000	3.93E-10	8.58E-12	1.37E-11	2.63E-13	1.41E-14	4.16E-10	
78	10000	1.86E-10	1.22E-10	6.56E-28	2.41E-13	I.84E-11	3.27E-10	
79	10000	9.82E-11	3.22E-12	5.15E-12	6.93E-15	3.58E-16	1.07E-10	ļ
23	10000	2.54E-11	1.30E-11	2.07E-11	1.11E-15	1.03E-15	5.92E-11	l
95	10000	4.75E-11	3.24E-13	5.19E-13	6.27E-16	7.81E-16	4.84E-11	
94	10000	1.59E-11	5.36E-12	8.59E-12	2.71E-14	1.15E-15	2.99E-11	l
19	10000	1.56E-11	1.21E-13	1.93E-13	2.58E-16	3.22E-16	1.59E-11	
38	10000	2.94E-12	2.62E-13	4.20E-13	2.72E-15	2.02E-16	3.63E-12	
93	10000	2.97E-12	9.47E-14	1.52E-13	1.18E-15	7.36E-17	3.22E-12	
10	10000	1.64E-12	5.31E-14	8.51E-14	3.86E-15	3.73E-17	1.78E-12	
56	10000	1.09E-12	5.68E-14	9.10E-14	1.69E-16	4.08E-17	1.23E-12	l
59	10000	3.29E-14	5.14E-15	8.23E-15	3.01E-17	1.01E-18	4.63E-14	ĺ
12	10000	3.72E-14	1.35E-15	2.16E-15	1.84E-18	2.29E-18	4.07E-14	l
6	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	ĺ
47	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	
65	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	
71	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	ĺ
73	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	
77	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	1
99	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	

Table C.18. s6 at 1000 years.

vector	time	EPA1BHRC	EPA2BHRC	EPA3BHRC	EPA4BHRC	EPA5BHRC	EPATBHRC
		²⁴¹ Am	²³⁹ Pu	²³⁸ Pu	$^{234}\mathrm{U}$	²³⁰ Th	Total - All MB
28	10000	1.70E+01	1.23E+00	8.85E-05	5.43E-04	2.08E-02	1.82E+01
54	10000	1.05E+01	2.80E+00	1.71E-04	1.05E-02	1.70E-02	1.33E+01
72	10000	8.95E+00	1.15E+00	6.43E-05	1.26E-02	1.47E-02	1.01E+01
80	10000	9.51E+00	2.62E-01	1.47E-05	7.37E-03	6.10E-03	9.79E+00
51	10000	5.77E+00	5.22E-01	1.42E-05	8.50E-03	7.49E-03	6.30E+00
57	10000	2.96E+00	2.15E+00	1.44E-04	9.09E-03	1.49E-02	5.13E+00
81	10000	2.22E+00	1.67E+00	9.18E-05	1.32E-03	4.97E-03	3.90E+00
49	10000	3.87E+00	2.57E-02	6.82E-07	5.88E-05	2.83E-03	3.89E+00
55	10000	3.22E+00	6.30E-01	3.57E-05	3.67E-03	5.00E-03	3.86E+00
5	10000	3.42E+00	3.45E-01	1.68E-05	5.24E-03	8.00E-03	3.78E+00
74	10000	2.96E+00	5.26E-01	3.05E-05	9.89E-03	7.83E-03	3.50E+00
88	10000	3.11E+00	1.13E-01	8.06E-06	2.15E-04	8.64E-03	3.23E+00
53	10000	2.77E+00	1.03E-01	4.93E-06	3.54E-03	4.73E-03	2.88E+00
83	10000	1.11E+00	1.75E+00	9.43E-05	1.30E-02	4.42E-03	2.88E+00

66	10000	2.32E+00	2.70E-01	1.37E-05	1.97E-03	3.08E-03	2.60E+00	١
29	10000	1.27E+00	7.57E-02	4.92E-06	4.27E-03	3.99E-03	1.35E+00	١
64	10000	1.25E+00	6.88E-02	4.96E-06	9.87E-05	4.39E-03	1.33E+00	
30	10000	8.64E-01	1.41E-01	1.68E-06	4.58E-03	3.76E-03	1.01E+00	I
60	10000	9.54E-01	2.50E-02	9.33E-07	4.58E-05	2.51E-03	9.82E-01	ĺ
50	10000	8.05E-01	2.43E-02	1.12E-06	4.91E-05	2.64E-03	8.32E-01	
82	10000	6.49E-01	6.79E-02	8.91E-06	3.44E-04	6.53E-04	7.18E-01	ĺ
87	10000	6.17E-01	4.23E-03	6.78E-07	1.24E-06	2.42E-05	6.21E-01	
17	10000	4.83E-01	2.63E-02	6.07E-07	1.96E-03	3.38E-03	5.15E-01	1
97	10000	4.08E-01	3.85E-02	4.70E-06	2.05E-03	3.30E-04	4.48E-01	
63	10000	3.05E-01	8.80E-02	2.63E-07	1.34E-03	6.69E-04	3.95E-01	l
86	10000	2.73E-01	1.08E-02	3.87E-07	1.72E-05	9.82E-04	2.85E-01	
26	10000	2.54E-01	1.99E-02	2.58E-07	4.18E-05	2.94E-03	2.77E-01	l
43	10000	1.67E-01	7.56E-02	3.74E-06	7.41E-04	1.43E-03	2.45E-01	
33	10000	1.96E-01	8.64E-03	1.50E-06	1.61E-06	1.59E-04	2.05E-01	
40	10000	1.44E-01	6.50E-04	1.33E-07	2.12E-06	8.01E-05	1.44E-01	١
32	10000	1.32E-01	1.58E-03	3.91E-07	4.94E-06	1.32E-04	1.34E-01	ŀ
39	10000	7.67E-02	3.38E-03	4.36E-07	4.62E-06	1.20E-04	8.02E-02	ľ
21	10000	4.73E-02	1.28E-03	4.56E-07	2.42E-05	1.39E-05	4.86E-02	l
22	10000	1.07E-02	1.97E-02	5.82E-07	4.14E-04	3.26E-04	3.11E-02	
91	10000	6.04E-03	2.14E-02	9.72E-06	4.53E-05	4.84E-06	2.75E-02	
13	10000	2.43E-02	5.99E-04	2.22E-07	9.42E-07	1.40E-05	2.49E-02	l
75	10000	1.67E-02	8.25E-04	1.00E-07	1.67E-06	9.33E-05	1.77E-02	l
35	10000	1.40E-02	2.62E-04	1.26E-07	3.26E-07	4.69E-06	1.43E-02	l
52	10000	1.39E-02	1.31E-04	4.66E-08	2.88E-07	4.34E-06	1.40E-02	l
46	10000	1.35E-02	3.96E-05	1.12E-08	5.34E-08	8.22E-07	1.35E-02	
1	10000	9.24E-03	7.79E-05	2.26E-08	1.25E-07	2.23E-06	9.32E-03	
90	10000	8.53E-03	1.15E-05	4.00E-09	3.85E-08	5.75E-07	8.54E-03	
61	10000	7.32E-03	7.27E-04	2.33E-07	1.95E-05	2.17E-06	8.06E-03	ĺ
100	10000	6.51E-03	7.79E-05	2.18E-08	2.28E-07	3.58E-06	6.60E-03	
34	10000	6.39E-03	1.87E-04	5.80E-08	2.27E-07	3.47E-06	6.58E-03	ĺ
16	10000	4.62E-03	7.50E-05	2.75E-08	1.42E-07	2.12E-06	4.70E-03	ĺ
15	10000	4.46E-03	2.88E-05	1.79E-08	7.71E-07	2.11E-07	4.49E-03	ĺ
96	10000	4.39E-03	8.14E-05	3.59E-08	1.72E-07	2.51E-06	4.48E-03	ĺ
45	10000	3.35E-03	1.27E-04	2.10E-09	3.63E-07	2.14E-05	3.49E-03	l
8	10000	3.22E-03	3.46E-05	4.59E-09	8.16E-08	1.51E-06	3.25E-03	
31	10000	2.90E-03	2.98E-04	1.09E-07	7.63E-08	1.14E-06	3.20E-03	
2	10000	2.71E-03	2.85E-04	1.77E-07	1.63E-06	8.98E-07	2.99E-03	
7	10000	2.93E-03	2.93E-05	1.67E-08	6.34E-08	1.27E-06	2.96E-03	
69	10000	2.53E-03	7.29E-05	3.40E-08	7.50E-08	1.08E-06	2.60E-03	
24	10000	1.77E-03	2.15E-05	1.33E-08	3.50E-08	4.86E-07	1.79E-03	
9	10000	5.06E-04	1. 69E-0 5	6.61E-09	1.68E - 06	9.74E-08	5.24E-04	ĺ
44	10000	4.4 8 E-04	1.49E-05	9.24E-09	9.24E-09	1.28E-07	4.63E - 04	
48	10000	1.92E-04	4.47E-06	2.78E-09	2.09E-09	2.90E-08	1.97E-04	
89	10000	1.17E-04	1.82E-06	4.13E-09	5.36E-09	2.70E-07	1.19E-04	
98	10000	1.04E-04	1.39E-06	6.59E-10	2.66E-09	3.85E-08	1.05E-04	
18	10000	9.90E-05	3.25E-07	2.02E-10	4.85E-10	6.74E-09	9.93E-05	

1	1	1 -	•	•			
41	10000	•	3.98E-07	1.47E-10	8.05E-10	1.20E-08	3.26E-05
14	10000	ł	4.55E-07	3.07E-10	3.10E-10	4.30E-09	1.95E-05
92	10000	7.88E-06	8.74E-07	1.53E-07	5.44E-09	1.37E-09	8.91E-06
84	10000	7.12E-06	4.92E-07	3.05E-10	1.56E-08	1.82E-09	7.63E-06
4	10000	1.60E-06	9.41E-08	5.62E-12	2.56E-10	1.75E-08	1.71E-06
70	10000	9.29E-07	2.07E-08	1.28E-11	2.48E-11	3.44E-10	9.50E-07
36	10000	3.97E-07	1.94E-08	1.64E-10	1.01E-11	1.27E-10	4.17E-07
76	10000	2.25E-08	1.43E-09	1.07E-11	1.82E-11	7.71E-12	2.39E-08
68	10000	7.05E-09	3.68E-10	2.90E-11	1.26E-11	1.81E-12	7.46E-09
62	10000	3.53E-09	1.02E-09	1.64E-09	2.62E-12	8.43E-14	6.20E-09
11	10000	5.40E-09	1.54E-11	2.47E-11	3.00E-14	3.74E-14	5.44E-09
58	10000	4.63E-09	1.01E-10	1.62E-10	4.99E-12	1.56E-13	4.90E-09
67	10000	3.37E-09	1.37E-10	2.19E-10	8.91E-14	5.10E-14	3.72E-09
3	10000	3.38E-09	1.37E-11	2.19E-11	1.97E-14	2.45E-14	3.41E-09
85	10000	2.99E-09	2.16E-11	3.47E-11	1.99E-12	7.15E-14	3.05E-09
42	10000	1.71E-09	3.89E-10	6.22E-10	1.19E-12	9.19E-14	2.72E-09
37	10000	1.72E-09	7.74E-12	1.24E-11	1.61E-14	2.00E-14	1.74E-09
25	10000	1.15E-09	6.25E-12	1.00E-11	1.57E-14	1.96E-14	1.17E-09
27	10000	4.14E-10	1.40E-10	2.24E-10	7.52E-14	6.46E-15	7.78E-10
20	10000	3.93E-10	8.58E-12	1.37E-11	2.63E-13	1.41E-14	4.16E-10
78	10000	1.33E-10	1.06E-10	3.94E-30	2.08E-13	1.64E-11	2.55E-10
79	10000	9.82E-11	3.22E-12	5.15E-12	6.93E-15	3.58E-16	1.07E-10
23	10000	2.54E-11	1.30E-11	2.07E-11	1.11E-15	1.03E-15	5.92E-11
95	10000	4.75E-11	3.24E-13	5.19E-13	6.27E-16	7.81E-16	4.84E-11
94	10000	1.59E-11	5.36E-12	8.59E-12	2.71E-14	1.15E-15	2.99E-11
19	10000	1.56E-11	1.21E-13	1.93E-13	2.58E-16	3.22E-16	1.59E-11
38	10000	2.94E-12	2.62E-13	4.20E-13	2.72E-15	2.02E-16	3.63E-12
93	10000	2.97E-12	9.47E-14	1.52E-13	1.18E-15	7.36E-17	3.22E-12
10	10000	1.64E-12	5.31E-14	8. 51E-14	3.86E-15	3.73E-17	1.78E-12
56	10000	1.09E-12	5.68E-14	9.10E-14	1.69E-16	4.08E-17	1.23E-12
59	10000	3.29E-14	5.14E-15	8.23E-15	3.01E-17	1.01E-18	4.63E-14
12	10000	3.72E-14	1.35E-15	2.16E-15	1.84E-18	2.29E-18	4.07E-14
6	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
47	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
65	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
71	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
73	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
77	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
99	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00

Table C.19. s6 at 2000 years.

vector	time	EPA1BHRC	EPA2BHRC	EPA3BHRC	EPA4BHRC	EPA5BHRC	EPATBHRC
		²⁴¹ Am	²³⁹ Pu	²³⁸ Pu	²³⁴ U	²³⁰ Th	Total - All MB
54	10000	4.48E+00	2.60E+00	6.54E-08	9.75E-03	1.82E-02	7.11E+00
28	10000	5.28E+00	1.16E+00	3.41E-08	5.14E-04	2.37E-02	6.47E+00
72	10000	4.06E+00	1.07E+00	2.47E-08	1.18E-02	1.58E-02	5.15E+00

57	10000	2.25E+00	2.01E+00	5.50E-08	8.55E-03	1.65E-02	4.29E+00	l
80	10000	3.14E+00	2.39E-01	5.63E-09	6.73E-03	6.25E-03	3.39E+00	ı
81	10000	1.51E+00	1.52E+00	3.55E-08	1.20E-03	5.05E-03	3.04E+00	Ì
51	10000	2.47E+00	4.87E-01	5.44E-09	7.95E-03	8.13E-03	2.97E+00	Ì
55	10000	2.03E+00	5.76E-01	1.37E-08	3.36E-03	5.29E-03	2.61E+00	
74	10000	2.11E+00	4.89E-01	1.17E-08	9.21E-03	8.41E-03	2.61E+00	ļ
88	10000	2.30E+00	1.06E-01	3.09E-09	2.03E-04	9.64E-03	2.42E+00	l
5	10000	2.06E+00	3.16E-01	6.45E-09	4.81E-03	8.27E-03	2.39E+00	l
83	10000	7.09E-01	1.64E+00	3.61E-08	1.22E-02	4.74E-03	2.37E+00	l
53	10000	1.62E+00	9.57E-02	1.93E-09	3.30E-03	5.01E-03	1.73E+00	l
66	10000	1.41E+00	2.42E-01	5.25E-09	1.77E-03	3.05E-03	1.66E+00	ĺ
49	10000	1.30E+00	2.42E-02	2.61E-10	5.55E-05	3.08E-03	1.33E+00	l
64	10000	1.03E+00	6.32E-02	1.90E-09	9.09E-05	4.61E-03	1.09E+00	
29	10000	9.31E-01	7.01E-02	1.89E-09	3.96E-03	4.24E-03	1.01E+00	l
30	10000	5.04E-01	1.27E-01	6.42E-10	4.14E-03	3.73E-03	6.39E-01	l
82	10000	5.63E-01	6.21E-02	3.44E-09	3.15E-04	7.02E-04	6.26E-01	l
50	10000	5.85E-01	2.18E-02	4.29E-10	4.42E-05	2.61E-03	6.09E-01	
60	10000	5.72E-01	2.27E-02	3.57E-10	4.17E-05	2.53E-03	5.97E-01	
97	10000	3.26E-01	3.75E-02	1.80E-09	2.01E-03	4.32E-04	3.66E-01	
17	10000	3.03E-01	2.34E-02	2.32E-10	1.74E-03	3.27E-03	3.32E-01	
63	10000	1.96E-01	8.72E-02	3.40E-10	1.33E-03	8.16E-04	2.86E-01	
26	10000	2.38E-01	1.57E-02	9.90E-11	3.31E-05	2.43E-03	2.56E-01	
43	10000	1.28E-01	6.63E-02	1.43E-09	6.51E-04	1.36E-03	1.97E-01	l
87	10000	1.87E-01	4.18E-03	3.14E-10	1.24E-06	3.83E-05	1.91E-01	l
33	10000	1.79E-01	5.78E-03	5.75E-10	1.07E-06	8.60E-05	1.85E-01	
86	10000	1.70E-01	9.73E-03	1.48E-10	1.55E-05	9.71E-04	1.80E-01	ı
40	10000	1.29E-01	5.53E-04	5.11E-11	1.81E-06	7.19E-05	1.30E-01	ĺ
32	10000	1.19E-01	1.56E-03	1.50E-10	4.91E-06	1.85E-04	1.20E-01	
39	10000	6.47E-02	3.34E-03	1.67E-10	4.59E-06	1.70E-04	6.82E-02	
21	10000	4.63E-02	1.27E-03	1.75E-10	2.41E-05	2.47E-05	4.76E-02	
91	10000	5.92E-03	2.12E-02	3.76E-09	4.50E-05	8.76E-06	2.71E-02	
13	10000	2.38E-02	5.93E-04	8.51E-11	9.36E-07	2.50E-05	2.44E-02	
22	10000	9.38E-03	1.17E-02	2.23E-10	2.46E-04	1.96E-04	2.15E-02	
75	10000	1.55E-02	7.12E-04	3.84E-11	1.44E-06	8.63E-05	1.63E-02	
35	10000	1.37E-02	2.60E-04	4.83E-11	3.24E-07	8.51E-06	1.40E-02	
52	10000	1.36E-02	1.30E-04	1.88E-11	2.86E-07	7.69E-06	1.38E-02	
1	10000	7.96E-03	7.71E-05	8.66E-12	1.25E-07	3.67E-06	8.04E-03	
61	10000	7.06E-03	7.19E-04	1.44E-10	1.94E-05	3.60E-06	7.80E-03	
46	10000	7.15E-03	3.92E-05	4.28E-12	5.31E-08	1.44E-06	7.19E-03	
100	10000	6.37E-03	7.71E-05	8.37E-12	2.26E-07	6.22E-06	6.45E-03	
34	10000	6.25E-03	1. 85E- 04	2.22E-11	2.25E-07	6.11E-06	6.44E-03	
90	10000	5.93E-03	1.13E-05	1.53E-12	3.83E-08	1.03E-06	5.94E-03	
16	10000	4.53E-03	7.42E-05	1.50E-11	1.41E-07	3.77E-06	4.61E-03	
15	10000	4.38E-03	2.85E-05	7.39E-12	7.66E-07	3.90E-07	4.41E-03	
96	10000	4.31E-03	8.06E-05	1.38E-11	1.71E-07	4.52E-06	4.39E-03	
8	10000	3.10E-03	3.42E-05	2.13E-12	8.11E-08	2.44E-06	3.14E-03	
31	10000	2.84E-03	2.95E-04	4.19E-11	7.58E-08	2.03E-06	3.14E-03	

2	10000	2.66E-03	2.82E-04	7.14E-11	1.62E-06	1.66E-06	2.94E-03
7	10000	2.88E-03	2.90E-05	6.55E-12	6.30E-08	1.98E-06	2.91E-03
69	10000	2.48E-03	7.21E-05	1.31E-11	7.45E-08	1.96E-06	2.55E-03
45	10000	2.40E-03	1.10E-04	8.19E-13	3.15E-07	1.99E-05	2.53E-03
24	10000	1.74E-03	2.13E-05	5.13E-12	3.48E-08	8.97E-07	1.76E-03
9	10000	4.96E-04	1.67E-05	1.59E-11	1.67E-06	1.74E-07	5.14E-04
44	10000	4.40E-04	1.47E-05	3.58E-12	9.18E-09	2.37E-07	4.55E-04
48	10000	1.89E-04	4.42E-06	1.23E-12	2.08E-09	5.36E-08	1.93E-04
98	10000	1.02E-04	1.38E-06	2.82E-13	2.65E-09	6.97E-08	1.03E-04
18	10000	9.72E-05	3.22E-07	2.18E-13	4.82E-10	1.24E-08	9.76E-05
89	10000	9.26E-05	1.68E-06	2.18E-11	4.97E-09	2.82E-07	9.45E-05
41	10000	3.16E-05	3.94E-07	5.63E-14	8.00E-10	2.14E-08	3.20E-05
14	10000	1.87E-05	4.50E-07	3.22E-12	3.08E-10	7.94E-09	1.91E-05
92	10000	7.81E-06	8.65E-07	3.28E-10	5.51E-09	3.75E-09	8.69E-06
84	10000	6.99E-06	4.87E-07	1.17E-13	1.55E-08	3.36E-09	7.50E-06
4	10000	1.10E-06	8.02E-08	8.75E-13	2.18E-10	1.59E-08	1.19E-06
70	10000	9.12E-07	2.04E-08	4.91E-15	2.46E-11	6.36E-10	9.33E-07
36	10000	3.91E-07	1.92E-08	3.05E-11	1.00E-11	2.47E-10	4.11E-07
76	10000	2.21E-08	1.42E-09	3.79E-12	1.81E-11	1.42E-11	2.35E-08
68	10000	6.93E-09	3.64E-10	1.55E-11	1.26E-11	3.34E-12	7.32E-09
11	10000	5.39E-09	1.54E-11	1.20E-13	3.60E-14	3.91E-13	5.40E-09
58	10000	4.63E-09	1.01E-10	1.78E-11	5.89E-12	1.38E-12	4.75E-09
62	10000	3.52E-09	1.02E-09	2.95E-11	3.14E-12	7.34E-13	4.58E-09
67	10000	3.36E-09	1.37E-10	3.54E-11	1.04E-13	3.42E-13	3.53E-09
3	10000	3.38E-09	1.37E-11	1.38E-11	2.12E-14	5.96E-14	3.40E-09
85	10000	2.98E-09	2.17E-11	5.62E-13	2.39E-12	5.52E-13	3.01E-09
42	10000	1.71E-09	3.88E-10	5.30E-12	1.42E-12	8.98E-13	2.10E-09
37	10000	1.72E-09	7.75E-12	3.26E-12	1.85E-14	1.05E-13	1.73E-09
25	10000	1.15E-09	6.24E-12	1.86E-14	1.89E-14	2.20E-13	1.16E-09
27	10000	4.14E-10	1.40E-10	1.22E-10	8.22E-14	1.89E-14	6.76E-10
20	10000	3.93E-10	8.60E-12	6.19E-12	2.92E-13	4.45E-14	4.08E-10
78	10000	8.79E-11	7.96E-11	1.51E-33	1.57E-13	1.30E-11	1.81E-10
79	10000	9.82E-11	3.22E-12	5.15E-12	6.93E-15	3.58E-16	1.07E-10
23	10000	2.54E-11	1.30E-11	1. 7 0E-11	1.15E-15	1.69E-15	5.54E-11
95	10000	4.74E-11	3.24E-13	5.80E-15	7.52E-16	7.38E-15	4.78E-11
94	10000	1.59E-11	5.37E-12	1.31E-12	3.18E-14	7.23E-15	2.26E-11
19	10000	1.56E-11	1.21E-13	1.93E-13	2.5 8 E-16	3.22E-16	1.59E-11
38	10000	2.94E-12	2.62E-13	3. 79 E-13	2. 77 E-15	2.49E-16	3.59E-12
93	10000	2.97E-12	9.48E-14	3.13E-14	1.37E-15	4.23E-16	3.09E-12
10	10000	1.64E-12	5.32E-14	4.79E-14	4.21E-15	1.21E-16	1.75E-12
56	10000	1.08E-12	5.66E-14	5.20E-17	2.03E-16	5.22E-16	1.14E-12
59	10000	3.29E-14	5.14E-15	8.23E-15	3.01E-17	1.01E-18	4.63E-14
12	10000	3.72E-14	1.35 E -15	2.1 6E- 15	1.84E-18	2.29E-18	4.07E-14
6	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
47	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
65	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
71	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00

73	10000	0.00E+00	0.00E+00	0.00E+00	0.00E÷00	0.00E+00	0.00E+00	
77	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	
99	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	ĺ

Table C.20. s6 at 4000 years.

vector	time	EPA1BHRC	EPA2BHRC	EPA3BHRC	EPA4BHRC	EPA5BHRC	EPATBHRC
		²⁴¹ Am	²³⁹ Pu	²³⁸ Pu	²³⁴ U	²³⁰ Th	Total - All MB
54	10000	2.44E-01	2.19E+00	9.59E-15	8.25E-03	1.92E-02	2.46E+00
57	10000	2.36E-01	1.74E+00	-3.90E-11	7.44E-03	1.83E-02	2.00E+00
83	10000	1.07E-01	1.38E+00	5.30E-15	1.03E-02	4.85E-03	1.50E+00
81	10000	1.46E-01	1.21E+00	-5.65E-13	9.61E-04	4.81E-03	1.36E+00
28	10000	2.50E-01	1.03E+00	4.99E-15	4.56E-04	2.75E-02	1.31E+00
72	10000	2.29E-01	9.01E-01	-4.65E-13	9.98E-03	1.67E-02	1.16E+00
55	10000	1.78E-01	5.13E-01	-4.12E-08	3.01E-03	6.28E-03	7.01E-01
74	10000	1.91E-01	4.12E-01	1.71E-15	7.81E-03	8.88E-03	6.20E-01
51	10000	1.47E-01	4.15E-01	-1.92E-08	6.81E-03	8.74E-03	5.78E-01
5	10000	1.76E-01	2.58E-01	9.46E-16	3.94E-03	8.18E-03	4.46E-01
80	10000	1.6 8E -01	1.91E-01	-5.53E-14	5.42E-03	6.01E-03	3.71E-01
88	10000	2.18E-01	9.23E-02	4.53E-16	1.7 8E -04	1.08E-02	3.21E-01
66	10000	1.07E-01	1.86E-01	7.69E-16	1.37E-03	2.74E-03	2.97E-01
64	10000	1.60E-01	5.22E-02	-9.97E-12	7.54E-05	4.70E-03	2.17E-01
53	10000	1.18E-01	8.02E-02	-1.06E-13	2.77E-03	5.15E-03	2.06E-01
29	10000	1.39E-01	5.83E-02	2.76E-16	3.31E-03	4.36E-03	2.05E-01
30	10000	5.10E-02	9.77E-02	-1. 87 E-10	3.19E-03	3.33E-03	1.55E-01
82	10000	8.17E-02	5.27E-02	-1.53E-11	2.69E-04	7.87E-04	1.35E-01
63	10000	2.24E-02	8.14E-02	-3.67E-09	1.25E-03	9.98E-04	1.06E-01
50	10000	8.33E-02	1.69E-02	6.28E-17	3.42E-05	2.36E-03	1.03E-01
49	10000	7.35E-02	2.09E-02	3.83E-17	4.83E-05	3.31E-03	9.78E-02
43	10000	3.66E-02	4.79E-02	2.10E-16	4.71E-04	1.11E-03	8.61E-02
97	10000	4.56E-02	3.57E-02	2.64E-16	1.92E-03	6.05E-04	8.39E-02
60	10000	6.29E-02	1.75E-02	5.24E-17	3.23E-05	2.27E-03	8.28E-02
17	10000	5.27E-02	1.74E-02	3.41E-17	1.30E-03	2.78E-03	7.41E-02
26	10000	3.68E-02	8.05E-03	1.45E-17	1.70E-05	1.29E-03	4.61E-02
32	10000	3.18E-02	1.51E-03	2.20E-17	4.77E-06	2.70E-04	3.35E-02
33	10000	2.84E-02	4.63E-03	-1.92E-10	8.62E-07	8.45E-05	3.31E-02
86	10000	2.24E-02	7.40E-03	2.17E-17	1.18E-05	8.56E-04	3.06E-02
91	10000	3.26E-03	2.07E-02	-3.34E-08	4.45E-05	1.56E-05	2.41E-02
39	10000	1. 86E-02	3.28E-03	2.45E-17	4.54E-06	2.57E-04	2.21E-02
87	10000	1.11E-02	4.10E-03	4.61E-17	1.22E-06	6.27E-05	1.52E-02
21	10000	1.23E-02	1.24E-03	2.56E-17	2.38E-05	4.35E-05	1.36E-02
40	10000	1.19E-02	4.46E-04	-8.44E-10	1.46E-06	7.23E-05	1.24E-02
13	10000	8.75E-03	5.81E-04	-4.62E-13	9.25E-07	4.42E-05	9.38E-03
75	10000	6.23E-03	4.79E-04	5.63E-18	9.72E-07	6.34E-05	6.78E-03
35	10000	5.32E-03	2.54E-04	7.09E-18	3.20E-07	1.52E-05	5.59E-03
52	10000	3.69E-03	1.27E-04	-1.47E-09	2.83E-07	1.35E-05	3.83E-03
22	10000	1.97E-03	1.67E-03	-1.45E-08	3.49E-05	2.22E-05	3.70E-03

1	61	10000	1.73E-03	7.05E-04	-2.67E-11	1.91E-05	6.11E-06	2.46E-03	Į
	34	10000	1.89E-03	1.81E-04	3.26E-18	2.23E-07	1.07E-05	2.08E-03	۱
	96	10000	1.98E-03	7.90E-05	-3.38E-12	1.69E-07	8.03E-06	2.06E-03	ĺ
	100	10000	1.71E-03	7.56E-05	1.23E-18	2.23E-07	1.08E-05	1.80E-03	
	16	10000	1.51E-03	7.28E-05	-5.98E-14	1.39E-07	6.65E-06	1.59E-03	İ
Ì	1	10000	9.10E-04	7.56E-05	1.27E-18	1.23E-07	6.16E-06	9,92E-04	1
	2	10000	6.85E-04	2.76E-04	-1.05E-08	1.60E-06	2.98E-06	9.66E-04	
1	31	10000	6.64E-04	2.89E-04	-5.06E-10	7.49E-08	3.58E-06	9.57E-04	1
	69	10000	6.64E-04	7.07E-05	-3.62E-09	7.36E-08	3.49E-06	7.38E-04	ı
١	15	10000	6.42E-04	2.80E-05	-1.91E-10	7.57E-07	7.02E-07	6.71E-04	l
	8	10000	5.95E-04	3.36E-05	3.13E-19	8.02E-08	4.06E-06	6.33E-04	
i	7	10000	5.45E-04	2.61E-05	-4.62E-09	5.70E-08	2.68E-06	5.73E-04	
	46	10000	5.29E-04	3.84E-05	6.28E-19	5.25E-08	2.53E-06	5.70E-04	
l	45	10000	3.87E-04	7.80E-05	-3.25E-10	2.24E-07	1.59E-05	4.81E-04	ļ
	90	10000	4.63E-04	1.11E-05	2.25E-19	3.78E-08	1.81E-06	4.76E-04	l
l	24	10000	3.53E-04	2.08E-05	-2.30E-11	3.44E-08	1.61E-06	3.75E-04	ı
	9	10000	1.26E-04	1.64E-05	-6.92E-13	1.65E-06	3.09E-07	1.44E-04	l
	44	10000	7.81E-05	1.44E-05	-2.08E-09	9.07E-09	4.26E-07	9.29E-05	
l	48	10000	5.78E-05	4.34E-06	-6.89E-09	2.05E-09	9.63E-08	6.22E-05	
	98	10000	4.88E-05	1.35E-06	4.14E-20	2.62E-09	1.24E-07	5.03E-05	
l	89	10000	4.23E-05	1.38E-06	3.22E-18	4.10E-09	2.80E-07	4.39E-05	ł
ĺ	18	10000	2.43E-05	3.15E-07	-1.33E-10	4.76E-10	2.24E-08	2.47E-05	l
	14	10000	1.33E-05	4.41E-07	-2.01E-12	3.04E-10	1.43E-08	1.38E-05	
h	41	10000	1. 06E-05	3.86E-07	8.25E-21	7.90E-10	3.78E-08	1.10E-05	l
P	92	10000	6.51E-06	8.47E-07	4.83E-17	5.44E-09	7.90E-09	7.38E-06	ı
ĺ	84	10000	4.99E-06	4.77E-07	1.72E-20	1.53E-08	6.05E-09	5.49E-06	l
ļ	70	10000	6.51E-07	2.00E-08	7.21E-22	2.43E-11	1.14E-09	6.73E-07	l
	4	10000	5.41E-07	5.21E-08	1.29E-19	1.42E-10	1.15E-08	6.05E-07	ĺ
	36	10000	2.89E-07	1.88E-08	-7.16E-14	9.91E-12	4.55E-10	3.09E-07	l
	76	10000	1.58E-08	1.39E-09	5.59E-19	1.79E-11	2.56E-11	1.72E-08	
	68	10000	5.03E-09	3.57E-10	2.29E-18	1.25E-11	6.16E-12	5.41E-09	ŀ
	58	10000	4.35E-09	9.90E-11	-3.39E-11	6.13E-12	5.30E-12	4.43E-09	
	62	10000	3.33E-09	1.00E-09	4.33E-18	3.11E-12	2.62E-12	4.34E-09	
	11	10000	4.49E-09	1.39E-11	-3.89E-10	1.29E-13	8.79E-12	4.13E-09	l
	67	10000	3.21E-09	1.34E-10	-1.55E-12	1.06E-13	1.51E-12	3.34E-09	l
	3	10000	3.29E-09	1.34E-11	2.04E-18	2.34E-14	6.34E-13	3.30E-09	ĺ
	85	10000	2.84E-09	2.12E-11	-4.77E-12	2.42E-12	2.29E-12	2.86E-09	l
	42	10000	1.60E-09	3.80E-10	7.77E-19	1.41E-12	2.94E-12	1.99E-09	ĺ
	37	10000	1.65E-09	7.58E-12	-5.31E-12	2.05E-14	6.76E-13	1.65E-09	l
	25	10000	1.07E-09	6.11E-12	2.74E-21	1. 86 E-14	6.50E-13	1.08E-09	ĺ
	20	10000	3.82E-10	8.43E-12	9.13E-19	3.12E-13	3.74E-13	3.91E-10	
	78	10000	2.94E-11	2.93E-11	0.00E+00	5.79E-14	5.15 E-1 2	6.39E-11	
	95	10000	4.47E-11	3.17E-13	8.52E-22	7.44E-16	2.48E-14	4.50E-11	
	23	10000	2.48E-11	1.28E-11	-1.55E-12	1.34E-15	2.69E-14	3.61E-11	
	19	10000	1.53E-11	1.19E-13	2.85E-20	3.08E-16	7.94E-15	1.54E-11	
	93	10000	2.85E-12	9.29E-14	4.62E-21	1.40E-15	2.11E-15	2.94E-12	
	56	10000	9.92E-13	5.54E-14	7.63E-24	2.00E-16	1.41E-15	1.05E-12	İ

59	10000	3.22E-14	5.06E-15	1.22E-21	3.58E-17	2.49E-17	3.73E-14
6	10000	0.00E+00	0.00E+00	0.00E÷00	0.00E+00	0.00E+00	0.00E+00
47	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
65	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
71	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
73	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
77	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
99	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
12	10000	-1.08E-11	-3.10E-13	-9.87E-11	1.67E-14	1.35E-12	-1.08E-10
27	10000	3.94E-10	1.35E-10	-7.23E-10	1.37E-13	4.39E-13	-1.94E-10
38	10000	-3.33E-11	-2.30E-12	-8.11E-10	1.04E-12	5.03E-12	-8.41E-10
10	10000	-9.34E-11	-2.38E-12	-7.73E-10	6.95E-12	4.37E-12	-8.58E-10
94	10000	-7.91E-12	-9.22E-13	-1.96E-09	1.26E-12	3.42E-12	-1.97E-09
79	10000	-7.71E-09	-2.00E-10	-6.44E-08	1.71E-11	5.76E-11	-7.22E-08

Table C.21. s6 at 6000 years.

vector	time	EPA1BHRC		EPA3BHRC	EPA4BHRC	EPA5BHRC	EPATBHRC
		²⁴¹ Am	²³⁹ Pu	²³⁸ Pu	²³⁴ U	²³⁰ Th	Total - All MB
54	10000	3.17E-02	1.76E+00	1.40E-21	6.66E-03	1.82E-02	1.82E+00
57	10000	3.15E-02	1.45E+00	-4.41E-11	6.21E-03	1.83E-02	1.50E+00
83	10000	2.13E-02	1.01E+00	7.76E-22	7.61E-03	4.08E-03	1.04E+00
28	10000	3.21E-02	8.81E-01	7.31E-22	3.93E-04	2.87E-02	9.42E-01
81	10000	2.45E-02	9.07E-01	-6.00E-13	7.22E-04	4.14E-03	9.36E-01
72	10000	3.10E-02	7.26E-01	-4.88E-13	8.07E-03	1.59E-02	7.81E-01
55	10000	2.79E-02	4.83E-01	-4.40E-08	2.85E-03	7.48E-03	5.21E-01
51	10000	2.61E-02	3.46E-01	-2.05E-08	5.71E-03	8.72E-03	3.87E-01
74	10000	2.88E-02	3.32E-01	2.51E-22	6.32E-03	8.47E-03	3.76E-01
5	10000	2.76E-02	1.98E-01	1.38E-22	3.04E-03	7.29E-03	2.36E-01
80	10000	2.63E-02	1.43E-01	-5.85E-14	4.07E-03	5.17E-03	1.79E-01
66	10000	1.83E-02	1.29E-01	1.13E-22	9.54E-04	2.14E-03	1.51E-01
88	10000	3.04E-02	7.74E-02	6.63E-23	1.50E-04	1.10E-02	1.19E-01
53	10000	2.25E-02	6.17E-02	-1.11E-13	2.14E-03	4.60E-03	9.09E-02
30	10000	1.37E-02	6.57E-02	-2.04E-10	2.15E-03	2.51E-03	8.41E-02
29	10000	2.39E-02	4.85E-02	4.05E-23	2.76E-03	4.33E-03	7.95E-02
63	10000	7.39E-03	6.37E-02	-3.86E-09	9.81E-04	9.11E-04	7.29E-02
64	10000	2.56E-02	4.19E-02	-1.04E-11	6.07E-05	4.45E-03	7.19E-02
82	10000	1.34E-02	5.03E-02	-1.60E-11	2.58E-04	9.83E-04	6.49E-02
97	10000	8.04E-03	3.36E-02	3.86E-23	1.82E-03	7.29E-04	4.42E-02
43	10000	8.65E-03	2.92E-02	3.08E-23	2.88E-04	7.38E-04	3.88E-02
49	10000	1.68E-02	1.60E-02	5.61E-24	3.71E-05	2.93E-03	3.58E-02
50	10000	1.67E-02	1.18E-02	9.20E-24	2.39E-05	1.85E-03	3.04E-02
60	10000	1.35E-02	1.16E-02	7.67E-24	2.14E-05	1.67E-03	2.68E-02
17	10000	1.25E-02	9.97E-03	4.99E-24	7.47E-04	1.73E-03	2.50E-02
91	10000	6.19E-04	2.04E-02	-3.54E-08	4.39E-05	2.12E-05	2.11E-02
86	10000	5.37E-03	4.72E-03	3.18E-24	7.55E-06	6.03E-04	1.07E-02
26	10000	5.44E-03	2.77E-03	2.13E-24	5.84E-06	4.14E-04	8.63E-03

1	39	10000	4.97E-03	3.20E-03	3.59E-24	4.44E-06	3.25E-04	8.50E-03	i
	33	10000	3.68E-03	4.54E-03	-2.12E-10	8.52E-07	1.14E-04	8.34E-03	1
	32	10000	5.83E-03	1.32E-03	3.22E-24	4.21E-06	2.95E-04	7.45E-03	
	87	10000	1.65E-03	4.03E-03	6.75E-24	1.21E-06	8.31E-05	5.76E-03	
	21	10000	2.05E-03	1.22E-03	3.75E-24	2.35E-05	5.91E-05	3.36E-03	
1	40	10000	1.65E-03	4.38E-04	-8.94E-10	1.45E-06	9.71E-05	2.19E-03	1
	13	10000	1.34E-03	5.71E-04	-5.09E-13	9.14E-07	6.01E-05	1.97E-03	
1	75	10000	1.34E-03	3.00E-04	8.24E-25	6.11E-07	4.25E-05	1.68E-03	
	22	10000	2.38E-04	1.01E-03	-1.62E-08	2.12E-05	1.36E-05	1.28E-03	İ
	61	10000	2.63E-04	6.93E-04	-2.83E-11	1.89E-05	8.19E-06	9.83E-04	
	35	10000	6.56E-04	2.50E-04	1,04E-24	3.16E-07	2.07E-05	9.27E-04	l
	52	10000	5.53E-04	1.25E-04	-1.69E-09	2.79E-07	1.84E-05	6.96E-04	
1	34	10000	4.01E-04	1.78E-04	4,77E-25	2.20E-07	1.45E-05	5.93E-04	l
	96	10000	4.72E-04	7.76E-05	-3.54E-12	1.67E-07	1.10E-05	5.61E-04	
	16	10000	3.47E-04	7.15E-05	-6.33E-14	1.37E-07	9.04E-06	4.27E-04	
	31	10000	8.51E-05	2.84E-04	-5.71E-10	7.41E-08	4.87E-06	3.74E-04	l
	2	10000	8.31E-05	2.72E-04	-1.11E-08	1.58E-06	4.08E-06	3.60E-04	
l	100	10000	2.32E-04	7.42E-05	1.80E-25	2.21E-07	1.46E-05	3.22E-04	l
	1	10000	1.30E-04	7.43E-05	1.86E-25	1.22E-07	8.24E-06	2.13E-04	
	69	10000	8.29E-05	6.95E-05	-3.90E-09	7.28E-08	4.76E-06	1.57E-04	l
	45	10000	9.19E-05	5.06E-05	-3.44E-10	1.46E-07	1.14E-05	1.54E-04	
	8	10000	1.02E-04	3.30E-05	4.58E-26	7.93E-08	5.41E-06	1.40E-04	
	46	10000	6.84E-05	3.77E-05	9.19E-26	5.19E-08	3.43E-06	1.10E-04	ł
	15	10000	7.79E-05	2.75E-05	-1.99E-10	7.48E-07	9.61E-07	1.07E-04	
7	7	10000	6.61E-05	2.56E-05	-4.92E-09	5.64E-08	3.67E-06	9.54E-05	
	90	10000	5.86E-05	1.09E-05	3.29E-26	3.74E-08	2.46E-06	7.20E-05	ĺ
	24	10000	4.28E-05	2.05E-05	-2.41E-11	3.40E-08	2.21E-06	6.55E-05	l
	9	10000	1.59E-05	1.61E-05	-7.42E-13	1.63E-06	4.20E-07	3.41E-05	
	44	10000	9.47E-06	1.42E-05	-2.18E-09	8.97E-09	5.84E-07	2.42E-05	l
	89	10000	1.49E-05	1.02E-06	4.71E-25	3.03E-09	2.36E-07	1.61E-05	
	98	10000	1.09E-05	1.33E-06	6.06E-27	2.59E-09	1.69E-07	1.24E-05	
	48	10000	7.00E-06	4.26E-06	-7.49E-09	2.03E-09	1.32E-07	1.14E-05	l
ľ	18	10000	2.95E-06	3.10E-07	-1.39E-10	4.71E-10	3.06E-08	3.29E-06	l
	92	10000	1.94E-06	8.32E-07	7.08E-24	5.38E-09	1.14E-08	2.79E-06	
l	14	10000	2.07E-06	4.33E-07	-2.24E-12	3.01E-10	1.96E-08	2.53E-06	
l	41	10000	1.83E-06	3.79E-07	1.21E-27	7.81E-10	5.14E-08	2.26E-06	İ
	84	10000	8.79E-07	4.69E-07	2.51E-27	1.51E-08	8.28E-09	1.37E-06	
ĺ	4	10000	2.32E-07	2.31E-08	1.89E-26	6.33E-11	5.52E-09	2.61E-07	ĺ
	70	10000	1.66E-07	1.97E-08	1. 06E-28	2.41E-11	1.57E-09	1.87E-07	l
	36	10000	7.27E-08	1.85E-08	-7.49E-14	9.80E-12	6.29E-10	9.19E-08	ļ
	76	10000	3.78E-09	1.37E-09	8.19E-26	1.76E-11	3.51E-11	5.20E-09	
•	62	10000	1.78E-09	9.84E-10	6.34E-25	3.07E-12	4.20E-12	2.77E-09	l
	58	10000	1.91E-09	9.68E-11	-3.65E-11	6.07E-12	8.62E-12	1.99E-09	
1	67	10000	1.35E-09	1.32E-10	-1.62E-12	1.05E-13	2.48E-12	1.48E-09	
_	68	10000	1.09E-09	3.50E-10	3.36E-25	1.24E-11	8.50E-12	1.46E-09	ł
	42	10000	8.38E-10	3.73E-10	1.14E-25	1.39E-12	4.64E-12	1.22E-09	
	85	10000	1.19E-09	2.07E-11	-5.01E-12	2.39E-12	3.75E-12	1.21E-09	

3	10000	1.14E-09	1.32E-11	2.99E-25	2.31E-14	1.11E-12	1.15E-09
37	10000	5.27E-10	7.39E-12	-5.55E-12	2.03E-14	1.16E-12	5.30E-10
25	10000	2.65E-10	5.99E-12	4.01E-28	1.84E-14	1.01E-12	2.72E-10
20	10000	2.55E-10	8.27E-12	1.34E-25	3.09E-13	6.47E-13	2.64E-10
23	10000	1.73E-11	1.25E-11	-1.62E-12	1.32E-15	4.79E-14	2.82E-11
19	10000	1.09E-11	1.16E-13	4.18E-27	3.04E-16	1.43E-14	1.10E-11
95	10000	8.38E-12	3.11E-13	1.25E-28	7.35E-16	3.92E-14	8.73E-12
93	10000	1.22E-12	9.11E-14	6.77E-28	1.39E-15	3.51E-15	1.31E-12
56	10000	4.58E-13	5.44E-14	1.12E-30	1.98E-16	2.15E-15	5.15E-13
59	10000	2.30E-14	4.96E-15	1.78E-28	3.53E-17	4.47E-17	2.80E-14
6	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
47	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
65	[10000]	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
71	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
73	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
77	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
78	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
99	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
12	10000	-1.10E-10	-9.92E-13	-1.03E-10	1.68E-14	2.59E-12	-2.11E-10
27	10000	1.70E-10	1.27E-10	-7.86E-10	1.39E-13	8.32E-13	-4.88E-10
38	10000	-3.76E-10	-8.14E-12	-8.72E-10	1.08E-12	9.93E-12	-1.25E-09
10	10000	-9.76E-10	-7.83E-12	-8.19E-10	7.08E-12	8.49E-12	-1.79E-09
94	10000	-2.33E-10	-1.51E-11	-2.10E-09	1.29E-12	6.71E-12	-2.34E-09
11	10000	-7.42E-09	1.09E-11	-4.09E-10	1.30E-13	1.65E-11	-7.80E-09
79	10000	-1.99E-07	-6.53E-10	-6.81E-08	1.74E-11	1.12E-10	-2.68E-07

Table C.22. s6 at 9000 years.

vector	time	EPA1BHRC	EPA2BHRC	EPA3BHRC	EPA4BHRC	EPA5BHRC	EPATBHRC
<u> </u>		²⁴¹ Am	²³⁹ Pu	²³⁸ Pu	²³⁴ U	²³⁰ T h	Total - All MB
54	10000	1.80E-02	9.73E-01	7.81E-32	3.70E-03	1.23E-02	1.01E+00
57	10000	1.80E-02	8.80E-01	-4.66E-11	3.79E-03	1.37E-02	9.16E-01
28	10000	1. 82E-02	5.48E-01	4.01E-32	2.46E-04	2.21E-02	5.89E-01
81	10000	1.17E-02	4.49E-01	-6.12E-13	3.59E-04	2.47E-03	4.64E-01
72	10000	1.77E-02	3.88E-01	-4.96E-13	4.34E-03	1.03E-02	4.21E-01
83	10000	6.93E-03	2.59E-01	4.34E-32	1.96E-03	1.16E-03	2.69E-01
55	10000	1.51E-02	2.38E-01	-4.50E-08	1.41E-03	4.49E-03	2.59E-01
74	10000	1.62E-02	1.85E-01	1.38E-32	3.54E-03	5.75E-03	2.11E-01
51	10000	1.36E-02	1.43E-01	-2.10E-08	2.37E-03	4.37E-03	1.63E-01
5	10000	1.41E-02	8.55E-02	7.62E-33	1.32E-03	3.76E-03	1.05E-01
80	10000	1.30E-02	6.76E-02	-5.94E-14	1.93E-03	2.93E-03	8.55E-02
88	10000	1.74E-02	4.72E-02	3.40E-33	9.17E-05	8.24E-03	7.29E-02
66	10000	7.87E-03	5.89E-02	6.27E-33	4.37E-04	1.16E-03	6.84E-02
82	10000	7.01E-03	3.88E-02	-1.63E-11	2.00E-04	9.83E-04	4.70E-02
64	10000	1.33E-02	2.43E-02	-1.06E-11	3.55E-05	3.18E-03	4.09E-02
29	10000	1.08E-02	2.08E-02	2.22E-33	1.19E-03	2.22E-03	3.51E-02
53	10000	8.83E-03	2.05E-02	-1.13E-13	7.12E-04	1.76E-03	3.18E-02

1	97	10000	3.65E-03	2.05E-02	2.14E-33	1.11E-03	5.51E-04	2.58E-02	
	30	10000	3.76E-03	1.66E-02	-2.11E-10	5.43E-04	7.19E-04	2.16E-02	
₽	91	10000	3.45E-04	1.99E-02	-3.62E-08	4.32E-05	2.80E-05	2.03E-02	
	63	10000	1.83E-03	1.64E-02	-3.94E-09	2.54E-04	2.73E-04	1.88E-02	ı
1	43	10000	3.32E-03	1.23E-02	1.72E-33	1.22E-04	3.57E-04	1.61E-02	
1	50	10000	6.32E-03	4.50E-03	4.87E-34	9.18E-06	8.20E-04	1.16E-02	
ĺ	49	10000	5.55E-03	4.49E-03	2.68E-34	1.04E-05	9.39E-04	1.10E-02	ł
	60	10000	4.01E-03	3.47E-03	4.15E-34	6.42E-06	5.72E-04	8.06E-03	
	17	10000	3.52E-03	2.58E-03	2.61E-34	1.94E-04	5.06E-04	6.80E-03	
	33	10000	2.09E-03	4.42E-03	-2.20E-10	8.35E-07	1.48E-04	6.66E-03	ĺ
	26	10000	3.06E-03	2.33E-03	6.92E-35	4.94E-06	4.43E-04	5.84E-03	l
	39	10000	2.62E-03	1.69E-03	1.94E-34	2.36E-06	2.11E-04	4.52E-03	
	87	10000	8.98E-04	3.44E-03	3.74E-34	1.04E-06	9.28E-05	4.43E-03	١
-	32	10000	2.92E-03	1.01E-03	1.55E-34	3.22E-06	2.84E-04	4.22E-03	ĺ
	86	10000	1.18E-03	1.16E-03	1.76E-34	1.86E-06	1.65E-04	2.51E-03	l
	21	10000	1.15E-03	1.19E-03	2.10E-34	2.31E-05	7.78E-05	2.44E-03	ļ
	40	10000	9.23E-04	4.04E-04	-9.15E-10	1.34E-06	1.19E-04	1.45E-03	I
	13	10000	7.51E-04	5.57E-04	-5.29E-13	8.99E-07	7.91E-05	1.39E-03	1
	22	10000	1.27E-04	9.36E-04	-1.69E-08	1.97E-05	1.67E-05	1.10E-03	Ì
ł	75	10000	7.04E-04	2.47E-04	4.56E-35	5.05E-07	4.44E-05	9.96E-04	l
	61	10000	1.43E-04	6.27E-04	-2.90E-11	1.72E-05	9.76E-06	7.97E-04	
	35	10000	3.65E-04	2.44E-04	5.80E-35	3.11E-07	2.73E-05	6.36E-04	
ĺ	52	10000	3.09E-04	1.22E-04	-1.79E-09	2.74E-07	2.42E-05	4.55E-04	l
	34	10000	2.26E-04	1.74E-04	2.64E-35	2.17E-07	1.91E-05	4.19E-04	
7	96	10000	2.62E-04	7.58E-05	-3.59E-12	1.64E-07	1.44E-05	3.52E-04	ļ
	31	10000	4.81E-05	2.78E-04	-5.99E-10	7.28E-08	6.41E-06	3.32E-04	l
	2	10000	4.57E-05	2.65E-04	-1.13E-08	1.55E-06	5.39E-06	3.18E-04	
	16	10000	1.93E-04	6.98E-05	-6.46E-14	1.35E-07	1.19E-05	2.75E-04	l
l	100	10000	1.35E-04	7.25E-05	8.00E-36	2.17E-07	1.92E-05	2.27E+04	
	1	10000	6.25E-05	5.75E-05	1.03E-35	9.47E-08	8.34E-06	1.28E-04	
	69	[10000]	4.63E-05	6.79E-05	-4.02E-09	7.16E-08	6.28E-06	1.20E-04	l
	8	10000	5.71E-05	2.91E-05	1.77E-36	7.04E-08	6.30E-06	9.26E-05	l
ļ	46	10000	3.88E-05	3.69E-05	4.96E-36	5.10E-08	4.50E-06	8.02E-05	l
	15	10000	4.29E-05	2.68E-05	-2.02E-10	7.36E-07	1.27E-06	7.17E-05	
	7	10000	3.63E-05	2.50E-05	-5.05E-09	5.54E-08	4.85E-06	6.62E-05	
İ	45	10000	2.85E-05	1.88E-05	-3.51E-10	5.45E-08	4.91E-06	5.23E-05	l
	90	10000	3.30E-05	1.07E-05	1.56E-36	3.68E-08	3.24E-06	4.69E-05	
	24	[10000]	2.36E-05	2.00E-05	-2.44E-11	3.34E-08	2.92E-06	4.65E-05	
	9	10000	8.87E-06	1.57E-05	-7. 6 1E-13	1.61E-06	5.53E-07	2.68E-05	ĺ
	44	10000	5.20E-06	1.38E-05	-2.22E-09	8.82E-09	7.71E-07	1.98E-05	۱
	48	10000	3.78E-06	4.16E-06	-7.77E-09	1.99E-09	1.74E-07	8.11E-06	1
1	98	10000	6.06E-06	1.30E-06	2.16E-37	2.54E-09	2.23E-07	7.58E-06	
	89	10000	3.62E-06	3.20E-07	2.57E-35	9.56E-10	8.53E-08	4.02E-06	
	18	10000	1.61E-06	3.03E-07	-1.42E-10	4.63E-10	4.05E-08	1.96E-06	l
	14	10000	1.14E-06	4.23E-07	-2.35E-12	2.96E-10	2.58E-08	1.59E-06	
	92	10000	7.49E-07	8.12E-07	3.96E-34	5.29E-09	1.55E-08	1.58E-06	
	41	10000	1.02E-06	3.71E-07	0.00E+00	7.68E-10	6.76E-08	1.46E-06	

84	10000	4. 8 4E - 07	4.58E-07	0.00E+00	1.49E-08	1.09E-08	9.68E-07
70	10000	9.15E-08	1.92E-08	0.00E+00	2.37E-11	2.07E-09	1.13E-07
36	10000	3.76E-08	1.81E-08	-7.63E-14	9.64E-12	8.36E-10	5.65E-08
76	10000	2.06E-09	1.33E-09	4.41E-36	1.74E-11	4.65E-11	3.46E-09
62	10000	3.47E-10	9.59E-10	3.52E-35	3.02E-12	6.07E-12	1.31E-09
68	10000	5.09E-10	3.42E-10	1.87E-35	1.22E-11	1.13E-11	8.75E-10
42	10000	3.37E-10	3.63E-10	6.06E-36	1.37E-12	6.66E-12	7.08E-10
67	10000	1.78E-10	1.28E-10	-1.64E-12	1.03E-13	3.63E-12	3.09E-10
3	10000	1.09E-10	1.28E-11	1.65E-35	2.27E-14	1.68E-12	1.24E-10
58	10000	1.72E-11	9.40E-11	-3.77E-11	5.96E-12	1.26E-11	9.21E-11
20	10000	6.22E-11	8.06E-12	7.20E-36	3.03E-13	9.73E-13	7.15E-11
85	10000	4.79E-11	2.02E-11	-5.12E-12	2.35E-12	5.51E-12	7.08E-11
25	10000	5.94E-11	5.84E-12	0.00E+00	1.81E-14	1.43E-12	6.67E-11
4	10000	3.34E-11	3.29E-12	8.50E-37	8.97E-15	6.86E-13	3.73E-11
23	10000	4.00E-12	1.22E-11	-1.64E-12	1.30E-15	7.31E-14	1.46E-11
95	10000	1.57E-12	3.03E-13	0.00E+00	7.22E-16	5.65E-14	1.93E-12
19	10000	1.46E-12	1.13E-13	2.34E-37	2.99E-16	2.18E-14	1.60E-12
93	10000	1.64E-13	8.88E-14	0.00E+00	1.36E-15	5.18E-15	2.59E-13
56	10000	1.61E-13	5.30E-14	0.00E+00	1.94E-16	3.03E-15	2.17E-13
59	10000	4.58E-15	4.84E-15	0.00E+00	3.47E-17	6.84E-17	9.52E-15
6	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
47	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
65	[10000]	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
71	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
73	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
77	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
78	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
99	10000	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
37	10000	-2.40E-10	7.15E-12	-5.65E-12	1.99E-14	1.75E-12	-2.37E-10
12	10000	-5.64E-10	-1.93E-12	-1.05E-10	1.61E-14	4.20E-12	-6.66E-10
27	10000	-5.33E-10	1.16E-10	-8.16E-10	1.36E-13	1.33E-12	-1.23E-09
38	10000	-1.96E-09	-1.63E-11	- 8.97 E-10	1.05E-12	1.62E-11	-2.86E-09
94	10000	-1.24E-09	-3.46E-11	-2.16E-09	1.26E-12	1.09E-11	-3.42E-09
10	10000	-5.56E-09	-1.54E-11	-8.38E-10	6.85E-12	1.38E-11	-6.39E-09
11	10000	-4.03E-08	6.75E-12	-4.17E-10	1.26E-13	2.64E-11	-4.06E - 08
79	10000	-6.64E-07	-1.28E-09	-6.96E-08	1.68E-11	1.82E-10	-7.34E-07

APPENDIX D

SECOTP2D RESULTS FOR CULEBRA TRANSPORT

Appendix D includes two Tables (one for partial mining and one for full mining) which contain results from Culebra transport calculations performed using SECOTP2D. Each Table contains the following values:

<u>Column</u>	Description
1	Rank according to ²³⁴ U discharge
2	Vector number
3	Integrated discharge of ²³⁴ U (kg) to LWB from a 1 kg source
	(Conditional Fraction of Source Released)
4	MINP_FAC - mining impact factor
5	CLIMTIDX - climate index
6	APOROS - fracture porosity
7	DPOROS - matrix porosity
8	HMBLKT - half-block length of the matrix
9	OXSTAT - actinide oxidation state parameter
10	MKD_U - k _d value for matrix sorption

Appendix D also includes the following Figures:

Figures

- D.1 D.5 Mass Balance Errors for Partial Mining
- D.6 D.10 Mass Balance Errors for Full Mining

U234 CUMULATIVE RELEASE R1 PARTIALLY MINED

Information Only

U234 CUMULATIVE RELEASE R1 PARTIALLY MINED

RNK	VEC	CUM REL	MINP_FAC	CLIMTID	X APOROS	DPOROS	HMBLKT	OXSTAT	MKD_U
75555555555555555555555555555555555555	-0948665438333333333427254371098765432 -1098965438333334272224211211111111115			1.15 1.13 1.23 1.023 1.006 1.0	7.04E-03 4.2E-03 4.38EE-03 1.02E-03 4.38EE-03 1.029E-03 4.029E-03 4.029E-03 4.029E-03 4.029E-03 4.029E-03 4.029E-03 4.029E-03 4.033 4.0	0.159 0.101 0.173 0.173 0.173 0.173 0.173 0.174 0.1216 0.1216 0.145 0.140 0.142 0.183 0.149 0.185 0.1179 0.185 0.1185 0.1185 0.1185 0.1185 0.1185 0.1186 0.1229 0.139 0.1480 0.1480 0.1480 0.1580 0.179 0.1885 0.1185 0.1185 0.1185 0.1186 0.1229 0.1886	0.2352 0.4250.4960.33200.4960.33307 0.23900.330900.329000.329000.329000.329000.329000.329000.329000.329000.3290000.3290000.3290000000000	0.268	
				1.00	9.77E-03	0.153	0.144	0.234 1.62	E+00

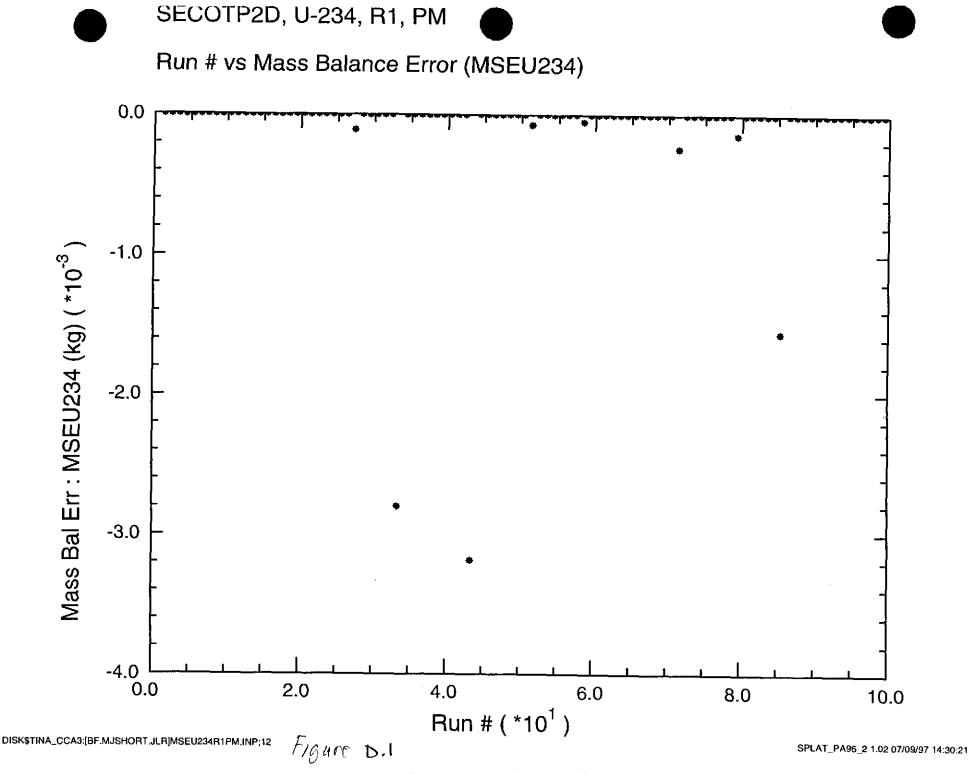
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J234 CUMULATIVE RELEASE R1 FULLY MINED

79 1.00E+00 562.5 1.64 7.10E-03 0.155 0. 74 9.20E-01 45.6 1.23 6.30E-03 0.205 0. 85 8.56E-01 794.6 1.05 1.36E-03 0.106 0. 4 33 7.86E-01 349.0 1.93 1.13E-04 0.164 0. 5 51 6.81E-01 374.2 1.72 3.32E-04 0.168 0. 6 43 6.70E-01 429.3 1.25 6.63E-04 0.106 0.	MBLKT OXSTAT MKD_U .421
74 9.20E-01 45.6 1.23 6.30E-03 0.205 0. 85 8.56E-01 794.6 1.05 1.36E-03 0.106 0. 4 33 7.86E-01 349.0 1.93 1.13E-04 0.164 0. 5 51 6.81E-01 374.2 1.72 3.32E-04 0.168 0. 6 43 6.70E-01 429.3 1.25 6.63E-04 0.106 0.	075 0.534 7.91E-05 249 0.778 3.49E-05 330 0.617 1.17E-04 241 0.864 9.07E-05 434 0.841 3.26E-05 286 0.805 6.59E-05 054 0.528 1.78E-04
7 57 4.41E-01 885.4 1.08 7.25E-03 0.250 0. 8 58 2.07E-01 492.9 1.21 1.47E-03 0.166 0. 9 84 3.85E-02 312.1 1.21 6.47E-04 0.126 0. 10 68 3.06E-02 589.7 1.12 2.00E-04 0.144 0. 11 67 2.40E-02 333.8 1.54 5.84E-04 0.231 0. 12 80 1.02E-02 870.6 1.12 1.37E-04 0.115 0. 13 54 8.82E-03 518.2 1.81 3.69E-03 0.133 0. 15 66 9.59E-04 598.1 1.03 1.14E-03 0.165 0. 15 66 9.59E-04 706.7 1.10 5.33E-04 0.104 0. 17 42 2.88E-04 706.7 1.10 5.33E-04 0.104 0. 18 97 3.93E-05 609.1 1.19 2.82E-03 0.168 0. 19 <td>445 0.715 6.53E-04 465 0.938 1.58E-04 066 0.732 5.77E-04 246 0.638 1.30E-04 277 0.904 5.54E-05 411 0.728 4.96E-05 450 0.582 1.47E-04 339 0.786 5.41E-04 226 0.746 6.02E-05 317 0.543 4.53E-04 210 0.653 3.57E-03 192 0.966 8.60E-04 312 0.945 5.03E-04 358 0.005 1.08E+00 087 0.185 4.86E+00 170 0.764 2.63E-02</td>	445 0.715 6.53E-04 465 0.938 1.58E-04 066 0.732 5.77E-04 246 0.638 1.30E-04 277 0.904 5.54E-05 411 0.728 4.96E-05 450 0.582 1.47E-04 339 0.786 5.41E-04 226 0.746 6.02E-05 317 0.543 4.53E-04 210 0.653 3.57E-03 192 0.966 8.60E-04 312 0.945 5.03E-04 358 0.005 1.08E+00 087 0.185 4.86E+00 170 0.764 2.63E-02
31 88 1.00E-15 385.4 1.19 2.32E-03 0.118 0.4 32 81 1.00E-15 955.8 1.15 5.79E-03 0.109 0.2 33 99 1.00E-15 784.1 1.18 1.39E-04 0.127 0.4 34 73 1.00E-15 614.8 1.10 5.51E-03 0.170 0.3 35 90 1.00E-15 65.0 1.20 1.27E-04 0.105 0.1 36 65 1.00E-15 756.2 1.97 3.67E-04 0.113 0.6 37 64 1.00E-15 403.2 1.07 3.26E-04 0.147 0.4	410 0.445 2.49E+00 206 0.701 8.94E-03 417 0.285 3.68E+00 385 0.012 1.29E+00 108 0.229 9.89E-01 057 0.758 4.91E-03 490 0.317 6.47E+00
39 62 1.00E-15 973.8 1.03 1.57E-04 0.177 0.2 40 61 1.00E-15 966.7 1.22 4.67E-04 0.122 0.4 41 60 1.00E-15 5.4 1.58 1.94E-04 0.108 0.4 42 96 1.00E-15 111.7 1.02 4.83E-04 0.176 0.4	258

U234 CUMULATIVE RELEASE R1 FULLY MINED

Information Only



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Run # vs Mass Balance Error (MSEPU239)

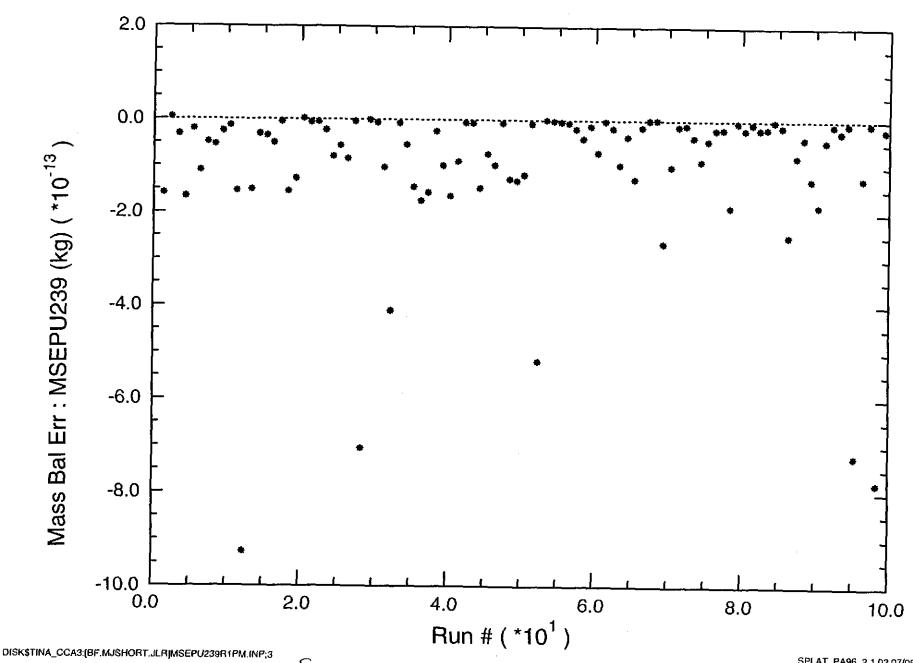


Figure D.2

SPLAT_PA96_2 1.02 07/09/97 14:30:28

APPENDIX E

CUTTINGS_S RESULTS FOR CUTTINGS, CAVINGS, AND SPALLINGS RELEASES Appendix E includes Tables and Figures which contain results from cuttings, cavings, and spallings calculations performed using CUTTINGS_S.

<u>Tables</u>	
E.1	Total volume removed (S1 with lower intrusion at 10,000 years)
E.2	Total volume removed (S2 with second intrusion at 10,000 years)
E.3	Total volume removed (S3 with second intrusion at 10,000 years)
E.4	Total volume removed (S4 with second intrusion at 10,000 years)
E.5	Total volume removed (S5 with second intrusion at 10,000 years)

Each Table contains the following values:

<u>Column</u>	Description
1	Vector number
2	TAUFAIL - sampled waste shear strength (Pa)
3	PRESGAS0 - repository pressure from BRAGFLO (Pa)
4	VOL_C - cuttings and cavings volume removed (m ³)
5	VOL_S - spallings volume removed (m³)
6	VOL_T - total cuttings/cavings plus spallings volume (m³)

Figures

<u>rigure</u>	<u> </u>	
E.1		PAVT cuttings and cavings volumes
E.2	- E.6	PAVT spallings volumes (S1 through S5)
E.7		PAVT cuttings and cavings releases (EPA units)
E.8	- E.12	PAVT spallings release (EPA units) (S1 through S5)
E.13		CCA cuttings and cavings volumes
E.14	- E.18	CCA spallings volumes (S1 through S5)
E.19		CCA cuttings and cavings releases (EPA units)
E.20	- E.24	CCA spallings release (EPA units) (S1 through S5)

					rage 1
Vect	or TAUFAIL	PRESGAS0	VOL_C	****	
1	1.881000E+01	8.313978E+06		VOL_S	VOL_T
2		0.3139/8E+00	3.410087E-01	3.513000E+00	3.854008E+00
	1.856000E-01	1.304271E+07	1.527955E+00	2.425000E+00	3.952954E+00
3	8.527000E-02	1.324386E+07	2.338110E+00	3.825000E+00	6.163110E+00
_ 4	5.363000E+00	1.302371E+07	4.686572E-01	1.599000E+00	· · · · · · · · · · · · · · · · · · ·
5	1.307000E+00	1.064915E+07			2.067657E+00
5 6	1.665000E+00		7.783863E-01	3.869999E+00	4.648386E+00
		6.983255E+06	1.004044E+00	0.000000E+00	1.004044E+00
7	6.758000E+01	1.349429E+07	3.011097E-01	7.293000E-01	1.030410E+00
8	4.290000E+01	1.306052E+07	3.011097E-01	1.719000E+00	
9	4.501000E+00	8.624728E+06			2.020110E+00
10	3.408000E+00		5.203530E-01	3.043000E+00	3.563353E+00
11		7.533316E+06	5.401012E-01	0.000000E+00	5.401012E-01
	2.629000E-01	1.327372E+07	1.506051E+00	3.304000E+00	4.810051E+00
12	2.512000E-01	1.168348E+07	1.510852E+00	3.204000E+00	4.714851E+00
13	2.191000E-01	4.522048E+06	1.544774E+00	0.000000E+00	
14	2.677000E+01	8.058337E+06			1.544774E+00
15	2.879000E+01		3.059013E-01	9.920999E-01	1.298001E+00
16		8.034358E+06	3.504883E-01	1.655000E+00	2.005488E+00
	3.997000E+01	7.050389E+06	3.300808E-01	0.000000E+00	3.300808E-01
17	3.024000E+01	1.313897E+07	3.280894E-01	2.021000E+00	2.349089E+00
18	4.025000E+00	7.491482E+06	5.199128E-01	0.000000E+00	
19	1.170000E+00	1.316570E+07			5.199128E-01
20	1.595000E+01		8.439972E-01	2.695000E+00	3.538997E+00
21		8.832614E+06	3.659891E-01	6.424999E-01	1.008489E+00
	5.307000E-02	6.902767E+06	3.937950E+00	0.000000E+00	3.937950E+00
22	4.204000E-01	1.272474E+07	1.242349E+00	3.378000E+00	4.620349E+00
23	1.067000E+01	9.299010E+06	4.607563E-01	2.743000E+00	
24	1.471000E+01	1.176252E+07	3.906219E-01		3.203756E+00
25	1.159000E-01	1.338674E+07		3.547000E+00	3.937622E+00
26	2.891000E+00		2.291612E+00	5.713000E-01	2.862912E+00
27		1.462004E+07	6.177633E-01	3.717999E+00	4.335763E+00
	7.333000E+01	8.864839E+06	3.011097E-01	3.300000E+00	3.601110E+00
28	5.119000E-01	1.683461E+07	1.091107E+00	1.537000E+00	2.628106E+00
29	7.923000E-02	1.159344E+07	2.397515E+00	3.839999E+00	
-20	1.227000E+01	1.205750E+07	3.947803E-01		6.237515E+00
	5.314000E-01	1.222787E+07		7.084000E-01	1.103180E+00
- - - - - - - - - -	1.966000E+01	7.146465E+06	9.645854E-01	2.887000E+00	3.851585E+00
33	1.291000E+01		3.492019E-01	0.000000E+00	3.492019E-01
34		6.839583E+06	3.902639E-01	0.000000E+00	3.902639E-01
	3.983000E-01	8.686502E+06	1.376624E+00	1.186000E+00	2.562624E+00
35	1.402000E+01	8.089325E+06	4.537664E-01	1.355000E+00	1.808766E+00
36	5.004000E+00	1.316047E+07	5.526043E-01	1.230000E+00	
37	7.433000E-01	9.732669E+06	9.596525E-01		1.782604E+00
38	9.944000E-02	1.278467E+07		2.282000E+00	3.241652E+00
39	1.989000E-01		2.164160E+00	2.046000E+00	4.210160E+00
40	4.705000E+01	1.375919E+07	1.750881E+00	1.740000E+00	3.490881E+00
	4.703000E+01	1.298037E+07	3.011097E-01	3.924999E+00	4.226109E+00
41	6.327000E+01	9.727151E+06	3.011097E-01	3.121000E+00	3.422110E+00
42	1.707000E+01	1.371927E+07	3.234804E-01	3.424000E+00	3.747480E+00
43	3.711000E+01	7.129679E+06	3.198346E-01	0.000000E+00	
44	1.734000E+00	9.791367E+06	6.452036E-01		3.198346E-01
45	5.943000E+00	5.125256E+06		2.457000E+00	3.102204E+00
46	3.466000E-01		4.657365E-01	0.000000E+00	4.657365E-01
47	5.680000E+00	9.754826E+06	1.382688E+00	3.623000E+00	5.005688E+00
	3.600000E+00	9.641884E+06	4.817018E-01	2.193000E+00	2.674702E+00
48	5.527000E-02	8.157126E+06	3.384981E+00	6.075999E-01	3.992581E+00
49	3.108000E-01	1.362422E+07	1.379820E+00	2.389000E+00	3.332301E+UU
50	1.047000E-01	8.863648E+06	2.011564E+00		3.768820E+00
51	6.825000E-01	1.505480E+07		1.822000E+00	3.833564E+00
52	7.967000E+00	1 0175155.00	1.228051E+00	1.850000E+00	3.078051E+00
53	8.730000E-01	1.017515E+07	5.047065E-01	1.501000E+00	2.005707E+00
	0./30000E-01	1.073825E+07	9.183298E-01	2.615000E+00	3.533330E+00
54	9.179000E-02	7.225482E+06	2.305037E+00	0.000000E+00	2.305037E+00
55	1.832000E+00	1.227937E+07	8.002669E-01	9.075000E-01	
	5.001000E+01	9.230021E+06	3.011097E-01	9.730999E-01	1.707767E+00
	9.015000E+00	7.067443E+06	4.179258E-01		1.274210E+00
56	1.508000E+00	1.594324E+07		0.000000E+00	4.179258E-01
59	7.061000E+00	エ・コラセンム4511/	9.178399E-01	2.293000E+00	3.210840E+00
60	2.222000E+00	1.261428E+07	4.990718E-01	2.843000E+00	3.342072E+00
61		1.198334E+07	6.345150E-01	2.498000E+00	3.132515E+00
	1.043000E+01	1.351048E+07	3.987798E-01	1.677000E+00	2.075780E+00
62	4.675000E-01	1.355103E+07	1.201360E+00	3.502000E+00	4.703360E+00
63	1.005000E+00	1.013145E+07	1.004293E+00	1.274000E+00	2.278293E+00
				TOURTUU	4.410473E+UU
				_	

1.952000E+00

100

1.541000E-01

8.725798E+06

1.386064E+00

3.732258E+00

Vol. C	_			_K132_H_110000_1	REPORT. TBL; 2	RE62 Page 1
1 1.883000E+01	Vect	tor TAUFAIL	PRESGAS0	VOI. C	WOI. C	IIOI m
2 1.856000B-01 6.13200EB-06 1.52795EB-00 0.00000B-00 1.52795EB-00 4 5.363000B-00 1.321200E-07 4.68657ZE-01 1.59900B-00 6.16110B-00 5.130700CP-00 7.235729E0-66 7.738363E-01 0.00000CB-00 7.335729E0-66 7.38863E-01 0.00000CB-00 7.335729E0-66 7.0000CB-00 0.00000CB-00 7.33573EB-00 0.00000CB-00 7.335729E0-66 7.0000CB-00 0.00000CB-00 3.174044E-00 0.0000CB-00 3.174044E-00 0.0000CB-00 3.0000CB-00 3.0000CB-00 3.0000CB-00 3.0000CB-00 3.0000CB-00 3.0000CB-00 3.0000CB-00 3.0000CB-00 3.0000CB-00 3.0000CB-00 3.0000CB-00 3.0000CB-00 3.0000CB-00 3.0000CB-00 3.0000CB-00 3.0000CB-00 3.000CB-00 3.0000CB-00 3	1	1.881000E+01				
3 8.527000E-02 1.149932E+07 2.338110E+00 3.22500E+00 6.163110E7+01 1.321200E+01 1.321200E+07 4.565000E+00 1.321200E+07 6.758000E+00 1.321200E+07 6.758000E+00 2.75657E+00 0.00000E+00 3.07657E+00 0.00000E+00 3.07657E+00 0.00000E+00 3.011097E+01 0.00000E+00 3.011097E+01 0.00000E+00 3.011097E+01 0.00000E+00 3.011097E+01 0.00000E+00 3.011097E+01 0.00000E+00 3.011097E+01 0.00000E+00 3.011097E+01 0.00000E+00 3.011097E+01 0.00000E+00 3.011097E+01 3.00000E+00 3.011097E+01 3.00000E+00 3.011097E+01 3.00000E+00 3.011097E+01 3.00000E+00 3.011097E+01 3.00000E+00 3.011097E+01 3.000000E+00 3.011097E+01 3.00000E+00 3.011097E+01 3.00000E+00 3.011097E+01 3.00000E+00 3.011097E+01 3.00000E+00 3.011097E+01 3.00000E+00 3.011097E+01 3.00000E+00 3.00000		1.856000E-01				
4 5.363300e+00 7.235729e+06 7.368363e-01 0.000000E+00 3.174048c-01 7.6575000E+01 1.160827E+07 1.004044e+00 2.170000E+00 3.174048c-01 0.00000E+00 3.174048c-01 0.00000E+00 3.010097E-01 0.000000E+00 3.010097E-01 0.00000E+00 3.0110097E-01 0.00000E+00 3.0110097E-01 1.02654E+07 7.000E+00 3.011097E-01 0.00000E+00 3.0110097E-01 1.02654E+07 7.000E+00 3.043000E+00 4.52300E+00 1.02654E+07 7.000E+00 3.043000E+00 4.52300E+00 1.02654E+07 7.000E+00 3.043000E+00 4.26310E+00 1.02654E+07 7.000E+00 3.043000E+00 4.26310E+00 1.02654E+07 7.000E+00 3.043000E+00 4.26310E+00 1.02654E+00 1.02654E+00 1.02654E+00 3.045000E+00 4.26310E+00 1.02654E+00	3	8.527000E-02				
1.307000E+00	4	5.363000E+00				
6 1.665000B+00	5	1.307000E+00				
7 6.758000E+01 3,918475E+06 3.011097E-01 0.00000DE+00 3.14097E-01 0.00000DE+00 3.011097E-01 1.018000E+00 1.028654E+07 5.201530E-01 3.04300BE+00 3.011097E-01 1.01800E+00 1.627367E+07 5.201530E-01 3.04300BE+00 4.26310BE+00 1.262900CE+01 1.01806CE+07 1.506051E+00 3.04300BE+00 4.26310BE+00 1.22512000E+01 1.01806CE+07 1.51805DE+00 3.04400CE+00 4.26310BE+00 1.22512000E+01 1.01806CE+07 1.51085DE+00 3.04000E+00 4.26310BE+00 1.22500E+01 1.310919E+07 3.059013E-01 9.92099E+01 1.246774E+00 3.059013E-01 9.92099E+01 1.246774E+00 3.059013E-01 9.92099E+01 1.246774E+00 3.059013E-01 9.92099E+01 1.246774E+00 3.059013E-01 9.92099E+01 1.258013E-01 9.92099E+01 1.258013E-01 9.92099E+01 1.258013E-01 9.92099E+01 1.25900E+01 1.257660E+07 8.439972E-01 2.12900E+00 2.58893E+01 0.00000E+00 1.58893E+01 1.257660E+07 8.439972E-01 2.12900E+00 2.58893E+00 1.257660E+07 8.439972E-01 2.12900E+00 1.58893E+00 0.00000E+00 1.58893E+00 0.00000E+00 1.58893E+00 0.00000E+00 1.2						
8 4.29000E+01	7					
9 4.501000E+00	8					
10 3.408000E+00 1 6.37367E+07 5.201012E-01 1 2.629000E-01 1 8.558381E+06 1 1.506551E+00 3.30400E+00 4.81051E+00 1 2.91100DE-01 1 0.18060E+07 1 5.506551E+00 3.30400E+00 4.81051E+00 1 2.91100DE-01 1 0.18060E+07 1 5.506551E+00 3.20400B+00 4.714851E+00 1 2.9100DE-01 1 3.01919E+07 3.05901B+01 1 3.92099E+01 1 3.01919E+07 3.05901B+01 1 3.92099E+01 1 3.00999E+01 3.00999E+01 3.00999E+01 3.00999E+01 3.00999E+01 3.00999E+01 3.009					· 	
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13 2 191000E-01 6.38645P=06 1.51082E=10 3.204000E+00 4.71485IP+00 1.51082E=10 3.20400E+01 1.524774E+00 0.00000E+00 1.544774E+00 0.00000E+00 1.544774E+00 1.524774E+00 0.00000E+00 1.544774E+00 0.00000E+00 3.304883E=01 1.52400E+01 1.52400E+01 1.310919E+06 3.305803E=01 0.000000E+00 3.300808E=01 1.52400E+01 1.52400E+01 1.55451E+06 3.305803E=01 0.000000E+00 3.300808E=01 1.55451E+06 3.305803E=01 0.000000E+00 3.306883E=01 0.000000E+00 3.280894E=01 1.55451E+06 3.280894E=01 0.000000E+00 3.30688E=01 0.000000E+00 3.280894E=01 1.55451E+06 3.280894E=01 0.000000E+00 3.30688E=01 0.000000E+00 3.280894E=01 1.55400E+01 9.1577660E+07 8.439972E=01 2.595000E+00 3.538997E+00 0.000000E+00 3.30688E=01 0.000000E+00 3.30688E=01 0.000000E+00 3.30680E=01 3.538997E+00 0.000000E+00 3.393750E=00 0.000000E+00 3.393750E=00 0.000000E+00 3.393750E=00 0.000000E+00 3.393750E=00 0.000000E+00 3.393750E=00 0.000000E+00 3.393750E=00 0.000000E+00 3.393750E=00 0.00000E+00 3.3						
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6.877000E-02

3.784000E+00

1.541000E-01

2.553392E+06

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8.345177E+06

1.489029E+07

9.316133E+06

1.079000E+00

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7.807999E-01

8.500999E-01

1.952000E+00

2.030356E+00

6.020899E-01

1.225604E+00

3.491716E+00

1.386064E+00

3.732258E+00

Information Only

				METORI.IDE, Z	Page 1
Vect	or TAUFAIL	PRESGAS0	VOL_C	VOL_S	7.70.T m
1	1.881000E+01	9.181916E+06	3.410087E-01	3.513000E+00	VOL_T
2	1.856000E-01	2.833049E+06	1.527955E+00		3.854008E+00
3	8.527000E-02	1.159213E+07		0.000000E+00	1.527955E+00
4	5.363000E+00		2.338110E+00	3.825000E+00	6.163110E+00
5	1.307000E+00	1.251198E+07	4.686572E-01	1.599000E+00	2.067657E+00
5		7.278415E+06	7.783863E-01	0.000000E+00	7.783863E-01
6	1.665000E+00	1.051156E+07	1.004044E+00	2.170000E+00	3.174044E+00
7	6.758000E+01	3.171819E+06	3.011097E-01	0.000000E+00	3.011097E-01
8	4.290000E+01	4.383452E+06	3.011097E-01	0.000000E+00	3.011097E-01
9	4.501000E+00	9.390775E+06	5.203530E-01	3.043000E+00	3.563353E+00
10	3.408000E+00	1.391770E+07	5.401012E-01	3.723000E+00	4.263101E+00
11	2.629000E-01	7.682560E+06	1.506051E+00	0.000000E+00	1.506051E+00
12	2.512000E-01	9.888308E+06	1.510852E+00	3.204000E+00	
13	2.191000E-01	6.173831E+06	1.544774E+00	0.000000E+00	4.714851E+00
14	2.677000E+01	1.153201E+07			1.544774E+00
15	2.879000E+01	7.460009E+06	3.059013E-01	9.920999E-01	1.298001E+00
16	3.997000E+01		3.504883E-01	0.000000E+00	3.504883E-01
17	3.024000E+01	4.688450E+06	3.300808E-01	0.000000E+00	3.300808E-01
		3.521227E+06	3.280894E-01	0.000000E+00	3.280894E-01
18	4.025000E+00	1.544172E+07	5.199128E-01	2.129000E+00	2.648913E+00
19	1.170000E+00	1.379737E+07	8.439972E-01	2.695000E+00	3.538997E+00
20	1.595000E+01	8.354388E+06	3.659891E-01	6.424999E-01	1.008489E+00
21	5.307000E-02	5.292574E+06	3.937950E+00	0.000000E+00	3.937950E+00
22	4.204000E-01	3.551260E+06	1.242349E+00	0.000000E+00	1.242349E+00
23	1.067000E+01	1.292133E+07	4.607563E-01	2.743000E+00	3.203756E+00
24	1.471000E+01	5.831318E+06	3.906219E-01	0.000000E+00	
25	1.159000E-01	1.325589E+07	2.291612E+00	5.713000E-01	3.906219E-01
26	2.891000E+00	6.636365E+06	6.177633E-01		2.862912E+00
27	7.333000E+01	9.317105E+06		0.000000E+00	6.177633E-01
28	5.119000E-01	6.650263E+06	3.011097E-01	3.300000E+00	3.601110E+00
29	7.923000E-01		1.091107E+00	0.000000E+00	1.091107E+00
-20	1.227000E+01	6.764035E+06	2.397515E+00	0.000000E+00	2.397515E+00
		1.966041E+06	3.947803E-01	0.000000E+00	3.947803E-01
	5.314000E-01	7.413066E+06	9.645854E-01	0.00000E+00	9.645854E-01
32	1.966000E+01	6.246676E+06	3.492019E-01	0.000000E+00	3.492019E-01
33	1.291000E+01	4.320345E+06	3.902639E-01	0.000000E+00	3.902639E-01
34	3.983000E-01	4.962924E+06	1.376624E+00	0.000000E+00	1.376624E+00
35	1.402000E+01	3.049466E+06	4.537664E-01	0.00000E+00	4.537664E-01
36	5.004000E+00	5.798375E+06	5.526043E-01	0.000000E+00	5.526043E-01
37	7.433000E-01	8.835626E+06	9.596525E-01	2.282000E+00	3.241652E+00
38	9.944000E-02	1.237712E+07	2.164160E+00	2.046000E+00	4.210160E+00
39	1.989000E-01	2.622305E+06	1.750881E+00	0.000000E+00	1.750881E+00
40	4.705000E+01	1.693863E+06	3.011097E-01	0.000000E+00	
41	6.327000E+01	1.203676E+07	3.011097E-01		3.011097E-01
42	1.707000E+01	1.218296E+07	3.234804E-01	3.121000E+00	3.422110E+00
43	3.711000E+01	7.383605E+06		3.424000E+00	3.747480E+00
$\frac{13}{44}$	1.734000E+00	9.357676E+06	3.198346E-01	0.000000E+00	3.198346E-01
45	5.943000E+00	1.359956E+07	6.452036E-01	2.457000E+00	3.102204E+00
46	3.466000E-01		4.657365E-01	1.471000E+00	1.936736E+00
47	5.680000E-01	8.405049E+06	1.382688E+00	3.623000E+00	5.005688E+00
48		1.161298E+07	4.817018E-01	2.193000E+00	2.674702E+00
	5.527000E-02	1.116739E+07	3.384981E+00	6.075999E~01	3.992581E+00
49	3.108000E-01	4.794402E+06	1.379820E+00	0.00000E+00	1.379820E+00
50	1.047000E-01	6.914397E+06	2.011564E+00	0.000000E+00	2.011564E+00
51	6.825000E-01	5.986023E+06	1.228051E+00	0.000000E+00	1.228051E+00
52	7.967000E+00	4.354629E+06	5.047065E-01	0.000000E+00	5.047065E-01
53	8.730000E-01	7.044989E+06	9.183298E-01	0.000000E+00	9.183298E-01
54	9.179000E-02	6.885277E+06	2.305037E+00	0.000000E+00	2.305037E+00
55	1.832000E+00	6.410676E+06	8.002669E-01	0.000000E+00	8.002669E-01
	5.001000E+01	8.138215E+06	3.011097E-01	9.730999E-01	
	9.015000E+00	6.574536E+06	4.179258E-01	0.000000E+00	1.274210E+00
58	1.508000E+00	1.193428E+07	9.178399E-01		4.179258E-01
59	7.061000E+00	1.251928E+07	4.990718E-01	2.293000E+00	3.210840E+00
60	2.222000E+00	6.986306E+06		2.843000E+00	3.342072E+00
61	1.043000E+01	2.944606E+06	6.345150E-01	0.000000E+00	6.345150E-01
62	4.675000E+01	2.944606E+06 1.254759E+07	3.987798E-01	0.000000E+00	3.987798E-01
63	1.005000E=01		1.201360E+00	3.502000E+00	4.703360E+00
55	T.000000E+00	2.235494E+06	1.004293E+00	0.00000E+00	1.004293E+00
				\sim	

0.00000E+00

1.780258E+00

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1.541000E-01

7.853370E+06

Information Only

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Vect	or TAUFAIL	PRESGAS0	VOL_C	TOT C	1101
1	1.881000E+01	7.364022E+06		VOL_S	_ VOL_T
2			3.410087E-01	0.000000E+00	3.410087E-01
	1.856000E-01	2.526431E+06	1.527955E+00	0.000000E+00	1.527955E+00
3	8.527000E-02	1.150084E+07	2.338110E+00	3.825000E+00	6.163110E+00
4	5.363000E+00	1.249490E+07	4.686572E-01	1.599000E+00	2.067657E+00
5	1.307000E+00	6.531023E+06			
6	1.665000E+00		7.783863E-01	0.00000E+00	7.783863E-01
7		6.996461E+06	1.004044E+00	0.00000E+00	1.004044E+00
	6.758000E+01	3.168365E+06	3.011097E-01	0.000000E+00	3.011097E-01
8	4.290000E+01	4.248073E+06	3.011097E-01	0.000000E+00	3.011097E-01
9	4.501000E+00	7.437265E+06	5.203530E-01	0.000000E+00	·
10	3.408000E+00	7.483395E+06	5.401012E-01		5.203530E-01
$\overline{11}$	2.629000E-01			0.000000E+00	5.401012E-01
12		7.704410E+06	1.506051E+00	0.00000E+00	1.506051E+00
	2.512000E-01	9.561047E+06	1.510852E+00	3.204000E+00	4.714851E+00
13	2.191000E-01	1.708907E+06	1.544774E+00	0.000000E+00	1.544774E+00
14	2.677000E+01	7.669393E+06	3.059013E-01	0.000000E+00	3.059013E-01
15	2.879000E+01	5.550863E+06	3.504883E-01		
16	3.997000E+01	3.424555E+06		0.000000E+00	3.504883E-01
17			3.300808E-01	0.00000E+00	3.300808E-01
	3.024000E+01	1.170526E+06	3.280894E-01	0.000000E+00	3.280894E-01
18	4.025000E+00	7.205866E+06	5.199128E-01	0.000000E+00	5.199128E-01
19	1.170000E+00	1.312598E+07	8.439972E-01	2.695000E+00	3.538997E+00
20	1.595000E+01	7.397721E+06	3.659891E-01		
21	5.307000E-02	1.779050E+06		0.000000E+00	3.659891E-01
22	4.204000E-01		3.937950E+00	0.000000E+00	3.937950E+00
		3.427146E+06	1.242349E+00	0.000000E+00	1.242349E+00
23	1.067000E+01	9.274472É+06	4.607563E-01	2.743000E+00	3.203756E+00
24	1.471000E+01	5.052162E+06	3.906219E-01	0.000000E+00	3.906219E-01
25	1.159000E-01	1.328498E+07	2.291612E+00	5.713000E-01	2.862912E+00
26	2.891000E+00	6.337056E+06	6.177633E-01	0.000000E+00	
27	7.333000E+01	7.415667E+06			6.177633E-01
28	5.119000E-01	6.323043E+06	3.011097E-01	0.000000E+00	3.011097E-01
29			1.091107E+00	0.00000E+00	1.091107E+00
	7.923000E-02	6.367837E+06	2.397515E+00	0.000000E+00	2.397515E+00
	1.227000E+01	1.218354E+06	3.947803E-01	0.000000E+00	3.947803E-01
	5.314000E-01	7.951466E+06	9.645854E-01	0.000000E+00	9.645854E-01
32	1.966000E+01	1.440322E+06	3.492019E-01	0.000000E+00	3.492019E-01
33	1.291000E+01	1.361270E+06	3.902639E-01	0.000000E+00	
34	3.983000E-01	1.936708E+06			3.902639E-01
35	1.402000E+01		1.376624E+00	0.000000E+00	1.376624E+00
36	5.004000E+00	2.406716E+06	4.537664E-01	0.000000E+00	4.537664E-01
		5.694559E+06	5.526043E-01	0.000000E+00	5.526043E-01
37	7.433000E-01	8.473705E+06	9.596525E-01	2.282000E+00	3.241652E+00
38	9.944000E-02	1.237620E+07	2.164160E+00	2.046000E+00	4.210160E+00
39	1.989000E-01	1.397828E+06	1.750881E+00	0.000000E+00	1.750881E+00
40	4.705000E+01	1.365788E+06	3.011097E-01	0.000000E+00	
41	6.327000E+01	9.723825E+06			3.011097E-01
42	1.707000E+01		3.011097E-01	3.121000E+00	3.422110E+00
43		1.221530E+07	3.234804E-01	3.424000E+00	3.747480E+00
	3.711000E+01	1.410218E+06	3.198346E-01	0.000000E+00	3.198346E-01
44	1.734000E+00	8.256639E+06	6.452036E-01	2.457000E+00	3.102204E+00
45	5.943000E+00	4.925884E+06	4.657365E-01	0.000000E+00	4.657365E-01
46	3.466000E-01	7.719559E+06	1.382688E+00	0.000000E+00	1.382688E+00
47	5.680000E+00	9.649041E+06	4.817018E-01		
48	5.527000E-02	7.835438E+06		2.193000E+00	2.674702E+00
49	3.108000E-01		3.384981E+00	0.000000E+00	3.384981E+00
		1.582511E+06	1.379820E+00	0.000000E+00	1.379820E+00
50	1.047000E-01	2.583637E+06	2.011564E+00	0.000000E+00	2.011564E+00
51	6.825000E-01	1.110775E+06	1.228051E+00	0.000000E+00	1.228051E+00
52	7.967000E+00	2.612925E+06	5.047065E-01	0.000000E+00	5.047065E-01
53	8.730000E-01	6.449974E+06	9.183298E-01	0.000000E+00	
54	9.179000E-02	6.363511E+06			9.183298E-01
55	1.832000E+00	6.157295E+06	2.305037E+00	0.000000E+00	2.305037E+00
	5.001000E+01		8.002669E-01	0.000000E+00	8.002669E-01
		8.041371E+06	3.011097E-01	9.730999E-01	1.274210E+00
	9.015000E+00	6.349460E+06	4.179258E-01	0.000000E+00	4.179258E-01
58	1.508000E+00	1.391216E+07	9.178399E-01	2.293000E+00	3.210840E+00
59	7.061000E+00	1.254465E+07	4.990718E-01	2.843000E+00	3.342072E+00
60	2.222000E+00	5.321256E+06	6.345150E-01	0.000000E+00	6.345150E-01
61	1.043000E+01	2.965174E+06	3.987798E-01		
62	4.675000E-01	1.277453E+07		0.000000E+00	3.987798E-01
63	1.005000E+00	1.771434E+06	1.201360E+00	3.502000E+00	4.703360E+00
J.J	-・000000100	エ・ノノナ4つ年11十月日	1.004293E+00	0.00000E+00	1.004293E+00

0.000000E+00

1.780258E+00

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1.541000E-01

5.936306E+06

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Vect	or TAUFAIL	PRESGAS0	NOT C	770T G	
1	1.881000E+01	7.373383E+06	VOL_C	VOL_S	_ VOL_T
2			3.410087E-01	0.000000E+00	3.410087E-01
	1.856000E-01	2.535215E+06	1.527955E+00	0.000000E+00	1.527955E+00
3	8.527000E-02	1.159446E+07	2.338110E+00	3.825000E+00	6.163110E+00
-4	5.363000E+00	1.251483E+07	4.686572E-01	1.599000E+00	2.067657E+00
5	1.307000E+00	6.531374E+06	7.783863E-01	0.000000E+00	7.783863E-01
6	1.665000E+00	6.994745E+06	1.004044E+00		
7	6.758000E+01	3.144333E+06		0.000000E+00	1.004044E+00
8	4.290000E+01		3.011097E-01	0.000000E+00	3.011097E-01
		4.321098E+06	3.011097E-01	0.00000E+00	3.011097E-01
9	4.501000E+00	7.457330E+06	5.203530E-01	0.000000E+00	5.203530E-01
10	3.408000 E +00	7.478015E+06	5.401012E-01	0.000000E+00	5.401012E-01
11	2.629000E-01	7.698039E+06	1.506051E+00	0.000000E+00	1.506051E+00
12	2.512000E-01	9.548139E+06	1.510852E+00	3.204000E+00	
13	2.191000E-01	1.708567E+06	1.544774E+00		4.714851E+00
14	2.677000E+01	7.645779E+06		0.000000E+00	1.544774E+00
15	2.879000E+01		3.059013E-01	0.000000E+00	3.059013E-01
		5.520873E+06	3.504883E-01	0.000000E+00	3.504883E-01
16	3.997000E+01	3.444735E+06	3.300808E-01	0.000000E+00	3.300808E-01
17	3.024000E+01	1.395969E+06	3.280894E-01	0.000000E+00	3.280894E-01
18	4.025000E+00	7.183680E+06	5.199128E-01	0.000000E+00	5.199128E-01
19	1.170000E+00	1.307667E+07	8.439972E-01	2.695000E+00	
20	1.595000E+01	7.405975E+06			3.538997E+00
21	5.307000E-01		3.659891E-01	0.000000E+00	3.659891E-01
22	· · · - · -	1.754674E+06	3.937950E+00	0.000000E+00	3.937950E+00
	4.204000E-01	3.394991E+06	1.242349E+00	0.000000E+00	1.242349E+00
23	1.067000E+01	9.271284E+06	4.607563E-01	2.743000E+00	3.203756E+00
24	1.471000E+01	5.049310E+06	3.906219E-01	0.000000E+00	3.906219E-01
25	1.159000E-01	1.325597E+07	2.291612E+00	5.713000E-01	2.862912E+00
26	2.891000E+00	6.190234E+06	6.177633E-01	0.000000E+00	
27	7.333000E+01	7.392509E+06			6.177633E-01
28	5.119000E-01		3.011097E-01	0.000000E+00	3.011097E-01
29		6.324246E+06	1.091107E+00	0.000000E+00	1.091107E+00
29	7.923000E-02	6.351389E+06	2.397515E+00	0.000000E+00	2.397515E+00
	1.227000E+01	1.213401E+06	3.947803E-01	0.000000E+00	3.947803E-01
	5.314000E-01	7.896204E+06	9.645854E-01	0.000000E+00	9.645854E-01
32	1.966000E+01	1.388802E+06	3.492019E-01	0.000000E+00	3.492019E-01
33	1.291000E+01	1.351480E+06	3.902639E-01	0.000000E+00	
34	3.983000E-01	1.960507E+06			3.902639E-01
35	1.402000E+01		1.376624E+00	0.000000E+00	1.376624E+00
36	5.004000E+00	2.407676E+06	4.537664E-01	0.000000E+00	4.537664E-01
		5.783576E+06	5.526043E~01	0.000000E+00	5.526043E-01
37	7.433000E-01	8.487429E+06	9.596525E-01	2.282000E+00	3.241652E+00
38	9.944000E-02	1.239152E+07	2.164160E+00	2.046000E+00	4.210160E+00
39	1.989000E-01	1.399488E+06	1.750881E+00	0.000000E+00	1.750881E+00
40	4.705000E+01	1.343836E+06	3.011097E-01	0.000000E+00	3.011097E-01
41	6.327000E+01	9.722180E+06	3.011097E-01	3.121000E+00	
42	1.707000E+01	1.209046E+07			3.422110E+00
43	3.711000E+01		3.234804E-01	3.424000E+00	3.747480E+00
$\frac{44}{44}$		1.365489E+06	3.198346E-01	0.000000E+00	3.198346E-01
	1.734000E+00	8.170832E+06	6.452036E-01	2.457000E+00	3.102204E+00
45	5.943000E+00	4.894963E+06	4.657365E-01	0.000000E+00	4.657365E-01
46	3.466000E-01	7.747220E+06	1.382688E+00	0.000000E+00	1.382688E+00
47	5.680000E+00	9.659723E+06	4.817018E-01	2.193000E+00	2.674702E+00
48	5.527000E-02	7.804548E+06	3.384981E+00	0.000000E+00	3.384981E+00
49	3.108000E-01	1.470191E+06	1.379820E+00		
50	1.047000E-01	2.390125E+06		0.000000E+00	1.379820E+00
51	6.825000E-01		2.011564E+00	0.000000E+00	2.011564E+00
		1.312145E+06	1.228051E+00	0.000000E+00	1.228051E+00
52	7.967000E+00	2.588183E+06	5.047065E-01	0.000000E+00	5.047065E-01
53	8.730000E-01	6.487796E+06	9.183298E-01	0.000000E+00	9.183298E-01
54	9.179000E-02	6.363378E+06	2.305037E+00	0.000000E+00	2.305037E+00
55	1.832000E+00	6.164639E+06	8.002669E-01	0.000000E+00	8.002669E-01
	5.001000E+01	8.053402E+06	3.011097E-01	9.730999E-01	
	9.015000E+00	6.348591E+06	4.179258E-01		1.274210E+00
58	1.508000E+00	1.410361E+07		0.000000E+00	4.179258E-01
59	7.061000E+00		9.178399E-01	2.293000E+00	3.210840E+00
60		1.252872E+07	4.990718E-01	2.843000E+00	3.342072E+00
	2.222000E+00	4.906160E+06	6.345150E-01	0.000000E+00	6.345150E-01
61	1.043000E+01	2.867572E+06	3.987798E-01	0.000000E+00	3.987798E-01
62	4.675000E-01	1.254951E+07	1 201360E+00	3.502000E+00	4.703360E+00
63	1.005000E+00	1.757106E+06	1.004293E+00	0.00000E+00	1.004293E+00
				5.550050E+00	エ・ロロセムタンピキロロ

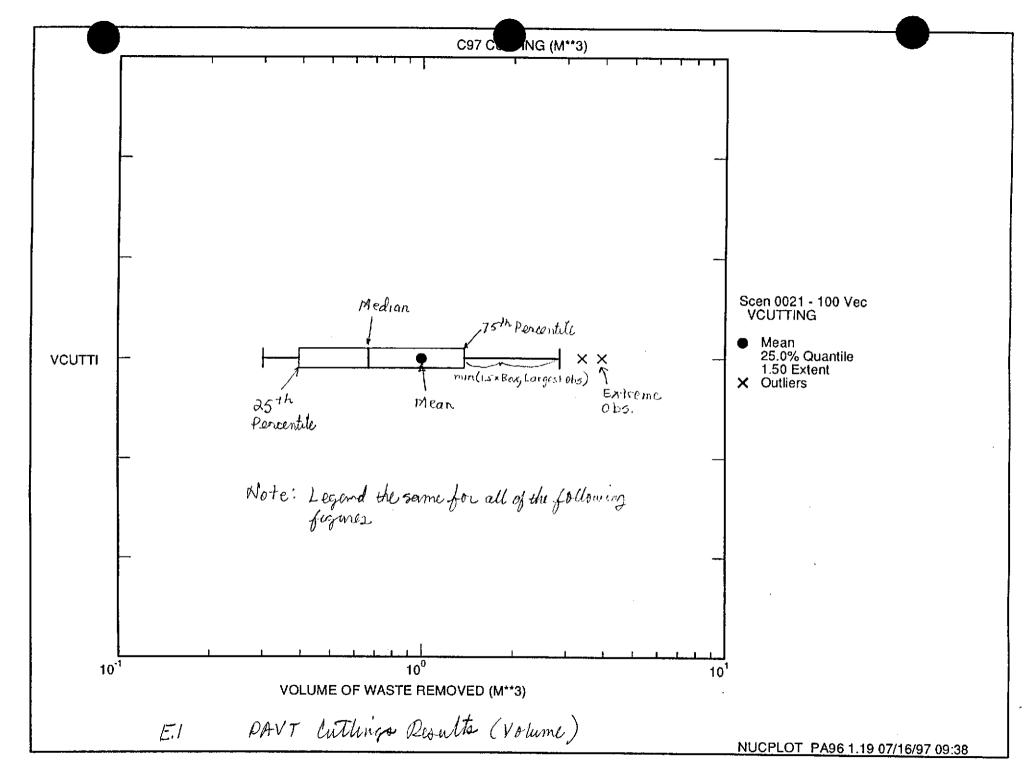
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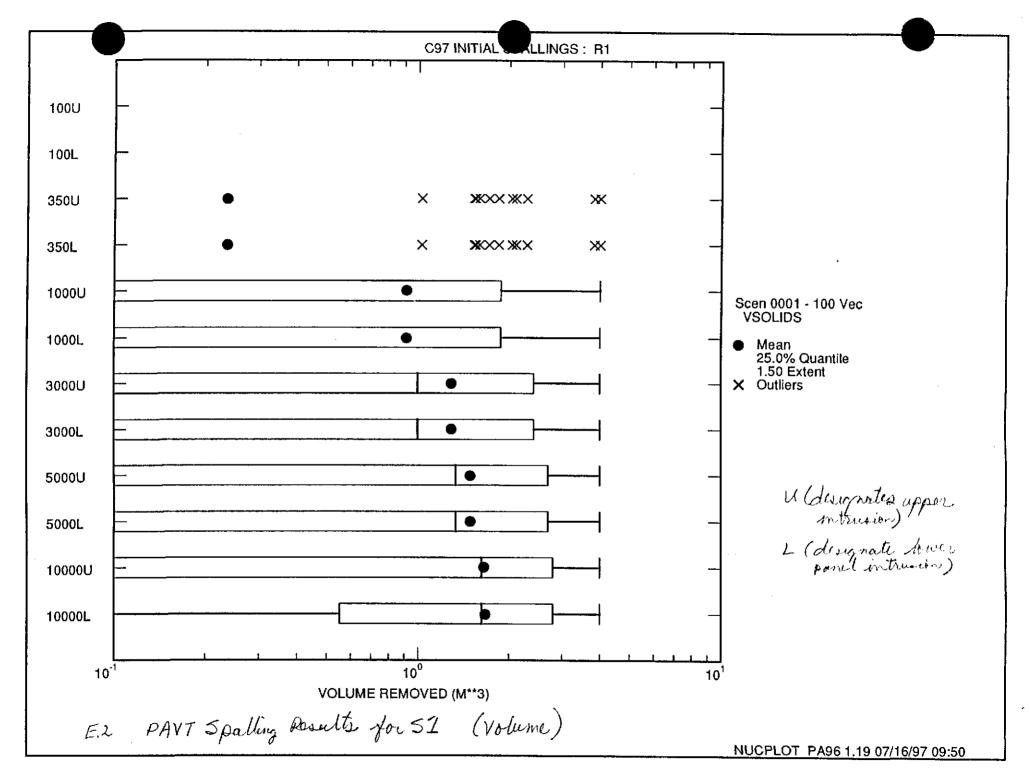
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1.541000E-01

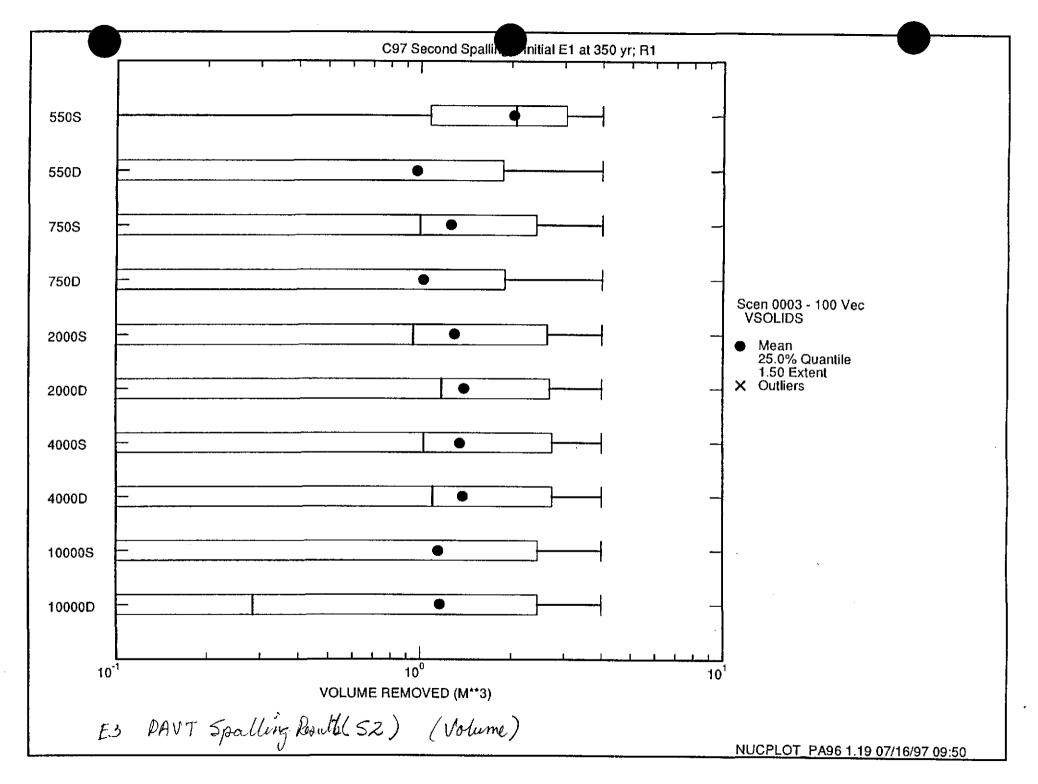
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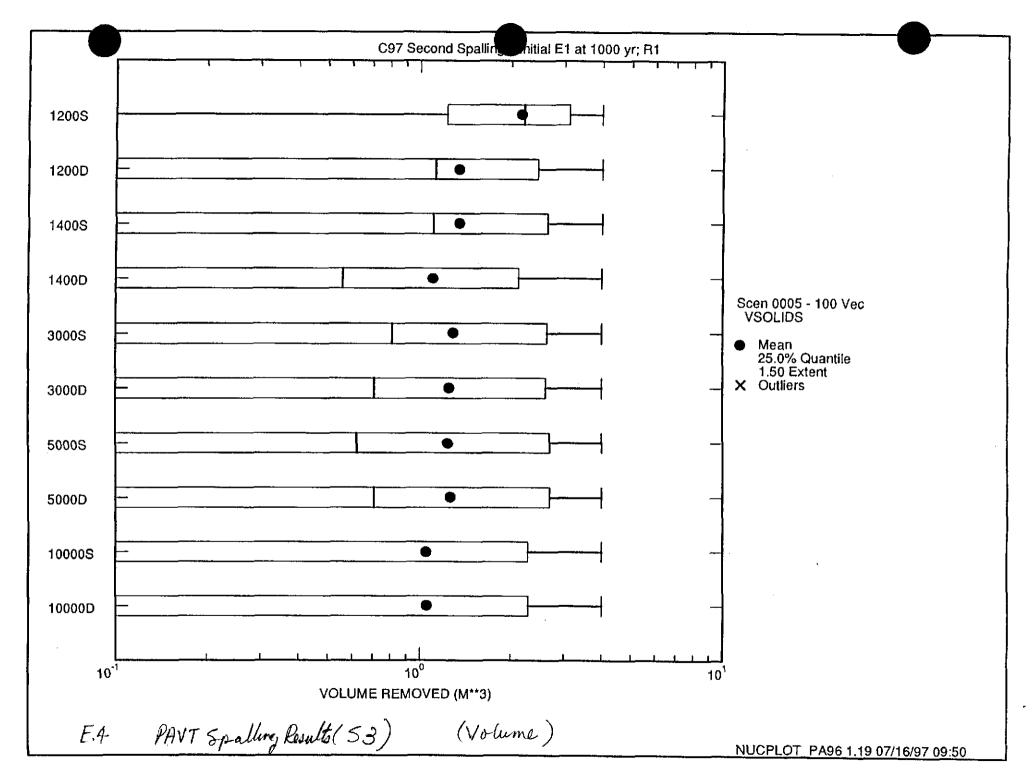
Information Only



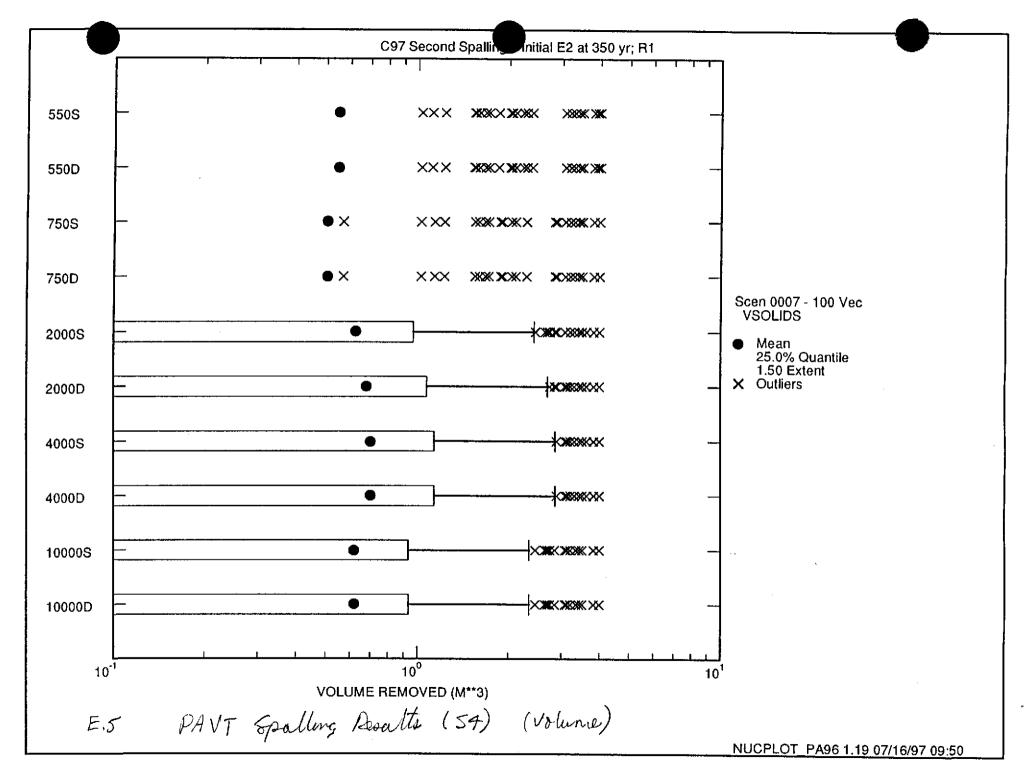
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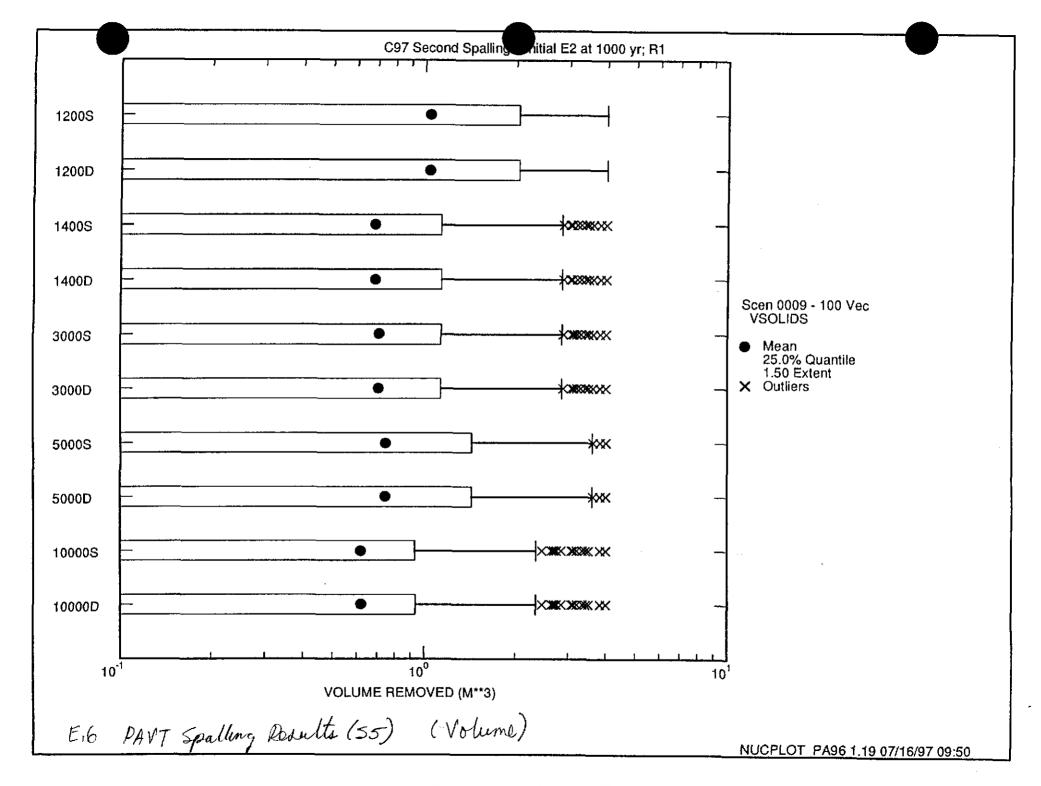
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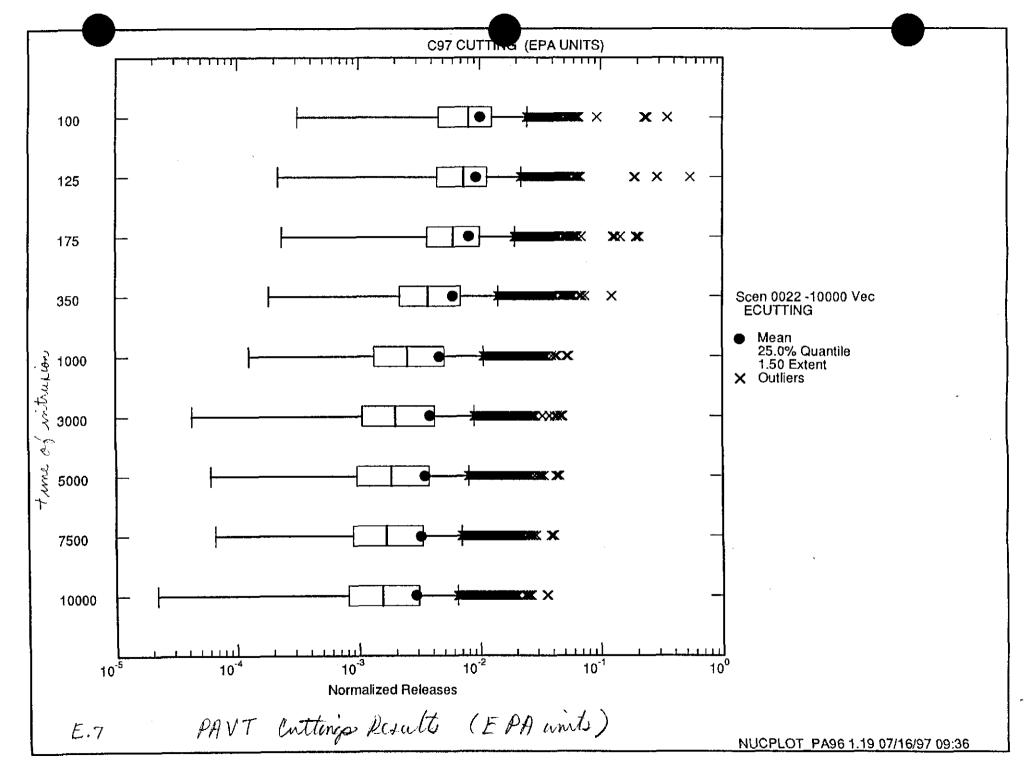
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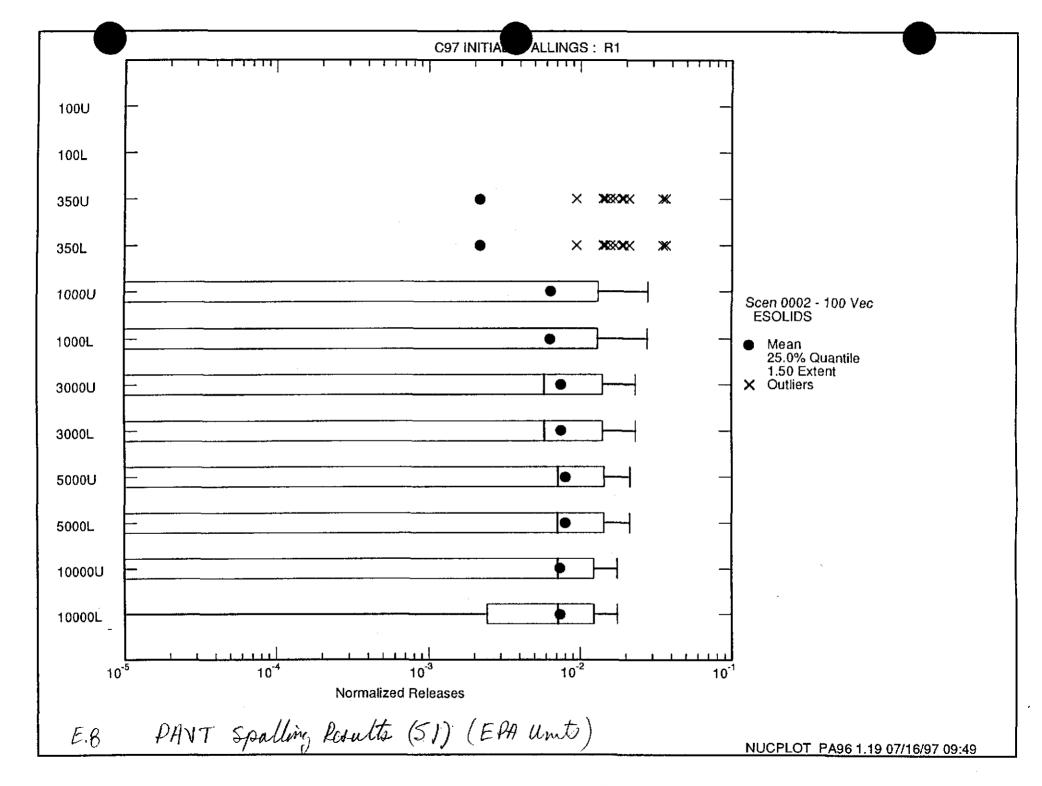
Information Only



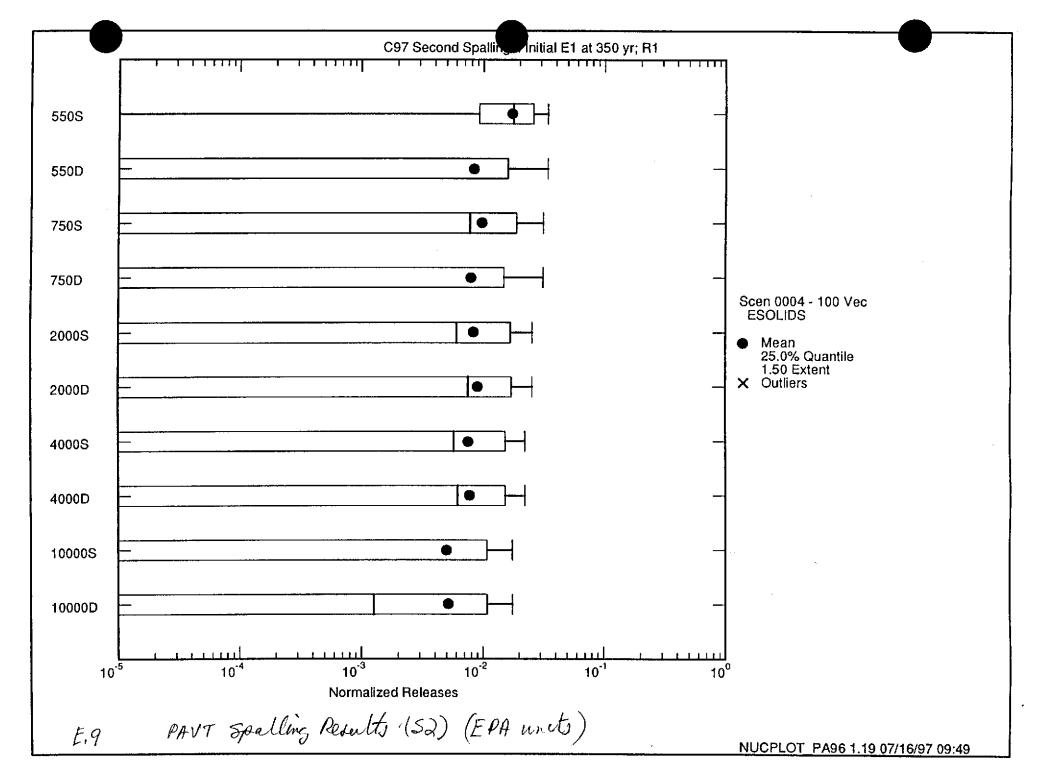
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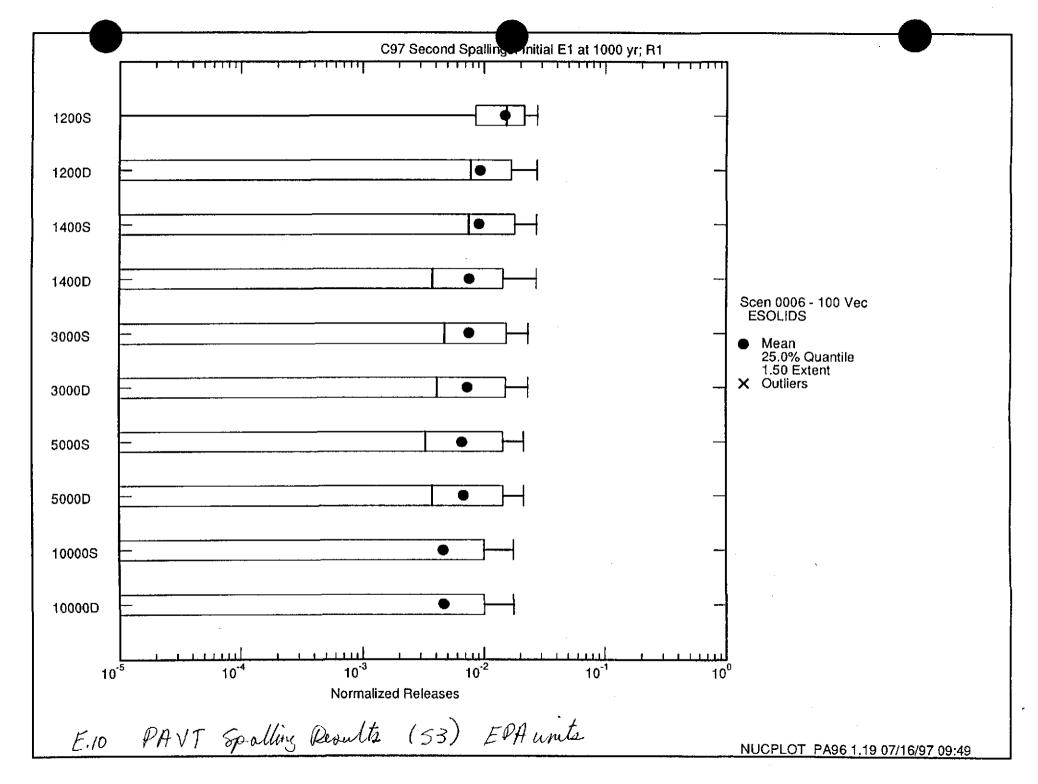
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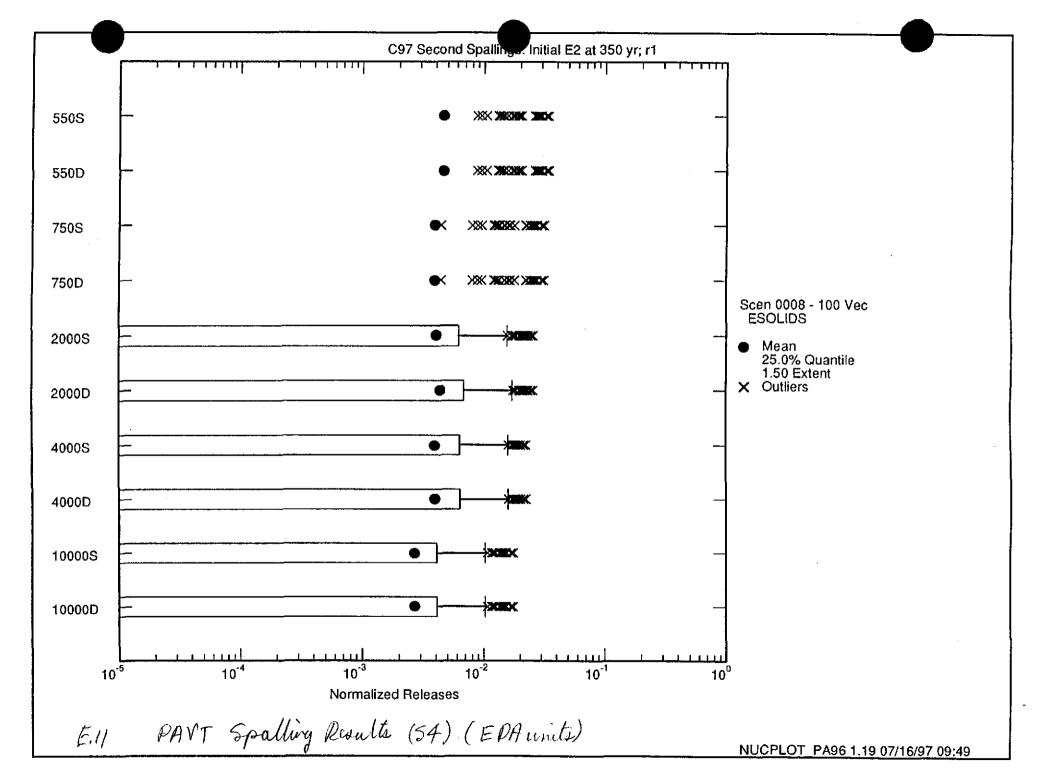
Information Only



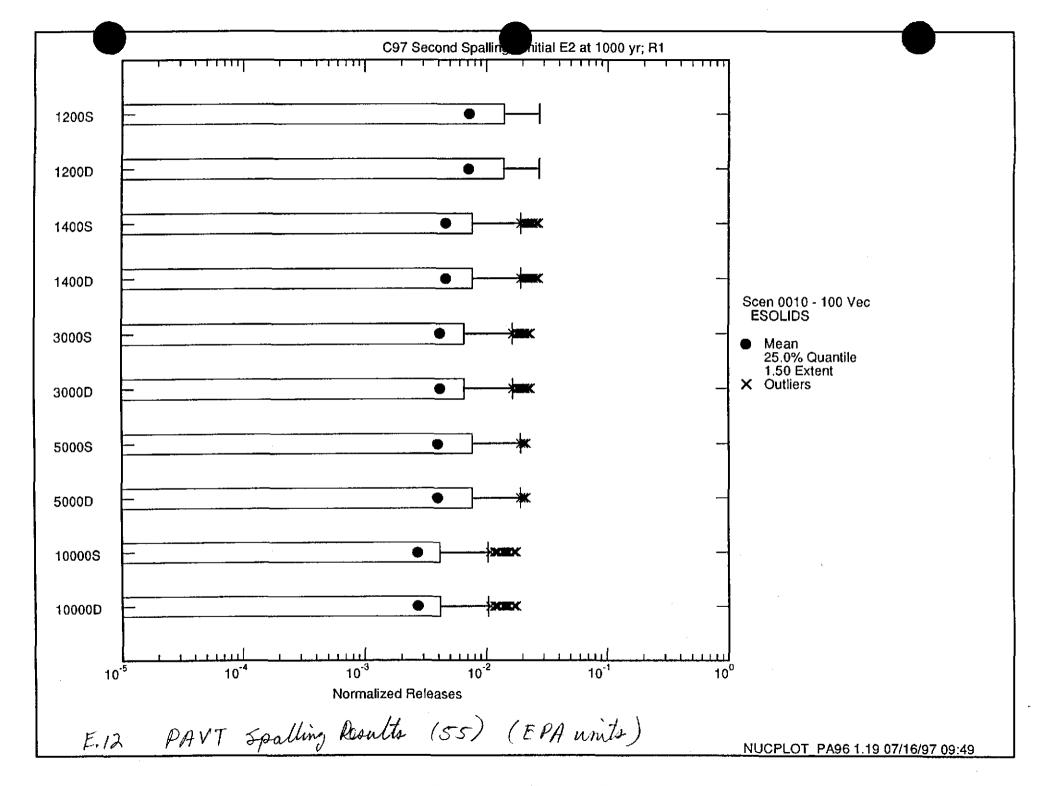
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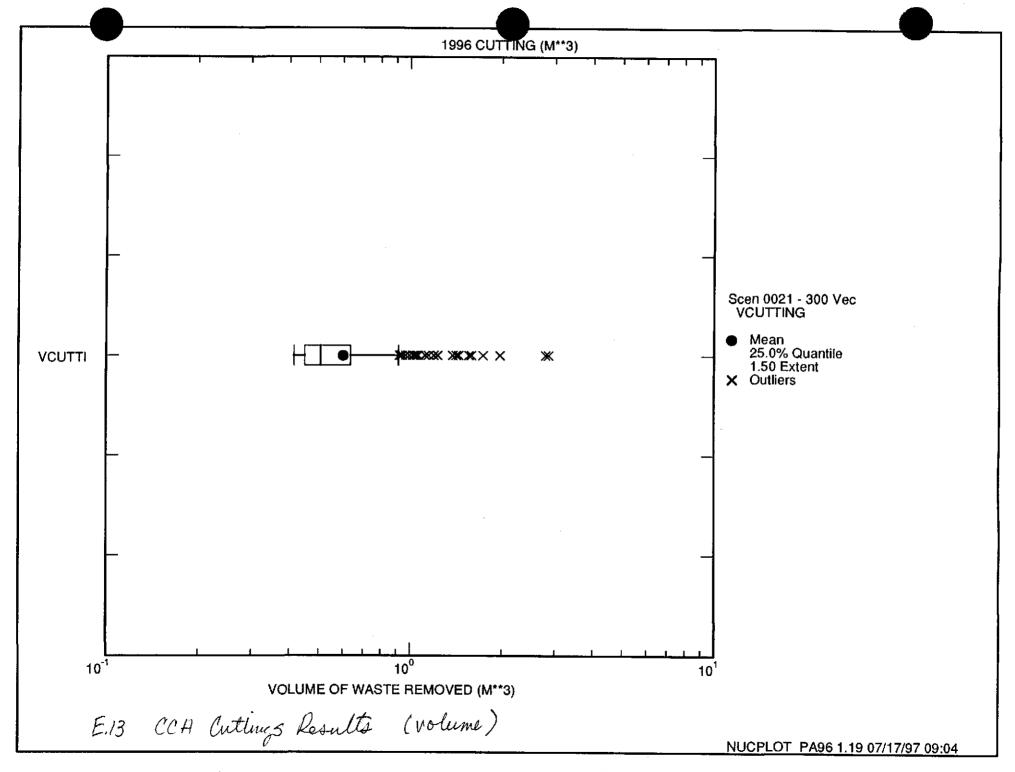
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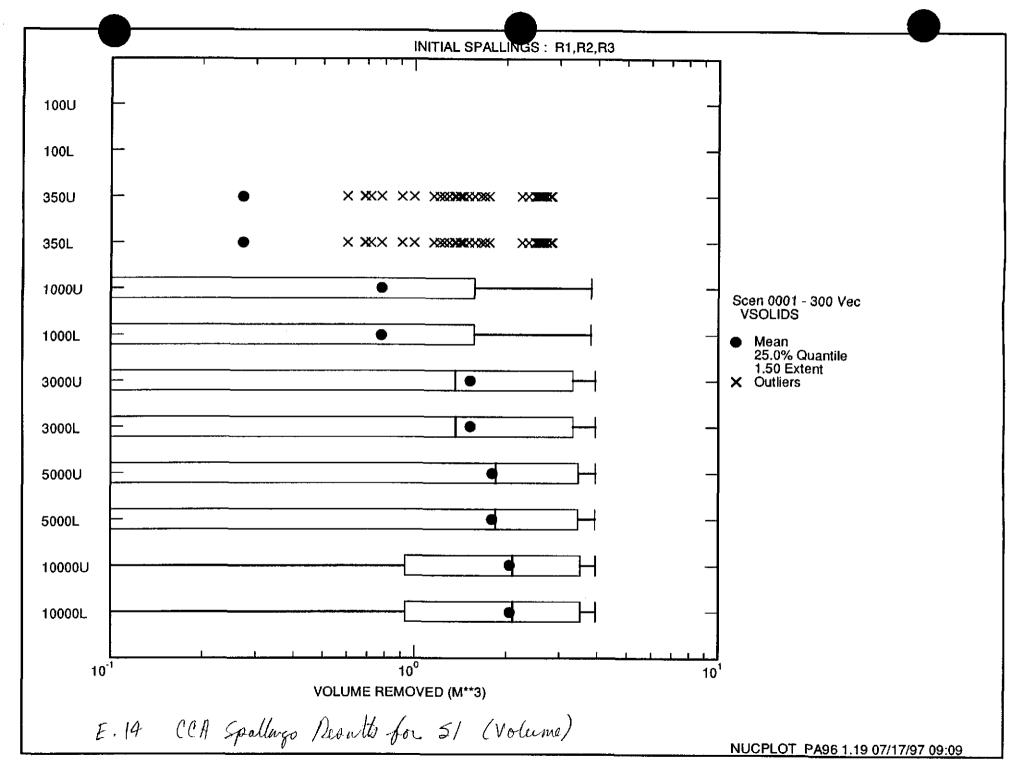
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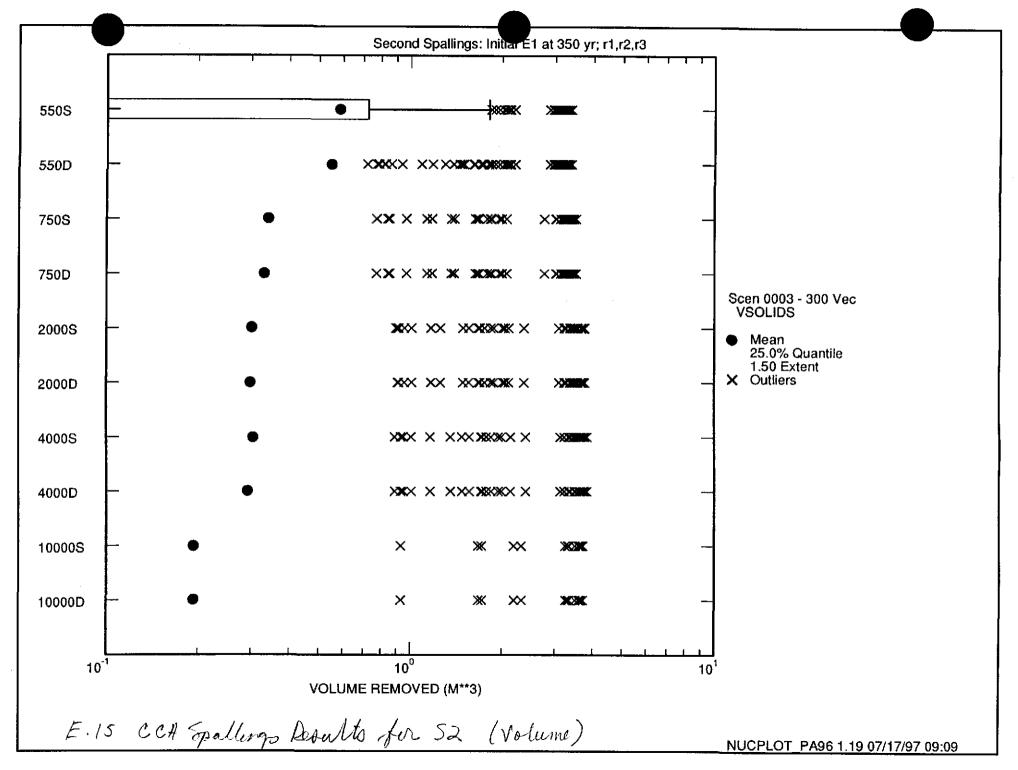
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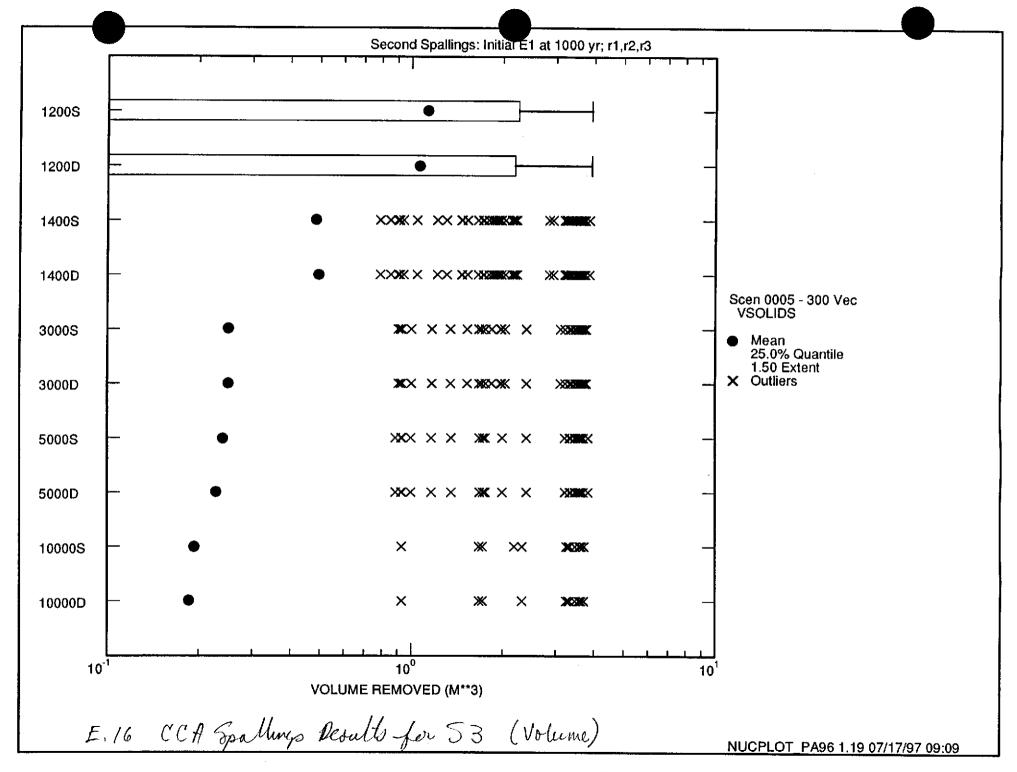
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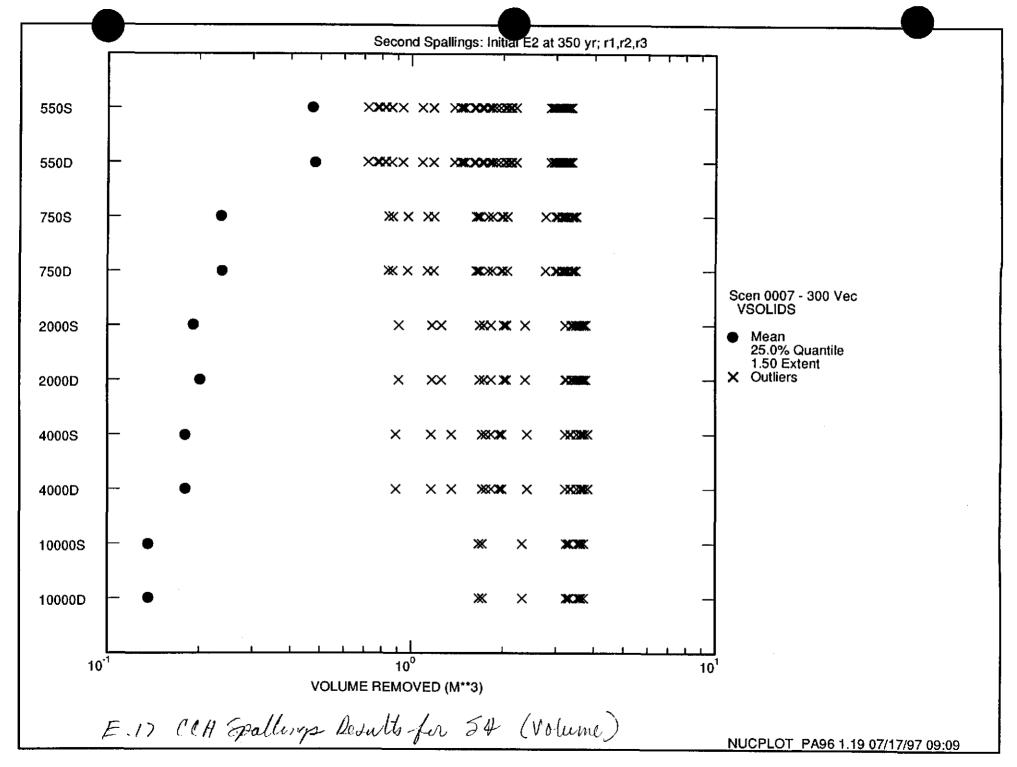
Information Only



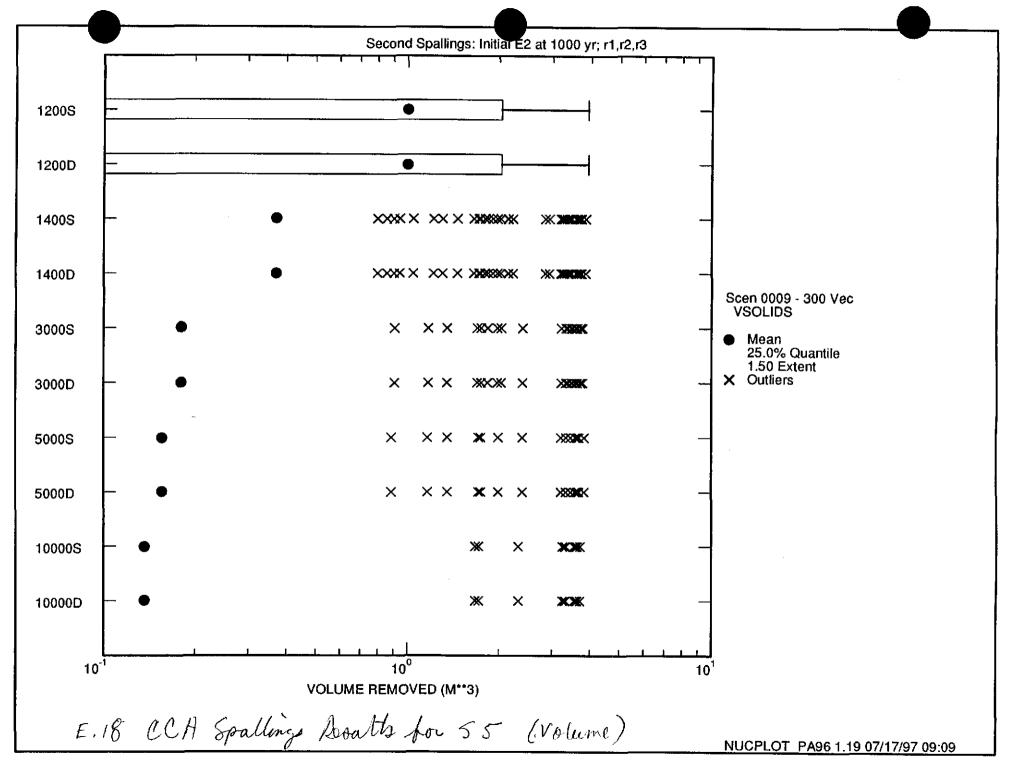
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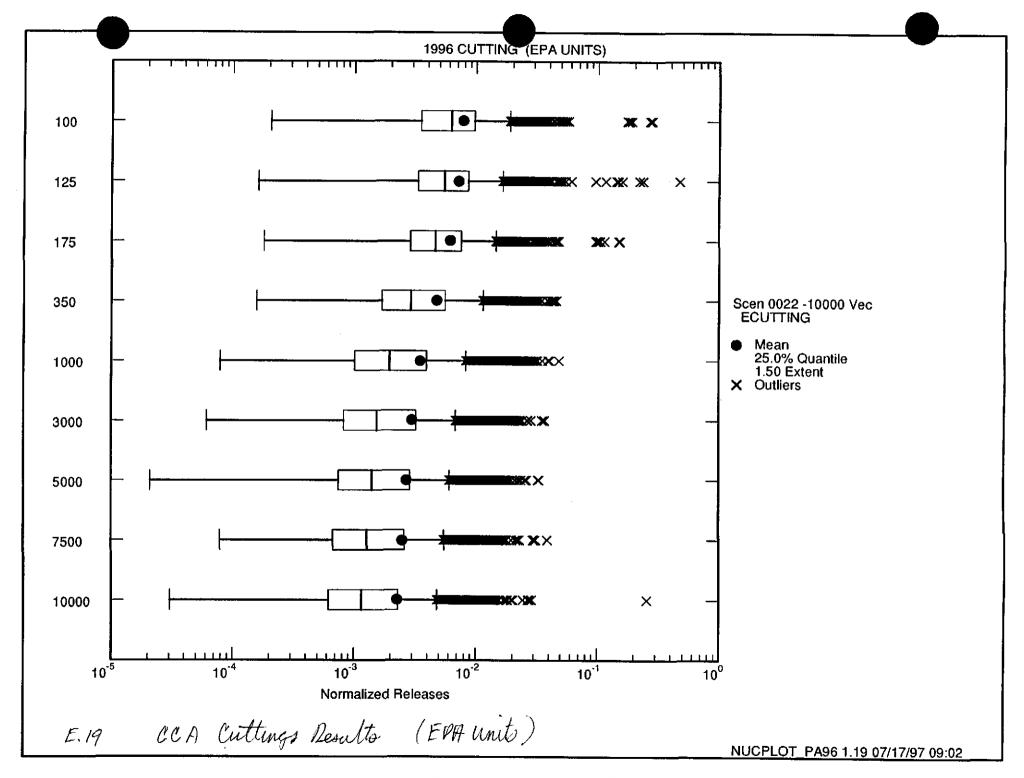
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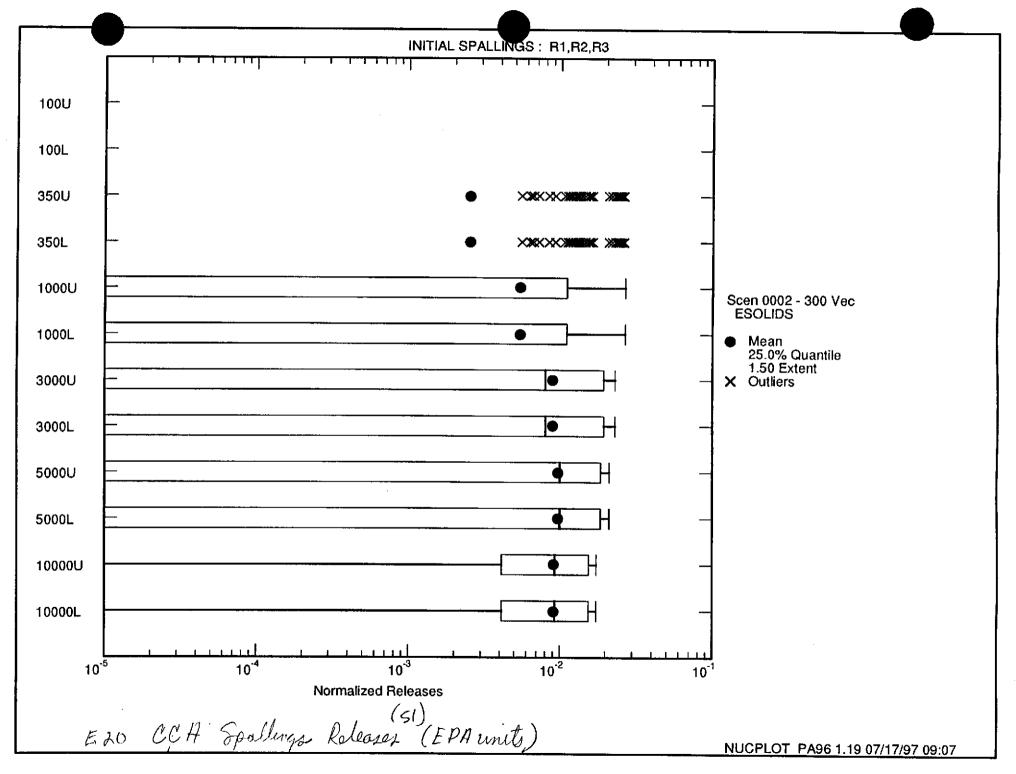
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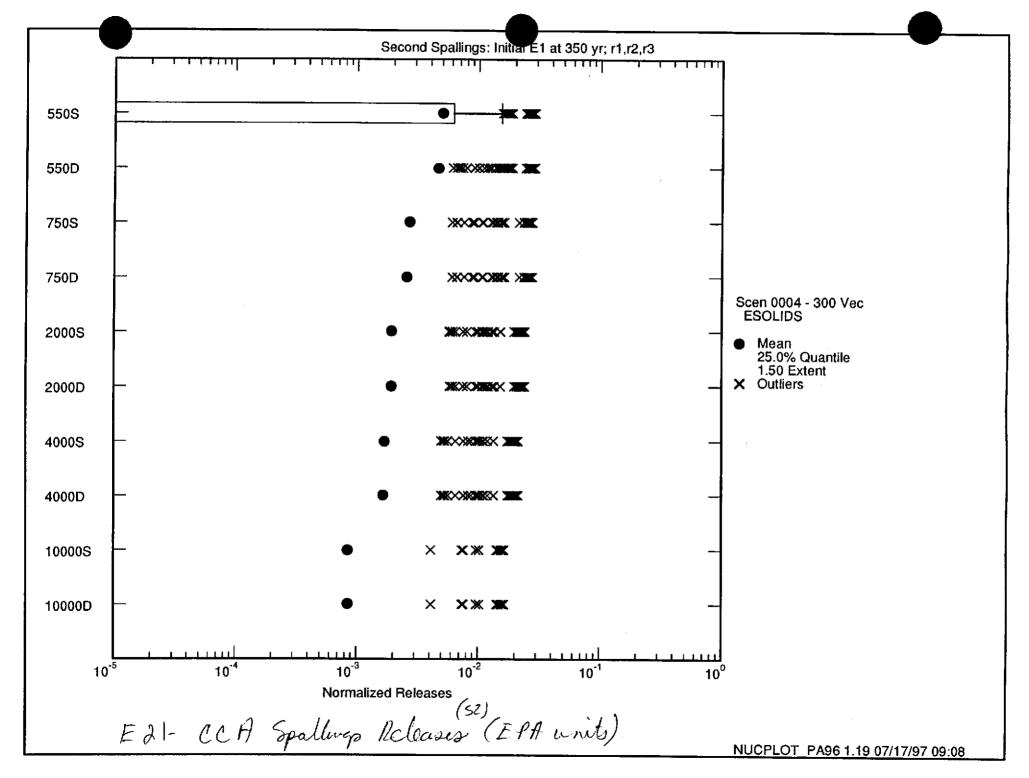
Information Only



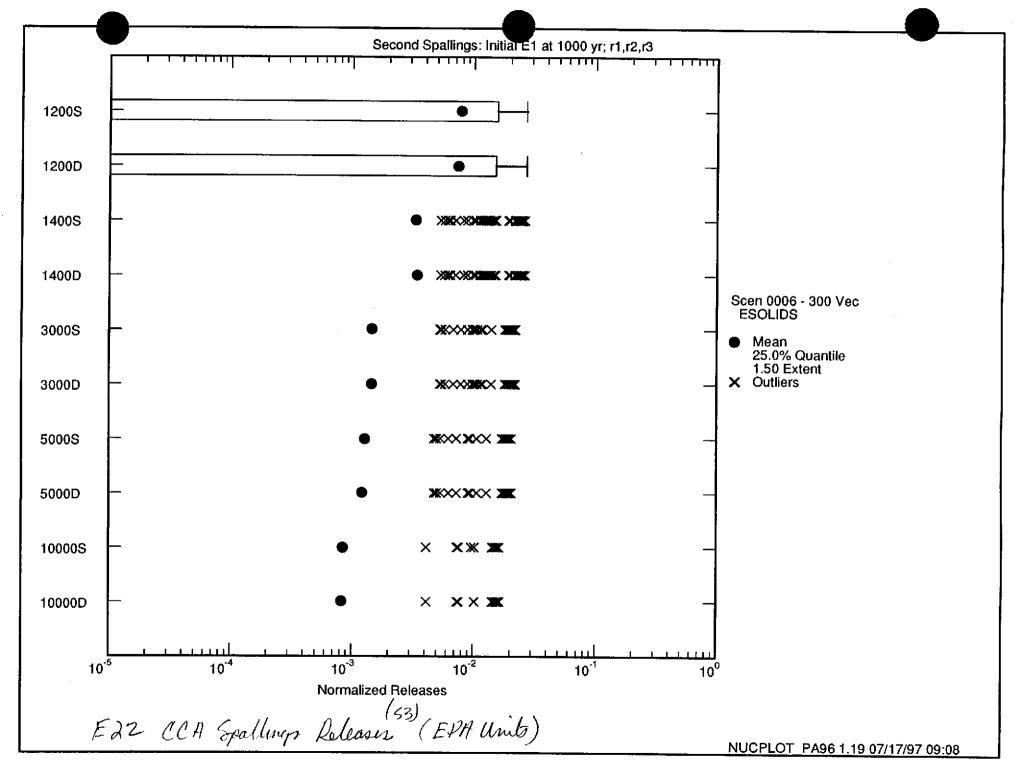
Information Only



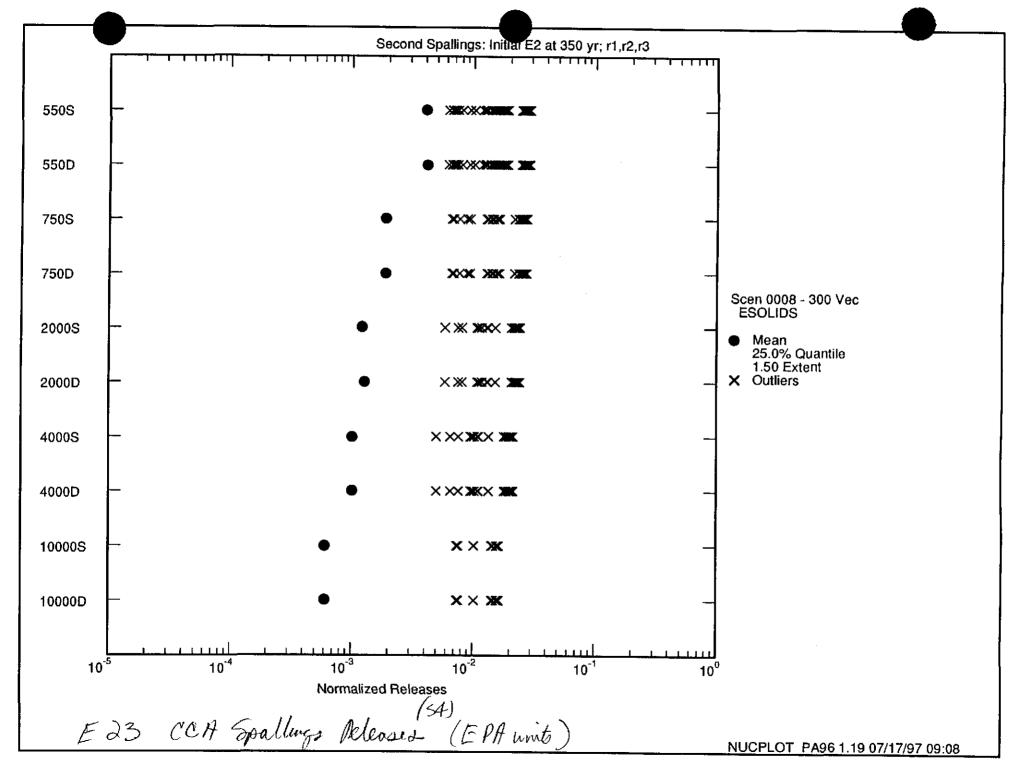
Information Only



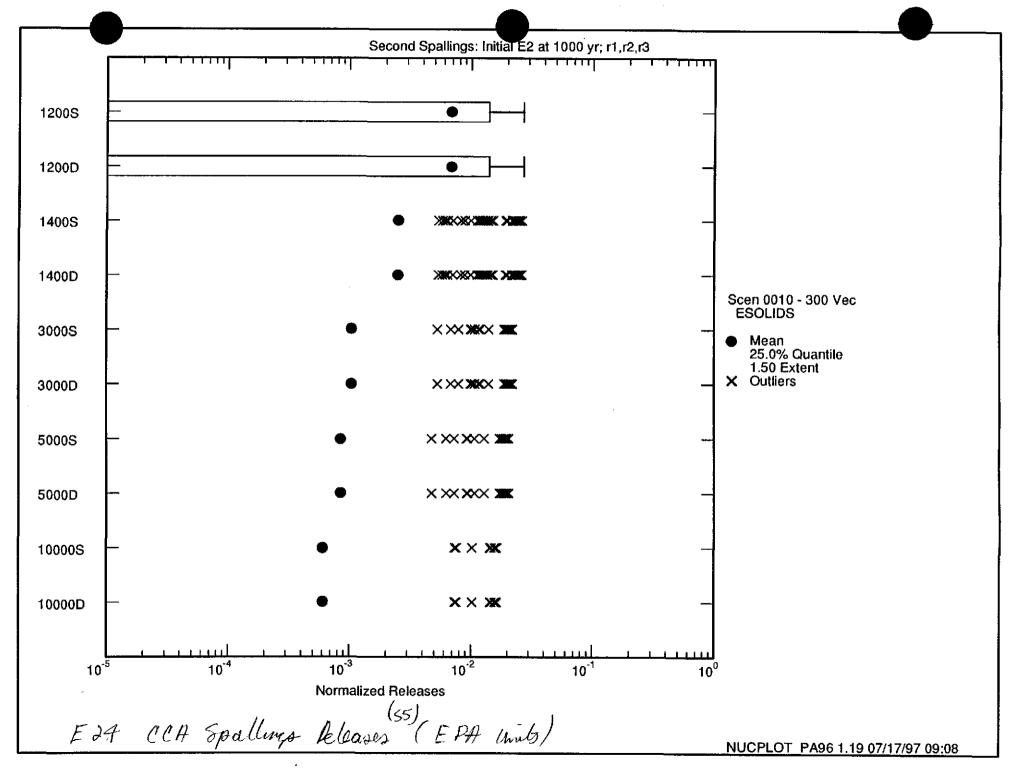
Information Only



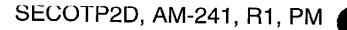
Information Only



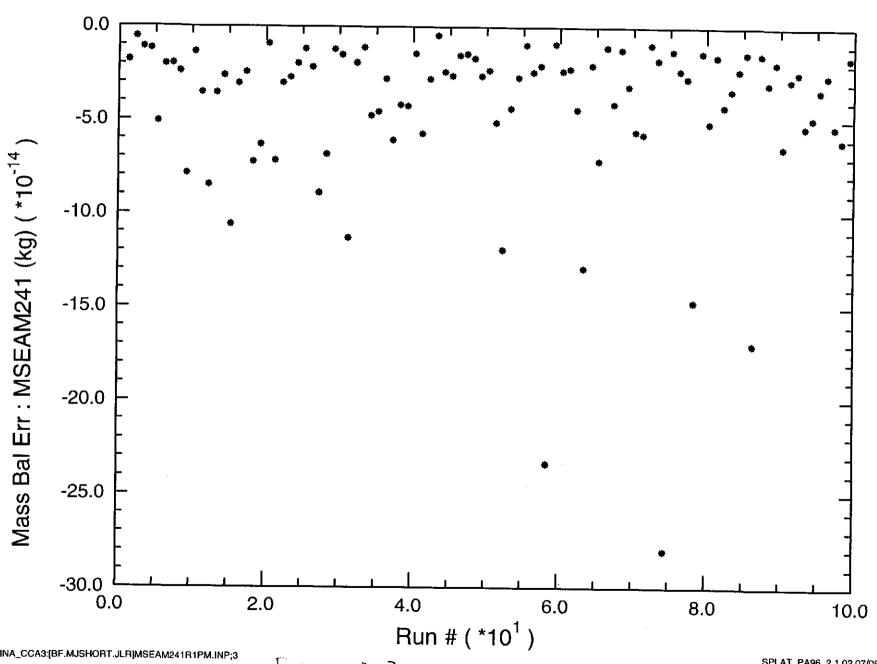
Information Only



Information Only







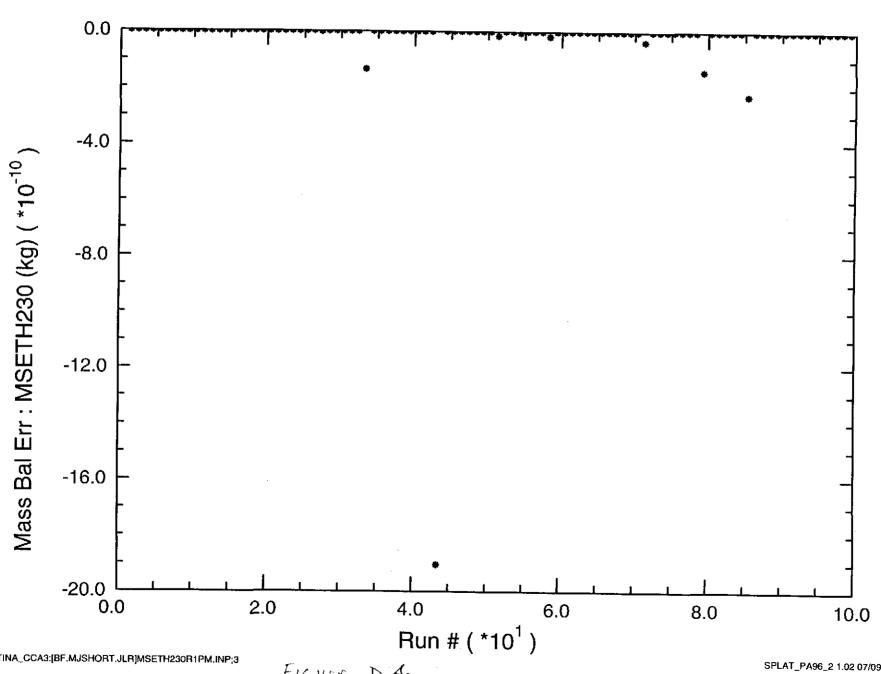
DISK\$TINA_CCA3:[BF.MJSHORT.JLR]MSEAM241R1PM.INP;3

Figure D.3

SPLAT_PA96_2 1.02 07/09/97 14:30:35



Run # vs Mass Balance Error (MSETH230)



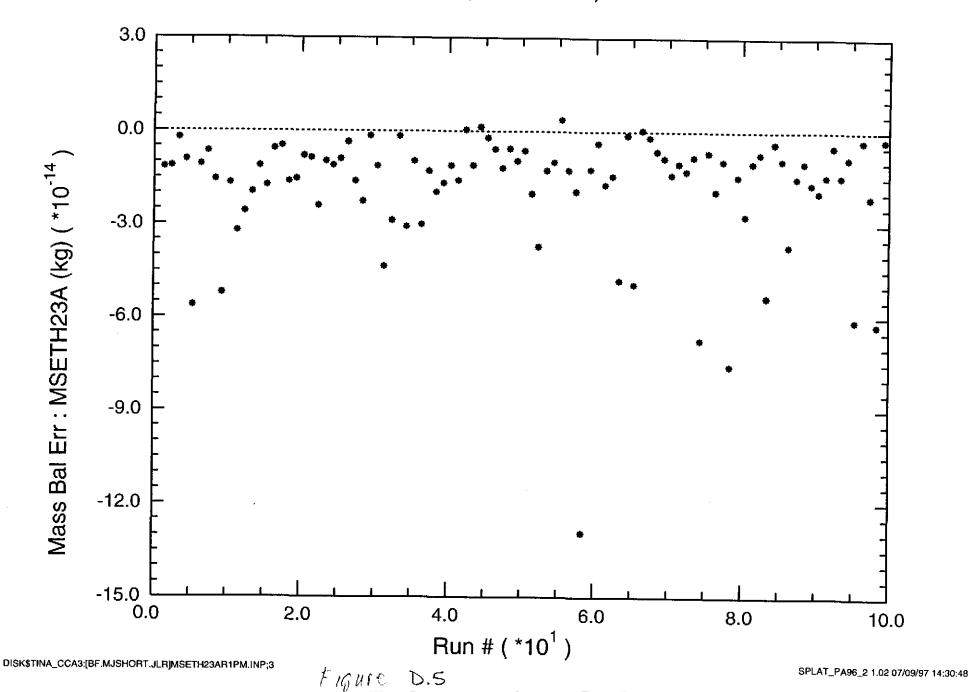
DISK\$TINA_CCA3:[BF.MJSHORT.JLR]MSETH230R1PM,INP;3

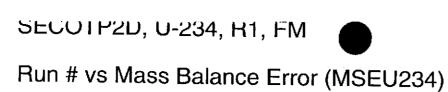
Figure D.4

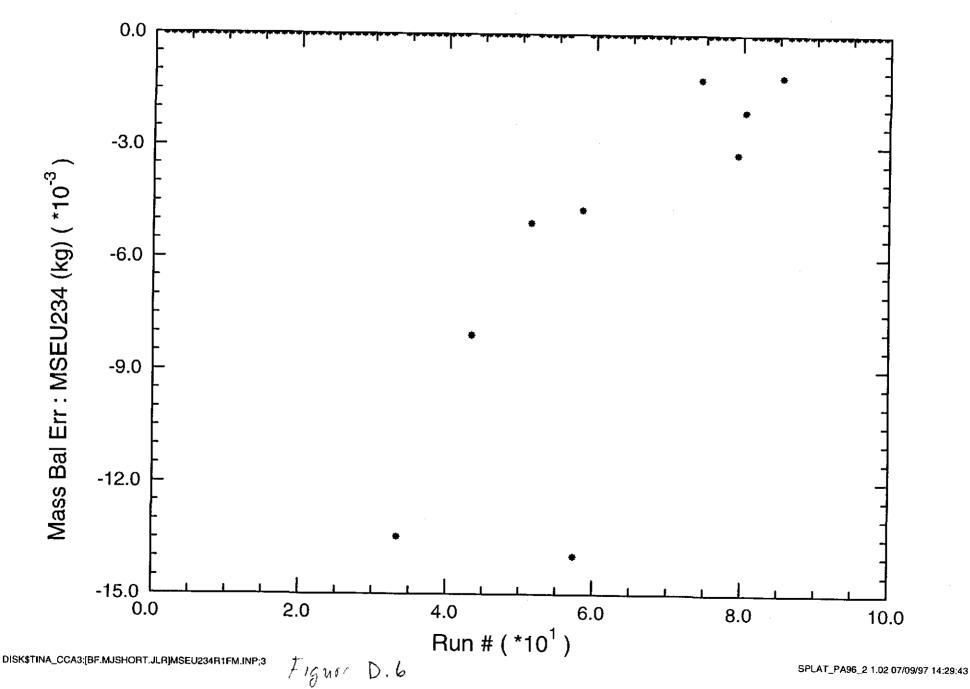
SPLAT_PA96_2 1.02 07/09/97 14:30:41



Run # vs Mass Balance Error (MSETH23A)

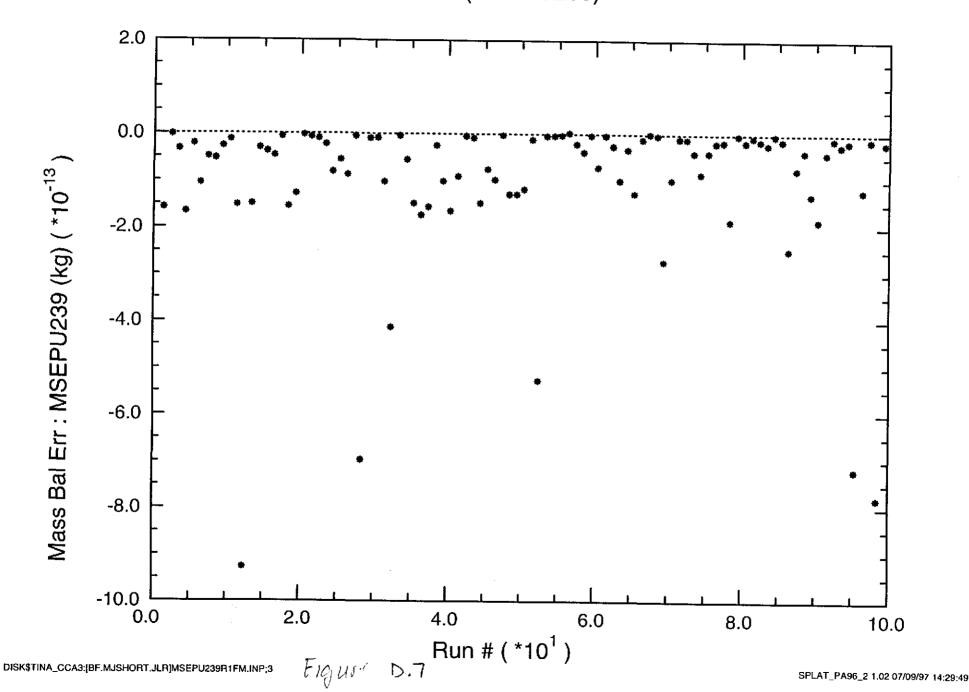






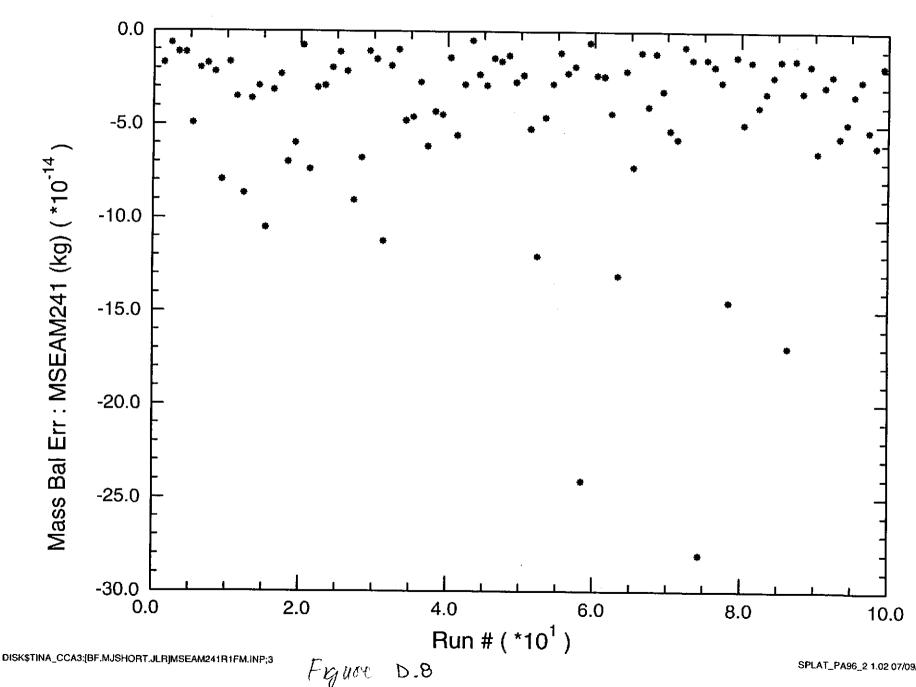


Run # vs Mass Balance Error (MSEPU239)





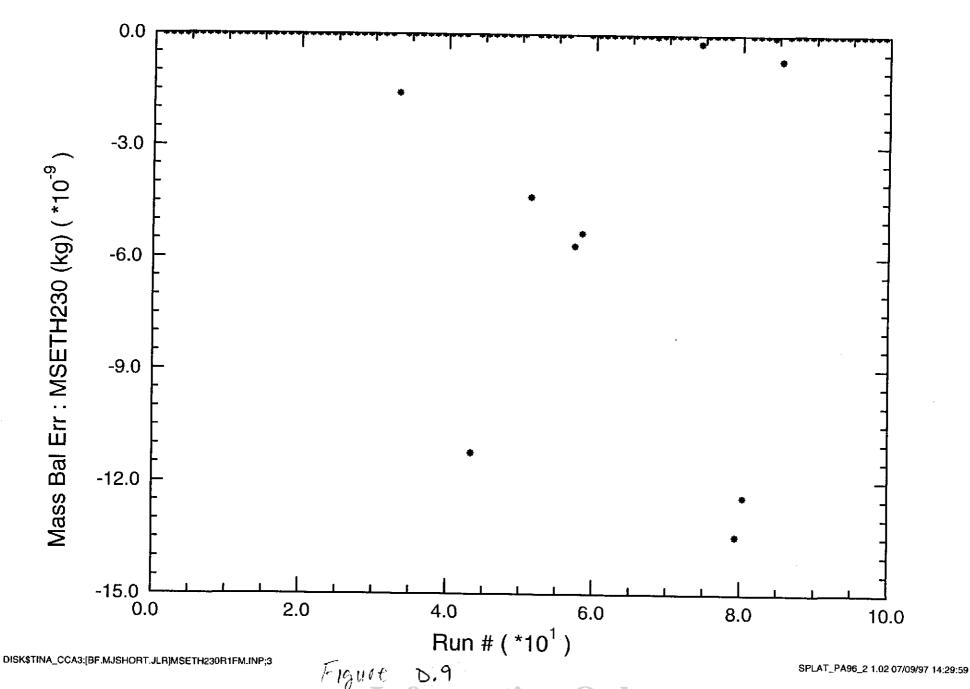
Run # vs Mass Balance Error (MSEAM241)

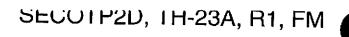


SPLAT_PA96_2 1.02 07/09/97 14:29:54

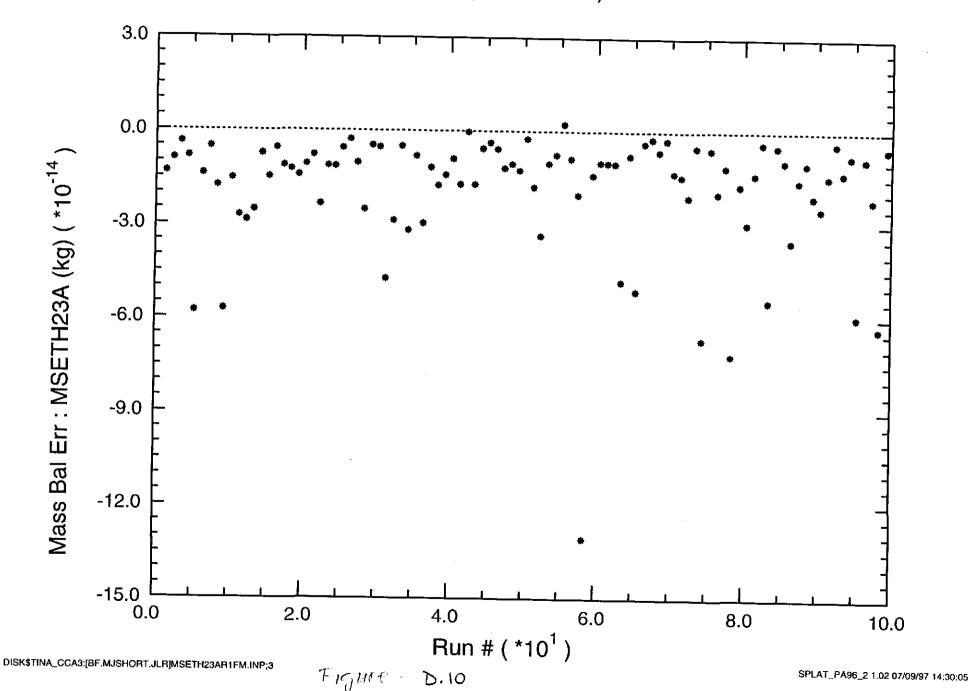


Run # vs Mass Balance Error (MSETH230)





Run # vs Mass Balance Error (MSETH23A)



APPENDIX F

BRAGFLO RESULTS FOR DIRECT BRINE RELEASE (DBR)

Appendix F includes Tables and Figures which contain results from direct brine release calculations performed using BRAGFLO.

Tables

F.1

PAVT replicate 1 direct brine release vectors

This Table contains values for all down-dip and up-dip vectors with releases.

Figures

F.1 - F.5 PAVT direct brine volumes (S1 through S5)

F.6 - F.10 PAVT direct brine releases (EPA units) (S1 through S5)

F.11 - F.15 CCA direct brine volumes (S1 through S5)

F.16 - F.20 CCA direct brine releases (EPA units) (S1 through S5)

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					Excavated												. ,						··				<u> </u>
1	•	٠	•	٠	Waste Porosity	Residual Gas Set Theologi	Residual Brins	Crushed Panel	Up-dip Avg	Up dip Avg	Down-dip Avg Presaure (Pa)	Down-dlp Avg	DRZ Porosity	ORZ Permeability	Salt Piller Porosity	Salt Pillar Permenality	Entrusion Time	Skin lactor	Well Productivity	80 well Sand		Castile	Castile Reservok	Up-dip Brine Relative	Up-dip Ges Relative	Down-dip Brine Fleinibre	Down-dip Gas
1					(fraction)		(# 00.00.01)	, anger hay	FIRSTON & (F.B)	Sec (meeson)	PTUSAKATA (PA)	SEL (RECEON)	(Fraction)	(114,5)	(Fraction)	(m/5)	(Years)	SIGN) ISCOM	Index (I/Pa)	Permeability (m/2)	nolide released	Pressure (Pa)	Permonbility	Permeability	Permeability	Permeability	Permeability
Na.		Replic.	Scen.	Vector	POROSITY		SAT_RBAN	HEIGHT	PRESPAN2	BSATPAN2	PRESPAN4	BSATPAN4	POROSITY	PERM X	POROSITY	PERM X	INTE THE	SKIN	WELLP	DOLL CAND	4DE4 TOT	DAGT DE	(m/S)	(fraction)	(Raction)	(Iraction)	(fraction)
1 !	Down-dip	!	?	51 58	6.32E-01	1,34E-01	3.63E-01	1.63E+00	9.80E+06	2.27E-01	9.81E+08	8.32E-01	1.46E-01	8.17E-14	1.53E-01	6.17E-14		-1.16E+00	1.55E-13	0.00E+00	AREA_TOT 7.77E-01	1.68E+07	PRM_CAST 1,00E-12	0.00E+00	KRG2 1.00E+00	4 15F-02	KRG4 1.42€-01
3	Down-dip	- 1	÷	26	6.30E-01	2.96E-02 9.72E-02	1.14E-01 1.79E-01	1.65E+00 1.62E+00	1.01E+07 9.64E+06	1.70E-01 1.76E-01	1.01E+07	1.81E-01	1.64E-01	1.45E-16	1.75E-01	1.45E-18		-1.18E+00	1.58E-13	0.00E+00	B.11E-01	1.26E+07	1.00E-12	3.76E-05	8.65E-01	7.53E-05	8.37E-01
4	Down-dip	1	í	26	5.28E-01	7.60E-02	4.97E-01	1.27E+00	9.71E+06	2.45E-01	9.66E+06 9.72E+06	1.80E-01 8.02E-01	1.68E-01 1.80E-01	4.79E-17 2.00E-14	1.81E-01 2.00E-01	4.79E-17 2.00E-14			1.50E-13		8.64E-01	1.48E+07	1.00E-12	0.00E+00	1.00E+00	9.44E-12	9.98E-01
5	Down-dip	1	1	40	5.46E-01	1.02E-01	3,54E-01	1.32E+00	1.10E+07	8.32E-02	1.10E+07	6,92E-01	1.36E-01	1.51E-13	1.39E-01	1.51E-13	1.00E+03	-1.33E+00	1,30E-13 1,34E-13	0.00E+00	1.10E+00	1.19E+07	1.00E-12	0.00E+00	1.00E+00	1.57E-01	3.57E-02
6	Down-dip	1	!	51	5.70E-01	1.34E-01	3.63E-01	1.40E+00	1.31E+07	2.46E-01	1.31E+07	8.85E-01	2.01E-01	4.87E-13	1.78E-01	6,17€-14	1.00E+03	-1.16E+00	1.33E-13	0.00E+00	1.07E+00 7.77E-01	1.47E+07 1.68E+07	1.00E-12 1.00E-12	0.00E+00	1.00E+00 1.00E+00	9.13E-02	7.99E-02
'	Down-dip	;	1	94 79	5.44E-01 5.40E-01	4.58E-03 1.23E-01	1.85E-01 3.88E-01	1.32E+00 1.31E+00	1.09E+07 1.06E+07	2.59E-01	1.09E+07	6.29E-01	2,03E-01	6.31E-15	2.11E-01	6.31€-15		-1.29E+00	1.32E-13	0.00E+00	9.95E-01	1.43E+07	1.00E-12	1.42E-04	6.12E-01	4.15E-01 1.06E-01	3.13E-08 1.30E-01
9	Down-dip	1	i	22	5.23E-01	2.51E-02	8.22E-02	1.31E+00	9.31E+06	4.35E-02	1.06E+07 9.36E+06	7.81E-01 9.72E-01	1.76E-01 1.33E-01	2.57E-13 7.41E-14	1.90E-01	2.576-13	1.00E+03	-1.10E+00	1.22E-13	0.00E+00	6.89E-01	1.31E+07	1.00E-12	0.00E+00	1.00E+00	1.95E-01	1.19E-02
10	Down-dip	1	1	19	5.02E-01	1.42E-01	2.97E-02	1.21E+00	6.04E+06	1.69E-01	B.05E+08	4.57E-01	2.02E-01	1.41E-15	2.26E-01	7.41E-14 1.41E-15		-1.37E+00 -1.23E+00	1.30£-13 1.18£-13	0.00E+00	1.17E+00 8.94E-01	1.39E+07	1.00E-12	0.00E+00	1.00E+00	8.91E-01	7.54E-08
111	Down-dip	1	1	30	5.55E-01	1.16E-01	4.16E-02	1.35E+00	1.18E+07	5.30E-02	1.18E+07	3.99E-01	3.52E-02	2.75E-14	4.11E-02	2.75€-14		-8.49E-01	1.07E-13	0.00E+00	2.79E-01	1.27E+07 1.47E+07	1.00E-12 1.00E-12	7.78E-04 7.74E-08	8.57E-01 9.73E-01	4.84E-02	1.58E-01
13	Down-dip	1	-	31 73	5.34E-01 5.20E-01	5.28E-02 5.61E-02	5.93E-02 3.03E-01	1.29E+00 1.25E+00	1.02E+07 9.12E+06	9.16E-03 7.82E-02	1.02E+07 9.13E+06	4.10E-01	7.42E-02	1.66E-15	9.05E+02	1.66E-15		-1.27E+00	1.29E-13	0.00E+00	9.73E-01	1.49E+07	1.00E-12	0.00E+00	1.00E+00	2.62E-02 2.60E-02	2.54E-01 2.91E-01
14	Down-dip	i	i	49	5.63E-01	3.07E-02	7.64E-02	1.23E+00	1.25E+07	5.42E-02	9.13E+06 1.25E+07	4.20E-01 1.61E-01	9.01E-02 3.92E-02	3.72E-16 4.27E-15	1.13E-01 4.18E-02	3.72€-16 4.27€-15		-8.01E-01	1.04E-13	0.00€+00	3.77E-01	1.39E+07	1.00E-12	0.00E+00	1.00E+00	1.37E-03	6.31E-01
15	Down-dip	1	1	5	5.08E-01	1.29E 01	1.21E-01	1.22E+00	8.38E+06	1.18E-02	8.42E+06	1.71E-01	1.32E-01	1.82E-17	1.55E-01	1.82E-17		-1.26E+00 -1.37E+00	1,36E-13 1,27E-13	0.00E+00	9.52E-01 1.17E+00	1.31E+07	1.00E-12	0.00E+00	1.00E+00	1.47E-04	8.04E-01
16	Down-dip	1	1	58	5.80E-01	2.96E-02	1.14E-01	1.43E+00	1.40E+07	1.37E-01	1.40E+07	1.55E-01	2.14E-01	1.59E-15	2.02E-01	1.45E-16		-1.18E+00	1.37E-13	0.00E+00	8.11E-01	1.57E+07 1.26E+07	1.00E-12 1.00E-12	0.00E+00 1.49E-06	1.00E+00 9.44E-01	2.59E-05 1.18E-05	8.61E-01
18	Down-dip	1	i	28 58	5.70E-01 5.99E-01	9.72E-02 2.96E-02	1.79E-01 1.14E-01	1.40E+00 1.50E+00	1.31E+07 1.60E+07	1.94E-01 1.80E-02	1.31E+07		2.00E-01	4.79E-17	2.11E-01	4.79E-17		-1.08E+00	1.29E-13	0.00E+00	6.64E-01	1.48E+07	1.00E-12	3.92E-07	9.57E-01	1.16E-05	9.01E-01 9.42E-01
19	Down-dip	1	i	51	5.85E-01	1.34E-01	3.63E-01	1.45E+00	1.47E+07	1.15E-01	1.60E+07 1.47E+07	7.65E-01 6.93E-01	2.62E-01 2.58E-01	2.30E-11 7.30E-11	1.93E-01 1.72E-01	1.45E-16 6.17E-14	3.00E+03	-1.18E+00	1.44E-13	0.00E+00	B.11E-01	1.26E+07	1,00E-12	0.00E+00	1.00E+00	3.20E-01	2.15E-02
20	Down-dip	1	1	22	5.56E-01	2.51E-02	8.22E-02	1.35E+00	1.21E+07	7.51E-06	1.21E+07	9.71E-01	1.37E-01	7.45E-14	1.38E-01		3.00E+03 3.00E+03	1.16E+00 -1.37E+00	1.38E-13 1.40E-13	0.00E+00 0.00E+00	7.77E-01 1.17E+00	1.68E+07 1.39E+07	1.00E-12	0.00E+00	1.00E+00	8.82E-02	6.05E-02
21	Down-dip Down-dip	1	1	94	5.52E-01 5.32E-01	4.58E-03 7.76E-03	1.85E-01	1.34E+00	1.18E+07	1.91E-01	1.18E+07		2.03E-01	6.91E-15	2.08E-01	6.31E-15	3.D0E+03	-1.29E+00	1.34E-13	0.00E+00	9.95E-01	1.43E+07	1.00E-12	0.00E+00 8.61E-09	1.00E+00 R 87F-01	8.88E-01 9.71E-01	1.38E-07 2.09E-08
23	Down-dip	i	i	55	5.32E-01	7.76E-03 7.03E-02	3.12E-01 2.38E-01	1.28E+00 1.27E+00	1.02E+07 9.77E+06	1.77E-01 7.74E-02	1.02E+07 9.78E+06	8.71E-01 7.70E-01	1.43E-01 9.42E-02	2.29E-13	1.59E-01				1.00E-13	0.00E+00	2.60E-01	1.36E+07	1.00E-12	0.00E+00	1.00E+00	4.63E-01	9.09E-08
24	Down-dip	1	1	44	5.24E-01	1.12E-01	1.61E-02	1.26E+00	9.67E+06	5.13E-06	9.78E+06 9.70E+06		9.42E-02 1.26E-01	8.71E-15 1.18E-13	1.07E-01 1.36E-01	8.71E-15 1.18E-13		-8.68E-01 -1.17E+00	1.08E-13 1.20E-13	0.00E+00	4.31E-01	1.2BE+07	1.00E-12	0.00E+00	1.00E+00	2.65E-01	1.92E-02
25	Down-dip	1	1	30	5,53E-01	1.16E-01	4.16E-02	1.34E+00	1.19E+07	4.82E-02	1.19E+07	4,39E-01	3.58E-02	2.75E-14	4.13E-02	2.75E-14	3.00E+03	-1.17E+00 -6.49E-01	1.20E-13	0.00E+00 0.00E+00	7.83E-01 2.79E-01	1.45E+07 1.47E+07	1.00E-12 1.00E-12	0.00E+00 1.04E-08	1.00E+00 9.84E-01	6.41E-01 3.86E-02	0.00E+00
26	Down-dip Down-dip	1	1	19 24	5.47E-01 5.01E-01	1.42E-01 9.01E-02	2.97E-02 1.37E-01	1.33E+00 1.20E+00	1.14E+07	5.46E-02	1.14E+07	3.73E-01	1.99E-01	1.41E-15	2.05E-01	1.41E-15		-1.23E+00	1.30E-13	0.00E+00	8.94E-01	1.27E+07	1.00E-12	1.04E-06	9.38E-01	3.86E-02 2.15E-02	2.01E-01 2.66E-01
28	Down-dip	i	i	31	5.46E-01		5.93F-02		8.47E+06 1.13E+07	1.11E-01 4.05E-06	8.53E+06 1.13E+07	9.08E-01 3.78E-01	1.99E-01 7.73E-02	2.82E-13	2.24E-01 8.83E-02	2.82E-13		-1.29E+00	1.21E-13	0.00E+00	9.94E-01	1.27E+07	1.00E-12	0.00E+00	1.00E+00	6.59E-01	3.23E-08
29	Down-dip	1	1	17	5.69E-01		2.26E-01	1.39E+00		8.46E-06	1.32E+07	4.50E-01	1.69E-01	1.66E-15 4.74E-14	8.83E-02 1.48E-01	1.66E-15 5.37E-15		-1.27E+00 -1.03E+00	1.32E-13 1.26E-13	0.00E+00 0.00E+00	9.73E-01	1.49E+07	1.00E-12	0.00E+00	1.00E+00	1.84E-02	3.38E-01
30	Down-dip	1	1	79	5.76E-01	1.23E-01	3.88E-01			2.50E-06			1.79E-01	3.65E-13	1.75E-01		3.00E+03		1.32E-13	0.00E+00	5.93E-01 6.89E-01	1.51E+07 1.31E+07		0.00E+00 0.00E+00	1.00E+00 1.00E+00	1.03E-02 1.88E-03	4.34E-01
31	Down-dip Down-dia	1	1	26	5.78E-01 5.09E-01	7.60E-02 1.14E-01	4.97E-01 1.70E-01		_	6.98E-02 2.96E-02	1.40E+07		1.B1E-01	2.53E-14	1.79E-01	2.00E-14	3.00E+03	-1.33E+00	1,45E-13	0.00E+00	1,10E+00	1.19E+07		0.00E+00	1.00E+00	2.65E-03	5 46E-01
	Down-dip	ì	í	2	5.81E-01	8.22E-02	4.02E-01	1.37E+00		9.10E-03	6.66E+06 1.25E+07		5.36E-02 1.69E-01	2.14E-14 8.06E-14	6.98E-02 1.66E-01			-1.01E+00 -1.29E+00	1.10E-13	0.00E+00	5.75E-01	1 13E+07		0.00E+00	1.00E+00	6.63E-00	4.306-01
34	Down-dip	1	1	60	5.21E-01	6.13E-02	4.70E-02		9.44E+08	6.74E-02	9.48E+06	1.98E-01	1.93E-01	5.75E-18	2.05E-01	5.75E-18			1.37E-13 1.20E-13	0.00E+00 0.00E+00	9.98E-01 7.91E-01	1.41E+07 1.35E+07	1.00E-12 1.00E-12	0,00E+00 6.77E-07	1.00E+00 9.53E-01	1.75E-03	5.84E-01
	Down-dip Down-dip	1	1	78 49	5.12E-01 5.73E-01	4.93E-02 3.07E-02	1.51E-01			8.79E-03	0.99E+06	2.41E-01	1.08E-01	2.46E-15	1.22E-01	2.46E-15	3.00E+03	-1.06E+00	1.12E-13	0.00E+00	6.28E-01	1.61E+07		0.00E+00	9.53E-01 1.00E+00	1.10E-03 2.50E-04	6.57E-01 7.69E-01
37	Down-dip	1	;	5	5.73E-01 5.21E-01	3.07E-02	7.84E-02 1.21E-01			6.93E-03 2.23E-05	1.36E+07 9.41E+06		4.44E-02 1.33E-01	6.45E-15 1.82E-17	4.08E-02				1.39E-13	0.00E+00	9.52E-01	1.31E+07			1.00E+00	4.63E-07	9.59E-01
38	Down-dip	1	1	91	5,69E-01	5.46E-02	3.06E-01			7.93E-06	1.32E+07	3.08E-01	1.90E-01	5.26E-15	1.51E-01 1.91E-01	1.82E-17 5.01E-15	3.00E+03 3.00E+03		1.30E-13 1.15E-13	0.00E+00 0.00E+00	1.17E+00	1.57E+07		0.00E+00	1.00E+00	2.61E-09	9.89E-01
1 ~~	Down-dip	1	1	58	6.09E-01	9.72E-02	1.79E-01	1.54E+00		5.22E-02	1.66E+07	7,71E-01	2.53E-01	9.84E-12	1.91E-01	4.79E-17			1.42E-13	0.00E+00	3.57E-01 6.64E-01	1.25E+07 1.48E+07		_	1.00E+00 1.00E+00	4.82E-10 3.00E-01	9.93E-01
40	Down-dip Down-dip	1	1	7 22	5.53E-01 5.64E-01	7.76E-03 2.51E-02	3.12E-01 B 22E-02	1.34E+00 1.38E+00	1.19E+07	1.12E-01	1.19E+07	7.08E-01	1.44E-01	2.29E-13	1.52E-01	2.29E-13	5.00E+03	-6.15E-01	1.05E-13	0.00E+00	2.60E-01	1.36E+07	1.00E-12	0.00E+00	1.00E+00	1.30F-01	9.49E-03
42	Down-dip	i	ì	69	5.03E-01	8.98E-02	4.08E-01			5.66E-06	1.28E+07 8.66E+06	9.09E-01 7.46E-01	1.40E-01 7.48E-02	1.12E-13 1.26E-14	1.35E-01 9.53E-02	7.41E-14		-1.37E+00	1.43E-13	0.00E+00	1.17E+00	1.39E+07	1.00E-12	0.00E+00	1.00E+00	6.79E-01	6.78€-04
43	Down-dip	1	i	58	6,03E-01	2.96E-02	1.14E-01	1.51E+00	1.62E+07	1.50E-05			2.67E-01	8.78E-11	1.91E-01			-1.29E+00 -1.18E+00	1.21E-13 1.45E-13	0.00E+00 0.00E+00	9.99E-01 8.11E-01	1.62E+07			1.00E+00	1.29E-01	5.02E-02
44	Down-dip	1	1	94	5.56E-01	4.58E-03		1.35E+00	1.21E+07	1.77E-01			2.03E-01	6.31E-15	2.06E-01			-1.29E+00	1.35E-13	0.00E+00	9.95F-01	1.26E+07 1.43E+07	1.00E-12 1.00E-12	0.00E+00 0.00E+00	1.00E+00 1.00E+00	5.70E-02 9.72E-01	1.96E-01 1.48E-08
	Down-dip Down-din	1	1	24	4.95E-01 5.34E-01	6.86E-02 9.01E-02	3.61E-02 1.37E-01	1.19E+00 1.29E+00		8.12E-03 7.45E-02			1.57E-01	3.02E-17	1.79E-01				1.18E-13	0.00E+00	9.43E-01	1.22E+07			1.00E+00	1.56E-01	6.28E-02
,,,	Down-dip	ì	ì	55	5.46E-01		2.38E-01	1.32E+00		2.83F-02			1.94E-01 9.72E-02	2.82E-13 8.71E-15	2.10E-01 1.03E-01				1.29E-13	0.00E+00	9.94E-01	1.27E+07		0.00E+00	1.00E+00	6.59E-01	2.76E-08
	Down-dip	1	1	44	5.25E-01	1.12E-01	1.61E-02	1.26E+00		3.76E-06		6.69E-01	1.28E-01	1.18E-13	1.36E-01		5.00E+03 5.00E+03		1.13E-13 1.21E-13	0.00E+00	4.31E-01 7.83E-01	1.28E+07 1.45E+07	1.00E-12 1.00E-12	0.00E+00	1.00E+00	8.44E-02	1.18E-01
	Down-dip	1	1	31	5.50E-01	5.28E-02	5.93E-02	1.34E+00		3.28E-06	*****		7.80E-02	1.66E-15	B.75E-02		5.00E+03		1.33E-13		9.73E-01	1.49E+07		0.00E+00 0.00E+00	1.00E+00	6.42E-01 5.86E-02	0.00E+00 1.81E-01
50	Down-dip Down-dip	1	1	10	5.54E-01 5.61E-01	1.16E-01 1.42E-01	4.16E-02 2.97E-02	1.35E+00 1.37E+00	1.20E+07 1.26E+07	4.60E-02 1.60F-02			3.60E-02	2,75E-14	4.13E-02	2.75€-14	5.00E+03	-6.49E-01	1.06E-13	0.00E+00	2.79E-01	1.47E+07			9.90E-01	4.45E-02	1.83E-01
1	Down-dip	1	i	17	5.69E-01	1.41E-02	2.26E-01	1.39E+00		3.93E-06	1.26E+07 1.32E+07	4.01E-01 4.85E-01	1.98E-01 1.69E-01	1.45E-15 4.64E-14	1.99E-01 1.48E-01		5.00E+03 5.00E+03		1,34E-13	0.00E+00	8.94E-01	1.27E+07	1.00E-12	0,005+00	1.00E+00	2.89E-02	2.25E-01
	Down-dip	1	1	79	5.76E-01		3.88E-01	1.42E+00	1.39E+07	1.67E-06	1.39E+07	5.08E-01	1.79E-01	3.67E-13	1.75E-01	2.57E-13		-1.03E+00	1.26E-13 1.32E-13	0.00E+00	5.93E-01 6.89E-01	1.51E+07 1.31E+07			1.00E+00 1.00E+00	1.75E-02	3.65E-01
54 55	Down-dip Down-dip	1	1	63	5.24E-01 5.71E-01	1.14E-01 5.46E-02	1.70E-01	1.26E+00	9.67E+06	1.12E-04		3.99E-01	5.52E-02	2.14E-14	6.76E-02	2.14E-14		-1.01E+00	1.13E-13	0.00E+00	5.75E-01	1.13E+07	1.00E-12		1.00E+00	2.42E-03 8.58E-03	5.18E-01 3.96E-01
	Down-dip	j	i	26	5.88E-01		3,06E-01 4,97E-01	1.40E+00 1.46E+00		5.78E-06 5.20E-03		4.89E-01 5.64F-01	1.90E-01 1.89E-01	6,11E-15	1.90E-01				1.15E-13	0.00E+00	3.57E-01	1.25E+07	1.00E-12	0.00E+00	1.00E+00	7.33E-03	4.47E-01
	Down-dip	1	1	78	5.24E-01	4.93E-02	1.51E-01		9.65E+06	1.97E-05	,	2.86E-01	1.08E-01	1.01E-13 2.46E-15	1.75E-01 1.19E-01	2.00E-14 2.46E-15			1.49E-13 1.15E-13	0.00E+00 0.00E+00	1.10E+00 6.28E-01	1.19E+07			1.00E+00	5.97E-04	6.78E-01
58	Down-dip	1	1	53	4.99E-01			1.20E+00	8.51E+06	7.26E-02		3.82E-01	1.57E-01	8,51E-18	1.84E-01				1.15E-13	0.00E+00	8.28E-01 8.92E-01	1,61E+07 1,42E+07		0.00E+00 0.00E+00	1.00E+00 1.00E+00	1.13E-03 1.57E-03	6.56E-01
	Down-dip Down-dip	1	1		5.05E-01 5.67E-01	3.40E-02 8.22E-02	6.64E-02 4.02E-01	1.21E+00 1.39E+00		2.19E-02			1.46E-01	1.70E-19	1,61E-01	1.70E-19	5.00E+03	-1.22E+00	1.18E-13	0.00E+00	8.64E-01	1.51E+07			1.00E+00	1.57E-03 4.49E-04	6.26E-01 7.36E-01
	Down-dip	i	i	_	5.39E-01				1.30E+07 1.08E+07	8.11E-06 3.00E-02	1.30E+07 1.08E+07	4.40E-01 1.21E-01	1.74E-01 1.92E-01	1.12E-13 5.75E-18	1.64E-01 1.98E-01	4.47E-14 5.75E-18			1.39E-13	0.00E+00	9.98E-01	1.41E+07			1.00E+00	3.89E-05	8.47E-01
	Down-dip	1	1	12	5.38E-01	7.06E-02	1.02E-01			5.96E-08			3.23E-02	1.78E-13	1.98E-01 4.46E-02				1.25E-13 1.35E-13	0.00E+00 0.00E+00	7.91E-01 1.19E+00	1.35E+07 1.44E+07			1.00E+00	7.91E-05	8.29E-01
	Down-dip	1	1		5.27€-01	_	1.21E-01		9.64E+06	1.38E-05		1.54E-01	1.34E-01	1.82E-17	1.49E-01	1.82E-17			1.32E-13	0.00E+00	1.19E+00 1.17E+00	1.44E+07 1.57E+07			1.00E+00	1.33E-05 5.52E-06	8.93E-01 9.09E-01
	Down-dip Down-dip	1	1	40	5.66E-01 4.93E-01	1.02E-01 6.75E-02	3.54E-01 1.61E-01	1.39E+00 1.19E+00	1.30E+07 B.30E+06	1.91E-06 5.44E-02		3.67E-01		7.47E-13	1.32E-01	1.51E-13		-1.32E+00	1.41E-13	0.00E+00	1.07E+00	1.47E+07			1.00E+00	5.52E-06 6.04E-07	9.50E-01
	Down-dip	i	i	31	5.58 E- 01	5.28E-02	5.93E-02			5.44E-02 2.03E-06		1.62E-01 7.13E-01	1.50E-01 7.92E-02	6.92E-18 1.66E-15	1.66E-01 8.60E-02	6,92E-18			1.10E-13	0.00E+00	6.75E-01	1.24E+07		0.00E+00	1.00E+00	8.47E-11	9.96E-01
67	Down-dip	1	1	58	6.04E-01	2.96E-02	1.14E-01	1.52E+00		2.56E-06			2.55E-01	1.00E-15 1.29E-11	1.90E-01	1.66E-15 1.45E-16			1.35E-13 1.46E-13	0.00E+00 0.00E+00	9.73E-01	1.49E+07			1.00E+00	2.60E-01	2.83E-02
	Down-dip	1	1		5.26E-01		4.08E-01			4.72E-02	9.78E+06	7.54E-01	7.61E-02	1.26E-14	9.08E-02	1.26E-14			1.27E-13	0.00E+00	B.11E-01 9.99E-01	1.26E+07 1.62E+07			1.00E+00 1.00E+00	1.03E-01 1.37E-01	1.22E-01 4.56E-02
	Down-dip Down-dip	1	1		5.63E-01 5.66E-01	2.51E-02 4.58E-03	B.22E-02 1.85E-01			2.80E-06		8.67E-01	1.39E-01	1.02E-13	1.35E-01	7.41E-14	1.00E+04	-1.37E+00	1.42E-13	0.00E+00	1.17E+00	1.39E+07		0.00E+00	1.00E+00	1.3/E-01 5.60E-01	4.56E-02 2.88E-03
,	Down-dip	1	í		5.52E-01		1.85E-01			1.48E-01 3.71E-02			2.03E-01 1.93E-01	8.93E-15 2.82E-13	2.01E-01 2.02E-01	6.31E-15 2.82E-13			1.38E-13	0.00E+00	9.95E-01	1.43E+07	1.00E-12	0.00E+00	1.00E+00	9.72E-01	1.26E-08
72	Down-dip	1	1	19	5.69E-01	1.42E-01	2.97E-02	1.39E+00	1.32E+07	5.91E-05			1.99E-01	2.62E-13 2.70E-15	2.02E-01 1.95E-01				1.34E-13 1,36E-13	0.00E+00 0.00E+00	9.94E-01 8.94E-01	1.27E+07			1.00E+00	6.79E-01	0 00E+00
	Down-dip	1	1		6.39E-01	9.72E-02	1.79E-01			1.21E-05	1.68E+07	5.52E-01	2.45E-01	6.39E-11	1.77E-01				1.54E-13	0.00E+00	8.94E-01 6.64E-01	1.27E+07 1.48E+07		0.00E+00 0.00E+00	1.00E+00 1.00E+00	1.11E-01 5.46E-02	6.55E-02
	Down-dip Down-dip	1	1		5.73E-01 5.16E-01						_						1.00E+04	-6.15E-01	1.10E-13	0.00E+00		1.36E+07			1.00E+00	5.46E-02 4.88E-02	1.58E-01 2.28E-01
, ,,	-carirup	,	•	ا ••	J. 10E-V1	1.336-01	1.78E-02	1.24E+00	9.15E+06	1.07E-06	9.17E+06	5.49E+01	5.62E-02	3.39E-16	7.41E-02	3.39E-16	1.00E+04	1.53E+00	1.38E-13	0.00E+00		1.26E+07			1.00E+00	1.04E-01	7.69E-02

Part	$\overline{}$						1 '	Down-dip																		
	i						Up-dip Flowing	Flowing			Brim Retu	Gas Rate (ref	Max Brine	Mex Gas Flets	Produced Liquid/Gas	Curn Brine from Boundary	Gas Role			Cum Brine		Avg Bress Seturation		Avg Brina Saturation	Excevaled	
Part	ı								Character (Da)		(m/G/a)	m/3/s)	Rate (m^1/a)	(rel m^9/s)		Condition Well				Pioleages Intr/31	Panel 5 (Pa)	Panel 5				
Demons	No.	. 10) В	lepiic.	Scen	Vector	FBHP2			time	BRINCELW	CASELIM	MAY DON	May car					,,	(111 5)	and thousand	blowout		blowout	(fraction)	(m^3)
1	┰	Do	wn-dip	1	1		0.00E+00	3.10E+05		411.74			101 07111													
	2			1	1								5,56E-08													
5	3			1	•														5.32E-09	5.13E-09	3.22E+08					
Demonstration 1	;			i																				2.49E-01		3.14E+04
	6	Dov	vm-dip	1	Ť																					
	7			1	1	94			-,		1.78E-05	1.86E-01	7.05E-05													
	8			!	1																					
1	10			i	1				0.002																7.39E+04	2.92E+04
10 Demoke 1 1 31 000-000 2 7-76-00 000-00 1 100-00 177-00 200-00 170-00 200-00 170-00 200-00	11	Do	₩n-dβp	1	1	, -	4,																			
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20	٠.			!	1															1.05E+02	1.53E+07					
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90 Dominds 1 50 000000 3 Meeting 0.000000 3 Meeting 0.000000 3 Meeting 0.000000 3 Meeting 0.0000000000000000000000000000000000				1	1	7			_,		9.37E-05	6.38E-03	9.37E-05	3.92E-02	7.43E+03	0.00E+00										
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20		Dov	wn-dip	1	1	19		2.98E+05	0.00E+00	1,10E+01	3.41E-06															
1 1 1 1 1 1 1 1 1 1				1	1								2.06E-05	5.23E-08		0.00E+00										****
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50 Down-dig 1 7 0.000-00 2.555-0.5 0.000-00 1.105-01 7.255-01 0.000-00 0.000-00 0.0000-00 0.000-0	33			1	1	_	4,444																	9.11E-03	8.60E+04	
1 49 0.000-00 1 49 0.000-00 3.78-168 0.000-00 1.000-00 3.78-168 0.000-00 1.000-00 3.78-168 0.000-00 0.000-00 0.000-00 3.78-168 0.000-00 0.000-00 3.78-168 0.000-00 0.000-00 3.78-168 0.000-00 0.000-00 3.78-168 0.000-00 0.	35			ì	i																					
1	36	Dov	vn-dlp	1	1	49	0.00E+00	4.37E+05					=													
1				1	1	5	*****												3.36E-07							
	-	=		1	1																		1.30E+07	1.98E-05	6.68E+04	7.10E+03
1 1 22 0.0000-00 7.950-00 0.000-00 2.895-00 1.000-00 1.000-00 2.750-00 5.200-00 4.500-00 1.000-			,,, 	i	ì		****																			
42 Down-dip 1 5 69 0.000-froid 3.28f-vis 5 0.000-froid 1.000-froid 1.000-froid 3.200-froid 3.28f-vis 5 0.000-froid 3.200-froid 3.28f-vis 5 0.000-froid	41	Dov	vn-dip	1	1	22	0.00E+00	7.95E+06																		
44 Down-dip 1 1 94 DOWN-dip 2 1 1 94 DOWN-dip 3 1 1 94 DOWN-dip 1 1 86 DOWN-dip 1 1 86 DOWN-dip 1 1 86 DOWN-dip 1 1 86 DOWN-dip 1 1 86 DOWN-dip 1 1 84 DOWN-dip 1 1 24 DOWN-dip 1 24 DOWN-dip 1 1 24 DOWN-dip 1 1 24 DOWN-dip 1 1 24 DOWN-dip				!	1												1.62E+02	6.89E+04	2.91E+01							
45 Down-dip 1 1 96 0.000-dip 3.2E-0.6 0.00E-0.0 1.0E-0.1 1.77E-0.5 5.46E-0.2 7.0E-0.6 5.2E-0.1 2.4E-0.0 1.7E-0.5 7.4EE-0.4 1.7E-0.0 2.4E-0.0 1.7E-0.5 1.7E-0.0 1.7E-0.0 2.4E-0.0 1.7E-0.5 2.4E-0.0 1.7E-0.0 2.4E-0.0 1.7E-0.0 2.4E-0.0 1.7E-0.0 2.4E-0.0 1.7E-0.0 2.4E-0.0 1.7E-0.0 2.4E-0.0 1.7E-0.0 2.4E-0.0 1.7E-0.0 2.4E-0.0 2.4E-0.0 1.7E-0.0 2.4E-0.0 2.4E-0.0 1.7E-0.0 2.4E-0.0 2.4E-0.0 2.4E-0.0 1.7E-0.0 2.4E-0	43			1	1																					
46 Down-dp 1 1 24 Down-dp 1 1 24 Down-dp 1 1 25 Down-dp 1 25 Down-dp 1 1 25 Down-dp 1 2 Down-dp 1 2 Down-dp 1 2 Down-dp 1 2 Down-dp 2 Do	45			i	1																					
47 Down-dip 1 1 55 0000-40 3895-05 0.000-40 1 1.000-40 1 1.000-40 0 1.000-40				1	1						7.B1E-05	1.99E-06	9.82E-05													
49 Down-dp 1 1 31 Down-dp 1 325 Down-dp 1 1 32 Down				!	1																	6.28E-01			8.11E+04	
50 Down-dip 1 1 90 0.0000-00 3.98E-05 0.0000-00 1.000-01 5.98E-05 0.000-00 1.000-01 1.000-01 3.98E-05 0.000-00 1.000-01 5.98E-05 0.000-00 1.000-01 1.000-01 3.98E-05 0.000-00 1.000-01 1.000-01 3.98E-05 0.000-00 1.000-01 1.000-01 3.98E-05 0.000-00 1.000-01 1.000-01 3.98E-05 0.000-00 1.000-01 1.000-01 3.98E-05 0.000-00 1.000-01 1.000-01 3.98E-05 0.000-00 1.000-01 1.000-01 3.98E-05 0.000-00 1.000-01 1.000-01 3.98E-05 0.000-00 1.000-01 1.000-01 3.98E-05 0.000-00 1.000-01 1.000-01 3.98E-05 0.000-00 3.98E-05 0.000-00 1.000-01 1.000-01 3.98E-05 0.000-00 3.98E-05 0.000-00 1.000-01 1.000-01 3.98E-05 0.000-00 3.98E-05 0.000-00 1.000-01 1.000-01 3.98E-05 0.000-00 3.98E-05 0.000-00 1.000-01 1.000-01 3.98E-05 0.000-00 3.98E-05 0.000-00 1.000-01 1.000-01 3.98E-05 0.000-00 3.98E-05 0.000-00 1.000-01 1.000-01 3.98E-05 0.000-00 3.98E-05 0.000-00 1.000-01 1.000-01 3.98E-05 0.0000-01 1.000-01 3.98E-05 0.0000-01 1.0000-01 3.98E-05 0.0000				1	1																					
51 Down-dp 1 1 1 9 0.00E+00 3.27E+05 0.00E+00 1.01E-01 5.19E+06 8.39E-01 1.2E-04 0.00E+00 4.11E-00 0.00E+00 4.11E-00 0.00E+00 4.57E-00 7.2E-06 8.39E-01 1.2E-04 0.00E+00 1.2E-05				1	1		4.16E+05	3,53E+05	0.00E+00													4.53€-01				
52 Down-dp 1 1 77 0.0004-00 3.25E-05 0.0004-00 1.0004-01	٠.			1	1	,.									1.20E+01		1.01E+03	5.72E+05	6.83E+00							
54 Down-dp 1 1 63 0.00E+00 2.246E+05 0.00E+00 1.10E+01 1.25E+06 4.22E-01 4.38E+06 4.22E-01 4.38E+06 4.22E-01 4.38E+06 4.22E-01 4.38E+06 4.22E-01 4.38E+06 1.25E+06 5 Down-dp 1 1 26 0.00E+00 3.22E+05 0.00E+00 1.0E+01 1.0E+07 5.31E+06 0.3E+00 1.3E+07 0.00E+00 3.2E+06 1.3E+07 1.3E+07 0.00E+07 5.3E+06 0.00E+00 1.3E+07 0.00E+07 1.3E+07 0.00E+07 0.00E+07 0.00E+07 0.3E+07 0.00E+07 0.00E+07 0.00E+07 0.3E+07 0.00E+07 0.00E+07 0.00E+07 0.3E+07 0.00E+07 0.3E+07 0.00E+07 0.00E+07 0.00E+07 0.3E+07 0.00E+07 0.3E+07 0.00E+07 0.00E+07 0.00E+07 0.3E+07 0.00E+07 0.3E+07 0.00E+07 0.00E+07 0.00E+07 0.3E+07 0.00E+07 0.3E+07 0.00E+07 0.00E+07 0.00E+07 0.3E+07 0.00E+07 0.3E+07 0.00E+07 0.00E+07 0.00E+07 0.3E+07 0.00E+07 0.3E+07 0.00E+07 0.00E+07 0.00E+07 0.3E+07 0.00E+07 0.00E+07 0.00E+07 0.3E+07 0.00E+07 0.00E+07 0.00E+07 0.3E+07 0.00E+07 0.00E+07 0.00E+07 0.3E+07 0.00				1	1																		1.27E+07		8.88E+04	
55 Down-dip 1 1 91 0.00E-00 3.22E-05 0.00E-00 1.0E-01 1.2E-06 4.57E-01 5.3E-06 0.00E-00 1.7E-00 0.00E-00 5.4E-06 0.00E-00 5.4				i	i																					
56 Own-dip 1 1 2 6 0.00E+00 3.7FE-05 0.00E+00 0 1.0E-01 0.50E-01 0				1	1	91	0.00E+00	3.22E+05	0.00E+00	1.10E+01	1.12E-06	4.57E-01	5,31E-06	9.31E+00	1.71E+00											
58 Own-dp 1 1 5 3 0.00E+00 2.28E+05 0.00E+00 1.0E+01 5.9E+04 1.0E+01 5.2E+01 0.00E+00 1.0E+01			•	1	1												5.46E+03	2.24E+08	3.52E-01	3.26E-01	7.17E+06	5.68E-01	1.37E+07	5.25E-03		
59 Down-dip 1 1 41 0.00E-00 3.7EE-05 0.00E-00 1.10E-01 1.4EE-08 1.17E-01 2.16E-07 8.8SE-010 1.17E-01 0.00E-00 3.7EE-05 0				1	1																					
80 Down-dip 1 1 2 2 0.00E+00 3.09E+05 0.00E+00 1 10E+01 1.42E-08 2.07E+00 3.27E-08 1.99E+01 1.53E-02 0.00E+00 1 1 60 0.00E+00 3.09E+05 0.00E+00 1 10E+01 1.00E+01 1.00E+01 1.00E+01 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1				i	i																					
61 Down-dip 1 1 60 0.00E+00 3.98E+05 0.00E+00 1 1 1 60 0.00E+00 3.98E+05 0.00E+00 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1				1	1	_									5.21E-03		6.31E+03	2.66E+06	1,39E-02	1.33E-02						
63 Down-dip 1 1 5 0.00E+00 3.18E+05 0.00E+00 1.0E+01 4.12E+10 2.17E+01 3.30E+09 1.7E+01 1.2E+03 0.90E+00 6.83E+02 5.58E+03 6.31E+04 5.96E+04 2.9EE+03 6.30E+04 0.00E+00 1.7E+04 2.9EE+03 6.30E+04 0.00E+00 1.7E+04 0.00E+00 1.0E+01 1.2E+03 0.00E+00 1.0E+01 2.2EE+01 6.50E+06 0.00E+00 1.7EE+01 6.50E+06 0.00E+00 1.7EE+01 6.50E+06 0.00E+00 1.7EE+04 0.00E+00 1.7EE+04 0.00E+00 1.7EE+04 0.00E+00 1.7EE+04 0.00E+00 1.7EE+04 0.00E+00 1.7EE+04 0.00E+00 1.7EE+04 0.00E+00 1.7EE+04 0.00E+00 1.7EE+04 0.00E+00 1.7EE+04 0.00E+00 1.7EE+04 0.00E+00 1.7EE+01 0.00E+00 1.				1	1														9.53E-03			1.21E-01		2.74E-02	7.90E+04	6.20E+03
54 Down-dip 1 1 40 0.00E+00 3.15E+05 0.00E+00 1.10E+01 2.8EE+10 3.8EE+01 5.1EE-10 2.5EE+10 5.00E+00 3.15E-05 0.00E+00 1 1.0E+01 2.8EE+10 3.8EE+01 5.1EE-10 2.5EE+10 5.00E+00 3.1EE-05 0.00E+00 3.1EE-05 0.00E+00 3.1EE-05 0.00E+00 3.1EE-05 0.00E+00 3.1EE-05 0.00E+00 3.1EE-05 0.00E+00 3.1EE-05 0.00E+00 4.2EE-05 0.00E+00 3.1EE-05 0.00E+00 4.2EE-05 0.00E+00 4				i	i											*****					.,					
65 Down-dip 1 1 4 7 0.00E+00 3.15E+05 0.00E+00 1.10E+01 8.83E-15 1.41E-01 3.58E-14 7.89E+00 3.31E-08 0.00E+00 1 3.31E-08 0.00E+00 1 3.31E-08 0.00E+00 1 3.31E-08 0.00E+00 1 3.31E-08 0.00E+00 1.00E+00 1 3.31E-08 0.00E+00 1 3.31E-08 0.00E+00 1 3.31E-08 0.00E+00 1 3.31E-08 0.00E+00 1 3.31E-08 0.00E+00 1 3.31E-08 0.00E+00 1.00E+00 1 3.31E-08 0.00E+00 1 3.31E-08 0.00E+00 1 3.31E-08 0.00E+00 1 3.31E-08 0.00E+00 1 3.31E-08 0.00E+00 1 3.31E-08 0.00E+00 1 3.31E-08 0.00E+00 1 3.31E-08 0.00E+00 1 3.31E-08 0.00E+00 1.00E+00 1 3.31E-08 0.00E+00 1 3.31E-08 0.00E+00 1 3.31E-08 0.00E+00 1 3.31E-08 0.00E+00 1 3.31E-08 0.00E+00 1.30E+01 4.00E+00 1.30E+01 4.00E+00 1.30E+01 4.00E+00 1.30E+01 4.00E+00 1.30E+01 4.00E+00 1.30E+01 4.00E+00 1.30E+01 4.00E+00 1.30E+01 4.00E+00 1.30E+01 4.00E+00 1.30E+01 4.00E+00 1.30E+01 4.00E+00 1.30E+01 4.00E+01 4.00E+00 1.30E+01 4.00E+00 1.30E+01 4.00E+00 1.30E+01 4.00E+01 4.00E+00 1.30E+01 4.00E+01 4.00E+00 1.30E+01 4.00E+00 1.30E+01 4.00E+00 1.30E+01 4.00E+0				1	1		0.00E+00	4.19E+05	0.00E+00	1.10E+01	2.82E-10	3.82E+00	5.11E-10													
66 Down-dip 1 1 38 0.00E+00 2.25E+06 0.00E+00 1.10E+01 4.29E+05 7.4E=02 1.68E+04 4.89E+01 5.58E+02 0.00E+00 2.21E+02 9.56E+04 5.34E+01 5.76E+01 9.16E+06 7.09E+01 1.2E±07 8.22E+06 8.50E+04 1.56E±04 6.00E+00 1.10E+01 4.29E+05 7.4E±04 6.00E+00 1.10E+01 4.29E+05 7.4E±04 6.00E+00 1.10E+01 4.29E+05 7.4E±04 6.00E+00 1.10E+01 4.29E+05 7.4E±04 6.00E+00 1.10E+01 4.29E+05 7.4E±04 6.00E+00 1.10E+01 4.29E+05 7.4E±04 6.00E+00 1.10E+01 4.29E+05 7.4E±04 6.00E+00 1.10E+01 4.29E±05 7.4E±04 6.00E+00 1.10E+01 4.29E±05 7.4E±04 6.00E+00 1.10E+01 4.29E±05 7.4E±04 6.00E+00 1.10E+01 4.29E±05 7.4E±04 6.00E+00 1.10E+01 4.29E±05 7.4E±04 6.00E+00 1.10E+01 4.29E±05 7.4E±04 6.00E+00 1.10E+01 4.29E±05 7.4E±04 6.00E+00 1.10E+01 4.29E±05 7.4E±04 6.00E+00 1.20E±07 7.4E±05 7.20E±06 7.				1	1									7.69E+00	3.31E-08	0.00E+00	4.29E+02	3.88E+05	1.29E-08	1.21E-08	2.40E+06	1.63E-01				
98 Down-dip 1 1 6 9 0.006+00 3.48E+05 0.00E+00 1.10E+01 3.47E+05 6.45E+02 7.88E+06 1.72E+04 1	,			1	1							7.24E-02												8.22E-06	8.50E+04	1.56E+04
69 Down-dip 1 1 22 0.00E+00 7.50E+06 0.00E+00 2.88E+00 1.3EE+04 1.5EE+04 3.21E-07 4.32E+08 0.00E+00 9.80E+04 1.2EE+07 3.4EE+01 3.24E+01 3.24E+01 3.24E+01 3.24E+01 3.24E+01 3.24E+01 1.2EE+07 3.4EE+04 4.2EE+04 1.2EE+07 3.4EE+04 4.2EE+04 1.2EE+07 3.4EE+04 4.2EE+04 1.2EE+07 3.4EE+04 4.2EE+04 1.2EE+07 3.4EE+04 4.2EE+04 1.2EE+07 3.4EE+04 4.2EE+04 1.2EE+07 3.4EE+04 4.2EE+04 1.2EE+07 3.4EE+04 4.2EE+04 1.2EE+07 3.4EE+04 4.2EE+04 1.2EE+07 3.4EE+04 4.2EE+04 1.2EE+07 3.4EE+04 4.2EE+04 1.2EE+07 3.4EE+04 4.2EE+04 1.2EE+07 3.4EE+04 4.2EE+04 1.2EE+07 3.4EE+04 4.2EE+04 1.2EE+07 3.4EE+04 4.2EE+04 1.2EE+07 3.4EE+04 4.2EE+04 1.2EE+07 3.4EE+04 4.2EE+04 4.				i	;																					
70 Own-dip 1 1 94 0.00E+00 7.99E+06 0.00E+00 2.88E+00 1.16E-04 3.21E-07 3.18E-04 4.20E+07 0.00E+00 0.00E+00 1 1 24 0.00E+00 8.00E+00 8.00E+00 0.00E+00 1 2.88E+00 1.20E+07 1.50E-01 8.78E+04 4.40E+04 0.00E+00 9.60E+05 1.20E+07 9.32E+01 1.20E+07 9.3		Оом	m-dip	1	1	22	0.00E+00	7.50E+08	0.00E+00	2.88E+00	1.36E-04	7.67E-03	1.99E-04													
70 Down-dip 1 1 28 0.00E+00 3.88E+05 0.00E+00 1.28E+00 1.28E+00 1.28E+00 1.28E+00 1.5EE+00 1.5EE+00 1.16E+00 9.60E+00 9.				1	1									3.21E-07		0.00E+00	9.80E-04	7.74E-02	3,34E+01	3.27E+01						
73 Down-dip 1 1 28 0.00E+00 5.14E+05 0.00E+00 1.10E+01 2.93E+05 2.01E+00 6.54E+05 0.00E+00 1.55E+07 1.25E+07 1.				1	1																			3.19E-02		
74 Down-dip 1 1 7 0.00E-00 3.85E-05 0.00E-00 1.10E-01 2.77E-05 1.28E-00 3.36E-05 4.54E-00 1.87E-01 0.00E-00 3.75E-03 1.38E-06 2.59E-01 2.51E-01 8.99E-06 6.20E-01 1.28E-07 3.12E-02 9.03E-04 1.68E-04				i	i		0.002.77																			
				1	1	7 .	0.00€+00	3.85E+05	0.00E+00	1.10E+01			3.36E-05	4.54E+00	1.87E+01	0.00E+00	3.75E+03									
	75	Dov	vn-dlp	1	1	64	0.00E+00	6.36E+05	0.00E+00	1.10E+01	1.39E-05	8,49E-02	5.62E-05	8.70E-01	1.42E+02	0.00E+00	2.59E+02				6.18E+06					

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					Excavated Waste										Saft Pillar			-									
		•	•	•	Porosity	Set (hactor)	Residual Brine Set. (fraction)	Crushed Panel Height (m)	Up-dip Avg Presture (Pa)	Up-dip Avg Sel. (haction)	Down-dip Avg Pressure (Pa)	Down-dip Avg. Sat. (fraction)	DPIZ Perceity (Fraction)	Permeability	Selt Piller Porosity	Sall Piller Permeability	Intrusion Time (Years)	Skin factor	Well Productivity	BC well Sand Permeability	Total Area zolića relazans	Casille Reservoir	Castile Reservoir	Up-tāp Brins Flatative	Up-dip Gas Relativa	Down-dip Brims Relative	Down-dep Class Field tive
l	_				(fraction)									(m^2)	(Fraction)	(m^2)	(Years)		index (1/Pa)	(m^2)	(m/2)	Pressure (Pa)	Permeability (m²2)	Permeebility	Permeability	Permeability (fraction)	Permeability
76 Down		іеріс,	Scen.	Vector	POROSITY 5.26E-01	SAT_RGAS	SAT_RBRN 1.61F-02	HEIGHT	9.76E+06	BSATPAN2	PRESPAN4	BSATPAN4		PEAM_X	POROSITY	PERM_X	NTR_TME	SKIN	WELLPI	PRM_SAND	AREA_101	CAST_RE	PRM_CAST	KRW2	KRG2	KRW4	KBG4
77 Down	n-dip	i	1	30	5.56E-01	1.16E-01	4.16E-02	1.35E+00	1.21E+07		9.79E+06	8.80E-01 4.87E-01	1.28E-01 3.63E-02	1.18E-13 2.75E-14	1.36E-01 4.11E-02	1.18E-13 2,75E-14	1.00E+04	-1,17E+00 6,49E-01	1.21E-13	0.00E+00	7.83E-01	1.45E+07	1.00E-12	0.00E+00	1.00E+00	6.45E-01	0.00E+00
78 Down		1	1	100	5.04E-01	1.14E-01	3.43E-01	1.21E+00	8.72E+06	4.23E-02	8.73E+D6	6.62E-01	6.98E-02	9.12E-16	8.97E-02	9.12E-16	1.00E+04	1.26E+00	1.07E-13	0.00E+00 0.00E+00	2.79E-01 9.43E-01	1.47E+07 1.40E+07	1.00E-12 1.00E-12	5.53E-15 0.00E+00	1.00E+00 1.00E+00	4.97E-02	1.68E-01
79 Down 80 Down		i	i	91	4.93E-01 5.73E-01	9.81E-02 5.46E-02	2,56E-01 3,06E-01	1.18E+00 1.41E+00	8.30E+06 1.35E+07	1.19E-02 2.98E-06	8.31E+06 1.36E+07	7.57E-01	6.92E-02	7.24E-16	9.28E-02	7.24E-16	1.00E+04	-1.28E+00	1.18E-13	0.00E+00	9.73E-01	1.41E+07	1.00E-12	0.00E+00	1.00E+00	6.90E-02 2.32E-01	1.02E-01 1.77E-02
B1 Down		i	i	86	5.37E-01	6.86E-02	3.61E-02	1.30E+00	1.06E+07	3.12E-05	1.06E+07	5.69E-01 4.16E-01	1.90E-01 1.54E-01	6.86E-15 3.02E-17	1.89E-01 1.65E-01	5.01E-15 3.02E-17	1.00E+04	-7.73E-01	1.16E-13	0.00E+00	3.57E-01	1.25E+07	1.00E-12	0.00E+00	1.00E+00	2.78E-02	2.70E-01
82 Down		1	1	17	5.69E-01	1.41E-02	2.26E-01	1.39E+00	1.31E+07	1.43E-06	1.31E+07	4.86E-01	1.67E-01	3.90E-14	1.48E-01	5.37E-15	1.00E+04 1.00E+04	-1.26E+00 -1.03E+00	1.28E-13 1.26E-13	0.00E+00 0.00E+00	9.43E-01 5.93F-01	1.22E+07 1.51E+07	1.00E-12 1.00E-12	0.00E+00	1.00E+00	3.22E-02	2.54E-01
B3 Down B4 Down		1	1	63 55	5.31E-01 5.58E-01	1.14E-01 7.03E-02	1,70E-01 2,38E-01	1.28E+00 1.36E+00	1.01E+07	1.07E-06	1.01E+07	4.50E-01	5.64E-02	2.14E-14	6.67E-02	2.14E-14	1.00E+04	-1.01E+00	1.15E-13	0.00E+00	5.75E-01	1.31E+07	1.00E-12	0.00E+00 0.00E+00	1.00E+00 1.00E+00	1.78E-02 1.82E-02	3.63E-01 2.95E-01
85 Down		i	i	79	5.77E-01	1.23E-01	3.88E-01	1.42E+00	1.23E+07 1.39E+07	6.80E-06 8.94E-07	1.23E+07 1.39E+07	4.84E-01 5.13E-01	9.90E-02 1.79E-01	8.71E-15 3.69E-13	1.00E-01 1.75E-01	8.71E-15 2.57E-13	1.00E+04	-B.68E-01	1.16E-13	0.00E+00	4.31E-01	1.28E+07	1.00E-12	0.00E+00	1.00E+00	1.54E-02	3.43E-01
86 Down		1	1	48	4.88E-01	1.02E-01	2.11E-01	1.17E+00	8.15E+06	3.46E-06	8.16E+06	4.32E-01	4.74E-02	7.78E-14	6.53E-02	7.76E-14	1.00E+04 1.00E+04	-1.10E+00 -1.29E+00	1.32E-13 1.16E-13	0.00E+00 0.00E+00	6.89E-01	1.31E+07	1.00E-12	0.06E+00	1.00E+00	2.87E-03	4.98E-01
87 Down		1	1	78 26	5.29E-01 5.86E-01	4.93E-02	1.51E-01	1.28E+00	1.00E+07	1.04E-05		3.75E-01	1.09E-01	2.46E-15	1.18E-01	2.46E-15		-1.06E+00	1.17E-13	0.00E+00	1.01E+00 6.28E-01	1.16E+07 1.61E+07	1.00E-12 1.00E-12	0.00E+00 0.00E+00	1.00E+00 1.00E+00	9.15E-03 7.27E-03	3.92E-01 4.59E-01
89 Down		i	i	73	5.65E-01	7.60E-02 5.61E-02	4.97E-01 3.03E-01	1.45E+00 1.38E+00	1.46E+07 1.29E+07	7.81E-06 3.22E-06	1.46E+07 1.29E+07	5.74E-01 4.47E-01	1.84E-01 9.71E-02	5.40E-14	1.76E-01	2.00E-14			1.48E-13	0.00E+00	1.10E+00	1.19E+07	1.00E-12	0.00E+00	1.00E+00	1.01E-03	6.32E-01
90 Down		t	1	2	5.67E-01	8.22E-02	4.02E-01	1.39E+00	1.30E+07	4.11E-06	1.30E+07	4.77E-01	1.73E-01	3.72E-16 1.15E-13	1.02E-01 1.63E-01	3.72E-16 4.47E-14	1.00E+04 1.00E+04	-8.01E-01 -1.29E+00	1.15E-13 1.39E-13	0.00E+00	3.77E-01	1.39E+07	1.00E-12	0.00E+00	1.00E+00	2.99E-03	5,52E-01
91 Down		1	1	41	5.24E-01	3.40E-02	8.64E-02			B.44E-03		2.41E-01	1.44E-01	1.70E-19	1.54E-01	1.70E-19	1.00E+04	-1.22E+00	1.23E-13	0.00E+00	9.98E-01 8.64E-01	1.41E+07 1.51E+07	1.00E-12 1.00E-12	0.00E+00 0.00E+00	1.00E+00 1.00E+00	4.77E-04 1.42F-03	7.01E-01
92 DOWN	·	1	;	53	5.39E-01 5.51F-01	4.46E-02 7.06E-02	2.52E-01 1.02E-01	1.30E+00 1.34E+00	1.07E+07 1.17E+07	1.21E-04 2.38F-07		3.30E-01 1.64E-01	1.54E-01	8.51E-18	1.70E-01	8.51E-18		-1.23E+00	1.27E-13	0.00E+00	8.92E-01	1.42E+07	1.00E-12	0.00E+00	1.00E+00	2.33E-04	6.43E-01 7.73E-01
94 Down	-dip	1	1	5	5.38E-01	1.29E-01	1.21E-01	1.30E+00	1.06E+07	8.68E-06	1.17E+07	1.79E-01	3,50E-02 1,34E-01	1.78E-13 1.82E-17	4.34E-02 1.45E-01	1.78E-13 1.82E-17	1.00E+04 1.00E+04	-1.38E+00 -1.37E+00	1.39E-13 1.35E-13	0.00E+00	1.19E+00	1.44E+07	1.00E-12	0.00E+00	1.00E+00	5.29E-05	8.44E-01
95 Down		1	1	40	5.67E-01	1.02E-01	3.54E-01	1.39E+00	1.30E+07	8.35E-07		3.81E-01	1.53E-01	6.91E-13	1.32E-01	1.51E-13		-1.32E+00	1.41E-13	0.00E+00 0.00E+00	1.17E+00 1.07E+00	1.57E+07 1.47E+07	1.00E-12 1.00E-12	0.00E+00	1.00E+00	4.43E-05	8.40E-01
96 Down		1	1	60 22	5.55E-01 5.70F-01	6.13E-02 2.51F-02	4,70E-02 8 22E-02	1.35E+00 1.40E+00	1.20E+07	1.86E-04		6.73E-02	1.92E-01	7.83E-18	1.91E-01	5.75E-18	1.00E+04	-1.17E+00	1.29E-13	0.00E+00	7.91E-01	1.35E+07	1.00E-12	0.00E+00 0.00E+00	1.00E+00 1.00E+00	8.17F-06 6.64E-07	8.98E-01 9.54E-01
98 Down		i	Ş	79	5.63E-01	1.23E-01	3.88E-01		9.43E+06 8.97E+06	9.12E-01 6.30E-01	9.42E+06 8.98E+06	6.34E-01 6.96E-01	1.21E-01 1.61E-01	7 41E-14 2.57E-13	1.33E-01 1.81E-01	7.41E-14 2.57E-13	5.50E+02	-1.37E+00	1.45E-13	1.74E-13	1.17E+00	1.30E+07	1.59E-12	6.90E-01	5.75E-04	1.52E-01	8.15E-02
99 Down		1	2	36	5.B1E-01	3.71E-03	1.39E-01	1.43E+00	1.03E+07	1.18E-02		6.96E-01	3,90E-02	7.03E-20	4.96E-02	8.61E-20	5.50E+02 5.50E+02	-1.10E+00 -8.89E-01	1.28E-13 1.23E-13	1.51E-16 8.13E-15	6.89E-01 4.50E-01	1.22E+07 1.36E+07	4.37E-15 1.45E-13	3.23E-02	1.78E-01	7.91E-02	7.45E-02
100 Down		1	2	69 46	5.87E-01 5.51E-01	8.98E-02 2.03E-02	4.08E-01 2.35E-01	1.45E+00 1.34E+00	1.08E+07 7.38E+06	9.22E-01		7.13E-01	6.98E-02	1.26E-14	7.91E-02	1.26E-14	5.50€+02	-1.29E+00	1.46E-13	9.33E-15	9.99E-01	1.42E+07	1.45E-13 4.07E-13	0.00E+00 5.94E-01	1.00E+00 0.00E+00	2.00E-01 8.62E-02	6.35E-02 8.81E-02
102 Down		i	2	54	5.27E-01	1.25E-01	2.39E-02	1.34E+00	7.38E+06 5.69E+06	4.65E-02 8.46E-06		9.66E-01 8.48E-01	3.75E-02 2.59E-02	1.59E-17 5.01E-18	5.94E-02 4.98E-02	1.59E-17 2.57E-18		-1.41E+00	1.42E-13	1.45E-14	1.26E+00	1.50E+07	1.15E-11	0.00€+00	1.00E+00	8.46E-01	1.02E-05
103 Down		1	2	5 [5.35E-01	1.29E-01	1.21E-01	1.30E+00	6.19E+06	8.90E-02		8.53E-01	1.17E-01	1.91E-17	1.45E-01	1.82E-17		-1.16E+00 -1.37E+00	1.22E-13 1.35E-13	4.68E-12 1.82E-12	7.76E-01 1.17E+00	1.55E+07 1.53E+07	1.66E-12	0.00E+00	1.00E+00	5.35E-01	5.50E-05
104 Down 105 Down		1	2	31 16	5.82E-01 5.12E-01	5.28E-02 5.75E-02		1.44E+00 1.25E+00	1.03E+07	1.31E-01			6.71E-02	1.66E-15	B.12E-02	1.66E-15	5.50E+02	-1.27E+00	1.43E-13	3.31E-14	9.73E-01	1.53E+07 1.40E+07	3.31E-13 6.31E-13	0.00E+00 7.44E-05		5.09E-01 7.81E-01	2.16E-05 1.29E-06
106 Down		i	2	78	5.12E-01 5.84E-01	5.75E-02 4.93F-02	2.76E-01 1.51E-01	1.25E+00 1.44E+00	4.92E+06 1.04E+07	1.62E-02 9.44E-01				2.24E-19	1.25E-01	2.14E-19		-1.29E+00	1.25E-13	1.91E-14	1.01E+00	1.52E+07	1.86E-12	0.00E+00	1.00E+00	6.45E-01	7.46E-05
107 Down		1	2	41	5.14E-01	3.40E-02	8.64E-02		5.10E+06	8.43E-02		9.41E-01	1.27E-01	2.46E-15 1.70E-18	1,04E-01 1,56E-01	2.46E-15 1.70E-19		-1.06E+00 -1.22E+00	1.32E-13 1.21E-13	8.32E-17 3.24E-16	6.28E-01	1.40E+07	1.07E-12	7.79E-01	7.96E-07	7.78E-01	R 42E-07
108 Down		:	2	52	5.73E-01	3.68E-02				9.60E-01			9.67E-02	1.70E-15	1.17E-01	1.70E-15		-9.48E-01	1.24E-13	4.17E-14	8.84E-01 5.07E-01	1.47E+07 1.43E+07	3.47E-12 2.63E-13	0.00E+00 7.57E-01	1.00E+00 4.27E-07	7.82E-01 7.56E-01	3.80E-05 4.64E-07
109 Down		1	2	43 23	4.90E-01 5.44E-01	5.88E-02 7.29E-02	2.07E-01 4.80E-01		3.82E+06 6.80E+06	5.43E-02 6.39E-02			1.51E-01 2.53E-02	2.87E-19	1.97E-01	9.77E-20	6.60E+02	-1.26E+00	1.19E-13	3.63E-13	9.52E-01	1.49E+07		0.00E+00	1.00E+00	6.64E-01	6 24E-05
111 Down		1	2	45	5.72E-01	5.05E-02	2.04E-01		9.55E+06	9.85E-01			6.78E-02	1.18E-16 5.13E-14	4.60E-02 8.12E-02	1.18E-16 5.13E-14	5.50E+02 5.50E+02	-1.18E+00 -9.31E-01	1.27E-13 1.22E-13	7.94E-17 1.74E-15	8.09E-01	1.50E+07	6.03E-13	0.00E+00		5.52E-01	1.61E-06
112 Down		1	2	72	5.37E-01	2.36E-02	4.74E-03	1.30E+00	6.48E+06	1.61E-05	1.07E+07	9.38E-01	5.21E-02	4.62E-18	7.87E-02	1.82E-18		-8.26E-01	1.02E-13	6.37E-12	4.89E-01 2.66E-01	1.32E+07 1.43E+07	4.57E-13	9.30E+01 0.00E+00		9.27E-01 7.90E-01	0.00E+00 9.93E-05
113 Down		1	2	81 42	5.66E-01 5.92E-01	1.05E-02 1.04E-01	4.73E-01 3.92E-01		9.10E+06 1.12E+07	6.48E-02 7.95E-02		8.69E-01 8.20E-01		2.31E-18	7.61E-02	1.00E-18		-1.37E+00	1.44E-13	2.51E-12	1.19E+00	1.31E+07	8.91E-11	0.00E+00		3.48E-01	1.97E-02
115 Down		1	2	44	5.69E-01	1.12E-01	1.61E-02			8.84E-01		8.84E-01	1.08E-01 1.15E-01	7.76E-17 1.18E-13	1.09E-01 1.23E-01	7.76E-17 1.18E-13		-1.26E+00 -1.17E+00	1.46E-13	1.38E-15	9.46E-01		3.63E-13	0.00E+00		2.74E-01	5.41E-03
116 Down		1	2	14	4.66E-01		3.28E-01			2,73E-01	1.11E+07	8.96E-01	1.14E-01	6.31E-19	1.57E-01	6.31E-19	-,,	-7.31E-01	1.33E-13 9.35E-14	3.80E-15 8.32E-16	7.83E-01 3.28E-01	1.29E+07 1.47E+07	1.12E-12 2.63E-14	6.30E-01 0.00E+00	1.08E-07	6.31E-01 5.36E-01	1.05E-07 0.00E+00
117 Down 118 Down		1	2	6 80	4.53E-01 4.89E-01	6.58E-02 6.43E-02				2.74E-01 5.02E-02			4.92E-02	5.76E-19	8.97E-02	5.75E-19	5.50E+02	-1.18E+00	1.07E-13	6.46E-17	8.02E-01	1.38E+07	3.09E-12	9.29E-04	1.002100	7.04E-01	5.45E-06
119 Down	•	í	ž	73	5.58E-01	5.61E-02	3,03E-01			8.51E-02			3.21E-02 8.03E-02	1.59E-18 3.72E-16	6.10E-02 1.04E-01	5.01E-19 3.72E-16	5.50E+02 5.50E+02	-8.21E-01 -8.01E-01	9.97E-14 1.13E-13	2.09E-12	3.93E-01	1.40E+07	2.04E-13	0.00E+00	1.00E+00	6.37E-01	4.34E-05
120 Down-		1	2	68	5.25E-01			1.27E+00	5.87E+06	6.56E-07	1.02E+07	9.91E-01		9.12E-17	3.27E-02	9.12E-17		-0.01E-01	1.13E-13 1.29E-13	6.17E-15 4.57E-16	3.77E-01 1.06E+00	1.35E+07 1.38E+07	9.77E-12 3.02E-13	0.00E+00 0.00E+00	1.00E+00 1.00E+00	7.04E-01 9.32E-01	2.31E-06
121 Down-		1	2	53	5.61E-01 4.63E-01		3.12E-01 2.52E-01			9.90E-01 5.36E-01		9.90E-01	1.28E-01	2.29E-13	1.49E-01	2.29E-13	5.50E+02	-6.15E-01	1.07E-13	7.94E-14	2.60E-01	1.24E+07	1.35E-12	9.46E-01	9.52E-08	9.32E-01	9.26E-06
123 Down		i	2	34	5.33E-01		3.26E-01		6.42E+06	4.15E-02		9.43E-01 9.56E-01	1.41E-01 1.32E-02	9.23E-18 2.30F-17	1.94E-01 3.12E-02	8.51E-18 2.29E-17		-1.23E+00	1.11E-13	1.38E-12	6.92E-01		4.57E-12	2.81E-02	2.79E-01	7.46E-01	9.67E-06
124 Down		1	2	97	5.22E-01	8.37E-02	4.34E-01			9.12E-01		9.12E-01	1.32E-01	5.63E-16	1.66E-01	5.62E-16		-1.07E+00 -8.88E-01	1.19E-13 1.09E-13	7.00E-14 4.57E-13	6.47E-01 4.49E-01		4.68E-14 3.02E-11	0.00E+00 5.36E-01		7,80E-01 5,37E-01	2 65E-05 9 86E-07
125 Down-		1	2	25 60	5.66E-01 5.08E-01	8.88E-02 6.13E-02	5.41E-01 4.70E-02		8.87E+06 5.03E+06	1.07E-01 1.91E-01			6.60E-02	3.39E-17	7.74E-02		5.50E+02	-1.13E+00	1.30E-13	1.26E-16	7.23E-01			0.00E+00		4.31E-01	1.03E-05
127 Down-		i	2	21	4.77E-01	7.93E-02						9.09E-01 9.06E-01	1.78E-01 1.65E-01	6.10E-18 1.58E-19	2.10E-01 1.95E-01	6.75E-18 6.32E-20		-1.17E+00	1.17E-13	6.61E-13	7.91E-01		2.34E-14	9.25E-04		6.89E-01	6.52E-05
128 Down-		1	2	39	5.78E-01	1.50E-01			1.01E+07	B.47E-01		8.19E-01	1.49E-02	3.02E-15	2.68E-02			-1.54E+00 -1.23E+00	1.30E-13 1.39E-13	1.45E-13 2.40E-13	1.65E+00 6.82E-01		4.90E-13 1.78E-13	0.00E+00 4.03E-01		5.26E-01	4.28E-05
129 Down-		1	2	B2	5.67E-01 5.42E-01	8.52E-02 1.35E-01	4.53E-01 5.34E-01					9.11E-01		2.14E-15	1.27E-01		5.50E+02	-1.39E+00	1.45E-13	1.48E-12	1.22E+00			0.00E+00	3.76E-07 1.00E+00	3.33E-01 5.20E-01	2.92E-04 8.22E-07
131 Down-		i	5	57	4.59E-01	7.43E-02				3,93E-02 1,36E-01		8.53E-01 9.07E-01		2.36E-19 6.52E-18	2.75E-02 8.80E-02			-1.24E+00 -1.19E+00	1.29E-13	2.63E-15	9.00E-01	1.42E+07	4.90E-11	0.00E+00	1.00E+00	2.47E-01	7 93E-05
132 Down-		1	2	2	5.62E-01	8.22E-02	4.02E-01	1.37E+00	8.95E+06				1.51E-01	4.47E-14	1.65E-01			-1.19E+00 -1.29E+00	1.09E-13 1.37E-13	8.13E-12 5.01E-14	8.25E-01 9.96E-01	1.32E+07 1.24E+07	7.94E-14 7.24E-11	0.00E+00 5.71E-01	1.00E+00	6.00E-01	4.25E-05
133 Down-		1	2	76	5.15E-Q1 5.95E-01					2.25E-03				3.16E-18	5.20E-02	3.16E-18	5.50E+02	-1.33E+00	1.27E-13	5.50E-16	1.09E+00	1.33E+07	7.24E-11 2.09E-12	5.71E-01 0.00E+00		5.71E-01 3.82E-01	1.25E-07
135 Down-		í	2	51	6.10E-01	1.34E-01	3.63E-01			1.98E-01 4.24E-01		4.94E-01 5.63E-01	1.09E-01 1.75E-01	5.28E-17 2.36E-13	1.98E-01 1.62E-01			-1.08E+00	1.37E-13	9.55E-12	6.64E-01		9.55E-14	6.66E-07	9.51E-01	2 92E 02	2.41E-01
136 Down-	_	1	2	90	4.71E-Q1			1.15E+00	3,15E+06				9.19E-03		3.92E-02	1.20E-17			1.47E-13 9.74F-14	1,006-12 2,09E-14	7.77E-01 4.15E-01		6.92E-12 3.02E-12	1.67E-04 0.00E+00	7.53E-01 1.00E+00	1.40E-02	2.86E-01
137 Down- 138 Down-		1	2	70 65	5.01E-01										2.41E-01		5.50E+02	-1.28E+00	1.21E-13	1.00E-16	9.91E-01					8.65E-01 6.50E-01	1.52E-05 5 60E-05
139 Down-		i	2	13	5.62E-01 4.30E-01	1.27E-01 1.83E-02						8.65E-01 9.81E-01	1.63E-02 4.82E-02	8.71E-16 1.69E-18	2.86E-02				1.30E-13	4.17E-15	7.73E-01	1.26E+07	3.72E-12	0.00E+00		5.53E-01	1.95E-06
140 Down-		1	2	20	5.38E-01	1.23E-01	1.27E-01	1.30E+00	6.92E+06				1.44E-02		9.03E-02 3.57E-02	1.62E-18 1.35E-17		-1.31E+00 -6.04E-01	1.09E-13	1.23E-13 3.31E-15	1.03E+00 2.55E-01					8.68E-01	1.72E-08
141 Down- 142 Down-		1	2	1	5.12E-01 4.75E-01							9.58E-01	5.45E-02	7.24E-16	8.91E-02	7.24E-16	5.50E+02		1.23E-13	1.66E-14	9.73E-01		1.20E-12 7.08E-14			5.18E-01 8.05E-01	3.11E-05 0.00F+00
142 Down- 143 Down-		1	2	100	4.75E-01 5.28E-01										3.82E-02	4.90E-20			1.22E-13	2.95E-16	1.25E+00	1.26E+07	3.55E-11	6.72E-06		5.08E-01	3.20E-05
144 Down-	dip	1	2	95	5.28E-01	1.46E-01								9.12E-16 6.03E-17	9.53E-02 1.71E-01			-1.26E+00 -9.54E-01	1.26E-13 1.12E-13	2.51E-14 1.10E-16	9.43E-01 5.13E-01	1.25E+07 1.30E+07	1.29E-13				0.00E+00
145 Down-		1	2	67 50	4.93E-01	1.21E-01 1.09E-01					9.00E+06	8.49E-01	1.57E-01	3.55E-18	1.94E-01				1.19E-13	7.24E-15	9.65E-01	1.30E+07 1.26E+07	1.70E-11 1.15E-14	0.00E+00 3.08E-04		3 48E-01 5.21E-01	1.84E-05 8.85E-05
146 Down-		1	2	66	5.09E-01 5.26E-01	,,,,,,			5.11E+06 6.22E+06						2.31E-01	2.88E-19			1.22E-13	1.125-12	9.68E-01	1.29E+07	2.75E-13	0.00E+00		3.15E-01	9.83E-05
148 Down-		1	ž	94	5.76E-01	4.58E-03	1.85E-01							6.23E-18 6.31E-15	1.05E-01 1.96E-01				1.32E-13 1.42E-13	1.66E-12 9.77E-16	1.18E+00 9.95E-01		1.48E-14	0.00E+00		3.70E-01	6.50E-05
149 Down-	- ·	1	2								8.76E+06	9.16E-01	1.62E-01	3.85E-17	2.14E-01								1.78E-12 7.94E-12			1.57E-02 5.26E-01	3.85E-01 6.47E-06
150 Down-	иħ	•	2	3E	4.67E-01	1.00E-01	5.29E-01	1.14E+00	2.98E+06	3.79E-01	8.98E+06	B.96E-01	3.31E-02	1.10E-16	6.84E-02	1.10E-16	5.50E+02	-9.74E-01	1.01E-13							3.98E-01	1.74E-06

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Г						T	Down-dip																		
		•	•	•	•	Up-dip Flowing Bottom-hole	Flowing Bottom-hole	BC well Injection	Blowout Duration	Brine Rate	Gas Rate (ref	Max Brine	Max Gau Rate			y Ges Rate	Cum Gas	Com Brine	Cum Brine	Avg Brina Pressure	Avg Brind Saturation	Avg Brine	Avg Brine Seturation	Joint Excepted	Total
						Pressure (Pa)	Pressure (Pa)	Pressure (Pa) (Days)	(m/3/a)	m^3/a)	Rate (m^3/s)	(ref m*\3/a)	Ratio (ny^3/s / ref m^3/s)	Condition Wel	(macf/day)	Produced (re m^3)	f Produced (m/3)	Roleases (m°3)	Panel 5 (Pa)	Panel 5 (fraction) after	Pressure Panel 0 (Pa)	Panel 0	Waste Pore	Excevated Brine Volume
H	o. <u>)(</u>		Raplic	Scer	n. Vecto		FBHP4	BHP_ABAN		BRINEFLW	GASFLW	MAX BRN	MAX GAS		(-)	GAS_RATE	- OAROUIT		*7	aher Blowoul	blowout	after blowout	(fraction) site biowout	(fraction)	(m^G)
1 7		wn-dip wn-dip	1	1	30	0.00E+00 3.76E+05	8.00E+06 3.67E+05	0.00L+00		4.85E-05	1.44E-07	6.66E-05	1.44E-07	6.08E+08		4,38E-04	2.11E-02		1.24E+01		8.89E-01	BANPRESO	SATBRING	WASTE PY	- 10/_DIMI4
7		An-dip	ij	,	100	0.00E+00				9.86E-06 7.82E-06	4.59E-01	2.97E-05		1.92E+01	0.00E+00	1.40E+03	6.16E+05	1.18E+01			4.65E-01	9.76E+06 1.17E+07	2.23E-06 4,18E-02		
7	9 Dox	wn-dip	1	i	1	0.00E+00				2.54E-05	7.07E-02 2.62E-02	3.32E-05 6.69E-05	9.39E-01 9.36E-02	8.79E+01 9.17E+02					9.57E+00		6.62E-01	8.71E+06	4.28E-02		
8		Mn-dip	1	1	91	0.00E+00			1,10E+01	4.87E-06	3.68E-01	2.03E-05	6.72E+00	9.72E+00			8.26E+03 6.36E+05				7.56E-01	6.30E+06	4.07E-02	6.55E+04	1.58E+04
1 8	,	vn-dip vn-din	!	1	86 17	0.00E+00				4.00E-06	1.81E-01	2.03E-05	3.69E+00	1.61E+01	0.00E+00	5.53E+02	3.31E+05				5.70E-01 4.16E-01	1.35E+07	3.06E-06		
B		vn-dfp	ì	i	63	0.00E+00	3.26E+05 2.66E+05	0.00E+00 0.00E+00	1.10E+01 1.10E+01	4.05E-06 2.86E-06	8,26E-01 3,85E-01	1.37E-05	7.87E+00	4.29E+00		2.52E+03	1.07E+06		4.49E+00		4.86E-01	1.06E+07 1.27E+07	5.40E-03 1.46E-08		
8		vn-dip	1	- 1	55	0.00E+00	3.06E+05	0.00E+00	1.10E+01	2.39E-08	3.85E-01 3.86E-01	9.83E-06 1.02E-05	3.53E+00 6.02E+00	6.17E+00 4.59E+00	0.00E+00	1.18E+03			3.25E+00	4.75E+06	4.51E-01	9.86E+06	1.07E-06		
8		vn-dlp	1	1	79	0.00E+00	3.34E+05	0.00E+00	1.10E+01	2.30E-06	2.79E+00	2.45E-06	1.26E+01	5.46E-01	0.00E+00 0.00E+00	1.18E+03 8.51E+03	6.60E+05 3.46E+06				4.85E-01	1.21E+07	6.87E-06	8.52E+04	1.07E+04
8		vπ-dip vπ-dio	1	1	48 78	0.00E+00	2.17E+05		1.10E+01	1.48E+06	5.09E-01	4.08E-06	3.15E+00	2.56E+00	0.00E+00	1.55E+03			1.70E+00 1.69E+00	8.08E+06 4.01E+08	5.17E-01 4.33E-01	1.15E+07	8.94E-07	9.19E+04	
a		m-dio	1	1	26	0.00E+00	2.52E+05 3.62E+05	0.00E+00 0.00E+00	1.10E+01 1.10E+01	7.69E-07 6.58E-07	2.42E-01 1.26E+00	3.95E-06	5.46E+00	2.15E+00	0.00E+00	7.39E+02	4.91E+05	1.06E+00	1,04E+00	4.01E+06	3.75E-01	7.57E+06 9.97E+06	3.43E-06 1.05E-05	6.44E+04 7.57E+04	
89		m-dip	1	1	73	0.00E+00	3.12E+05	0.00E+00	1.10E+01	2.70E-07	2.10E-01	1.02E-06 2.06E-06	1.98E+01 1.05E+01	2.98E-01 7.02E-01	0.00E+00 0.00E+00	3.84E+03	1.68E+06	5.02E-01	4.73E-01	6.31E+06	5.79E-01	1.39E+07	8.02E-06	9.55E+04	1.43E+04
90		m-dip	1	1	2		3.35E+05	0.00E+00	1.10E+01	1.83E-07	1.85E+00	4.03E-07	1.66E+01	7.43E-02	0.00E+00	5.64E+03	6.22E+05 2.33E+06		4.23E-01	3.62E+06	4.48E-01	1.28E+07	1.88E-05	8.76E+04	1.02E+04
9		vn-dip vn-dip	1	1	41 53		2.53E+05 2.93E+05		1.10E+01	9.36E-08	1.32E-01	7.08E-07	7.60E+00	3.83E-01	0.00E+00	4.02E+02			1.71E-01 1.51E-01	6.16E+06 2.79E+06	4.79E-01 2.42E-01	1.17E+07 9.63E+06	4.22E-06 8.44E-03		
9:	,	m-din	i	i	12	0.00E+00		0.00E+00 0.00E+00	1.10E+01	1.68E-08 1.45E-08	1.75E-01	1.48E-07	1.15E+01	5.32E-02	0.00E+00	5.35E+02			2.60E-02	2.86E+06	3.30E-01	1.07E+07	2.64E-03	7.42E+04 7.87E+04	5.10E+03 6.87E+03
94		m-dip	i	1	5		3.11E+05		1.10E+01	3.64E-09	2.26E+00 2.38E-01	3.99E-08 2.94E-08	1.61E+01 1.29E+01	5.14E-03 8.98E-03	0.00E+00	6.90E+03	3.32E+06		1.68E-02	4.97E+06	1.65E-01	8.40E+06	2.38E-07		3.52E+03
98		w-qib	1	1	40	0,00E+00	3.90E+05	0.00E+00	1.10E+01	3.44E-09	3.69E+00	6.92E-09	2.12E+01	7.16E-04	0.00E+00 0.00E+00	7.25E+02 1.13E+04	8.20E+05 5.21E+08		5.48E-03		1.79E-01	1.06E+07	2.65E-05	7.83E+04	3.63E+03
96		m-dlp m-dlo	1	1	55 60		3.89E+05 3.90E+05	0.00E+00	1.10E+01	6.36E-11	2.81E-01	4.74E-10	1.76E+01	1.06E-04	0.00E+00	B.56E+02	8.12E+05		3.65E-03 8.19E-05	8.48E+06 3.22E+08	3.82E-01 6.74E-02	8.95E+08 1.20E+07	8.35E-07 1.52E-03	8.81E+04	8.71E+03
98		m-dio	i	2	79	2.70E+05	8.77E+05	9.74E+06 1.63E+06	1.10E+01 1.10E+01	3.46E-05 3.61E-05	2.12E-01	9.50E-05	1.05E+00	1.42E+02	1.21E-04	6.47E+02	2.92E+05	4.14E+01	3.96E+01	5.87E+06	6.44E-01	9.37E+06	5.50E-01	8.40E+04 8.93E+04	
99	Dow	n-dip	1	2	36		3.60E+05	8.15E+06	1.10E+01	2.59E-05	1.69E-01 6.92E-02	4.16E-05 1.14E-04	7.26E-01 7.93E-01	1.84E+02 3.08E+02	0.00E+00 4.65E-05	5.14E+02			3.49E+01	6.80E+06	7.08E-01	B.94E+08	5.05E-01	8.68E+04	
10		n-dép	1	2	69		3.29E+05	1.01E+07	1.10E+01	2.40E-05	1.23E-01	6.20E-05	1.47E+00	1.40E+02	9.15E-05	2.11E+02 3.76E+02			3.46E+01 2.45E+01	5.89E+06	7.03E-01	1.03E+07	1.18E-02	9.34E+04	1.86E+04
10.		n-dip n-dip	1	2	46 54		8.04E+06	1.20E+07	2.88E+00	5.75E-05	5.64E-05	1.93E-04	6.92E-05	1.19E+06	1.44E-05	1.72E-01	1.52E+01		1.77E+01	6.51E+06 1.10E+07	7.29E-01 9.66E-01	1.07E+07 7.38E+06	9.16E-01	9.58E+04	
100		n-dip	i	2	5	0.00E+00	8.04E+06 8.04E+06	1.24E+07 1.18E+07	2.88E+00 2.88E+00	5.17E-05 4.94E-05	7.81E-04	1.20E-04	8.12E-04	8.88E+04	9.17E-06	2.38E+00	1.85E+02		1.61E+01	1.18E+07	8.50E-01	5.69E+06	4.66E-02 8.62E-06	8.31E+04 7.58E+04	2.82E+04 2.34E+04
10		n-dip	1	2	31	2.97E+05		1.09E+07	2.88E+00	5.20E-05	5.89E-04 1.61E-05	1.19E-04 1.30E-04	5.99E-04 1.61E-05	1.22E+05 4.16E+06	2.77E-06	1.80E+00	1.31E+02	1.59E+01	1.56E+01	1.15E+07	8.55E-01	6.19E+06	8.92E-02	7.81E+04	
10		n-dip	1	2	16	0.00E+00	8.04E+06	1.21E+07	2.88E+00	4.89E-05	4.93E-04	1.36E-04	5.85E-04	1.16E+05	9.29E-06 9.36E-06	4.90E-02 1.51E+00	3.72E+00 1.33E+02	1.55E+01 1.54E+01	1.52E+01	1.03E+07	9.40E-01	1.03E+07	9.53E-02	9.40E+04	4.86E+04
100		n-dip	1	2	78 41		0.01E+08	1.10E+07	2.88E+00	5.22E-05	1.27E-05	1.21E-04	1.27E-05	5.29E+06	1.11E-05	3.88E-02	2.88E+00	1.52E+01	1.51E+01 1.49E+01	1.13E+07 1.03E+07	9.19E-01 9.45E-01	4.92E+06 1.04E+07	1.62E-02		
101		.,	1	2	52		8.04E+06 8.01E+06	1.17E+07 1.09E+07	2.88E+00 2.88E+00	4.85E-05 5.01E-05	1.45E-04 1.48E-05	1.38E-04		3.84E+05	1.10E-05	4.42E-01	3,93E+01	1.51E+01	1.48E+01	1.08E+07	9.41E-01	5.10E+08	9.44E-01 8.43E-02	9.45E+04 7.21E+04	8.92E+04 2.95E+04
	Dow	n-dĺp	1	2	43		_	1.20E+07	2.88E+00	4.65E-05	3.60E-04	1.21E-04 1.25E-04	1,48E-05 4.16E-04	4.43E+06 1.49E+05	4.31E-06 1.02E-05	4.51E-02	3.28E+00	1.45E+01	1.42E+01	1.05E+07	9.60E-01	9.34E+06	9.60E-01	9.06E+04	8.69E+04
	Dow		1	2	23		8.02E+06	1.18E+07	2.88E+00	4.45E-05	1.92E-04	1.15E-04	1.92E-04	3.45E+05	6.36E-06	1.10E+00 5.85E-01	9.58E+01 4.05E+01	1.43E+01 1.40E+01	1.40E+01 1.37E+01	1.11E+07 1.13E+07	9.17E-01	3.82E+06	5.44E-02	6.59E+04	2.78E+04
	Dow		1	2	45 72		8.00E+06 8.04E+06	1.00E+07	2.88E+00	5.14E-05	0.00E+00	8.68E-05	0.00E+00	1.40E+22	1.51E-05	0.00E+00	0.00E+00	1.40E+01	1.37E+01	9.45E+06	9.24E-01 9.84E-01	6.60E+06 9.53E+08	5.40E-02 9.84E-01	8.99E+04	3.15E+04
	Dow		i	ž	81		4.01E+08	1.11E+07 1.01E+07	2.88E+00 2.88E+00	4.17E-05 3.89E-05	2.01E-04 3.34E-02	1.02E-04 1.30E-04		2.26E+05	8.12E-06	6.14E-01	5.60E+01	1.26E+01	1.24E+01	1.05E+07	9.39E-01	6.48E+06	1.61E-05	7.84E+04	8.85E+04 2.20E+04
	Dow		1	2	42		6.22E+06	1.11E+07	2.88E+00	3.56E-05	1.70E-02	9.35E-05	1.51E-01 4.46E-02	1.12E+03 2.06E+03	3.01E-05 B.88E-08	1.02E+02 5.18E+01	1.08E+04	1.22E+01	1.19E+01	8.44E+06	8.72E-01	9.10E+06	6.48E-02	8.79E+04	2.53E+04
	Dow		1	2	44			9.89E+06	2.88E+00	4.15E-05	1.50E-06	6.61E-05		3.51E+07	1.70E-05	4.58E-03	5.33E+03 3.10E-01	1.10E+01 1.08E+01	1.08E+01 1.06E+01	1.08E+07 9.37E+06	8.24E-01	1.12E+07	7.96E-02	9.78E+04	2.78E+04
	Dow		1	2	14 6		8.00E+06 8.03E+06	9.56E+06	2.88E+00	3.33E-05	3.26E-05	7.45E-05	3.26E-05	2.06E+06	0.00E+00	9.98E-02	5.00E+00	1.02E+01	1.00E+01	1.10E+07	8.87E-01 8.97E-01	9.38E+06 2.60E+06	8.11E-01 2.08E-01	8.91E+04 6.02E+04	7.52E+04
	Dow		i	2	80		8.04E+06	1.09E+07 1.06E+07	2.88E+00 2.88E+00	3.02E-05 3.04E-05	3.33E-05 1.53E-04	8.00E-05 7.23E-05	3.36E-05	1.18E+06	9.22E-06	1.02E-01	7.95E+00	9.37E+00	9.19E+00	1.01E+07	9.24E-01	2.08E+06	2.12E-01	5.70E+04	3.28E+04 3.21E+04
119	Dow	n-dip	1	2	73	0.00E+00	8.02E+06	1.05E+07	2.88E+00	3.09E-05	1.57E-05	7.18E-05		2.42E+05 2.60E+06	2.78E-06 1.17E-05	4.66E-01 4.78E-02	3.87E+01	9.35E+00	9.17E+00	1.03E+07	9.17E-01	3.88E+06	5.02E-02	6.52E+04	2.62E+04
120	Don		1	2	68			1.05E+07	2.88E+00	2.97E-05	9.49E-06	1.23E-04		3.27E+08	1.17E-05	2.89E-02	3.58E+00 2.85E+00	9.28E+00 9.32E+00	9.09E+00	9.83E+06 9.63E+06	9.38E-01	8.28E+06	9.57E-02		3.39E+04
120	+ · · · · · · ·		1	2	7 53	7.99E+06 0.00E+00			2.88E+00 2.88E+00	3.49E-05	3.84E-08	4.34E-05		9.31E+08	2.05E-05	1.17E-04	9.54E-03	8.89E+00	8.67E+00	8.86E+06	9.90E-01 9.91E-01	5.87E+06 8.82E+06	6.82E-07 7.20E-01	7.49E+04 8.60E+04	2.64E+04 7.23E+04
123			i	2	34	0.00E+00		9.31E+06	2.88E+00	2.78E-05 2.78E-05		7.87E-05 7.81E-05		1.14E+06	9.72E-06	8.90E-02	7.51E+00	8.59E+00	8.42E+00	9.87E+06	9.44E-01	2.58E+06	4.27E-01	5.91E+04	4.00E+04
124			1	2	97	0.00E+00	8.01E+06		2.88E+00	2.80E-05		6.16E-05		7.37E+05 B.60E+05	0.00E+00 1.11E-05	1.29E-01 1.38E-01	1.17E+01 8.88E+00	8.58E+00 8.49E+00		9.59E+06	9.56E-01	6.42E+06	4.15E-02		2.60E+04
125 126		, and	1	2	25 60	0.00€+00			2.88E+00	2.60E-05		5.94E-05		1.99E+05	5.60E-06	5.89E-01	4.12E+01	8.19E+00	8.33E+00 B.04E+00	1.02E+07 1.02E+07	9.14E-01 9.08E-01	5,66E+06 8,87E+06	8.19E-01	7.41E+04	6.38E+04
127				2	21	0.00E+00 0.00E+00		8.82E+06 1.03E+07	2.88E+00 2.88E+00	2.32E-05		5.71E-05			0.00E+00	2.66E-01	2.40E+01	7.22E+00		9.42E+06	9.10E-01	5.03E+06	1.07E-01	8.80E+04 7.00E+04	3.00E+04 3.39E+04
128	Down	n-dip	1	2	39	8.01E+06	7.93E+06			2.17E-05 2.20E-05		5.86E-05 4.26E-05	1.72E-04 1.02E-03	1.74E+05 2.86E+04	6.78E-06 1.86E-06		4.02E+01	6.99E+00	6.86E+00	9.76E+06	9.08E-01	3.38E+06	5.71E-02	6.24E+04	2.46E+04
129			1	2	82	0.00E+00	8.01E+06	9.81E+06	2.88E+00	2.08E-05	1.37E-05	4.59E-05		2.25E+06	1.05E-05		2.39E+02 2.81E+00	6.82E+00 6.30E+00		9.81E+06 9.26E+06	8.24E-01	1.01E+07	8.47E-01	9.24E+04	7.76E+04
	Down		1	2	9 57	0.00E+00			2.88E+00	1.87E-05	9.06E-04	4.01E-05	9.81E-04	2.86E+04	9.47E-06		2.13E+02	6.08E+00	5.97E+00	9.26E+06 1.06E+07	9.13E-01 8.57E-01	9.21E+06 6.85E+06	1.39E-01 3.93E-02	8.82E+04 8.00E+04	4.39E+04
132			i	2	2				2.88E+00 2.88E+00	1.94E-05 2.26E-05		4.82E-05 3.43E-05				2.49E-01	2.12E+01	6.08E+00	5.96E+00	9.4BE+06	9.08E-01	2.50E+06	1,36E-01		2.29E+04 2.93E+04
133	Down	r-dip	1	2	76	0.00E+00	8.04E+06	1.03E+07	2.88E+00	1.85E-05				2.58E+07 1.19E+05	1.69E-05 9.36E-06		2.35E-01 4.94E+01	6.04E+00		8.91E+06	9.18E-01	8.94E+06	9.16E-01	8.66E+04	7.93E+04
134			1	2	28				1.10E+D1	4.18E-06	2.09E-01						3.87E+05		5.76E+00 5.51E+00	9.71E+06 5.26E+06	8.51E-01 5.09E-01	5.37E+06	2.27E-03	7.19E+04	1.95E+04
	Down		1	2	51 90				1.10E+01 2.88E+00	5.28E-06			6.79E+00	4.86E+00	2.66E+04	2.10E+03	1.19E+06			5.95E+06	5.09E-01 5.87E-01	1.15E+07 1.26E+07	1.96E-01 3.43E-01		2.74E+04 5.50E+04
137			1	2	70				2.88E+00	1.80E-05 1.66E-05		5.27E-05 4.48E-05		1.96E+06	1.00E-05		2.79E+00			9.22E+06	9.73E-01	3.15E+06	B.50E-02		2.80E+04
138	Down	⊬dip	1	2	65	0.00E+00	8.02E+06		2.88E+00	1.65E-05					0.00E+00 1.20E-05		1.62E+01			9.12E+06	9.38E-01	4.74E+06	1.77E-03	6.82E+04	2.11E+04
139			1	2	13				2.75E+00	1.62E-05	1.46E-07	5.82E-05			9.81E-06		1.63E+00 3.40E-02			B.98E+06 9.11E+06	8.69E-01 9.81E-01				2.32E+04
140	Down		1	2	20	0.00E+00 (2.88E+00	1.56E-05			4.88E-05	4.03E+05		1.49E-01	1.17E+01		4.60E+00		8.61E-01	1.17E+06 6.92E+06			3.40E+04 2.22E+04
142			i	2	В 1				2.88E+00 2.88E+00	1.56E-05 1.39E-05							0.00E+00	4.66E+00	4.56E+00	8.81E+06	9.58E-01	5.34E+06			6.71E+04
143			1	2	100	0.00E+00	B.00€+06		2.88E+00					3.72E+05 4.30E+21							8.38E-01	3.43E+06	4.54E-02	6.18E+04	2.24E+04
144	Down		1	2	95			1,00E+07	2.88E+00	1.40E-05	9.27E-05	2.57E-05							4.22E+00 4.19E+00			6.28E+06		7.54E+04	7.01E+04
146	Down		1	2	67 50				2.88E+00 2.88E+00	1.34E-05		2.87E-05	1.00E-04	1.826+05	0.00E+00	2.64E-01	2.31E+01					6.18E+06 4.36E+06			3.29E+04
147	Down		i	2	66			/		1.14E-05 9.35E-06		2.43E-05 2.06E-05				7.27E-01	5.90E+01	3.61E+00	3.55E+00	9.31E+06	8.81E-01	5.11E+06		7.01E+04	2.87E+04 1.96E+04
148	Down	-dip	1	2	94	8.00E+06	2.53E+05			2.22E-06						2.67E-01 9.45E+02				8.87E+06	8.96E-01	6.22E+06	2.64E-02	7.51E+04	2.07E+04
	Down		!	2	29			9.39E+06	2.88E+00	6.99E-06	8.40E-06	2.32E-05				2.56E-02		2.96E+00 2.85E+00	2.88E+00 2.79E+00	4.43E+06			B.10E-01	9.15E+04	6.89E+04
150	DOWN	⊢aib	•	Z	32	0.00E+00 8	8.02E+06	9.59E+06	2.88E+00	B.94E-06	1.09E-05	1.84E-05				3.31E-02		2.75E+00	2.69E+00						4.07E+04 3.44E+04
																						T00			U.770 E +U/0 1

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			**		Escavaled																		_				
	•	•	•	•	Waste Potosity	Residual Gas Sat. (Iraction)	Residuel Brine Sul. (fraction)	Crushed Panel Height (m)	Up dip Avg Pressure (Pe)	Up-dip Avg	Down-dip Avg Pressure (Pa)	Down-dip Avg	DRZ Parasity (Fitterion)	DRZ Permeability	Salt Pillur Porosity	Seit Pëter Permushësi	Intrusion Time	9kin factor	Well Productivity	BC wall Sand	Total Area	Castile I Reservoir	Castile Reservoir	Up-dip Brime Relative	Up-dep Gas Relativa	Cown-dip Brine Relative	Down-rijn Gas Retalive
١.,	10.	~ "	_		(kaction)									(m^2)	(Fraction)	{m'2}	(Years)	O-SIT IBECO	index (1/Pa)	(m*2)	(m/2)	Pressure (Pa)	Permeability	Penmeability (fraction)	Permeability (traction)	Permeebility	Permeability
151	Down-dip	Replic.	Scen.	Vector 77	FOROSITY 5.10F-01	SAT_RGAS	6.84E-02	HEIGHT	PRESPAN2	BSATPAN2	PRESPAN4 8.70E+06	BSATPAN4			POROSITY	РЕЯМ Х	INTR_TME		WELLPI	PRM_SAND	AREA_TOT	CAST_RE	PRM CAST	KRW2	(RG2	(fraction) KRW4	(faction) KRG4
1	Down-dip	1	2	99	5.41E-01	1.28E-01	5.15E-01	1.31E+00	7.26E+06	2.01E-01	8.92E+06	8.21E-01	1.87E-01 1.56E-01	9.13E-19 5.89E-17	2.24E-01 1.83E-01	8.13E-19 5.89E-17	5.50E+02 5.50E+02	-7.13E-01 -7.63E-01	9,95E-14 1,08E-13	2.75E-16	3.17E-01	1.23E+07	1.20E-11	0.00E+00	1.00E+00	4.55E-01	1.01E-04
	Down-dip Down-dip	1	2	88 71	5.21E-01 5.17E-01	1.19E-01	2.88E-01	1.28E+00	5.96E+06	1.13E-06	8.54E+06	8.73E-01	1,66E-02	2.61E-16	3.93E-02	2.57E-16		-1.19E+00		6.17E-17 7.59E-12	3.50E-01 8.14E-01	1.25E+07 1.22E+07	2.29E-11 1.82E-14	0.00E+00 0.00E+00	1.00E+00 1.00E+00	3,05E-01 4,85E-01	7 24E-06
	Down-dlp	í	2	47	4.59E-01	1.57E-02 6.75E-02	1.06E-01 1.61E-01	1.25E+00 1.12E+00	5.81E+06 2.69E+06	2.31E-05 2.65E-01	8.34E+06 8.40E+06	9.48E-01 9.14E-01	3.41E-02 1.34E-01	2.19E-18 8.92F-18	6.48E-02 1.75E-01	2.19E-18	5.50E+02	-1.37E+00	1.29E-13	5.25E-17	1.18E+00	1.19E+07	6.76E-13	0.00E+00	1.00E+00	8.00E-01	4.65E-06 1.23E-04
,	Down-dlp	1	2	17	5.93E-01	1.41E-02	2.26E-01	1,48E+00	1.12E+07	1.03E-01	1.12E+07	4.36E-01	1.37E-01	5.37E-15	1.40E-01	6.92E-18 5.37E-15	5.50E+02 5.50E+02	-1.09E+00 -1.03E+00		2.19E-16 7.41E-13	6.75E-01 5.93E-01	1.20E+07 1.44E+07	1.55E-12	4.52E-04	7.23E-01	6.72E-01	2.23E-05
	Down-dip Down-dip	1	2	55 19	5.54E-01 5.47E-01	7.03E-02 1.42E-01	2.38E-01 2.97E-02	1,35E+00 1,33E+00	8.42E+06 7.87E+06	9.27E-01	8.36E+06	4.56E-01	8.29E-02	8.71E-15	1.01E-01	8.71E-15	5.50E+02	-8.68E-01	1.15E-13	6.03E-12	4.31E-01	1.44E+07	3.98E-12 1.62F-11	0.00E+00 6 88F-01	1.00E+00 1.62E-07	9.84E-03	4.63E-01
	Down-dip	1	2	27	5.25E-01	1.18E-01	4.62E-01	1.26E+00	6.24E+06	8.46E-01 7.10E-02	8.26E+06 8.34E+06	8.50E-01 8.78E-01	1.83E-01 2.09E-02	1.41E-15 1.86E-16	2.05E-01 4.22E-02	1.41E-15 1.86E-16	5.50E+02	-1.23E+00	1.30E-13	2.00E-16	8.94E-01	1.18E+07	1.45E-12	5.28E-01	4.86E-06	5.37E-01	1.51E-06
1	Down-dip Down-dip	1	2	64	4.87E-01	1.33E-01	1.78E-02	1.18E+00	4.22E+08	6.62E-01	8.25E+06	8.58E-01	4.25E-02	3.41E-16	7.79E-02	3.39E-16	5.50E+02 5.50E+02	-1.24E+00 -1.53E+00	1.24E-13 1.31E-13	2.40E-15 3.63E-12	9.09E-01 1.62E+00	1.19E+07 1.19E+07	1,26E-12 2,24E-12	0 00E+00 2 11F-01	1.00E+00 2.18E-02	3.86E-01	1.48E-06
1	Down-dip	i	2	37 49	5.27E-01 5.74E-01	4.07E-02 3.07E-02	2.28E-01 7.64E-02	1.27E+00 1.41E+00	6.41E+06 9.73E+06	1.07E-01 6.31E-02	8.22E+06 9.72E+06	9.51E-01 3.12E-01	9.98E-02	3.98E-16	1.22E-01	3.98E-16	5.50E+02			1.35E-15	8.19E-01	1.18E+07	6.17E-12	0.00E+00	1.00E+00	5.63E-01 7.83E-01	2.14E-06 2.94E-06
	Down-dip	1	2	91	5.60E-01	5.46E-02	3.06E-01	1.36E+00	8.76E+06	3.62E-01	8.76E+06	4.B0E+01	2.79E-02 1.74E-01	4.27E-15 5.01E-15	4.07E-02 1.95E-01	4.27E-15 5.01E-15	5.50E+02 5.50E+02	-1.26E+00 -7.73E-01	1,40E-13	8.91E-13 2.82E-13	9.52E-01 3.57E-01	1.25E+07	9.77E-13	0.00€+00	1.00E+00	6.42E-03	4 86E-01
	Down-dip Down-dip	1	2	59 33	5.38E-01	1.07E-02 1.31E-01	1.94E-01 1.22E-01	1.30E+00 1.39E+00	7.26E+06 9.26E+06	1.63E-01 8.65E-01	8.15E+06	9.76E-01	1.74E-01	1.66E-16	2.00E-01	1.66E-16	5.50E+02	-1.20E+00	1.26E-13	1.35E-16	8.44E-01	1.18E+07 1.17E+07	4.17E-14 5.89E-14	9.00E+00	8.20E-01 1.00E+00	6.01E-03 8.96E-01	4.72E-01 7.28E-06
	Down-dip	i	2	51	5.87E-01	8.73E-02	4.26E-01	1.46E+00	1.07E+07	6.35E-01	9.22E+06 1.08E+07	3.22E-01 5.61E-01	2.74E-02 7.16E-02	1.12E-14 2.19E-16	3.63E-02 7.64E-02	1.12E-14 2.19E-16	5.50E+02 5.50E+02	-1.24E+00	1.36E-13	8.32E-13	9.16E-01	1.15E+07	1.26E-13	5.39E-01	3.23E-07	4.22E-03	4.79E-01
	Down-dip Down-dip	1	2	98	5.13E-01	3.56E-02	5.00E-02	1.24E+00	5.63E+06	2.37E-05	8.10E+06	9.20E-01	5.01E-02	4.19E-19	8.36E-02	4.17E-19	5.50E+02	-9.65E-01 -1.23E+00	1.29E-13 1.21E-13	5.25E-14 4.79E-15	5.24E-01 8.82E-01	1.33E+07 1.17E+07	2.82E-14 3.98E-14	0.00E+00 0.00E+00	1.00E+00 1.00E+00	4.76E-03	4.63E-01
	Down-dip	1	2	65 62	5.89E-01 5.95E-01	7.34E-03 1.39E-01	2.60E-01 5.05E-01	1.46E+00 1.48E+00	1.09E+07 1.14E+07	9.65E-02 5.26E-02	1.09E+07 1.14E+07	4.18E-01 6.09E-01	5.87E-02 4.05E-02	4.90E-16 1.41E-18	8.52E-02	4.90E-16	5.50E+02	-1.23E+00	1.43E-13	7.08 E -16	8.95E-01	1.19E+07		0.00E+00	1.00E+00	7.21E-01 3.36E-03	1.96E-04 5.69E-01
1	Down-dip	1	2	74	5.77E-01	3.84E-02	3.53E-01	1.42E+00	9.94E+06	1.78E-02	9.89E+06	4.97E-01	5.27E-02	3.55E-18	5.06E-02 5.89E-02	1.41E-18 3.39E-19	6.50E+02 5.50E+02	-1.37E+00 -8.29E-01	1.54E-13 1.19E-13	1.70E-15 6 17E-12	1.19E+00 3.99E-01	1.38E+07 1.22F+07	1.00E-14	0.00€+00	1.00E+00	3.19E-03	4.37E-01
	Down-dlp Down-dlo	1	2	86 30	4.56E-01 5.96E-01	6,86E-02 1,16E-01	3.61E-02 4.16E-02	1.12E+00 1.49E+00	2.62E+06 1.15E+07	7.23E-01	8.09E+06	9.18E-01	1.42E-01	3.04E-17	1.91E-01	3.02E-17	5.50E+02	-1.28E+00	1.10E-13	4.07E-13	9.43E-01	1.22E+07 1.17E+07	8 32E-12 2.04E-11	0.00E+00 2.86E-01	1.00E+00 1.97E-02	3.91E-03 7.21E-01	5.32E-01 5.25E-06
	Down-dlp	i	2	87	5.93E-01	2.68E-02	4.16E-02 1.60E-01	1.49E+00 1.48E+00	1.15E+07 1.13E+07	8.38E-01 2.80E-02	1.15E+07 1.13E+07	1.98E-01 2.75E-01	3.08E-02 1.10E-01	2.75E-14 9.11E-20	3.73E-02 1.13E-01	2.75E-14 4.47E-20	5.50E+02	-6.49E-01	1,18E-13	2.19E-13	2.79E-01	1.34E+07	1.59E-13	5.05E-01	2.72E-04	1.25E-03	6.24E-01
1	Down-dip	1	2	15	5.65E-01	4.22E-02	5.21E-01		9.15E+06	9.52E-01	9.13E+06	5.74E-01	4.81E-02	1.32E-14	6.37E-02	1.32E-14	5.50E+02 6.50E+02	-9.15E-01 -9.48E-01	1.28E-13 1.21E-13	8.91E-14 1.32E-14	4.74E-01 5.06E-01	1.37E+07 1.06E+07	2.51E-12 4.47E-13	0.00E+00 6.75E-01	1.00E+00 4.76E+06	6.47E-04	7.10E-01
	Down-dip Down-dip	;	2	4 58	6.04E-01 6.01E-01	1.11E-01 2.96E-02	1.90E-01 1.14E-01	1.52E+00 1.51E+00	1.21E+07 1.19E+07	1.31E-06 1.72E-01	1.22E+07 1.19E+07	2.66E-01 1.84E-01	8.30E-02 1.87E-01	1.26E-19	8.48E-02	1.26E-19	5.50E+02	-9.63E-01	1.34E-13	4.17E-16	5.22E-01	1.47E+07	3.16E-14	0.00E+00	4.76E-06 1.00E+00	3.08E-04 1.60E-04	7.48E-01 7.76E-01
	Down-dip	1	2	26	5.56E-01	7.60E-02	4.97E-01	1.35E+00	8.55E+06	4.80E-01	8.53E+06	5.20E-01	1.65E-01	1.45E-16 2.00F-14	1.92E-01 1.88E-01	1.45E-16 2.00E-14	5.50E+02 5.50E+02	-1.18E+00 -1.33E+00	1.45E-13 1.38E-13	3.09E-15 3.02E-12	8.11E-01 1.10E+00	1.26E+07	1.07E-13	4.42E-05	8.59E-01	8.83E-05	8.29E-01
1	Down-dip Down-dip	1	2	93	6.06E-01 6.06E-01	4,00E-02 6,24E-02	5.11E-01		1.24E+07	6.67E-02	1.24E+07	5.29E-01	7.97E-02	1.70E-14	8.31E-02	1.70E-14	5.50E+02	-9.34E-01	1.33E-13	3.02E-12 2.95E-14	4.92E-01	1.14E+07 1.35E+07	6.76E-12 8.91E-13	0.00E+00 0.00E+00	1.00E+00 1.00E+00	1.27E-05 5.30E-06	8.85E-01 9.17E-01
	Down-dip	i	2	40	5.B5E-01	1.02E-01	4.15E-01 3.54E-01	1.52E+00 1.45E+00	1.24E+07 1.06E+07	3.55E-01 4.83E-01		4.30E-01 3.71E-01	5,37E-02 1,22E-01	3.56E-13 1.51E-13	4.32E-02 1.27E-01	1.35E-13		-1.39E+00	1.59E-13	1.20E-14	1.22E+00		5.37E-15	0.00E+00	1.00E+00	1.52E-06	9.39E-01
	Down-dip	1	2	12	5.97E-01	7.06E-02	1.02E-01	1.49E+00	1.16E+07	3.39E-02	1.16E+07		3.11E-02	1.78E-13	3.89E-02	1.51E-13 1.78E-13	5.50E+02 5.50E+02	-1.32E+00 -1.38E+00	1.47E-13 1.55E-13	3.02E-13 5.50E-15	1.07E+00	1.39E+07 1.39E+07		2.66E-03	5.30E-01	1.67E-06	9.34E-01
	Down-dip Down-dip	1	2	79 94	5.70E-01	1.23E-01 4.58E-03	3.88E-01 1.85E-01	1.40E+00 1.44E+00	1.11E+07 1.22E+07	4.12E-01 9.91E-01	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	7,76E-01 6,96E-01	1.07E-01	2.57E-13	1.78E-01	2.57E-13	7.50E+02	-1.10E+00	1.30E-13	1.51E-16	6.89E-01	1.23E+07	1.86E-13 4,37E-15	0.00E+00 8.18E-08	1.00E+00 9.00E-01	2.51E-09 1.86E-01	9.90E-01 1.38F-02
184 [Down-dip	1	2	11	5.93E-01	6.24E-02	4.15E-01			9.53E-01	1.22E+07 1.31E+07	9.36E-01	1.92E-01 7.33E-02	7.82E-15 1.36E-12	1.93E-01 4.46F-02	6.31E-15 1.35E-13		-1.29E+00 -1.39E+00	1.44E-13 1.54E-13	9.77E-16	9.95E-01	1.31E+07	1.78E-12	9.59E-01	2.93E-07	1.78E-01	7.44E-02
	Jown-dip Jown-dip	1	2	15 42	5.72E-01 5.87E-01	4.22E-02 1.04E-01	5.21E-01		1.13E+07	7.53E-01		7.95E-01	5.56E-02	1.32E-14	6.27E-02	1.32E-14		-9.48E-01	1.23E-13	1.20E-14 1.32E-14	1.22E+00 5.06E-01	1.35E+07 1.06E+07		0.00E+00 6.94E-02	1.00E+00 1.44E-01	6.50E-01 1.27E-01	9.85E-08 7.61E-02
	Jown-dip	i	2	10	5.46E-01	3.17E-02	3.92E-01 1.73E-01		1.26E+07 9.38E+06	7.05E-02 9.65E-01		7,88E-01 6,55E-01	1.24E-01 4.85E-02	5,18E-16 3,72E-14	1.11E-01 6.69E-02	7.76E-17 3.72E-14		-1.26E+00	1.44E-13	1.38E-15	9.46E-01	1.47E+07		0.00E+00	1.00E+00	2.06E-01	1.52E-02
	Down-dip	1	2	78	5.89E-01	4.93E-02	1.51E-01	1.46E+00	1.27E+07	9.46E-01		9.46E-01	1.19E-01	4.24E-14	1.03E-01		7.50E+02 7.50E+02	-1.33E+00 -1.06F+00	1.35E-13 1.33E-13	1.86E-16 8.32E-17	1.08E+00 6.28E-01	1.09E+07 1.40E+07	1.35E-11 1.07F-12	8.52E-01 7.85E-01	1.31E-07	1.36E-01	8.91E-02
1	Jown-dip Jown-dip	1	2	36 44	5.83E-01 5.76E-01	3,71E-03 1,12E-01	1.39E-01 1.61E-02		1.22E+07 1.15E+07	2.97E-03	1.21E+07	6.52E-01	4.68E-02	7.14E-20	4.94E-02	6.61E-20	7.50E+02	-8.89E-01	1,24E-13	8.13E-15	4.50E-01	1.36E+07		0.00E+00	3.35E-07 1.00E+00	7.85E-01 1.48E-01	3.39E-07 9.34E-02
	Down-dip	1	2	12	5.96E-01	7.06E-02	1.02E-01	1.42E+00	1.15E+07 1.35E+07	8.85E-01 1.63E-02		8.85E-01 5.19E-01	1,24E-01 3,85E-02	1.52E-13 1.79E-13	1.21E-01 3.90E-02	1,18E-13 1,78E-13	7.50E+02 7.50E+02	-1.17E+00	1.35E-13 1.55F-13	3.80E-15	7.83E-01	1.29E+07	1.12E-12	6.31E-01	7.78E-08	6.31E-01	7.72E-08
1	Down-dip Down-din	1	2	45	5.67E-01	5.05E-02	2.04E-01		1.08E+07	9.76E-01		9.76E-01	7.38E-02	5.13E-14	8.21E-02	5.13E-14	7.50E+02	-9.31E-01	1.00E-13 1.21E-13	5.50E-15 1.74E-15	1.19E+00 4.89E-01	1.39E+07 1.32E+07	1.86E-13 4.57E-13	0.00E+00 8.92E-01	1.00E+00 0.00E+00	5.91E-02 8.89E-01	1.68E-01 0.00F+00
I	<i>xown-ciip</i> Jown-diip	1	2	31 69	5.77E-01 5.75E-01	5.28E-02 8.98E-02	5.93E-02 4,08E-01	1.42E+00 1.41E+00	1.17E+07 1.15E+07	1.11E-01 9.10E-01		9.40E-01 9.13E-01	7.33E-02 7.49E-02	1.66E-15	8.22E-02			-1.27E+00	1.42E-13	3.31E-14	9.73E-01	1.40E+07	6.31E-13	2.22E-05	8.80E-01	7.82E-01	1.13E-06
	Jown-dip	1	2	2	5.65E-01	8.22E-02	4.02E-01		1.07E+07	9.16E-01		9.16E-01	1.58E-01	1.26E-14 4.47E-14	8.13E-02 1.64E-01			-1.29E+00 -1.29E+00	1.42E-13 1.38E-13	9.33E-15 6.01E-14	9.99E-01 9.98E-01	1.42E+07	4.07E-13	5.42E-01	4.53E-09	5.58E-01	0.00E+00
	Jown-dip Jown-din	1	2	52 39	5.71E-01 5.73E-01	3.68E-02 1.50E-01	4.49E-01 2.98E-01		1.12E+07 1.13E+07	9.60E-01		9.60E-01	1.04E-01	1.70E-15	1,17E-01	1.70E-15	7.50E+02	-9.48E-01	1.23E-13	4.17E-14	5.07E-01	1.24E+07 1.43E+07	7.24E-11 2.63E-13	5.71E-01 7.57E-01	9.13E-08 4.04E-07	5.71E-01 7.57E-01	9.05E-08
1 ,	Jown-dip	i	2	18	5.46E-01	1.06E-01	2.98E-01 3.40E-01		9.32E+06	8.47E-01 8.92E-01		8.47E-01 7.80E-01	1.90E-02 4.95E-02	3.02E-15 3.31E-14	2.71E-02 6.82E-02	3.02E-15 3.31E-14	7.50E+02 7.50E+02		1.37E-13	2.40E-13	8.82E-01		1.78E-13	4.04E-01	3.35E-07	4.04E-01	3.28E-07
1	Jown-dip	1	2	25	5.69E-01	8.68E-02	5.41E-01	1.39E+00	1.11E+07	1.00E-01	1.11E+07	9.07E-01	7.45E-02	3.40E-17	7.69E-02			-1.09E+00 -1.13E+00	1.22E-13 1.31E-13	6.17E-16 1.26E-16	6.69E-01 7.23E-01	1.05E+07 1.38E+07		5.17E-01 D.00E+00	1.10E-07 1.00E+00	2.24E-01	1.38E-02
	Jown-dip Jown-dip	1	2	65 24	5.54E-01 5.40E-01	1.27E-01 9.01F-02	8.96E-02 1.37E-01	1.35E+00 1.30E+00	9.86E+06 8.91E+06	0.00E+00 9.08E-01	9.89E+06 9.00E+06	8.56E-01 9.08E-01	1.96E-02	8.71E-16	2.91E-02			-1.16E+00	1.28E-13	4.17E-15	7.73E-01			0.00E+00	1.00E+00	4.31E-01 5.28E-01	9.82E-06 1.98E-05
202 0	Jown-dip	1	2	46	5.37E-01	2.03E-02	2,35E-01			3.21E-02		9.63E-01	1.85E-01 4.13E-02	2.82E-13 1.59E-17	2.07E-01 6.14E-02			-1.41E+00	1.31E-13 1.37E-13	2.63E-14 1.45E-14	9.94E-01 1.26E+00	1.09E+07 1.50E+07	7.41E-13	6.59E-01	2.82E-08	6.59E-01	2.79E-08
	Jown-dip Jown-dip	1	2	19 81	5.49E-01 5.46E-01	1.42E-01 1.05E-02		1.33E+00	9.51E+06	7.93E-01	9.62E+06	8.51 E-01	1.89E-01	1.41E-15	2.04E-01	1.41E-15	7.50E+02	-1.23E+00	1.30E-13	1,45E-14 2.00E-16	8.94E-01	1.50E+07 1.18E+07		0.00E+00 4.13E-01	1.00E+00 7.78E-04	8.33E-01 5.41E-01	1.83E-05 7.43E-07
	own-dip	i	2	73	5.46E-01 5.48E-01	1.05E-02 5.61E-02			9.23E+06 9.48E+06			8.99E-01 9.37E-01	6.96E-02 8.63E-02	2.31E-18 3.72E-16	7.97E-02 1.06E-01	1.00E-18 3.72E-16		-1.37E+00	1.37E-13	2.51E-12	1.19E+00	1.30E+07	8.91E-11	0.00E+00	1.00E+00	4.55E-01	8.63E-07
	Oown-dip	1	2	5	5.29E-01	1.29E-01	1.21E-01	1.28E+00	7.83E+06	6.22E-02	9.53E+06	8.50E-01	1.24E-01	1.91E-17	1.48E-01		7.50E+02 7.50E+02	-8.01E-01 -1.37E+00	1,11E-13 1,32E-13	6.17&-15 1.82E-12	3.77E-01 1.17E+00			0.00E+00		7.04E-01	2.27E-08
	Xown-dlp Xown-dlo	1	2	29 49	5.49E-01 5.40E-01	9.72E-02 1.02E-01			9.52E+06 8.90E+06				2.02E-01	5.28E-17	2.21E-01	4.79E-17	7.50E+02	-1.08E+00	1.23E-13	9.55E-12	6.64E-01	1.45E+07		0.00E+00 2.55E-05	1.00E+00 8.66E-01	5.03E-01 5.88E-01	3.26E-05 9.58E-06
209 [lown-dlp	í	2	54	5.16E-01	1.25E-01	2.11E-01 2.39E-02					8.95E-01 8.45E-01	4.55E-02 2.90E-02	7.76E-14 5.01E-18	5.88E-02 5.13E-02			-1.29E+00 -1.16E+00	1.31E-13 1.18E-13		1.01E+00		3.80E-12	4.38E-01	8.82E-04	5.91E-01	8.41E-08
	lown-dip	1	2	30	5.42E-01	1.16E-01		1.31E+00	9.07E+06	8.80E-01	9.16E+06	8.80E-01	2,61E-02	2.75E-14	4.23E-02			-1.16E+00 -6.49E-01	=	4.68E-12 2.19E-13	7.76E-01 2.79E-01	1.53E+07 1.34E+07		0.00E+00 6.10E-01	1.00E+00 2.22E-07	5.29E-01 6.10E-01	7.16E-05
	lown-dip lown-dip	1	2	59 35	5.42E-01 5.42E-01	1.07E-02 9.57E-02			9.07E+06 9.09E+06			9.77E-01 9.03E-01	1,80E-01	1.66E-16	1.99E-01	1.66E-16	7.50E+02	-1.20E+00	1.27E-13	1.35E-16	8.44E-01	1.17E+07		0.00E+00	1.00E+00	6.10E-01 8.98E-01	2.20E-07 6.56E-06
213 C	lown-dip	1	2	72	5.25E-01	2.36E-02	4.74E-03	1.26E+00	7.57E+06		01112100		5.00E-02 5.66E-02	7.24E-15 4.62E-18	6.29E-02 B.11E-02			-8.97E-01 -6.26E-01	1.13E-13 9.92E-14	1.38E-13 5.37E-12	4.57E-01 2.66E-01			4.94E-01	1.05E-07	4.94E-01	1.04E-07
	lown-dip lown-dip	1	2	82 56	5.40E-01 5.36E-01	8.52E-02 4.66E-02			8.77E+06		B.B9E+06	9.11E-01	1.21E-01	2.14E-15	1.35E-01	2.14E-15	7.50E+02	-1.39E+00	1.36E-13		1.22E+00			0.00E+00 0.00E+00		7.12E-01 5.20E-01	4.71E-04 7.40E-07
	own-dip Xown-dip	i	2	9	5.36E-01	4.66E-02 1.35E-01							7.84E-02 1.28E-02	1.05E-15 2.36E-19	9.31E-02 2.63E-02	· · · · · · · · · · · · · · · · · · ·		-7.21E-01	1.05E-13	1.05E-14	3.22E-01	1.12E+07	2.82E-12	0.00E+00	1.00E+00	7.41E-01	1.89E-06
	own-dip	1	2	23	5.24E-01	7.29E-02	4.80E-01	1.26E+00	7.70E+06	5.48E-02	8.46E+06		2.81E-02	1.18E-16	2.83E-02 4.83E-02			-1.24E+00 -1.18E+00	1,25E-13 1,21E-13	2.63E-15 7.94E-17	9.00€-01 8.09E-01				1.00E+00	2.15E-01	6.00E-04
	lown-dip lown-dip	1	2	99 76	5.32E-01 5.04E-01	1,28E-01			8.30E+06			8.67E-01	1.63E-01	5.89E-17	1.B7E-01	5.89E-17	7.50E+02	-7.63E-01	1.06E-13	6.17E-17	3.50E-01			0.00E+00 0.00E+00		5.50E-01 3.05E-01	2.23E-06
	own-dip	í	2	95	5.28E-01				6.37E+06 8.08E+06				3.02E-02 1.48E-01	3.16E-18 6.03E-17	5.34E-02 1.72E-01			-1.33E+00	1.24E-13		1.09E+00	1.33E+07	2.09E-12	0.00E+00	1.00E+00	3.28E-01	5.31E-04
	own-dip	!	2	61	5.68E-01	8.73E-02				5.25E-02	1.09E+07	5.80E-01	7.60E-02	2.19E-16	8.00E-02	6.03E-17 2.19E-16		-9.54E-01 -9.65E-01	1.12E-13 1.23E-13		5.13E-01 5.24E-01	1.30E+07 1.33E+07	, ,	0.00E+00		3.50E-01	1.44E-05
	own-dip own-dip	1	2	43 20	4.85E-01 5.26E-01	5.88E-02 1.23E-01								2.87E-19	2.01E-01	9.77E-20	7.50E+02	-1.26E+00	1.16E-13	3.63E-13	9.52E-01			0.00E+00 0.00E+00	1.00E+00 1.00E+00	7.89E-03 6.17E-01	3.99E-01 2.41E-04
224 D	own-dip	1	5	62	5.81E-01	1.39E-01			,		-,		1.66E-02 4.42E-02	1.35E-17 1.41E-1B		1.35E-17 1.41E-18			9.87E-14 1.49E-13					0.00E+00	1.00E+00	4.99E-01	7.81E-05
225 D	own-dip	1	2	34	5.28E-01	2.76E-02	3.26E-01	1.27E+00	8.13E+06	2.71E-02						2.29E-17							1.00E-14 4.68E-14			6.40E-03 7.70E-01	3.45E-01
																			-					~, ~~	7.00L#00	,,/UE-U1	J.80E-U5

A	

No. Commoding 1	Excevaled ine Volume (m*3)
No. O Replic Sets, Vertor Filtry SHIPP SHI	(m-53)
Committed 2	··· -/
153 Down-dip 1 2 88 000E+00 8/0ZE+06 8/0ZE+06 8/0ZE+06 8/0ZE+06 5/REF-06	.92€404
15 Down-dip 2 47 Down-dip 2 47 Down-dip 3 47 Down-dip 3 47 Down-dip 3 47 Down-dip 4 4 4 4 4 4 4 4 4	15E+04
100mm-dp 1 2 17 0.00E+00 2.75E+05 1.13E+07 1.10E+01 1.10E+01 1.10E+01 1.00E+00 2.75E+05 2.75E+05 0.75E+0	39E+04 98E+04
1.55 Down-dip 1 2 13 0.00E+00 8.0E+00 8.0E+00 8.0E+00 8.0E+00 3.85E+00 4.55	36E+04
199 Down-righ 1 2 27 0.00E-000 8.0EE+006 2.88EE+00 2.88EE+00 3.74E-06 8.3EE+00 3.74E-06 8.3EE+00 3.74E-06 8.74E-06 3.74E-06 8.74E-06 3.74E-06 8.74E-06 3.74E-06 8.74E-06 3.74E-06 8.74E-06 3.74E-06 8.74E-06 3.74E-06 8.74E-06 3.74E-06 8.74E-06 3.74E-06 8.74E-06 3.74E-06 8.74E-06 3.74E-06 8.74E-06 3.74E-06 8.74E-06 3.74E-06 8.74E-06 3.74E-06 8.74E-06 3.74E-06 8.74E-06 3.74E-06 8.74E-06 3.74E-06 8.74E-06 3.74E-06 3.74E-06 8.74E-06 3.74E-06 8.74E-06 3.74E-06 8.74E-06 3.74E-06 8.74E-06 3.74E-06 8.74E-06 3.74E-06 8.74E-06 3.74E-06 8.74E-06 3.74E-06 8.74E-06 3.74E-06 8.74E-06 3.74E-0	26E+04
181 Down-dp 1 2 37 0.00E+00 3.0E+06 8.88E+00 2.88E+00 3.74E-06 3.7	48E+04 54E+04
162 Down-dip 1 2 49 0,00E+00 245E+05 9,10E+00 1,10E+01 7,3E+01 6,17E+01 7,3E+01 6,17E+01 7,3E+01 6,17E+01 7,3E+01 6,17E+01 7,3E+01 6,17E+01 7,3E+01 6,17E+01 7,3E+01 6,17E+01 7,3E+01 6,17E+01 7,3E+01 6,17E+01 7,3E+01 6,17E+01 7,3E+01 6,17E+01 7,3E+01 6,17E+01 7,3E+01 6,17E+01 7,3E+01 6,17E+01 7,3E+01 6,17E+01 7,3E+01 6,17E+01 7,3E+01 6,3E+02	99E+04
164 Down-dip 1 2 59 0.00E+00 8.02E+06 8.06E+06 4.00E+00 1 2.9E+06 1.00E+01 5.01E+07 2.73E+01 2.47E+06 5.87E+00 1.23E+00 5.22E+00 1 2.35E+06 1.00E+01 1.33E+01 3.00E+00 1 2.35E+06 1.00E+01 3.9E+06 1.30E+01 3.00E+01 1.33E+01 3.00E+01 1.33E+01 3.00E+01 1.23E+01 1.23E+	35E+04 14E+04
186 Down-dp 1 2 33 8,00E+06 2,36E+05 6,35E+06 1,0E+01 3,0E+01 1,0E+01 1 2 61 0,0OE+00 0,0OE+0	22E+04
167 Down-dip 1 2 98	27E+04 27E+04
169 Down-dip 1 2 85 0,00e+00 2,70e+05 1,51e+06 1,10e+01 2,38e-01 2,38e-06 3,62e-02 9,8e-04 1,00e+00 1 2 60,00e+00 2,49e+05 9,14e+06 1,10e+01 2,38e-07 1,6e-01 1,0e-01	94E+04
170 Down-dip 1 2 74	85E+04 75E+04
177 Cown-dip 1 2 86 0.00E+00 8.02E+06 8.7E+06 2.8EE+00 1.11E-06 1.8EE-07 5.7IE-01 1.7EE-01 5.7IE-01 1.7EE-07 5.7IE-01 1.7EE-07 5.7IE-01 1.7EE-07 5.7IE-01 1.7EE-07 5.7IE-01 1.7EE-07 5.7IE-01 1.7EE-07 5.7IE-01 1.7EE-07 5.7IE-01 1.7EE-07 5.7IE-01 1.7EE-07 5.7IE-01 1.7EE-07 5.7IE-01 1.	97E+04
173 Down-dip 1 2 87 0.00E+00 2.99E+05 1.05E+07 1.10E+01 4.95E-08 1.77E-01 4.3E-07 1.16E+01 1.39E-01 2.99E+05 1.05E+07 1.10E+01 4.95E-08 1.77E-01 4.3E-07 1.16E+01 1.39E-01 2.90E-02 3.9E-06 2.90E+05 3.9E-06 2.90E+05 3.9E-06 2.90E+05 3.9E-06 2.90E+05 3.9E-06 2.90E+05 3.9E-06 2.90E+05 3.9E-06 2.90E+05 3.9E-06 2.90E+05 3.9E-06 2.90E+05 3.9E-06 2.90E+05 3.9E-06 2.90E+05 3.9E-06 2.90E+05 3.9E-06 2.90E+05 3.9E-06 2.90E+05 3.9E-06 2.90E+05 3.9E-06 2.90E+05 3.9E-06 2.90E+05 3.9E-06 2.90E-06 3.90E-06 3.90E-06 3.90E-06 3.9E-06 3.90	36E+04 89F+04
175 Down-dp 1 2 15 8.02E+06 2.56E+06 3.3E+06 8.07E+06 1.0E+01 1.2E+07 1.50E+01 1.5E+07 7.70E+00 1.1E+01 1.1E+01 5.10E+02 4.2E+06 4.57E+02 4.3E+04 1.7E+01 1.2E+07 1.5E+01 1.2E+07 1.2E	15E+04
178 Down-dip 1 2 58 3.32E-05 3.32E-05 6.77E-06 1.0E-01 1.21E-07 1.55E-01 3.09E-02 5.37E-02 7.04E-05 2.17E-02 2.13E-02 2.82E-06 2.88E-01 1.21E-07 1.31E-06 1.03E-05 1.70E-08 1.	44E+03 90E+04
177 Down-dp 1 2 93 0.00E+00 3.78E+05 1.01E+07 1.71E-01 1.02E+05 1.78 Down-dp 1 2 93 0.00E+00 3.78E+05 1.01E+07 1.10E+01 3.14E-09 9.08E+00 4.21E-03 1.70E-04 8.20E+02 5.98E+05 2.51E-03 2.47E-03	30E+03
179 Down-dip 1 2 11 0.00E+00 3.92E+05 1.99E+00 1.10E+01 1.87E+09 1.89E+00 1.08E+00 1.88E+00 1.07E+00 2.98E+03 1.07E+06 2.29E+03 2.66E+03 3.82E+06 5.55E-01 1.19E+07 6.72E+02 1.04E+05 1.00E+00 1.87E+09 2.29E+00 1.38E+00 1.07E+00 2.98E+00 1.27E+00 1.29E+00 1.27E+00 1.29E+00 1.27E+00 1.29E+00 1.27E+00 1.29E+00 1.27E+00 1.29E+00 1.27E+00 1.29E+00 1.27E+00 1.29E+00 1.27E+00 1.29E+00 1.27E+00 1.29E+00 1.27E+00 1.29E+00 1	81E+04 1 88F+04
180 Down-dip 1 2 40 2.64E+05 3.43E+05 1.09E+07 1.10E+01 2.76E+10 5.93E+01 1.20E+09 1.54E+01 2.49E+04 2.94E+04 1.81E+03 1.62E+06 4.02E+04 3.87E+04 2.66E+04 3.87E+04 2.66E+04 3.87E+04 2.66E+06 3.99E+01 1.05E+07 3.25E+01 1.05E+07 3	12E+04
182 Down-db 1 2 79 3.44E-05 3.29E+06 3.29E+06 3.29E+06 1.10E+01 8.18E-05 5.55E-02 1.03E+04 1.83E-01 1.93E+03 0.00E+00 1.69E+02 4.49E+04 8.66E+01 8.22E+01 1.03E+07 7.88E-01 1.11E+07 3.53E-01 8.18E-05 5.55E-02 1.03E-04 1.83E-01 1.93E+03 0.00E+00 1.69E+02 4.49E+04 8.66E+01 8.22E+01 1.03E+07 7.88E-01 1.11E+07 3.53E-01 8.18E-04 1.03E+04 1.03E+04 1.03E+07 1.	83E+04 42E+04
183 Down do 1 2 04 8 005-06 2 505-05 1 505-05 1 505-01 B 935-01 8 935-01 1 105-07 3 535-01 B 935-04 5	65E+04
188 Develop 1 2 34 6.00F-00 2.59E-05 1.00E-01 1.46E-04 1.60E-00 2.07E-02 0.00E-05 5.1E-02 2.36E-05 4.90E-01 4.62E-01 7.78E-06 7.04E-01 1.27E-107 7.61E-01 9.42F-04 1.00E-05 1.	24E+04 12E+04
185 Down-dip 1 2 15 3,75E+105 4,30E+05 3,00E+05 1,00E+01 4,30E+05 2,45E+04 4,33E+05 5,01E+06 0,00E+00 1,32E-01 9,19E+00 4,60E+01 4,49E+01 1,28E+07 9,35E-01 1,31E+07 2,23E-01 9,81E+04 4	42E+04
186 Down-dip 1 2 42 0.00E-00 3.32E-06 3.32E-06 3.32E-06 1.10E-01 3.12E-05 4.46E-02 1.32E-04 2.66E-01 6.81E-02 0.00E-00 1.38E-02 5.00E-04 4.02E-01 3.82E-01 3	82E+04 55E+04
188 Down-dip 1 2 78 8.01E+06 8	13E+04
189 Down-dip 1 2 36 0,00E+00 4,53E+05 4,53E+05 1,10E+01 1,96E-05 1,00E-01 1,02E-04 1,89E+00 1,47E+02 0,00E+00 3,06E+02 1,92E+05 2,81E+01 2,76E+01 2,76E+01 1,92E+05 2,81E+01 2,76E+01 2,76E+01 1,92E+05 2,81E+01 2,76E+01 2	52E+04 59E+04
191 Down-dip 1 2 12 0,00E+00 4,16E+05 1,16E+05 1,05E+04 1,89E+05 1,48E+04 1,89E+05 7,67E+06 0,00E+00 5,77E-02 3,83E+00 2,78E+01 2,71E+01 1,15E+07 8,86E+01 1,15E+07 6,82E-01 8,14E+04 2	06E+04
192 Down-dip 1 2 45 8,00E-406 8,00E-406 8,00E-406 8,00E-406 8,00E-406 8,00E-406 8,00E-406 0,00E-400 0,00E-	10E+04 59E+04
194 Down-dip 1 2 69 7-99E-108 8.00E-109 8.00E-109 8.90E-	52E+04
195 Down-dip 1 2 2 8.00E-106 8.00E-106 8.00E-106 8.00E-106 8.00E-107 1.95E-07 9.09E-01 1.95E-07 9.09E-01 1.95E-07 9.09E-01 8.05E-04 1.95E-07 9.09E-01 8.05E-04 1.95E-07 9.09E-01 8.05E-04 1.95E-07 9.09E-01 8.05E-04 1.95E-07 9.09E-01 8.05E-04 1.95E-07 9.09E-01 8.05E-04 1.95E-07 9.09E-01 8.05E-04 1.95E-07 9.09E-01 8.05E-04 1.95E-07 9.09E-01 8.05E-04 1.95E-07 9.09E-01 8.05E-04 1.95E-07 9.09E-01 8.05E-04 1.95E-07 9.09E-01 8.05E-04 1.95E-07 9.09E-01 8.05E-04 1.95E-07 9.09E-01 8.05E-04 1.95E-07 9.09E-01 8.05E-04 1.95E-07 9.09E-01 8.05E-05 1.95E-07 9.09E-01 8.05E-05 1.95E-07 9.09E-01 8.05E-05 1.95E-07 9.09E-01 8.05E-05 1.95E-07 9.09E-01 8.05E-05 1.95E-07 9.09E-01 8.05E-07 9.00E-	34E+04 73E+04
197 Down-dip 1 2 39 8.01e+06 8.01e+06 2.8ee+00 4.8ee+00 4.8ee+00 4.8ee+00 4.8ee+00 4.8ee+00 4.8ee+00 4.8ee+00 4.8ee+00 4.8ee+00 1.10e+07 9.60e-01 1.12e+07 9.60e-01 1.12e+07 9.60e-01 8.8ee+04 8.8ee+00 4	32E+04
198 Down-dip 1 2 18 7.99E-06 3.77E-06 3.77E-06 2.88E-00 4.70E-05 2.52E-02 7.27E-05 9.23E-02 1.41E+03 0.00E+00 7.69E+01 8.16E-03 1.15E-01 1.12E+07 8.50E-01 8.50E-01 8	57E+04
200 Down-dip 1 2 65 0.000E+00 8.04E+06 8.04E+06 8.04E+05 4.04E+05	00E+04
201 Down-dp 1 2 24 7.99E+06 7.99E+06 7.99E+06 7.99E+06 2.88E+00 3.36E+05 2.05E+07 2.05E+08 0.00E+09 8.25E+04 4.25E+03 4.26E+03 8.66E+04 8.25E+04 8.26E+03 8.26E+04 8.26E+03 8.26E+04 8.26E+03 8.26E+04 8.26E+03 8.26E+04 8.26E+03 8.26E+04 8.26E+03 8.26E+04 8.26E+03 8.26E+04 8.26E+03 8.26E+04 8.26E+03 8.26E+04 8.26E+03 8.26E+03 8.26E+04 8.26E+03 8.26E+04 8.26E+03 8.26E+04 8.26E+03 8.26E+03 8.26E+04 8.26E+03 8.26E+04 8.26E+03 8.26E+04 8.26E+03 8.26E+03 8.26E+04 8.26E+03 8.26E+04 8.26E+03 8.26E+04 8.26E+03 8.26E+03 8.26E+04 8.26E+03 8.26E+04 8.26E+03 8.26E+04 8.26E+03 8.26E+04 8.26E+03 8.26E+04 8.26E+03 8.26E+04 8.26E+03 8.26E+04 8.26E+03 8.26E+04 8.26E+03 8.26E+04 8.26E+03 8.26E+04 8.26E+03 8.26E+04 8.26E+03 8.	13E+04
203 Down-dip 1 2 19 17.79E+06 8.01E+06 8.01E+06 8.0E+05 1.98E+05 1.98E+05 1.98E+05 6.41E+05 8.02E+05 1.98E+05 6.41E+05 8.02E+05 1.98E+05 8.41E+05 8.20E+05 8.02E+05 8.41E+05 8.20E+05 8	70E+04
204 Down-dip 1 2 81 0.00E+00 6.22E+06 6.25E+06 2.88E+00 2.60E-05 9.01E-03 8.32E-05 3.13E-02 2.88E+03 0.00E+00 2.78E+03 8.10E+00 7.98E+00 9.50E+01 9	11E+04 10E+04
206 Domindip 2 5 0.00E400 8.04E406 8.07E406 2.88E400 2.75E405 1.1E04 4.75E40	28E+04
207 Down-dip 1 2 28 2.91E-105 8.03E-106 8.15E-106 2.28E-109 2.22E-05 3.33E-05 4.88E-05 3.33E-05 8.92E-105 0.00E-109 1.02E-01 7.72E-109 6.37E-109 6.74E-109 6.38E-106 8.92E-01 9.57E-108 2.27E-109 6.37E-109 6.	3E+04 9E+04
299 Down-dip 1 2 54 0.00E400 8.03E406 8	0E+04
210 Down-dip 1 2 30 8.00E-06 8.00E-06 8.00E-06 8.00E-06 2.88E-00 2.86E-05 1.73E-06 3.51E-05 1.73E-06 1.79E-07 0.00E+00 5.27E-03 3.46E-01 6.99E-00 6.05E-00 8.32E-05 8.00E-06 8	5E+04
212 Down-dap 1 2 35 7.99E-06 7	3E+04
213 Down-dp 1 2 72 0.00E-00 7.55E-06 8.01E-06 2.88E-00 1.57E-05 2.40E-04 3.50E-05 4.58E-04 6.74E-04 0.00E-00 7.35E-0-1 7.05E-01 4.76E-00 4.86E-00 9.05E-01 9.07E-06 9.01E-01 7.99E-04 7.25E-05 4.68E-00 1.57E-05 1.00E-05 7.44E-04 0.00E-00 7.35E-0-1 7.05E-01 4.76E-0-0 4.86E-00 9.05E-06 9.05E-01 9.07E-06 1.00E-05 7.44E-04 0.00E-00 7.35E-0-1 7.05E-01 4.76E-0-0 4.86E-00 9.05E-01 9.07E-06 1.00E-05 7.44E-04 0.00E-00 7.35E-0-1 7.05E-01 4.76E-0-0 4.86E-00 9.05E-01 9.07E-06 9.07E-06 9.07E-06 9.07E-06 9.07E-06 9.07E-01 9.07E-06 9.07E-01 9.07	X3E+04
215 Down-dip 1 2 55 0.00E+00 8.01E+06 8.0E+06 1.20E+05 1.45E-06 2.89E+07 1.5E-06 9.5E-06 4.25E+06 0.00E+00 1.40E-02 9.71E-01 4.12E+00 4.02E+00 8.85E+06 9.13E-01 8.77E+06 1.45E-01 7.91E+04 4	1E+04
216 Down-dip 1 2 9 0.00E-00 7.67E-06 7.67E-06 7.67E-06 2.88E-00 7.57E-06 6.74E-04 1.53E-05 8.55E-04 1.27E-04 0.00E-00 2.66E-00 1.90E-02 2.40E-00 3.40E-01 8.88E-06 8.48E-01 8.68E-06 2.78E-04 2.78E-04 3.00E-00 2.60E-00 1.90E-02 2.40E-00 3.40E-01 8.88E-06 8.48E-01 8.68E-06 2.78E-04 2.78E-04 3.00E-00 2.60E-00 1.90E-02 2.40E-00 3.40E-01 8.88E-06 8.48E-01 8.68E-06 2.78E-06 2.	IOE+04
218 Down-dip 1 2 99 0.00E+00 8.03E+06 8.03E+06 8.03E+06 1.22E-05 9.98E+06 9.22E-05 9.98E+06 9.22E-05 9.98E+06 9.22E-05 9.98E+06 9.22E-05 9.98E+06 9.22E-05 9.98E+06 9.22E-05 9.98E+06 9.22E-05 9.98E+06 9.22E-05 9.98E+06 9.22E-05 9.98E+06 9.22E-05 9.98E+06 9.22E-05 9	8E+04
219 Down-dp 1 2 78 0.00E-00 7.81E-06 7.81E-06 7.81E-06 1.85E-01 1.75E-04 1.29E-06 2.76E-04 2.84E-04 0.00E-00 5.41E-01 5.17E-01 1.47E-00 1.44E-00 8.76E-06 8.76E-06 8.76E-06 1.77E-04 1.29E-06 2.88E-07 0.00E-00 5.41E-01 5.17E-01 1.47E-00 1.44E-01 1.47E-00 1.44E-01 1.47E-00 1.44E-01 1.47E-00 1.44E-01 1.47E-00 1.44E-01 1.47E-00 1.44E-01 1.47E-01 1.	00€+04 10E+04
221 Down-dip 1 2 61 0.00E+00 2.00E+00 8.00E+00 8.00E+00 6.20E+00 6	8E+04
222 Down-dip 1 2 43 0.00E-00 7.98E-08 7.99E-08 2.89E-00 3.95E-06 2.49E-05 7.64E-06 5.42E-05 1.31E-05 0.00E-00 7.58E-02 7.50E-00 9.98E-01 9.73E-01 9	6E+04
224 Down-dip 1 2 62 0.00E+00 2.02E+05 1.0E+01 5.18E+07 8.40E+02 5.38E+05 1.0E+01 5.18E+07 8.40E+02 5.38E+05 1.0E+01 5.18E+07 8.40E+02 5.38E+05 1.0E+01 5.18E+07 8.40E+02 5.38E+05 1.0E+01 5.18E+07 8.40E+02 5.38E+05 1.0E+01 5.18E+07 8.40E+02 5.38E+05 1.0E+01 5.18E+07 8.40E+02 5.38E+05 1.0E+01 5.18E+07 8.40E+02 5.38E+05 1.0E+01 5.18E+07 8.40E+02 5.38E+05 1.0E+01 5.18E+07 8.40E+02 5.38E+05 1.0E+01 5.38E+01 5.	9E+04
225 Down-dip 1 2 34 0.00E+00 8.03E+06 8.03E+06 8.03E+06 2.88E+00 3.06E+06 8.13E+06 8	1E+04 (

7/13/97

	•				Escavaled																						
	•	•	•	•	Wasia Perceity	Residual Gas Sat. (traction)	Residual Brine Sal. (fraction)	Crushed Panel Height (m)	Up-dip Avg Pressure (Pa)	Up-dip Avg Sat. (fraction)	Down-dip Avg Pressure (Pa)	Down-dep Avg Sal. (fraction)	DPLZ Porosity	ORZ Permeability	Salt Piller Perceity	Salt Pittar Permesblity	Intrusion Time	Skin lactor	Well Productivity	BC well Sand Permeability	Total Area solids released	Cestile Reservoir	Castile Reservoir	Up-dip Brine Relative	Up-dip Gay Relative	Down-dip Brine Relative	Down-dip Gas Robitys
240	ın (Danka	Scan		(fraction)									(m^2)	(Fraction)	(m/2)	(Yease)		Index (1/Pa)	(m/2)	(m^2)	Pressure (Pa)	Parmeability (m^2)	Permeability (fraction)	Permeability (fraction)	Permeability (fraction)	Permeability (traction)
226 D	own-dip	Teolic.	2	85	5.76E-01	7.34E-03	2.60E-01	HEIGHT	PRESPANS 1.14E+07	BSATPAN2	PRESPAN4		6.30E-02		POROSITY 6.74E-02	PERM X	INTR_TME			PRM_SAND			PRM_CAST	KRW2	KRG2	KRW4	KRG4
	own-dip	1	2	66	5.20E-01	8.43E-02	5.49E-01	1.25E+00	7,49E+06	8.24E-03	8.13E+06	8.85E-01	7.92E-02	8.23E-18	1.06E-01	4.90E-16 5.37E-18	7.50E+02 7.50E+02	-1.23E+00 -1.37E+00	1,38E-13 1,30E-13	7.08E-16 1.66E-12	8.95E-01	1.19E+07 1.25E+07	7.76E-15	0.00E+00	1.00E+00	5.34E-03	5.18E-01
	own-dip own-dip	ì	2	57 87	4.60E-01 5.46E-01	7.43E-02 2.68E-02	2.79E-01 1.60E-01	1.12E+00 1.32E+00	3.97E+08 9.32E+06	2.69E-01 2.07E-02	8.14E+06 9.12E+06	9.06E-01 3.28E-01	5.60E-02	5.52E-18	8.89E-02	1.29E-18	7.50E+02	-1.19E+00	1.08E-13	8.13E-12	B.25E-01	1.30E+07	1.48E-14 7.84E-14	0.00E+00 0.00E+00	1.00E+00 1.00E+00	3.37E-01 5.97E-01	3.29E-04 4.87E-05
	own-dip	1	2	93	5.80E-01	4.00E-02	5.11E-01	1.43E+00	1.19E+07	6.34E-02	1.19E+07	5.77E-01	1.14E-01 8.30E-02	9.11E-20 1.70E-14	1.27E-01 8.84E-02	4.47E-20 1.70E-14		-9.15E-01 -9.34E-01	1.15E-13 1.25E-13	8.91E-14	4.74E-01	1.37E+07	2.51E-12	0.00E+00	1.00E+00	2.64E-03	5.85E-01
	own-dip own-dip	1	2	80	4.83E-01 5.89E-01	6.43E-02	2.68E-01			2.83E-02	8.04E+06	9.13E-01	3.58E-02	1.59E-18	6.23E-02	5.01E-19		-8.21E-01	9.77E-14	2.95E-14 2.09E-12	4.92E-01 3.93E-01	1.35E+07 1.39E+07	8.91E-13 2.04E-13	0.00E+00 0.00E+00	1.00E+00 1.00E+00	6.30E-04 6.26E-01	6.97E-01 6.75E-05
	own-dip	i	2	58	5.89E-01	1.11E-01 2.96E-02	1.90E-01 1.14E-01	1.46E+00 1.47E+00	1.27E+07 1.29E+07	1.43E-06 1.5BF-01	1.28E+07 1.28E+07	2.50E-01 1.71E-01	8.93E-02 1,96E-01	2.09E-19	8.79E-02	1.26E-19		-9.63E-01	1.29E-13	4.17E-16	5.22E-01	1.47E+07	3.16E-14	0.00E+00	1.00E+00	6.85E-05	8.22E-01
	own-dip	1	2	11	5.65E-01	6.24E-02	4.15E-01	1.38E+00	1.29E+07	2.68E-01	1.29E+07	8.02E-01	7.20E-02	1.67E-16 9.54E-13	1.97E-01 4.77E-02	1.45E-16 1.35E-13		-1.18E+00 -1.39E+00	1,41E-13 1,44E-13	3.09E-15 1.20E-14	8.11E-01 1.22E+00	1.26E+07	1.07E-13	1.53E-05	8.94E-01	4.09E-05	8.62E-01
	own-dip	1	2	10	5.86E-01 5.83E-01	3.17E-02 7.06E-02	1.73E-01	1.45E+00	1.48E+07	4.19E-01	1.49E+07	7.92E-01	7.28E-02	1.12E-13	6.10E-02	3.72E-14	2.00E+03	-1.33E+00	1.48E-13	1.86E-16	1.22E+00 1.08E+00	1.35E+07 1.09E+07	5.37E-15 1.35E-11	0.00E+00 1.13E-02	1 00E+00 4 12F-01	2.18E-01 3.42E-01	2.67E-02 1.71E-02
	own-dip	i	2	24	5.78E-01	9.01E-02	1.02E-01 1.37E-01	1.44E+00 1.42E+00	1.46E+07 1.40E+07	0.00E+00 9.08F-01	1.46E+07 1.41E+07	6.72E-01 9.08E-01	4.93E-02 1.94E-01	4.07E-13 4.31E-13	4.03E-02 1.90E-01	1.78E-13 2.82E-13	2.002,00	-1.38€+00	1.50E-13	5.50E-15	1.19E+00	1.39E+07	1.86E-13	0.00E+00	1.00E+00	1.87E-01	4 50E-02
	own-dip	1	2	94	5.84E-01	4.58E-03	1.85E-01	1.44E+00	1.46E+07	9.95E-01	1.47E+07	9.95E-01	2.24E-01	3.88E-13	1,93E-01	6.31E-15		-1.29E+00 -1.29E+00	1.42E-13 1.44E-13	2.63E-14 9.77F-16	9.94E-01 9.95E-01	1.09E+07 1.31E+07	7.41E-13 1.78E-12	6.60E-01 9.75E-01	1.82E-08	6.60E-01	1 81E-08
1	own-dip own-dip	1	2	73	5.64E-01 5.73E-01	5.61E-02 1.12E-01	3.03E-01 1.61E-02	1.38E+00 1.41E+00	1.28E+07 1.36E+07	2.57E-02 5.27E-01	1.28E+07	8,00E-01	9.73E-02	3.72E-16	1.03E-01	3.72E-16	2.00E+03	-8.01E-01	1.15E-13	6.17E-15	3.77E-01	1.35E+07	9.77E-12	0.00E+00	2.34E-09 1.00E+00	9.75E-01 2.88E-01	2.24E-09 1.75E-02
241 D		1	2	48	6.73E-01	1.02E-01	2.11E-01		1.36E+07	1.74E-01	1.37E+07 1.36E+07	B.86E-01 B.96E-01	1.80E-01 8.13E-02	5.30E-12 6.78F-13	1.22E-01 5.45E-02	1.18E-13 7.76E-14		-1.17E+00	1.34E-13	3.80E-15	7.83E-01	1.29E+07	1.12E-12	8.92E-02	1.02E-01	6.34E-01	2.17E-08
242 Di 243 Di		1	2	18	5.87E-01 5.65E-01	1.06E-01	3.40E-01		1.49E+07	4.17E-01	1.49E+07	8.93E-01	7.53E-02	1.16E-13	6.20E-02	3.31E-14		-1.29E+00 -1.09E+00	1.41E-13 1.34E-13	2.19E-15 6.17E-16	1.01E+00 6.69E-01	1.03E+07 1.05E+07	3.80E-12 5.25E-12	0.00E+00 3.55E-04	1.00E+00 7.16E-01	5.93E-01 5.19F-01	3.83E-08
244 D	own-dip wn-dwo	1	2	45 78	5.65E-01 5.95E-01	5.05E-02 4.93E-02	2.04E-01 1.51E-01	1.38E+00 1.48E+00	1.29E+07 1.57E+07	9.49E-01 6.49E-01	1.30E+07 1.57E+07	9.49E-01 8.62E-01	8.38E-02	5.57E-14	8.25E-02	5.13E-14	2.00E+03	-9.31E-01	1.20E-13	1.74E-15	4.89E-01	1.32E+07	4.57E-13	7.81E-01	3.41E-09	5.19E-01	4.54E-08 3.38E-09
245 D	own-dip	1	2	59	5.73E-01	1.07E-02	1.94E-01	1.41E+00	1.36E+07	3.90E-05	1.36E+07	6.76E-01	2.78E-01 1.91E-01	6.27E-10 4.49E-16	1.02E-01 1.86E-01	2.46E-15 1.66E-16	2.00E+03 2.00E+03	-1.06E+00 -1.20E+00	1.36E-13 1.36E-13	8.32E-17 1.35E-16	6.28E-01 8.44E-01	1.40E+07	1.07E-12	1.39E-01	7.87E-02	5.18E-01	2.25E-03
246 De		1	2	37 15	5.53E-01 5.77E-01	4.07E-02 4.22E-02	2.28E-01 5.21E-01	1.35E+00 1.42E+00	1.19E+07	7.75E-08	1.19E+07	6.92E-01	1.22E-01	9.92E-16	1.15E-01	3.98E-16		-1.19E+00	1.29E-13	1.35E-16 1.35E-15	8.44E-U1 8.19E-01	1.17E+07 1.18E+07	5.89E-14 6.17E-12	0.00E+00 0.00E+00	1.00E+00	1.49E-01 1.53E-01	8.92E-02 7.17E-02
248 D		i	2	19	5.77E-01	4.22E-02 1.42E-01	5.21E-01 2.97E-02	1.42E+00 1.41E+00	1.40E+07 1.37E+07	3.66E-01 3.21E-01	1.40E+07 1.38E+07	9.40E-01 8.53E-01	7.41E-02 2.05E-01	4,59E-14 8,99E-15	6.19E-02 1.93E-01	1.32E-14 1.41E-15	2.00E+03 2.00E+03	-9.48E-01	1.25E-13	1.32E-14	5.06E-01	1.06E+07	4.47E-13	0.00E+00	1 00E+00	6.10E-01	1.14E-04
	wn-dip	1	2	69	5.70E-01	8.98E-02	4.08E-01		1.33E+07	9.09E-01	1.34E+07	9.09E-01	8.52E-02	1.65E-14	8.23E-02	1.26E-14	2.00E+03 2.00E+03	-1.23E+00 -1.29E+00	1.38E-13 1.40E-13	2.00E-16 9.33E-15	8.94E-01 9.99E-01	1.18E+07 1.42E+07	1.45E-12 4.07E-13	1.17E-02 5.41E-01	3.49E-01 1.30E-08	5.44E-01	4.12E-07
250 De	wn-dio	1	2	52 31	5.63E-01 5.55E-01	3.68E-02 5.28E-02	4.49E-01 5.93E-02	,,,,,,	1.28E+07 1.20E+07	9.60E-01 1.99E-02	1.28E+07 1.20E+07	9.60E-01 7.84E-01	1.13E-01	1.70E-15	1.19E-01	1.70E-15		-9.48E-01	1.21E-13	4.17E-14	5.07E-01	1.43E+07	2.63E-13	7.57E-01	3.95E-07	5.41E-01 7.58E-01	1.29E-08
252 D	wn-dip	i	2	41	5.19E-01	3.40E-02	8.64E-02		9.29E+06	5.12E-02	9.51E+06	7.84E-01 6.03E-01	7.94E-02 1.44E-01	1.66E-15 1.70E-19	8.66E-02 1.56E-01	1.66E-15 1.70E-19	2.00E+03 2.00E+03	-1.27E+00 -1.22E+00	1.34E-13 1.22E-13	3.31E-14 3.24F-16	9.73E-01	1.40E+07	6.31E-13	0.00E+00	1.00E+00	3.82E-01	9.85E-03
253 Dx		1	2	2 39	5.36E-01 5.56E-01	8.22E-02	4.02E-01		1.05E+07	9.16E-01		9.16E-01	1.67E-01	4.47E-14	1.75E-01	4.47E-14		-1.29E+00	1.30E-13	5.01E-14	8.64E-01 9.98E-01	1.47E+07 1.25E+07	3.47E-12 7.24E-11	0.00E+00 5.71E-01	1.00E+00 1.15E-07	1.22E-01 5.71E-01	1.01E-01
	wn-dio	í	2	90	4.98E-01	1.50E-01 1.28E-02	2.98E-01 2.86E-01		1.21E+07 B.16E+06	8.47E-01 8.56E-03	1.22E+07 8.16E+06	8.47E-01 7.10E-01	2.24E-02 1.67E-02	3.02E-15 1.20E-17	2.83E-02	3.02E-15		-1.23E+00	1.32E-13	2.40E-13	8.82E-01	1.35E+07	1.78E-13	4.03E-01	3.55E-07	4.04E-01	3.51E-07
256 Do		1	2	65	5.53E-01	1.27E-01	8.96E-02			0.00E+00	1.19E+07			8.71E-16	3.77E-02 2.91E-02	1.20E-17 8.71E-16	2.00E+03 2.00E+03	-8.48E-01 -1.16E+00	1.01E-13 1.28E-13	2.09E-14 4.17E-15	4.15E-01 7.73E-01	1.29E+07 1.26E+07	3.02E-12	0.00E+00	1.00E+00	1.47E-01	8.92E-02
257 Do		1	2	67 46	5.35E-01 5.35E-01	1.21E-01 2.03E-02	6.61E-02 2.35E-01		1.05E+07 1.05E+07	8.24E-02		5.36E-01	1.70E-01	3.55E-18	1.80E-01	3.55E-18	2.00E+03		1.28E-13	7.24E-15	9.65E-01	1.28E+07	3.72E-12 1.15E-14	0.00E+00 0.00E+00	1.00E+00 1.00E+00	7.24E-02 7.93E-02	1 13E-01
259 Do		i	2	100	5.34E-01	1.14E-01	3.43E-01		1.03E+07	9.60E-06 8.84E-01	1.04E+07 1.05E+07	8.85E-01 8.84E-01	4.89E-02 7.15E-02	1.59E-17 9.12E-16	6.17E-02 8.43E-02	1.59E-17 9.12E-16		-1.41E+00 -1.26E+00	1.36E-13		1.26E+00	1.50E+07	1 15E-11	0.00E+00	1.00E+00	5.48E-01	3.34E-03
260 Do		1	2	35	5.34E-01	9.57E-02	4.39E-01		1.04E+07	9.03E-01	1.05E+07	9.03E-01	5.65E-02	7.24E-15	6.40E-02	7.24E-15			1.28E-13 1.11E-13	2.51E-14 1.38E-13	9.43E-01 4.57E-01	1.25E+07 1.12E+07	1.29E-13 3.98E-11	4.86E-01 4.94E-01	1.30E-07 1.08E-07	4.86E-01 4.94E-01	1.27E-07
	wn-dip wn-dip	1	2	20 30	5.32E-01 5.26E-01	1.23E-01 1.16E-01	1.27E-01 4.16F-02		1.02E+07 9.77E+06	5.96E-08 8.83E-01	1.03E+07 9.86E+06		2.27E-02 2.94E-02	1.35E-17 2.75E-14	3.62E-02 4.38E-02	1.35E-17	2.00E+03	-6.04E-01	1.00E-13		2.55E-01	1.28E+07	1.20E-12	0.00E+00	1.00E+00	6.70E-02	1.07E-07 1.21E-01
	wn-dip	1	2	36	5.50E-01	3,71E-03	1.39E-01	1.33E+00	1.17E+07	1.19E-07	1.16E+07	5.44E-01	4.78E-02	6.97E-20	5.33E-02	2.75E-14 6.61E-20			1.00E-13 1.15E-13	2.19E-13 B.13E-15	2,79E-01 4,50E-01	1.34E+07 1.36E+07	1.59E-13	6.19E-01	1.55E-09	6.19E-01	1.54E-09
264 Do	wn-dip	1	2	25 95	5.69E-01 5.56E-01	8.68E-02 1.46E-01	5.41E-01 3.69E-01		1.33E+07	8.22E-02	1.33E+07	7.47E-01	1.06E-01	1.75E-15	7.69E-02	3.39E-17	2.00E+03	-1.13E+00	1.31E-13	1.26E-16	7.23E-01	1.38E+07	1.45E-13 3.89E-13	0.00E+00	1.00E+00	6.16E-02 5.22F-02	2.00E-01
	wn-dip	i	5	60	5.19E-01	6.13E-02	4.70E-02		1.21E+07 9.41E+06	9.18E-02 1.10E-01	1.22E+07 9.12E+06	6.38E-01 7.87E-01	1.57E-01 1.94E-01	6.03E-17 6.05E-18	1.62E-01 2.06E-01	6,03E-17 5.75E-18		-9.54E-01 -1.17E+00	1.19E-13 1.19E-13	1,10E-16	5.13E-01	1.30E+07	1.70E-11	0.00E+00	1.00E+00	4.30E-02	1.25E-01
	wn-dip	1	2	47	4.98E-01	6.75E-02	1.61E-01	1.20E+00	B.13E+06	1.65E-01	8.26E+06	5.57E-01	1.48E-01	6.92E-18	1.64E-01	6.926-18		-1.17E400 -1.09E+00	1.19E-13	6.61E-13 2.19E-16	7.91E-01 6.75E-01	1.30E+07 1.20E+07	2.34E-14 1.55E-12	4.47E-05 3.78E-09	8.53E-01 9.89E-01	3.92E-01 6.24E-02	7.91E-03 1.61F-01
	wn-dip wn-dio	1	2	99 23	5.4BE-01 5.29E-01	1.28E-01 7.29E-02	5.15E-01 4.80E-01		1.15E+07 9.98E+06	1.18E-01 8.35F-03		8.26E-01 8.83E-01	1.72E-01 3.54E-02	5.89E-17	1.81E-01			-7.63E-01	1.09E-13	6.17E-17	3.50E-01	1.25E+07		0.00E+00	1.00E+00	1.95E-01	3.43E-03
270 Do	wn-dip	i	2	79	6.03E-01	1.23E-01	3.88E-01			3.07E-02		5.43E-01	2.41E-01	1.18E-16 6.49E-11	4.78E-02 1.64E-01	1.18E-16 2.57E-13	2.00E+03 2.00E+03	-1.18E+00	1.22E-13 1.41E-13	7.94E-17 1.51E-16	8.09E-01 6.89E-01	1.50E+07 1.24E+07	6.03E-13	0.00E+00	1.00E+00	3.92E-01	1.53E-03
271 Do		1	2	5 27	5.01E-01 5.13E-01	1,29E-01 1,18E-01	1.21E-01 4.62E-01		8.40E+06 8.96E+06	4.06E-05			1.34E-01	1.90E-17	1.57E-01	1.82E-17	2.00E+03	-1.37E+00	1.25E-13	1.82E-12	1.17E+00	1.50E+07	4.37E-15 3.31E-13	0.00E+00 0.00E+00	1.00E+00 1.00E+00	6.27E-03 2.69E-01	4.00E-01 9.00E-03
	wn-dip	i	2	71	5.13E-01	1.57E-02	4.02E-01		9.54E+06	1.59E-02 1.31E-06		8.10E-01 4.75E-01		1.86E-16 2.19E-18	4.33E-02 6.42E-02	1.86E-16 2.19E-16			1.21E-13	2.40E-15	9.09E-01	1.19E+07	1.26E-12	0.00E+00		2.00E-01	8.01E-03
274 Do		!	2	97	5.15E-01	8.37E-02	4.34E-01		9.06E+06	9.04E-01	9.13E+06	9.12E-01	1.48E-01	5.83E-16	1.70E-01			-1,37E+00 -8,88E-01	1.31E-13 1.06E-13	5.25E-17 4.57E-13	1.18E+00 4.49E-01	1.19E+07 1.38E+07	6.76E-13 3.02E-11	0.00E+00 5.03F-01	1.00E+00 2.77E-05	3 81E-02	2.59E-01
275 Do	wn-dip wn-dip	1	2	98 56	5.13E-01 5.57E-01	3.56E-02 4.66E-02	5.00E-02 3.20E-01		8.91E+06 1.22E+07	5.78E-06 1.67E-06	9.08E+06 1.22E+07	4.21E-01 5.57E-01	6.12E-02 9.18E-02	4.19E-19	8.38E-02	4.17E-19		-1.23E+00	1.20E-13	4.79E-15	8.82E-01	1.17E+07	3.98E-14	0.00E+00	1.00E+00	5.37E-01 3.09E-02	9.93E-07 2.77E-01
277 Do	wn-dip	i	2	42	5.78E-01	1.04E-01	3.92E-01			3.10E-02				1.45E-15 3.25E-13	8.89E-02 1.13E-01	1.05E-15 7.76E-17		-7.21E-01 -1.26E+00	1.10E-13 1.41E-13		3.22E-01			0.00E+00	1.00E+00	2.04E-02	3 18E-01
278 Do	wn-dip wn-dip	1	2	77 93	5.31 E-01 5.12 E-01	1.48E-01 4.00E-02	6.84E-02		1.01E+07	1.24E-04	1.03E+07	3.88E-01	2.00E-01	B.13E-19	2.16E-01	8.13E-19	2.00E+03	-7.13E-01	1.04E-13	1.38E-15 2.75E-16	9.46E-01 3.17E-01	1.47E+07 1.23E+07	3.63E-13 1.20E-11	0.00E+00 0.00E+00	1.00E+00 1.00E+00	8.20E-03 1.93E-02	3.82E-01 2.74E-01
	wn-dip	1	5	93 85	5.72E-01 5.56E-01	4.00E-02 7.34E-03	5.11E-01 2.60E-01		8.92E+06 1.22E+07	4.95E-03 9.45E-02		6.38E-01 4.46E-01	8.25E-02 6.94E-02	1.70E-14 4.90E-16	1.03E-01 7.03E-02	1.70E-14 4.90E-16		-9.34E-01	1.07E-13	2.95E-14	4.92E-01	1.35E+07	8.91E-13	0.00E+00	1.00E+00	6.68E-03	4.54E-01
	wn-dip	1	2		5,19E-01	5.75E-02	2.76E-01			2.70E-05				2.22E-19	1.24E-01				1.33E-13 1.25E-13	7.08E-16 1.91E-14	8.95E-01 1.01E+00	1.19E+07 1.52E+07		0.00E+00 0.00E+00	1.00E+00	6.12E-03	5.02E-01
	wn-dip wn-dia	1	2	70 76	5.05E-01 5.21E-01	4.63E-02 1.38E-01	4.24E-01 3.34E-01		8.48E+06 9.43E+06					6.17E-20	2.41E-01	8.17E-20	2.00E+03	-1.28E+00	1.21E-13	1.00E-16	9.91E-01	1.28E+07		0.00E+00	1.00E+00	8.65E-03 6.16E-03	4.26E-01 4.68E-01
284 Do	wn-dip	i	2	62	5.68E-01	1.39E-01	5.05E-01			4.17E-07 2.54E-02				3.16E-18 1.41E-18	5.16E-02 5.38E-02				1.28E-13 1.45E-13		1.09E+00	1.33E+07	2.09E-12	0.00E+00	1.00E+00	3.66E-03	4.65E-01
	wn-dip	1	2	6B	5.45E-01	6.78E-04	5.01E-01			0.00E+00		5.27E-01	2.95E-02	9.73E-17		9.12E-17		.,	1.34E-13		1.19E+00 1.06E+00	1.38E+07 1.38E+07		0.00E+00 0.00E+00	1.00E+00 1.00E+00	1 83E-03 1.95E-05	5.04E-01 8.91E-01
	wn-dip wn-dip	1	2	58 10	5.86E-01 6.07E-01	2.96E-02 3.17E-02	1.14E-01 1.73E-01		1.48E+07 1.65E+07	6.34E-02 3.38E-02		1.27E-01 7.54E-01		2.62E-14	1.99E-01				1.39E-13	3.09E-15	8.11E-01	1.26E+07		0.00E+00	1.00E+00	1.64E-07	9.69E-01
288 Do	wn-dip	1	2	12	5.60E-01	7.06E-02	1.02E-01	1.36E+00	1.24E+07	0.00E+00	1.25E+07			8.89E-12 1.78E-13	5.80E-02 4.26E-02				1.56E-13 1.42E-13		1.08E+00 1.19E+00	1.09E+07 1.39E+07		0.00E+00 0.00E+00		2.71E-01	3.00E-02
	wn-dio	1	2	24 94	5.77E-01 5.83E-01	9.01E-02 4.58E-03			1.39E+07	9.08E-01		9.08E-01	1.95E-01	4.73E-13	1.90E-01	2.82E-13	4.00E+03	-1.29E+00	1.42E-13		9.94E-01		7.41E-13	0.00E+00 6.60E-01	1.00E+00 1.99E-08	2.48E-01 6.60E-01	2.60E-02 1.97E-08
	wn-dip	i	2	48	5.77E-01	1.02E-01	2.11E-01			9.95E-01 6.20E-02				2.51E-13 1.67E-12	1.93E-01 5.40E-02				1.44E-13		9.95E-01	1.31E+07	1.78E-12	9.75E-01	2.65E-09	9.75E-01	2.53E-09
	wn-dip	1	2		5.72E-01	5.05E-02	2.04E-01		1.35E+07	9.49E-01	1.36E+07	9.49E-01	6.92E-02	1.01E-13	8.11E-02	5.13E-14		-1.29E+00 -9,31E-01	1.43E-13 1.22E-13	2.19E-15 1.74E-15	1.01E+00 4.89E-01	1.03E+07 1.32E+07	3.80E-12 4.57E-13	0.00E+00 7.82E-01	1.00E+00 2.64E-09	5.98E-01	8.52E-11
	wn-dip wn-dio	1	2	44 18	5.64E-01 6.07E-01	1.12E-01 1.06E-01	1.81E-02 3.40E-01			4.04E-01 1.96E-01				7.98E-13	1.25E-01	1.18E-13	4.00E+03	1.17E+00	1.31E-13	3.80E-15	7.83E-01	1.29E+07	1.12E-12	7.82E-01 3.23E-02	2.64E-09 2.29E-01	7.82E-01 6.39E-01	2.63E-09 2.57E-10
295 Co	wn-dib-nw	Í	2	78	6.04E-01	4.93E-02	1.51E-01			3.71E-01		8.41E-01 5,73E-01	1.37E-01 2.66E-01	8.85E-12 1.00E-09	5.90E-02 9.92E-02	3.31E-14 2.46E-15	4.00E+03 -		1.41E-13 1.39E-13			1.05E+07	5.25E-12	0.00E+00	1.00E+00	3.61E-01	1.46E-03
296 Do		1	2		5.96E-01		2.97E-02			9.68E-02	1.57€+07	8.34E-01	2.54E-01	2.28E-11	1.83E-01	1.41E-15				8.32E-17 2.00E-16	6.28E-01 8.94E-01			6.78E-03 5.19E-05	4.67E-01 8.33E-01	7.56E-02 4.99E-01	1.48E-01
	qib-mw cib-mw	1	2	69 11	5.79E-01 5.39E-01	8,98E-02 6,24E-02	4.08E-01 4.15E-01		1.41E+07 1.08E+07	9.09E-01 1.39E-01				4.77E-14	8.07E-02	1.26E-14	4.00E+03 ·	1,29E+00	1.43E-13	9.33E-16	9.99E-01	1.42E+07		5.41E-01		5.41E-01	4.15E-05 7.70E-09
299 Do	φn-dip	1	2	46	5.39E-01	2.03E-02	2.35E-01	1.30E+00	1.08E+07				4.82E-02 4.97E-02	1.35E-13 1.59E-17	5.05E-02 6.12E-02		4.00E+03 -		1.36E-13 1.37E-13		1.22E+00 1.26E+00			0.00E+00		6.56E-02	1.41E-01
300 Do	wn-dip	1	2	58	5.92E-01	2.96E-02	1.14E-01	1.47E+00	1.54E+07	7.73E-05	1.54E+07			4.04E-13			4.00E+03						1.15E-11 1.07E-13	0.00E+00 0.00E+00		1.56E-01 6.44E-02	7.93E-02 1.80E-01
																										J. 74C 7/2	7.00€~01

					I	Down-dip																	_	
1	•				Up-dip Flowing Bottom-hole	Flowing	BC well Injection	Duralism		Ges Rate (ref		Max Gas Rate		Cum Brine from Boundary	(One Plate	Clim Gee	Cum Brine	Cum Rone	Avg Brine Pressure	Avg Hima Saturation	Avg Birne	Avg Bride Seturation	Fxcetvetod	Total
					Pressure (Pa)	Bottom-hole Pressure (Pa)	D	(Days)	(m*3/s)	m/3/e)	Flate (m^3/s)	(ref m^Ua)	Ratio (m^3/s)	Condition Wall	(mac//day)	Produced (ref	Prockroad (m/3)	Relatoes (m/3)	Panel 5 (Pa)	Panel 5 (Iraction) after	Pressure Panel 0 (Pa)	Panel 0	Waste Pore	Excevated Brine Volume
No.	ID.	Replic	. Scan.	Vector	FBHP2	FBHP4	BHP_ABAN	time	BRINEFLW	GASFLW	MAX RAN	MAX GAS	LOR MET	· · · · · · · · · · · · · · · · · · ·	GAS_RATE	0.4001/T		· · · · ·	atter Biowout	blowout	after blowout	(traction) alter blowout	(fraction)	(m*3)
226	Down-dip	1	2	85	0,00E+00	2.78E+05	4	1.10E+01	4.97E-07	1.81E-01	3.91E-06	9.35E+00	1.53E+00	0.00E+00	5.52E+02		7.97E-01	7.72E-01	9RNPRES5 3.35E406	4.56E-01		SATBRNO	WASTE_PV	
	Down-dip Down-dip	1	2	66 57	0.00E+00	7.89E+06 8.03E+06		2.88E+00	2.33E-06	4.88E-05	4.89E-06	6.59E-05	5.01E+04	0.00E+00	1.49E-01	1.46E+01	7.32E-01	7.18E-01		8.88E-01	1.14E+07 7.49E+06	1.01E-01 B.25E-03	9.10E+04 7.30E+04	
	Down-dip	i	2	87	0.00E+00	2.36E±05		2.88E+00 1.10E+01	1.52E-06 1.68E-07	2.47E-06 1.17E-01	3.54E-06 1.28E-06	5,19E-06 5,70E+00	6.30E+05 7.83E-01		7.53E-03	7.49E-01	4.72E-01	4.63E-01	8.14E+06	9.08E-01	3.97E+06	2.04E-01	5.77E+04	
	Down-dip	1	2	93	0.00E+00	3.07E+05		1.10E+01	1.85E-07	4.59E-01	4.37E-07	1.25E+01	2.07E-01	0.00E+00 0.00F+00	3,58E+02 1,40E+03		2.73E-01 1.62E-01	2.64E-01	2.72E+06	3.47E-01	9.31E+06	2.07E-02	8.11E+04	
	Down-dip Down-dip	1	2	BO	0.00E+00	8.02E+06		2.88E+00	2.67E-07	5.19E-07	5.80E-07	1.11E-06	5.17E+05	8.01E-08	1.58E-03	1.58E-01	8.14E-02	1.61E-01 7.98E-02	3.90E+06 8.04E+06	5.92E-01 9.15E-01	1.16E+07 5.29E+06	6.38E-02 2.84E-02	9.33E+04	
	Down-din	1	2	- 4 - 58	0.00E+00 3,79E+05	3.56E+05 3.65E+05	3.56E+05 3.66E+05	1.10E+01	4.86E-09 4.68E-09	1.84E-01	5.24E-08	1.72E+01	1.24E-02	0.00E+00	5.62E+02	7.23E+05	8.95E-03	8.61E-03		2.71E-01	1.27E+07	1.46E-06	6.32E+04 9.67E+04	2.66E+04 6.48E+03
	Down-dip	1	2	11	0.00E+00	1.81E+06	1.91E+06	1.10E+01	1.14E-04	4.38E-01 2.38E-01	3.43E-08 1.65E-04	1.99E+01 5.61E-01	6.34E-03 6.08E+02	0.00E+00 0.00E+00	1.34E+03 7.28E+02		7.15E-03	6.78E-03	4.01E+06	1.94E-01	1.28E+07	1.56E-01	9.70E+04	
	Down-dip	1	2	10	3.56E+05	4.44E+06	4.44E+06	1.10E+01	1.06E-04	1.04E-01	2.52E-04	3.99E-01	1.15E+03		3.18E+02		1.22E+02 1.22E+02	1.16E+02 1.14E+02		8.14E-01	1.26E+07	1 61E-01	8.75E+04	
	Down-dip Down-dip	1	2	12 24	0.00E+00 8.00E+06	5.14E+05		1.10E+01	1.05E-04	7.00E-01	1.89E-04	1.41E+00	1.67E+02		2.14E+03			1.07E+02		7.99E-01 6.76E-01	1.48E+07 1.39E+07	2.63E-01 1.05E-07	9.56E+04 9.44E+04	
	Down-dip	í	2	94		8.00E+06 8.00E+06	8.00E+06 8.00E+06	2.88E+00 2.88E+00	2.15E-04 1.91E-04	2.69E-05 2.75E-07	2.76E-04 4.49E-04	2.69E-05 2.75E-07	1.12E+07	0.00E+00	8.22E-02	4.98E+00	5.55E+01	5.41E+01	1.38E+07	9.08E-01	1.40E+07	8.92E-01	9.23E+04	
239	Down-dip	1	2	73	0.00E+00	3.87E+06	3.87€+06	1.10E+01	3.56E-05	3.96E-02	1.41E-04	2.75E-07 2.38E-01	8.05E+08 8.36E+02	0.00E+00	8.40E-04 1.21E+02	6.39E-02	5.14E+01	5.02E+01	1.38E+07	9.94E-01	1.45E+07	7.60E-01	9.45E+04	8.17E+04
	Down-dip	1	2	44	4.48E+05	8.00E+06		2.88E+00	1.68E-04	4.46E-05	2.32E-04	4.46E-05	4.82E+06	0.00E+00	1.36E-01	5.44E+04 9.04E+00		4.29E+01 4.24E+01	9.68E+06 1.35E+07	8.03E-01 8.86E-01	1.28E+07 1.36E+07	2.63E-02		2.53E+04
	Down-dip Down-dip	1	2	48 18		8.00E+06	8.00E+06	2.88E+00	1.50E-04	1.08E-04	2.26E-04	1,08E-04	1.84E+06	0.00E+00	3.28E-01	2.15E+01	3.95E+01	3.86E+01	1.34E+07	8.96E-01	1.36E+07	2.95E-01 1.45E-01	9.05E+04	5.23E+04 4.61E+04
	Down-dip	1	2	45	7.99E+06	8.00E+06 7.99E+06		2.88E+00 2.88E+00	1.36E-04 1.37E-04	4.31E-04 1.13E-05	2.32E-04 2.24E-04	4.32E-04 1.13E-05	4.23E+05	0.00E+00	1.32E+00			3.63E+01	1.47E+07	8.93E-01	1.49E+07	3.38E-01	9.58E+04	
	Down-dip	1	2	78	3.13E+05	7.64E+06	7.64E+06	2.88E+00	1.32E-04	2.08E-02	2.71E-04	3,69E-02	1.83E+07 6.18E+03	0.00E+00 0.00E+00	3.43E-02 6.34E+01	2.04E+00 5.74E+03	3.71E+01 3.54E+01	3.63E+01 3.46E+01	1.25E+07	9.48E-01	1.29E+07	9.49E-01	B.75E+04	8.30E+04
	Down-dip	1	2	59	0.00E+00	3.89E+05	3.89E+05	1.10E+01	2.44E-05	1.40E-01	1.28E-04	2.23E+00	1.40E+02	0.00E+00	4.27E+02			3.19E+01	1.55E+07 6.94E+08	8.64E-01 6.83E-01	1.56E+07 1.36E+07	4.16E-01 8.92E-05	9.91E+04	6.42E+04
	Down-dlp Down-dlp	1	2	37 15	0.00E+00 0.00E+00	2.89E+05 8.04E+06	2.89E+05 8.04E+06	1.10E+01	2.38E-05	1.05E-01	1.10E-04	1.33E+00	1.90E+02		3.20E+02		3.15E+01	3.07E+01	6.77E+06	6.99€-01	1.19E+07	1.45E-05	9.03€+04 8.35E+04	1.70E+04 2.12E+04
	Down-dlp	i	2	19	3.34E+05	8.02E+06	8.02E+06	2.88E+00 2.88E+00	1.13E-04 8.97E-05	1.26E-03 6.65E-04	2.18E-04 2.07E-04	1.97E-03 6.65E-04	8.02E+04 2.27E+05	0.00E+00 0.00E+00	3.83E+00			3.04E+01	1 36E+07	9.40E-01	1.40E+07	3.43E-01	9.21E+04	5.19E+04
	Down-dip	1	2	69	7.99E+06	7.99E+06	7.99E+06	2.88E+00	9.71E-05	3.13E-04	1.96E-04	3.14E-04	4.39E+05	0.00E+00	2.03E+00 9.56E-01		2.80E+01 2.77E+01	2.75E+01 2.71E+01	1.36E+07	8.54E-01	1.37E+07	2.12E-01	9.11E+04	4.81E+04
	Down-dip Down-dip	1	2	52	B.01E+08	8.01E+06		2.BBE+00	8.44E-05	6.72E-05	2.11E-04	6.72E-05	1.66E+06	0.00E+00	2.05E-01	1.48E+01	2.45E+01	2.40E+01	1.32E+07 1.24E+07	9.10E-01 9.60E-01	1.33E+07 1.27E+07	9.06E-01 8.37E-01	8.94E+04 8.70E+04	8.11E+04 7.76E+04
	Down-dip	1	2	31 41	0.00E+00 0.00E+00	5.81E+06 7.42E+05	5.81E+06 7.42E+05	2.88E+00 1.10F+01	5.74E-05	3.16E-02	1.53E-04	1.03E-01	1.72E+03	D.00E+00	9.69E+01	9.97E+03	1.71E+01	1.68E+01	1.14E+07	7.88E-01	1.20E+07	1.11E-02	8.40E+04	3.02E+04
1	Down-dip	1	2	2		8.00E+06	8.00E+06	2.88E+00	1.20E-05 5.83E-05	6.89E-02 1.96E-05	6.19E-05 9.19E-05	1.07E+00 1.96E-05	1.36E+02 4.15E+06	0.00E+00 0.00E+00	2.10E+02	1.23E+05	1.68E+01	1.58E+01	5.12E+06	6.12E-01	9.30E+06	5.13E-02	7.29E+04	2.22E+04
	Down-dip	1	2	39	8.01E+06	8.01E+06	8.01E+05	2.88E+00	5.02E-05	5.21E-04	1.06E-04	5.21E-04	1.69E+05	0.00E+00	5.98E-02 1.59E+00	3.79E+00 9.21E+01	1.57E+01 1.55E+01	1.53E+01 1.52E+01	1.05E+07 1.21E+07	9.17E-01 0.50E-01	1.05E+07	7.42E-01	7.78E+04	6.37E+04
	Down-dip Down-dip	1	2	90 65	0.00E+00			1.10E+01	1.11E-05	4.10E-02	5.43E-05	5.96E-01	2.10E+02	0.00E+00	1.25E+02	7.39E+04	1.55E+01	1.49E+01	4.30E+06	7.17E-01	1.21E+07 8.16E+06	7.62E-01 6.51E-03	8.43E+04 6.67E+04	6.74E+04 2.11E+04
	оми-dio	1	2	67	0.00E+00 0.00E+00			1.10E+01 1.10E+01	1.11E-05 1.04E-05	1.41E-01 9.89E-02			6.07E+01	0.00E+00	4.30E+02	2.45E+05	1.49E+01	1.47E+01	6.40E+06	5.49E-01	1.19E+07	0.00E+00		1.17E+04
	Down-dip	i	2	46		7.36E+06		2.88E+00	3.72E-05	5.46E-03	4.85E-05 1.09E-04	1.49E+00 1.51E-02	8.17E+01 6.80E+03	0.00E+00 0.00E+00	3.02E+02 1.67E+01	1.69E+05	1.38E+01	1.36E+01	5.70E+06	5.48E-01	1.05E+07	5.89E-02		1.92E+04
	Down-dlp	1	2	100	8.00E+06	8.00E+06	8.00E+06	2.88E+00	3.25E-05	6.87E-05	7.26E-05	6.87E-05	8.38E+05	0.00E+00	2.105-01	1.71E+03 1.21E+01	1.16E+01 1.01E+01	1.14E+01 9.91E+00	1.01E+07 1.04E+07	8.87E-01 8.86E-01	1.05E+07 1.04E+07	1.02E-05	7.75E+04	
	Down-dip Down-dip	1	2	35 20				2.88E+00	3.44E-05	4.00E-05	6.44E-05	4.00E-05	1.37E+06	0.00E+00	1.22E-01	7.26E+00		9.68E+00	1.04E+07	9.04E-01	1.03E+07	8.65E-01 8.17E-01	7.72E+04 7.72E+04	6.70E+04 6.60E+04
	Xown-din	i	2	30			3.54E+05 7.99E+06	1.10E+01 2.88E+00	7.53E-06 3.50E-05	9.70E-02 2.08E-06	3.17E-05 5.55E-05	1.28E+00 2.08E-06	5.90E+01	0.00E+00	2.96E+02			9,61E+00	5.52E+06	5.59E-01	1.02E+07	5.96E-08		1.23E+04
263 [own-dip	1	2	36				1.10E+01	6.09E-06	1.09E-01	3.79E-05		2.67E+07 3.59E+01	0.00E+00 0.00E+00	6.36E-03 3.32E+02	3,60E-01 2,59E+05	9.59E+00 9.29E+00	9.37E+00		8.86E-01	9.75E+06	6.76E-01		0.1 12 101
,	>own-dip	1	2	25			4.22E+05	1.10E+01	6.19E-06	8.98E-02	4.20E-05		4.51E+01			2.12E+05	9.55E+00	9.18E+00 9.14E+00	4.46E+06 4.86E+06	5.56E-01 7.56E-01	1.17E+07 1.33E+07	1.19E-07 8.25E-02		1.17E+04
1	Down-dip Down-dip	1	2	95 60			3.79E+05	1,10E+01	5.79E-06	1.19E-01			3.57E+01	0.00E+00	3.62E+02	2.23E+05	7.95E+00	7.88E+00	5.78E+06	6.49E-01	1.21E+07	9.24E-02	8.91E+04 8.44E+04	
	Jown-dip	i	2	47				2.88E+00 1.10E+01	2.59E-05 5.40E-06	9.96E-03 6.97E-02	6.68E-05 2.63E-05	2.70E-02 1.24E+00	2.57E+03 5.69E+01		3.04E+01	3.11E+03	7.98E+00	7.83E+00	8.88E+06	7.91E-01	9.41E+06	1.00E-01		
	Down-dip	1	2	99				2.88E+00	2.26E-05	1.11E-02	5.20E-05		2.03E+01		2.13E+02 3.38E+01	1.29E+05 3.40E+03	7.32E+00 6.90E+00	7.03E+00 6.76E+00	4.14E+06	5.68E-01	8.13E+06	1.50E-01		2.48E+04
)own-dip	1	2	23				2.88E+00	2.19E-05	2.46E-03	5.56E-05				7.50E+00	7.53E+02	6.87E+00	6.73E+00	1.12E+07 9.85E+06	8.30E-01 8.86E-01	1.15E+07 9.98E+06	1.18E-01 8.48E-03	8.17E+04 7.56E+04	
	Down-dip Down-dip	1	2	79 5			3.90€+05 5.21E+06	1.10E+01	8.56E-06	4.18E+00	8.56E-06		1.25E+00	0.00E+00	1.27E+04	5.75E+06	7.20E+00	6.70E+00	1.16E+07	5.59E-01	1.20E+07	1.73E-02	1.02E+05	
	own-dip	i	2	27				2.88E+00 2.88E+00	1.84E-05 1.84E-05	1.03E-02 1.32E-02	4.74E-05 4.77E-05				3.15E+01	3.28E+03		5.61E+00	7.96E+06	7.43E-01	8.40E+06	9.05E-05		1.69E+04
	жи-фр	1	2	71	0.00E+00			1,10E+01	3.46E-06		2.24E-05		2.21E+01		4.01E+01	4.14E+03 2.33E+05	5.61E+00	5.50E+00 5.10E+00		8.14E-01 4.90E-01	8.96E+06	1.61E-02	7.10E+04	
	Xown-dip Xown-dip	1	2	97 98				2.88E+00	1.43E-05	6.69E-06	3.04E-05	6.69E-06	3,13E+06	0.00E+00	2.04E-02	1.39E+00	4.33E+00	4.24E+00		9.14E-01	9.54E+06 9.05E+06	1.31E-06 7.04E-01	7.39E+04 7.16E+04	9.21E+03 5.71E+04
1	Xown-dio	÷	2	56				1.10E+01 1.10E+01	2.61E-06 2.17E-06	9.81E-02	1.57E-05	2.80E+00	1.73E+01		2.99E+02	2.21E+05		3,71E+00	3.69E+06	4.36E-01	8.91E+06	5.81E-06		7.84E+03
277 ()owπ-dip	1	2	42			3.38E+05	1.10E+01	2.66E-06	1.80E-01 1.45E+00	4.28E-05 7.61E-06	5.25E+00 1.07E+01	7.60E+00 1.74E+00		5.48E+02 4.42E+03		3.18E+00	3.17E+00	4.38E+06	5.70E-01	1.22E+07	5.63E-06		1.60E+04
1	lown-dip	1	2	77		2.71E+05	2.71E+05	1.10E+01	1.79E-06	1.29E-01			9.06E+00		3.93E+02		2.77E+00 2.56E+00	2.76E+00 2.51E+00	9.47E+06 4.26E+06	5.72E-01 4.05E-01	1.29E+07 1.01E+07	3.14E-02 1.24E-04		1.60E+04
	own-dip	!	2	93 85	0.00E+00			1.10E+01	1.32E-06		3.06E-06		3.87E+00	0.00E+00	5.57E+02	3.15E+05	1.22E+00	1.11E+00	3.50€+06	6.52E-01	8.80E+06	5.40E-03		8.68E+03 1.29E+04
1	lown-dip	í	2	16	0.00E+00 0.00E+00		_,	1.10E+01 1.10E+01	5.61E-07 5.58E-07		4.61E-06 4.66E-06	9.94E+00 4.66E+00	1.73E+00 3.70E+00		5.45E+02	5.28E+05	9.11E-01	8.89E-01	3.45E+06	4.62E-01	1.22E+07	9.50E-02	8.46E+04	1.59E+04
282 (lown-dip	1	2	70	0.00E+00			1.10E+01	2.9BE-07		2.99E-06				2.51E+02 1.62E+02	2.49E+05 1.91E+05	9.20E-01 5.30E-01	8.77E-01 5.11E-01	2.71E+06 2.13E+06	4.91E-01	9.34E+05	2.70E-05		1.24E+04
	lown-dip	1	2	76				1.10E+01	2.39E-07	8.81E-02	2.09E-06				2.69E+02	2.72E+05	3.96E-01	3.87E-01	2.13E+06	5.B2E-01 4.95E-01	8.48E+06 9.44E+06	1.88E-05 4.17E-07		1.27E+04 9.78F+03
	lown-dip lown-dip	1	2	62	0.00E+00 0.00E+00	3.21E+05		1.10E+01	1.20E-07		1.63E-06	1.26E+01	6.20E-01	0.00E+00	2.51E+02	3.82E+05	2.37E-01	2.37E-01	2.40E+06	6.08E-01	1.32E+07	2.55E-02		1.56E+04
	own-dip	i	2	58	0.00E+00			1.10E+01 1.10E+01	9.94E-10 4.19E-11	7.77E-02 1.94E+00	1.36E-08 1.56E-10	1.52E+01 2.90E+01	5.08E-03 1.78E-05			3.97E+05	2.02E-03	1.99E-03	1.80E+06	5.42E-01	1.12E+07	0.00E+00	8.07E+04	
287 0	lown-dip	1	2	10	0.00E+00	2.20E+06		1.10E+01	1.48E-04	5.10E-01	2.89E-04		3.60E+02		5.91E+03 1.56E+03	2.66E+06 4.38E+05	4.74E-05 1.58E+02	4.66E-05 1.50E+02	7.00E+06 1.51E+07	1.50E-01 7.58E-01	1.40E+07	6.40E-02		9.56E+03
	lown-dip	1	2	12	0.00E+00			1.10E+01	9.36E-05	2.26E-01	1.70E-04	4.77E-01	4.64E+02	0.00E+00	6.89E+02	2.18E+05			9.98E+06	7.58E-01 7.21E-01	1.60E+07 1.23E+07	1.89E-02 2.10E-07		3.98E+04
	lown-dip Iown-dip	1	2	24 94				2.88E+00 2.88E+00	2.12E-04 1.82E-04		2.71E-04			0.00€+00	7.91E-02	4.82E+00	5.46E+01	5.33E+01	1.37E+07	9.08E-01	1.39E+07	6.84E-01		7.21E+04
	lown-dip	i	2	48				2.88E+00	1.82E-04 1.64E-04	2.80E-07 8.38E-05	4.39E-04 2.45E-04			0.00E+00 0.00E+00	8.53E-04 2.56E-01		4.95E+01	4.84E+01	1.36E+07	9.94E-01		7.58E-01	9.41E+04	8.12E+04
ı	lown-dip	1	2	45	7.99E+06	7.99E+06	7.99E+06	2.88E+00	1.59E-04	1.55E-05	2.57E-04	1.55E-05		0.00E+00	4.72E-02		4.29E+D1 4.27E+01	4.19E+01 4.18E+01	1.38E+07 1.32E+07	8.97E-01 9.48E-01	1.40E+07 1.35E+07	4.31E-02		3.35E+04
	lown-dip Iown-dip	1	2	44 18				2.88E+00	1.40E-04		1.94E-04	1.97E-05	9.90E+06	0.00E+00	6.02E-02	3.68E+00	3.84E+01	3.55E+01	1.27E+07	8.88E-01		9.49E-01 2.26E-01		8.56E+04 4.77E+04
	own-dlp	i	2	78				2.88E+00 1.10E+01	1.45E-04 4.31E-05		2.15E-04 7.94E-05				3.75E+01		3.61E+01	3.52E+01	1.63E+07	8.44E-01	1.65E+07	1.67E-01		4.51E+04
296 C	own-dlp	1	2	19	4.36€+05			2.88E+00	1.18E-04		7.946-05 2.67E-04				2.02E+03 9.54E+00			3.51E+01	1.44E+07	6.20E-01	1.51E+07	2.25E-01	1.03E+05	5.05E+04
	own-dip	1	2			7.99E+06	7.99E+06	2.88E+00	1.12E-04	4.30E-04	2.28E-04	4.37E-04	3.57E+05					3.50E+01 3.12E+01	1.55E+07 1.39E+07	8.35E-01 9.10E-01	1.57E+07 1.41E+07	6.60E-02 8.28F-01		4.53E+04
	own-dip own-dip	1	2				3.59E+05 3.42E+05						7.70E+01	0.00E+00	1.22E+03	4.33E+05	3.34E+01		6.80E+06	7.11E-01		7.81E-02		8.00€+04 2.05€+04
	own-dip	i	2		0.00E+00								2.11E+02			1.26E+05		2.63E+01		7.04E-01	1.08E+07	2.15E-06		1.52E+04
	•						12130			· ····································	v.+0E-03	G-03E+00	2.07E+01	0.00E+00	3.72E+03	1.24E+06	2.56E+01	2.53E+01	1.20E+07	5.46E-01	1.46E+07	7.36E-05	9.78E+04	1.45E+04

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					Excavated Waste	Residual Gas	Peakluat Brin	e Crushed Pane	Un-dio Ava	Lin-din Ava	Courselle Ave	Down do Aug	DDZ Davade	DRZ	Selt Piller	Sall Piller			Well	6C well Sand	Total Area	Castila	Castile	Un dip Brine	Uo dio Gas	Down dip	Down do Gas
1					Peresity (fraction)	Sal. (Nacion)) Sat [fraction]	} Height (m)	Plassure (Pa)	Sal. (fraction)	Pressure (Pa)	Set. (fraction)	(Fraction)	Permeability	Porosity	Permeability	Intrusion Time (Years)	Skin factor	Productivity	Permeability	noich trione	d Reservoir	Reservoir Permentiti	Refetive Permanbility	Relative Permanhito	Brite Fieletive	Palatya
No.	íD.	Replic.	Scen	. Vector	POROSITY	SAT ROAS	SAT ABAN	HEIGHT	PPESPANT	DEATRAND	PRESPAN4	00170444		[147.2]	(Fraction)	(1872)	,		Index (I/Pa)	{m,5}	(m/2)	Prousure (Pa)	(UL,51	(fraction)	(Inction)	(fraction)	Permenbility ((fraction)
	Down-dip	1	2	15	5.46E-01	4.22E-02	5.21E-01	1.32E+00	1.13E+07	1.97E-01	1.13E+07	9.57F-01	5.90F-02	PERM_X 1.32E-14	POROSITY 0.66F-02	1.32E-14	INTR_TME	5KIN -9.48E-01	WELLP!	PRM SAND			PRM_CAST	KRW2	KRG2	KRW4	KRG4
	Down-din	1	2	23	5,48E-01	7.29E 02	4.80E-01	1.32E+00	1.13E+07	2.98E-07	1,14E+07	7.51E-01	3.95E-02	1.18E-16	4.60E-02	1.18E-16		-9.48E-01		1.32E-14 7.94E-17	5.06E-01 8.09E-01	1.66E+07	4.47E-13 6.03E-13	0.00E+00 0.00E+00	1.00E+00	7.09E-01	1.74E-09
	Down-dip	1	2	59 100	6.81E-01 5.38E-01	1.07E-02 1.14E-01	1.94E-01 3.43E-01	1.43E+00 1.30E+00	1.43E+07 1.07E+07	3.63E-05 8.83E-01	1.43E+07	5.59E-01	2.00E-01	3.58E-15	1.82E-01	1.66E-16		-1.20E+00		1.35E-18	B.44E-01	1.17E+07	5.89E-14	0.00E+00	1.00E+00	8.99E-02 5.34E-02	8.69E-02 2.15E-01
305	Down-dip	i	2	52	5.30E-01	3.68E-02	4.49E-01	1.28E+D0	1.01E+07	9.58E-01	1.08E+07 1.02E+07	8.84E-01 9.60E-01	7.21E-02 1.10E-01	9.12E-16 1.70E-15	8.35E-02 1.28E-01	9.12E-16 1.70E-15	7.001, 100	-1.26E+00		2.51E-14	9.43E-01	1.25E+07	1.29E-13	4.86E-01	1.39E-07	4.86E-01	1.36E-07
	Down-dip		2	30	5.19E-01	1.16E-01	4.16E-02	1.25E+00	9.27E+06	8.83E-01	9.37E+08	8,83E-01	2.81E-02	2.75E-14	4.45E-02	2.75E-14	4.00E+03 4.00E+03	-9.48E-01 -6.49E-01	1.12E-13 9.87E-14	4.17E-14 2.19E-13	5.07E-01 2.79E-01	1.43E+07 1.34E+07	2.63E-13	7.43E-01	2.31E-06	7.56E-01	4.65E-07
307	Down-dip Down-dip	1	2	39	5.25E-01 5,20E-01	1.50E-01 9.81E-02	2.98E-01 2.56E-01	1.27E+00	9.73E+06	8.48E-01	9.82E+06	8.48E-01	1.60E-02	3.02E-15	3.02E-02	3.02E-15	4.00E+03	-1.23E+00	1.24E-13	2.40E-13	8.82E-01	1.35E+07	1.59E-13 1.78E-13	6.19E-01 4.05E-01	1.39E-09 2.05E-07	6.19E-01 4.05E-01	1.33E-09 2.02E-07
	Down-dip	i	2	31	5.09E-01	5.28E-02		1.25E+00 1.22E+00	9.36E+06 8.88E+06	8.99E-01 8.52E-06	9.44E+06 9.01E+06	8.99E-01 9.46E-01	6.96E-02 7.44E-02	7.24E-16	8.79E-02	7.24E-16		-1.28E+00	1.25E-13	1.66E-14	9.73E-01	1.25E+07	7.08E-14	5.84E-01	1.29E-07	5.84E-01	1.26E-07
	Down-dip	1	2	53	4.97E-01	4.46E-02	2.52E-01	1.19E+00	8.49E+06	2.53E-01	8.01E+06	8,36E-01	1.57E-01	1.66E-15 9.13E-18	9.54E-02 1.85E-01	1,66E-16 8.51E-18		-1.27E+00	1,22E-13 1,17E-13	3.31E-14	9.73E-01	1.40E+07	6.31E-13	0.00E+00	1.00E+00	8.04E-01	5.37E-09
	Down-dip Down-dip	1	2	65	5.48E-01	1.27E-01	8.96E-02	1.33E+00	1.15E+07	0.00E+00	1.15E+07	4.33E-01	2.60E-02	8.71E-16	2.95E-02	8.71E-16	4.00E+03	-1.16E+00	1.26E-13	1.38E-12 4.17E-15	8.92E-01 7.73E-01	1.33E+07 1.26E+07	4.57E-12 3.72E-12	1.38E-11 0.00E+00	9.98E-01 1.00F+00	4.00E-01 2.72F-02	7.88E-03
1	Down-dio	1	2	27 37	5.28E-01 5.62E-01	1.18E-01 4.07E-02	4.62E-01 2.28E-01	1.27E+00 1.37E+00	9.96E+06 1.27E+07	3.57E-05 9.00E-06	9.97E+06 1.27E+07	6.76E-01	3.22E-02	1,86E-16	4.19E-02	1.86E-16		-1.24E+00	1.25E-13	2.40E-15	9.09E-01	1 19E+07	1.26E-12	0.00E+00	1.00E+00	3.32E-02	2.38E-01 1.64E-01
	Down-dip	i	2	56	5.38E-01	4.66E-02	3.20E-01	1.30E+00	1.07E+07	1.79E-06		4.97E-01 5.77E-01	1.34E-01 8.71E-02	4.85E-15 1.05E-15	1.13E-01 9.28E-02	3.98E-18 1.05E-15		-1.19E+00	1.32E-13	1,35E-15	8.19E-01	1.18E+07	6.17E-12	0.00E+00	1.00E+00	2.04E-02	3.26E-01
1	Down-dip	1	2	79	6.07E-01	1.23E-01	3.88E-01	1.53E+00	1.65E+07	4.35E-06		5.20E-01	2.44E-01	1.08E-10	1.62E-01	2.57E-13	4.00E+03 4.00E+03	-7.21E-01 -1.10E+00	1.05E-13 1.42E-13	1.05E-14 1.51E-16	3.22E-01 6.89E-01	1.12E+07 1.24E+07	2.82E-12 4.37E-15	0.00E+00	1.00E+00	2 77E-02	2.76E-01
	Down-dip Down-dip	1	2	35 67	5.05E-01 5.50E-01	9.57E-02 1.21E-01	4.39E-01	1.21E+00	8.72E+06	9.02E-01	8.81E+06	9.02E-01	5.26E-02	7.24E-15	6.80E-02	7.24E-15	4.00E+03	-8.97E-01	1.05E-13	1.38E-13	4.57E-01	1.12E+07	3.98E-11	0.00E+00 4.94E-01	1.00E+00 1.28E-07	3.51E-03 4.94E-01	4.74E-01 1.27E-07
	Down-dip	i	2	41	5.50E-01	3.40E-02	6.61E-02 8.64E-02	1,33E+00 1,32E+00	1.17E+07 1.12E+07	9.53E-03 2.36E-02		3.63E-01 3.79E-01	1.70E-01	3.55E-18	1.74E-01	3.55E-18	4.00E+03	-1.27E+00	1.33E-13	7.24E-15	9.65E-01	1.26E+07	1.15E-14	0.00E+00	1.00E+00	1.46E-02	3.30E-01
4	Down-dip	1	2	90	5.21E-01	1.28E-02	2.86E-01	1.25E+00	9.48E+06	1.31E-06	9.41E+06	5.19E-01	1.46E-01 1.92E-02	1.70E-19 1.20E-17	1.48E-01 3.60F-02	1.70E-19 1.20E-17	4.00E+03 4.00E+03	-1.22E+00 -8.48E-01	1.28E-13 1.06E-13	3.24E-16 2.09E-14	8.64E-01	1.47E+07	3.47E-12	0.00E+00	1.00E+00	1.49E-02	3.77E-01
4	Down-dip Down-dip	!	2	6 71	5.01E-01	6.58E-02	1.45E-01	1.20E+00	8.49E+06	1.09E-01	8.62E+06	4.18E-01	6.63E-02	5.76E-19	8.36E-02	5.75E-10	4.00E+03	-0.48E+00	1.06E-13	2.09E-14 B 46F-17	4.15E-01 8.02E-01	1.29E+07 1.38E+07	3.02E-12 3.09F-12	0.00E+00 0.00E+00	1.00E+00 1.00E+00	1.61E-02 1.47E-02	3.76E-01
1	Down-dip	i	2	71 86	5.29E-01 4.95E-01	1.57E-02 6.86E-02	1.06E-01 3.61E-02	1.27E+00 1.19E+00	1.00E+07 8.29E+08	1.01E-06 1.80E-01		3.73E-01	4.63E-02	2.19E-18	6.34E-02	2.19E-18	4.00E+03	-1.37E+00	1.32E-13	5.25E-17	1.18E+00	1.19E+07	8.76E-13	0.00E+00	1.00E+00	1.17E-02	3 58E-01 4 20E-01
323	Down-dip	i	2	98	5.12E-01	3.56E-02	5.00E-02	1.23E+00	9.00E+06	4.71E-06		9.18E-01 3.25E-01	1.56E-01 6.17E-02	3,04E-17 4,19E-19	1.79E-01 8.40E-02	3.02E-17 4.17E-19	4.00E+03 4.00E+03	-1.26E+00 -1.23E+00	1.18E-13	4.07E-13	9.43E-01	1.16E+07	2.04E-11	9.02E-04	6.72E-01	7.21E-01	5.50€-06
	Down-dip	ţ	2	73	5.76E-01	5.61E-02	3.03E-01	1.42E+00	1.39E+07	5.42E-06	1.39E+07	4.84E-01	9.93E-02	3.75E-16	9.98E-02	3.72E-16	4.00E+03	-1.23E+00 -8.01E-01	1.20E-13 1.18E-13	4.79E-15 6.17E-15	8.82E-01 3.77E-01	1.17E+07 1.35E+07	3.98E-14 9.77F-12	0.00E+00	1.00E+00 1.00E+00	1.03E-02	4.25E-01
	Down-dip Down-dip	1	2	36 84	5.20E-01 5.10E-01	3.71E-03 1.44E-01	1.39E-01 6.88E-03	1.25E+00 1.22E+00	9.42E+06 8.89E+06	2.98E-07 5.96E-08		3.87E-01	4.14E-02	6.97E-20	5.69E-02	6.61E-20	4.00E+03	-8.89E-01	1.07E-13	8.13E-15	4.50E-01	1.36E+07	1.45E-13	0.00E+00 0.00E+00	1.00E+00 1.00E+00	6.92E-03 1.01E-02	4.54E-01 4.43E-01
	Down-dip	i	2	20	5.37E-01	1.23E-01	1.27E-01	1.30E+00	1.06E+07	5.96E-08		2.66E-01 3.50E-01	2.26E-02 2.38E-02	4.91E-20 1.35E-17	3,61E-02 3,58E-02	4.90E-20 1.35E-17	4.00E+03	-1.40E+00	1.29E-13	2.95E-16	1.25E+00	1.26E+07	3.55E-11	0.00E+00	1.00E+00	7.05E-03	4.18E-01
	Dawn-аёр	t	2	85	5.60E-01	7.34E-03	2.80E-01	1.36E+00	1.24E+07	7.31E-02		4.08E-01	7.02E-02	5.06E-16	5.98E-02	4.90E-16	4.00E+03 4.00E+03	-6.04E-01 -1.23E+00	1.01E-13 1.34E-18	3.31E-15 7.68E-16	2.55E-01 8.95E-01	1.28E+07	1.20E-12	0.00E+00	1.00E+00	6.44E-03	4.31E-01
	Down-dip Down-dip	1	2	47	5.38E-01 5.47E-01	6.75E-02	1.61E-01	1.30E+00	1.07E+07	9.04E-02		3.26E-01	1.48E-01	6.92E-18	1.51E-01	6.92E-18	4.00E+03	1.09E+00	1.20E-13	2.19E-16	6.75E-01	1.19E+07	7.76E-15 1.55E-12	0.00E+00 0.00E+00	1.00E+00 1.00E+00	2.60E-03 2.50E-03	5.95E-01 5.71E-01
	Down-dip	1	2	16	4.94F-01	1.48E-01 6.75E-02	6.84E-02 2.76E-01	1.33E+00 1.19E+00	1.14E+07 8.28E+06	5.94E-05 3.52E-05		2.29E-01 3.86E-01	1.99E-01	8.13E-19	2.09E-01	8.13E-19	4.00E+03	-7.13E-01	1.07E-13	2.75E-16	3.17E-01	1.23E+07	1.20E-11	0.00E+00	1.00E+00	1.52E-03	5.71E-01 5.89E-01
	Down-dlp	1	2	14	5.26E-01	1.07E-01	3.28E-01	1.27E+00	9.80E+06	1.28E-01	0,100	3.94E-01	1.04E-01 1.31F-01	2.22E-19 6.31E-19	1.31E-01 1.42E-01	2.14E-19 6.31E-19	4.00E+03 4.00E+03	-1.29E+00 -7.31E-01	1.19E-13 1.03E-13	1.91E-14	1.01E+00	1.52E+07	1.86E-12	0.00E+00	1.00E+00	9.51E-04	6.64E-01
	Down-dip	1	2	42	5.79E-01	1.04E-01	3.92E-01	1.43E+00	1.41E+07	1.23E-05	1.41E+07	4.15E-01	1.84E-01	2.97E-13	1.13E-01	7.76E-17	4.00E+03	1.26E+00	1.41E-13	8.32E-16 1.38E-15	3.28E-01 9.46E-01	1.47E+07	2.63E-14 3.63E-13	0.00E+00 0.00E+00	1.00E+00 1.00E+00	1.92E-04 5.64E-06	7.59E-01
T	Dawn-dip Dawn-dip	1	2	99	5.76E-01 6.19E-01	1.28E-01 3.17F-02	5.15E-01 1.73E-01	1.42E+00 1.58E+00	1.39E+07 1.64E+07	4.00E-02	1,39E+07 .		1.75E-01	1.74E-16	1.70E-01	5.89E-17	4.00E+03	-7.63E-01	1.18E-13	6.17E-17	3.50E-01	1.25E+07	2.29E-11	0.00E+00	1.00E+00	1.02E-07	9.06E-01 9.65E-01
1	Down-dip	i	2	18	6.27E-01	1.06E-01	3.40E-01	1.61E+00	1.66E+07	1.37E-06 1.66E-02		8.34E-01 8.07E-01	1.22E-01 1.36E-01	5.48E-12 1.18E-11	5.62E-02 5.59E-02	3.72E-14 3.31E-14	1.00E+04	-1.33E+00	1.60E-13	1.86E-16	1.08E+00		1.35E-11	0.00E+00	1.00E+00	4.37E-01	7.69E-03
	Down-dip	1	2	58	5.77E-01	2.96E-02	1.14E-01	1.42E+00	1.39E+07	1.79E-07		7.76E-01	2.13E-01	1.07E-15	2.03E-01	1.45E-16	1.00E+04 1.00E+04	-1.09E+00	1.49E-13 1.36E-13	6.17E-16 3.09E-15	6.69E-01 8.11E-01	1.05E+07 1.26E+07	5.25E-12	0.00E+00	1.00E+00	2.78E-01	6.30E-03
	Down-dip Down-dip	1	2	45	5.85E-01	5.05E-02	2.04E-01	1,45E+00	1.45E+07	9.49E-01		9.49E-01	1.11E-01	6.10E-13	7.87E-02	5.13E-14	1.00E+04	-9.31E-01	1.26E-13	1.74E-15	4.89E-01	1.32E+07	1.07E-13 4.57E-13	0.00E+00 7.82E-01	1.60E+00 1.60E-09	3.41E-01 7.82E-01	1.82E-02 1.59E-09
	Down-dio	ì	2	19	5.80E-01 6.02E-01	4.58E-03 1.42E-01	1.85E-01 2.97E-02	1.43E+00 1.51E+00	1.41E+07 1.57E+07	9.94E-01 7.96E-03		9.94E-01 8.60E-01	2.15E-01	9.08E-14	1.95E-01	6.31E-15	1.00E+04	-1.29E+00	1.43E-13	9.77E-16	9.95E-01	1.31E+07	1.78€-12	9.75E-01	3.88E-09	9.75E-01	3.63E-09
341	Down-dlp	1	2	73	5.53E-01	5,61E-02	3.03E-01	1.34E+00	1.18E+07	4.83E-06		8.03E-01	2.52E-01 9.53E-02	2.42E-11 3.72E-16	1.80E-01 1.06E-01	1.41E-15 3.72E-16	1.00E+04 1.00E+04	-1.23E+00 -8.01E-01	1.48E-13 1.12E-13	2.00E-16 6.17E-15	8.94E-01 3.77E-01	1.18E+07	1.45E-12	0.00E+00	1.00E+00	5.62E-01	0.00E+00
	Dawn-dip	1	2	59	5.83E-01	1.07E-02	1.94E-01	1.44E+00	1.44E+07	5.42E-06	1.44E+07	6.61E-01	2.00E-01	3.79E-15	1.81E-01	1.66E-16	1.00E+04	-1.20E+00	1.12E-13	6.17E-16 1.35E-16	3.77E-01 8.44E-01	1.35E+07 1.17E+07	9.77E-12 5.89F-14	0.00E+00 0.00E+00	1.00E+00 1.00E+00	2.93E-01 1.33E-01	1.66E-02
	Down-dip Down-dip	1	2	78 48	6.00E-01 5.55E-01	4.93E-02 1.02E-01	1.51E-01 2.11E-01	1.60E+00 1.35E+00	1.56E+07 1.20E+07	3.47E-01		5.58E-01	2.73E-01	5.83E-10	1.00E-01	2.46E-15	1.00E+04	-1.06E+00	1.37E-13	8.32E-17	6.28E-01	1.40E+07	1.07E-12	4.42E-03	5.18E-01	6.68E-02	1.01E-01 1.63E-01
	Down-dlo	ì	2	69	5.68E-01	8.98E-02	4.08E-01	1.39E+00	1.20E+07	2.62E-06 9.09E-01		8.97E-01 9.09E-01	5.75E-02 8.35E-02	7.96E-14 1.30E-14	5.68E-02 8.28E-02	7.76E-14 1.26E-14	1.00E+04 1.00E+04	-1.29E+00 -1.29E+00	1.35E-13	2.19E-15	1.01E+00	1.03E+07	3.80E-12	0.00E+00	1.00E+00	5.98E-01	3.58E-10
	Down-dip	1	2	37	5.50E-01	4.07E-02	2.28E-01	1.34E+00	1.16E+07	1.19E-06		6.69E-01	1.18E-01	5.21E-16	1.16E-01	3.98E-16	1.00E+04	-1.19E+00	1.39E-13 1.28E-13	9.33E-15 1.35E-15	9.99E-01 8.19E-01	1.42E+07 1.18E+07	4.07E-13	5.41E-01	1.64E-08	5.41E-01	1.62E-08
	Down-dip Down-dip	1	2	12	5.31E-01 5.32E-01	7.06E-02 1.12E-01	1.02E-01	1.28E+00	1.02E+07	1.19€-07		9.29E-01	3.07E-02	1.78E-13	4.53E-02	1.78E-13	1.00E+04	-1.38E+00	1.33E-13	5.50E-15	1.19E+00	1.39E+07	6.17E-12 1.86E-13	0.00E+00 0.00E+00	1.00E+00 1.00E+00	1.26E-01 7.39E-01	9.08E-02
	Down-dio	1	2	1	5.32E-01	9.81E-02	1.61E-02 2.56E-01	1,28E+00 1,30E+00	1.02E+07 1.05E+07	6.60E-01 8.99E-01		8.87E-01 8.99E-01	1.29E-01 7.21E-02	1.18E-13 7.24E-16	1.34E-01	1.18E-13	1.00E+04	-1.17E+00	1.22E-13	3.80E-15	7.83E-01	1.29E+07	1.12E-12	1.98E-01	3.09E-02	6.38E-01	3.57E-10
	Down-dip	1	2	46	5.03E-01	2.03E-02	2.35E-01	1.21E+00	8.69E+06	6.80E-06		8.06E-01	4.51E-02	1.59E-17	6.49E-02 6.60E-02	7.24E-16 1.59E-17	1.00E+04	-1.28E+00	1.29E-13 1.27E-13	1.66E-14	9.73E-01	1.25E+07	7.08E-14	5.84E-01	1.20E-07	5.85E-01	1.17E 07
4	Down-dip	1	2	24	5.13E-01	9.01E-02	1.37E-01	1.23E+00	9.02E+06	9.10E-01	9.11E+06	9.10E-01	1.96E-01	2.82E-13	2.19E-01	2.82E-13	1.00E+04	-1.29E+00	1.27E-13	1.45E-14 2.63E-14	1.26E+00 9.94E-01	1.50E+07 1.09E+07	1.15E-11 7.41E-13	0.00E+00 6.66E-01	1.00E+00 2.14E-13	3.40E-01 6.66E-01	1.96E-02 2.09E-13
	Down-dip Down-dip	1	2	71 65	5.31E-01 5.33E-01	1.57E-02 1.27E-01	1.06E-01 8.96E-02	1.28E+00 1.29E+00	1.01E+07 1.03E+07	8.94E-07 0.00E+00		5.07E-01 4.83E-01	4.66E-02	2.19E-18	6.31E-02	2.19E-18	1.00E+04	-1.37E+00	1.33E-13	5.25E-17	1.18E+00	1.19E+07	6.76E-13	0.00E+00	1.00E+00	5.15E-02	2.09E-13 2.18E-01
354	Down-dip	i	2	67	5.10E-01	1.21E-01	6.61E-02	1.29E+00	8.97E+06	1.03E-04	1,000	4.63E-01	2.21E-02 1.72E-01	8.71E-16 3.55E-18	3.04E-02 1.89E-01	8.71E-16 3.55E-18	1.00E+04 1.00E+04	-1.16E+00 -1.27E+D0	1.22E-13 1.22E-13	4.17E-15	7.73E-01	1.26E+07		0.00E+00	1.00E+00	4.50E-02	1.71E-01
	Down-dip	1	2	100	5.18E-01	1.14E-01	3.43E-01	1.25E+00	9.22E+06	8.83E-01	9.32E+06	8.83E-01	6.96E-02	9.12E-16	8.72E-02	9.12E-16	1.00E+04	-1.27E+00	1.22E-13 1.23E-13	7.24E-15 2.51E-14	9.65E-01 9.43E-01	1.26E+07 1.25E+07	1.15E-14 1.29E-13	0.00E+00 4.85E-01	1.00E+00 1.83E-07	4.25E-02 4.86E-01	1.84E-01
	Down-dip Down-dip	1	2	30 56	5.04E-01 6.09E-01	1,16E-01 4.66E-02	4.16E-02 3.20E-01	1.21E+00 1.22E+00	8.69E+06 8.85E+06	8.83E-01		8.83E-01	2.70E-02	2.75E-14	4.59E-02	2.75E-14	1.00E+04	-8.49E-01	9.57E-14	2.19E-13	2.79E-01	1.34E+07	1.59E-13	4.85E-01 6.19E-01	1.03E-07 1.25E-09	4.86E-01 6.19E-01	1.59E-07 1.23E-09
	Down-dip	i	2	79	6.08E-01	1.23E-01	3.88E-01	1.53E+00	1.61E+07	1.43E-08 8.94E-07		9.06E-01 5.23E-01	8.40E-02 2.24E-01	1.05E-15 3.26E-11	9.88E-02 1.62E-01	1.05E-15 2.57E-13	1.00E+04 1.00E+04	-7.21E-01	9.88E-14	1.05E-14	3.22E-01	1.12E+07	2.82E-12	0.00E+00	1.00E+00	5.79E-01	6.75E-04
	Down-dip	1	2	11	5.00E-01	6.24E-02	4.15E-01	1.20E+00	8.55E+06			9.18E-01	4.18E-02	1.35E-13	5.48E-02	1.35E-13	1.00E+04	-1.10E+00 -1.39E+00	1.43E-13 1.25E-13	1.51E-16 1.20E-14	6.89E-01 1.22E+00	1.24E+07 1.35E+07	4.37E-15	0.00E+00	1.00E+00	3.75E-03	4.65E-01
	Down-dip Down-dip	!	2	98	4.95E-01	3.56E-02	5.00E-02					3.96E-01	6.14E-02	4.19E-19	8.68E-02	4.17E-19	1.00E+04	-1.23E+00	1.16E-13	4.79E-15	8.82E-01	1.35E+07 1.17E+07		0.00E+00 0.00E+00	1.00E+00 1.00E+00	5.71E-01 2.39E-02	9.34E-05 3.12E-01
***	Jown-dip	i	2	20 42	5.17E-01 5.68E-01	1.23E-01 1.04E-01	1.27E-01 3.92E-01		9.20E+06 1.31E+07	1.19E-07 4.17E-07		4.10E-01 5.30E-01	2.03E-02 1.42E-01	1.35E-17 2.38E-15	3.74E-02	1.35E-17	1.00E+04	-6.04E-01	9.68E-14	3.31E-15	2.55E-01	1.28E+07	1.20E-12	0.00E+00	1.00E+00	1.57E-02	3.12E-01
363	Down-dip	1	2	41	5.62E-01	3.40€-02	8.64E-02	1.37E+00	1.26E+07			2.50E-01	1.53E-01	2.39E-15 1.34E-18	1.16E-01 1.42E-01	7.76E-17 1.70E-19	1.00E+04 1.00E+04	-1.26E+00 -1.22E+00	1.38E-13 1.33E-13		9.46E-01	1.47E+07	3.63E-13	0.00E+00	1.00E+00	4.15E-03	4.69E-01
	Down-dip	1	2	77	5.56E-01	1.48E-01	6.84E-02	1.35E+00		2.29E-05	1.20E+07	2.37E-01	1.99E-01	8.13E-19	2.05E-01	8.13E-19		-7.13E-01	1.09E-13	3.24E-16 2.75E-16	8.64E-01 3.17E-01	1.47E+07 1.23E+07	3.47E-12 1.20E-11	0.00E+00	1.00E+00	1.76E-03 1.80E-03	6.23E-01
	Down-dip Down-dip	1	2	84 85	5.30E-01 5.63E-01	1.44E-01 7.34E-03	6.88E-03 2.60E-01	1.28E+00 1.38E+00		0.00E+00 3.10E+02	1.00E+07	1.27E-01	2.59E-02	4.91E-20	3.46E-02	4.90E-20	1.00E+04	-1.40E+00	1.34E-13	2.95E-16	1.25E+00	1.26E+07	3.55E-11	0.00E+00	1.00E+00	1.80E-03 4.04E-04	5.71E-01 7.12E-01
	Down-dip	ì	2	6	5.49E-01	6.58E-02	1.45E-01	1.33E+00	1.27E+07 1.15E+07	3.10E-02 1.55E-02	1.27E+07 1.16E+07	3.13E-01 1.84E-01	7.12E-02 7.31E-02	6.03E-16 5.76E-19	6.92E-02 7.56E-02	4.90E-16 5.75E-19	1.00E+04	-1.23E+00	1.35E-13	7.08E-16	8.95E-01	1.19E+07	7.76E-15	0.00E+00	1.00E+00	6.01E-05	8 50E-01
	Oown-dip	1	2	47	5.60E-01	6.75E-02	1.61E-01	1.36E+00	1.24E+07	1.98E-02	1.24E+07	1.74E-01	1.59E-01	8.13E-17	1.44E-01	6.92E-19		-1.18E+00 -1.09E+00	1.28E-13 1.26E-13	6.46E-17 2.19E-16	8.02E-01 6.75E-01	1.38E+07 1.20E+07		0.00E+00	1.00E+00	1.09E-05	8.99E-01
	Down-dip Down-dip	1	3	22	5.32E-01 5.68E-01	2.51E-02	8.22E-02	1.28E+00			1.03E+07	7.66E-01	1.35E-01	7.41E-14	1.45E-01	7.41E-14		-1.37E+00	1.33E-13	2.19E-16 1.74E-13	6.75E-01 1.17E+00	1,20E+07 1,38E+07	1.55E-12 1.59E-12	0.00E+00 0.00E+00	1.00E+00 1.00E+00	2.41E-07 3.37E-01	9.64E-01 2.00E-02
	Jown-dip	1	3	51 46	5.88E-01 5.26E-01	1.34E-01 2.03E-02	3.63E-01 2.35E-01	1.39E+00 1.27E+00	1.33E+07 9.32E+08	2.36E-01 1.21F-02		6.66E-01	2.06E-01	7.45E-13	1.79E-01	6.17E-14		-1.16E+00	1.32E-13	1.00E-12	7.77E-01	1.68E+07		0.00E+00	1.00E+00		9.12E-02
372	Jown-dip	i	3	78	5.41E-01	4.93E-02	1.51E-01	1.31E+00		9.44E-01		9.66E-01 9.45E-01	4.59E-02 1.10E-01	1.59E-17 2.46E-15	6.28E-02 1.15E-01	1.59E-17 2.48E-15		-1.41E+00 -1.06E+00	1.34E-13 1.20E-13	1.45E-14	1.26E+00	1.51E+07	1.15E-11	0.00E+00	1.00E+00	8,46E-01	1.04E-05
	own-dip	1	3	69	5.42E-01	8.98E-02			1.10E+07	9.13E-01	1.11E+07	9.30E-01	7.88E-02	1.26E-14	8.77E-02	1.26E-14		-1.06E+00 -1.29E+00	1.20E-13 1.31E-13	8.32E-17 9.33E-15	6.28E-01 9.99E-01	1.48E+07 1.47E+07	1.07E-12 4.07E-13	7.79E-01 5.54E-01	8.41E-07 0.00E+00	7.79E-01 6.28E-01	7.82E-07
	Jown-dip Jown-dip	1	3	52 5	5.37E-01 5.30E-01	3.68E-02 1.29E-01	4.49E-01 1.21E-01					9.60E-01	1.09E-01	1.70E-15	1.27E-01	1.70E-15	1.20E+03	9.48E-01	1.14E-13				2.63E-13		4.18E-07	,	0.00E+00
5.5	. Janna Garp	•	-		0.000-01		*.212701	1.202+00	a.30E+00	4.29E-04	1.18E+07	8.53E-01	1.32E-01	1.91E-17	1.48E-01	1.82E-17	1.20E+03	-1.37E+00	1,33E-13	1.82E-12	1.17E+00	1.54E+07					2.31E-05
																											•

		4

					1	Down-dia																		
1					Up-dip Flowing Bottom-hote	Flowing Bottom-hole	BC weil Injection	Blowoul Duration		Gas Rete (rel	Max Brine	Max Gas Rate	Produced Liquid/Gas	Cum Brine from Boundary		Cum Gas Produced tree	Ouro Brine	Cum Brine	Avg Brine Pressure	Avg Brine Seturation	Avg Brina Pressupe	Avg Brine Salvertion	Facevaled	Total
Ì					Pressure (Pa)	Pressure (Pa)	Pressure (Pa)	(Days)	(m/E/m)	m^3/s)	Rate (m^3/s)	(ref m^3/s)	Patio (m^3/s : ref m^3/s)	Condition Well	(mact/day)	m/3)	Produced (m/3)	Releases (m^3)	Panel 5 (Pa)	Panel 5 (fraction) alta	Panel 0 (Pa)	Panel 0 (fraction) after	Waste Pore Volume	Excensied Brine Volume
No.	IO Down-dip	Replic	. Scen	Vector	FBHP2	FBHP4	BHP_ABAN	time		GASFLW		MAX_GAS		BRINE_BC	GAS_RATE	GASOUT	BRINEOUT	BRIN_REL	BRNPRES5	blowout SATBRNS	BRNPRESO	blowout	(fraction)	(m^3) ∕TOT BRIN
	Down-dip	1	2	23	0.00E+00	7.99E+06 9.10E+05	7.99E+06 9.10E+05		6.64E-05 8.87E-08	1.24E-05 6.02E-02	1.31E-04 5.70E-05	1.24E-05 1.39E+00		0.00E+00 0.00E+00	2.7 02 02		1.86E+01	1.82E+01	1.11E+07	9.58E-01	1.13E+07	1.83E-01	8.09E+04	3.86E+04
	Down-dlp	1	2	59	0.00E+00	4.17E+05		1.10E+01	9.80E-06	3.32E-01	4.94E-05			0.D0E+00 0.D0E+00	1.84E+02 1.01E+03			1.33E+01 1.25E+01		7.59E-01	1.13E+07	2.98E-07	8.11E+04	2.3BE+04
	Down-dip Down-dip	1	2	100 52	8.00E+06 8.02E+06	8.00E+06 8.00E+06	8.00E+06	2.88E+00	3.69E-05	1.04E-04	0.33E-05	1.04E-04	6.23E+05	0.00E+00	3.19E-D1	1.85E+01		1.13E+01		5.71E-01 8.85E-01	1.43E+07 1.07E+07	4.99E-05 7.67E-01	9.35E+04 7.86E+04	1.40E+04 8.43E+04
	Down-dip	i	2	30	7.99E+06	7.99E+06	8.00E+06 7.99E+06	2.88E+00 2.88E+00	3.67E-05 2.56E-05	7.58E-06 7.01E-07	8.85E-05 4.02E-05	7.58E-06 7.01E-07	6.21E+06 5.76E+07	0.00E+00 0.00E+00	2.31E-02	1.71E+00		1.04E+01		9.60E-01	1.01E+07	7.26E-01	7.61E+04	6.32E+04
	Down-dip	1	2	39	8.00E+06	8.00€+06	8.00E+06	2.88E+00	2.25E-05	3.99E-05	4.34E-05	3.99E-05	1.05E+06	0.00E+00	2.14E-03 1.22E-01	1.22E-01 6.54E+00		6.70E+00		8.86E-01 8.51E-01	9.25E+06 9.71E+06	6.79E-01 6.86E-01	7.26E+04	
	Down-dip Down-dip	1	2	1 31	8.00E+06 0.00E+00	8.00E+06 7.99E+06	8.00E+06 7.99E+06	2.88E+00 2.88E+00	2.19E-05	6.74E-06	6.04E-05		5.27E+06	0.00E+00	2.06E-02	1.29E+00	6.76E+00	6.63E+00		9.01E-01	9.33E+06	8.07E-01	7.46E+04 7.30E+04	5.66E+04 6.19E+04
	Down-dip	i	2	53	3.16E+05		6.15E+06	2.88E+00	1.90E-05 1.67E-05	1.36E-07 5.74E-03	4.79E-05 4.55E-05	1.36E-07 1.62E-02	1.92E+08 2.89E+03	0.00E+00 0.00E+00	4.16E-04 1.75E+01	2.94E-02		5.51E+00		9.47E-01	8.88E+06	3.67E-05	6.99E+04	2.99E+04
	Down-dip	1	2	65	0.00E+00	3.09E+05	3.09E+05	1.10E+01	3.38E-06	1.73E-01	1.83E-05			0.00E+00	5.27E+02	1.79E+03 3 59E+05		5.07E+00 4.68E+00	7.00E 100	8.39E-01 4.48E-01	8.49E+06 1.14E+07	2.01E-01 0.00E+00	6.67E+04 8.16E+04	
	Down-dip Down-dip	1	2	27 37	0.00E+00	2.97E+05 3.20E+05	2.97E+05 3.20E+05	1.10E+01 1.10E+01	3.15E-06 3.08E-06	6.94E-02 3.19E-01	1.92E-05 1.59E-05	2.06E+00		0.00E+00	2.12E+02	1.58E+D5	4.82E+00	4.40E+00	3.99E+06	6.B6E-01	9.96E+06	3.91E-05		9 27E+03 1.73E+04
314	Down-dip	1	2	56	0.00E+00	2.88E+05	2.88E+05	1.10E+01	2.66E-06	1.35E-01	1.45E-05	6.92E+00 3.35E+00	7.03E+00 1.28E+01	0.00E+00 0.00E+00	9.74E+02	5.76E+05 2.98E+05	4.05E+00	3.84E+00		5.11E-01	1.26E+07	1.53E-05	8.65E+04	1.49E+04
	Down-dip	1	2	79	0.00E+00	3.92E+05	3.92E+05	1.10E+01	4.56E-06	4.84E+00	4.56E-06	1.80E+01	5.58E-01	0.00E+00	1.48E+04	6.89E+06	3.84E+00	3.76E+00 3.50F+00	4.22E+06 1.11E+07	5.90E-01 5.37E-01	1.07E+07 1.14E+07	5.31E-06 4.38E-06	7.84E+04 1.04E+05	1.46E+04
	Down-dip Down-dip	1	2	35 67	7,99E+06 0.00E+00	7.99E+06 2.91E+05	7.99E+06 2.91E+05	2.88E+00 1.10E+01	1.12E-05 1.63E-06	1.36E-06 1.77E-01	2.00E-05	1.36E-06	1.23E+07	0.00E+00	4.14E-03	2.61E-01	3.21E+00	3.14E+00	8.78E+06	9.05E-01	8.70E+06	7.40E-01	6.88E+04	5.59E+04
318	Down-dip	1	2	41	0.00E+00	2.84E+05	2.84E+05	1.10E+01	1.33E-06	1.36E-01	1.04E-05 1.01E-05	5.91E+00 6.25E+00	5.83E+00 5.56E+00	0.00E+00 0.00E+00	5.40E+02 4.16E+02	4.08E+05 3.81E+05		2.28E+00		3.81E-01	1.17E+07	8.22E-03	8.24E+04	1.13E+04
	Down-dip Down-dip	1	2	90	0.00E+00		2.46E+05	1.10E+01	1.05E-06	8.64E-02	7.47E-06	3.61E+00	6.98E+00	0.00E+00	2.64E+02	2.37E+05		2.10E+00 1.64E+00		3.96E-01 5.33E-01	1.12E+07 9.47E+06	2.36E-02 1.31E-06	8.07E+04 7.34E+04	1.57E+04 1.49E+04
	Down-dip	1	2	6 71	0.00E+00 0.00E+00	2.30E+05 2.54E+05	2.30E+05 2.54E+05	1.10E+01 1.10E+01	1.03E-06 9.47E-07	8.79E-02 1.25E-01	6.78E-06 7.11E-06	3.14E+00	7.12E+00	0.00E+00	2.68E+02	2.19E+05	1.56E+00	1.51E+00	3.12E+06	4.34E-01	8.49E+06	6.76E-02	6.78E+04	2.08E+04
322	Down-dlp	1	2	86	2.28E+05	8.02E+06	8.02E+06	2.88E+00	3.92E-06	7.24E-07	9.76E-06	5.68E+00 1.36E-06	4.46E+00 6.74E+08	0.00E+00 0.00E+00	3.80E+02 2.21E-03	3,31E+05 2,12E-01	1.47E+00 1.22E+00	1.45E+00 1.20E+00		3.91E-01	1.00E+07	1 D1E-06	7.57E+04	7.45E+03
	Down-dip Down-dip	1	2	98 73	0.00E+00 0.00E+00	2.32E+05	2.32E+05	1.10E+01	7.66E-07	1.10E-01	5.14E-06	4.17E+00	4.14E+00	0.00E+00	3.34E+02	2.79E+05	1.15E+00	1.10E+00		9.20E-01 3.44E-01	8.29E+06 9.00E+06	1.22E-01 4.74E-06	6.60E+04 7.06E+04	3.42E+04 6.08E+03
	Down-dip	1	2	73 36		3.32E+05 2.40E+05	3.32E+05 2.40E+05	1.10E+01 1.10E+01	7.03E-07 6.63E-07	2.15E-01 1.01E-01	5.30E-06 4.72E-06	1.03E+01	1.81E+00	0.00E+00	6.56E+02	6.2BE+05	1.14E+00	1.09E+00	4.00E+06	4.99E-01	1.39E+07	3.14E-05	9.17E+04	1.33E+04
326 (Dawn-dip	1	2	84	0.00E+00	2.32E+05	2.32E+05	1.10E+01	5.61E-07	1.18E-01	3.80E-06	4.24E+00 4.45E+00	3.72E+00 2.89E+00	0.00E+00 0.00E+00	3.09E+02 3.59E+02	2.83E+05 2.93E+05		1,02E+00 8,09E-01	2.99E+06 3.28E+06	4.04E-01 2.87E-01	9.42E+06 8.89E+06	2.98E-07 5.96E-08	7.29E+04	7.45E+03
	Down-dip Down-dip	1	2	20 85	0.00E+00 0.00E+00	2.63E+05	2.63E+05	1.10E+01	5.15E-07	1.50E-01	3.21E-06	4.95E+00	2.05E+00	0.00E+00	4.58E+02	3.82E+05	7.82E-01	7.48E-01	3.67E+06	3.68E-01	1.06E+05	5.96E-08 5.96E-08	7.00E+04 7.81E+04	9.78E+03 7.30E+03
	Down-dip	1	2	47		3.04E+05 2.69E+05	3.04E+05 2.69E+05	1.10E+01 1.10E+01	2.30E-07 2.02E-07	1.94E-01 1.73E-01	2.01E-06 1.50E-06	1.23E+01 8.03E+00	6.29E-01 6.84E-01	0.00E+00 0.00E+00	5.92E+02	6.04E+05		3.71E-01	3.27E+06	4.25E-01	1.24E+07	7.40E-02	8.56E+04	1.39E+04
	Own-dip	1	2	77	0.00E+00	2.86E+05	2.86E+05	1.10E+01	1.15E-07	1.76E-01	8.64E-07	8.29E+00	3.58E-01	0.00E+00	5.28E+02 5.38E+02	4.51E+05 5.17E+05	3.08E-01 1.85E-01	3.00E-01 1.80E-01	3.34E+06 3.35E+06	3.45E-01 2.50E-01	1.07E+07	B.19E-02	7.85E+04	1.69E+04
	Down-dip Down-din	1	2	16 14		2.26E+05	2.26E+05	1.10E+01	4.53E-08	7.39E-02	4.30E-07	5.44E+00	3,13E-01	0.00E+00	2.26E+02	2.49E+05	7.81E-02	7.74E-02	2.12E+06	4.03E-01	1.14E+07 8.27E+06	5.94E-05 3.52E-05	8.13E+04 6.59E+04	5.01E+03 8.17E+03
	Jown-dip	i	2	42		2.77E+05 4.26E+05	2.77E+05 4.26E+05	1.10E+01 1.10E+01	9.21E-09 1.92E-09	9.45E-02 2.61E+00	9.09E-08 5.21E-09	7.79E+00 2.52E+01	4.66E-02 6.50E-04	0.00E+00 0.00E+00	2.88E+02	3.56E+05	1.66E-02	1.61E-02	2.22E+06	4.11E-01	9.B0E+06	8.43E-02		2.00E+04
	Down-dip	1	2	99	0.00E+00	4.58E+05	4.58E+05	1.10E+01	1.68E-11	1.84E-01	7.79E-11	2.13E+01	3.97E-05	0.00E+00	7.96E+03 5.61E+02	3.11E+06 6.64E+05	2,02E-03 2,64E-05	1.86E-03 2.83E-05	8.26E+06 2.63E+06	4.32E-01 5.36E-01	1.19E+07 1.39E+07	1.30E-05 4.18E-02	9.26E+04	1.01E+04
	Down-dip Down-dip	1	2 2	10 18		6.54E+06 6.17E+06	6.54E+06 6.17E+06	1.10E+01	1.77E-04	1.15E-01	3.30E-04	2.00E-01	2.17E+03	0.00E+00	3.52E+02	8.54E+04	1.86E+02	1.76E+02	1.57E+07	8.35E-01	1.62E+07	1.32E-06	9.15E+04 1.09E+05	1.\$5E+04 3.82E+04
	Down-dip	i	2	58		4.25E+06	4.25E+06	1.10E+01 1.10E+01	1.21E-04 4.93F-05	1.12E-01 5.55E-02	2.06E-04 2.15E-04	1.63E-01 3.41E-01	1.59E+03 8.64E+02	0.00E+00 0.00E+00		8.00E+04	1.27E+02	1.21E+02		8.09E-01	1.65E+07	9.28E-03	1.13E+05	3.44E+04
	Down-dip	1	2	45		8.00E+06	8.00€+06	2.BBE+00	1.98E-04	2.03E-05	3.10E-04	2.03E-05	1.33E+07	0.00E+00	6.19E-02	7.37E+04 3.94E+00	6.37E+01 5.23E+01	5.97E+01 5.10E+01	1.06E+07 1.41E+07	7.77E-01 9.48E-01	1.39E+07 1.45E+07	5.46E-07 9.49E-01	9.20E+04 9.48E+04	1.87E+04
	Down-dip Down-dip	1	2	94 19		7.99E+06 8.00E+06	7.99E+06 8.00E+06	2.88E+00 2.88E+00	1.63E-04 1.36E-04	2.94E-07	4.13E-04	2.94E-07	6.63E+08	0.00E+00	8.98E-04	6.83E-02	4.52E+01	4.42E+01	1.32E+07	9.94E-01	1.41E+07	7.51E-01	9.40E+04 9.30E+04	9.00E+04 7.99E+04
	Down-dip	i	2	73		4.05E+06	4.05E+06	1.00E+01	3.29E-05	7.96E-04 3.31E-02	3.09E-04 1.22E-04	8.00E-04 1.77E-01	2.81E+05 9.34E+02	0.00E+00 0.00E+00	2.43E+00 1.01E+02	1.46E+02 3.99E+04	4.10E+01 3.73E+01	4.01E+01	1.55E+07	8.60E-01	1.57E+07	4.46E-03	1.02E+05	4.43E+04
	Down-dip	1	2	59		5.91E+05	5.91E+05	1.10E+01	2.50E-05	2.06E-01	1.22E-04	2.85E+00	1.03E+02	0.00E+00	6.29E+02	3.99E+04	3.73E+01	3.55E+01 3.26E+01	9.40E+06 7.62E+06	8.06E-01 6.69F-01	1.18E+07 1.43E+07	2.10E-05 5.53E-06	8.33E+04 9.41E+04	1.92E+04 1.96E+04
	Down-dip Down-din	1	2	78 48		4.91E+05 8.00E+06	4.91E+05 8.00E+06	1.10E+01 2.88E+00	3.50E-05	1.05E+00	6.64E-05	5.37E+00	2.39E+01	0.00E+00	3.21E+03	1.26E+06	3,01E+01	2.95E+01	1.37E+07	5.97E-01	1.43E+07	1.94E-01		4.76E+04
345 E)own-dip	i	2	69		7.99E+06	7.99E+06	2.88E+00	1.03E-04 9.15E-05	3.02E-05 2.71E-04	1.56E-04 1.84E-04	3.02E-05 2.71E-04	5.12E+06 4.84E+05	0.00E+00 0.00E+00	9.21E-02 B.27E-01	5.38E+00 5.41E+01	2.74E+01 2.61E+01	2.68E+01 2.56E+01	1.18E+07 1.29E+07	B.98E-01	1.20E+07	3.17E-06	8.41E+04	3.08E+04
	own-dip	1	2	37		5.72E+05	5.72E+05	1.10E+01	1.77E-05	1.10E-01	B.57E-05	1.55E+00	1.31E+02	0.00E+00	3.35E+02	1.82E+05	2.38E+01	2.33E+01	6.37E+06	9,10E-01 6,77E-01	1.30E+07 1.16E+07	7.44E-01 1.32E-06	8.85E+04 8.24E+04	7.23E+04 1.84E+04
	Down-dip Down-dip	1	2	12 44		8.00E+06 7.99E+06	8.00E+06 7.99E+06	2.88E+00 2.88E+00	7.36E-05 6.16E-05	4.24E-07 1.71E-06	1.03E-04 8.49E-05	4.24E-07	2.76E+08	0.00E+00	1.29E-03	7.07E-02	1.94E+01	1.89E+01	1.00E+07	9.30E-01	1.02E+07	1.19E-07	7.63E+04	1.84E+04
349 E	Down-dip	1	2	f	8,00E+06	8.00E+06	8.00E+06	2.88E+00	3.98E-05	4.44E-05	9.45E-05	1.71E-06. 4,44E-05	5.31E+07 1.50E+06	0.00E+00 0.00E+00	5.23E-03 1,35E-01	3.05E-01 8.27E+00	1.81E+01 1.23E+01	1.58E+01 1.21E+01	1.02E+07 1.05E+07	8.89E-01 9.01E-01	1.02E+07	3.64E-01	7.65E+04	4.67E+04
	Jown-dip	1	2 2	46 24			3.95E+06	2.88E+00	3.16E-05	2.62E-02	9.70E-05	1.06E-01	1.16E+03	0.00E+00	7.99E+01	8.38E+03	9.72E+00		7.94E+06	8.10E-01	1.05E+07 8.69E+06	7.22E-01 6.74E-06	7.80E+04 6.82E+04	6.24E+04 1.43E+04
	yown-dip	i	2	24 71		8.04E+06 3.08E+05	8.04E+06 3.08E+05	2.88E+00 1.10E+01	3.38E-05 5.09E-06	2.73E-08 1.02E-01	4.19E-05 3.22E-05	2.73E-08 3.02E+00	1.89E+09 3.29E+01	0.00E+00 0.00E+00	8.34E-05	4.63E-03	B.69E+00	8.48E+00	9.07E+06	9.12E-01	9.00E+06	6.69E-01	7.09E+04	5.\$0E+04
353 E	Own-dip	1	2	65	0.00E+00	3.17E+05	3.17E+05	1.10E+01	5.52E-06	1.31E-01	2.63E-05	2.26E+00	3.29E+01	0.00E+00	3.12E+02 4.00E+02	2.29E+05 2.43E+05	7.52E+00 7.48E+00	7.35E+00 7.28E+00	4.14E+06 5.13E+06	5.20E-01 4.96E-01	1.01E+07 1.03E+07	8.94E-07 0.00E+00	7.63E+04	1.01E+04
	Down-dip Down-din	1	2 2	67 100		2.77E+05 8.00E+06	2.77E+05 B.00E+06	1,10E+01 2,88E+00	4.29E-06	9.47E-02	2.13E-05	1.80E+00	3.29E+01	0.00E+00	2.89E+02	1.76E+05	5.79E+00	5,49E+00	4.42E+06	4.77E-01	8.98E+06	1.71E-04	7.70E+04 7.02E+04	9.73E+03 1 1.14E+04
	Jown-dip	i	2	30				2.88E+00	1.76E-05 1.44E-05	9.86E-06 1.01E-07	3.77E-05 2.24E-05	9.86E-06 1.01E-07	3.08E+06 2.20E+08	0.00E+00 0.00E+00	3.01E-02 3.07E-04	1.77E+00 1.79E-02	5.43E+00	5.33E+00	9.27E+06	8.86E-01	9.20E+06	7.05E-01	7.24E+04	5.68E+04
	own-dip	1	2	56	0.00E+00	7.88E+06	7.88E+06	2.88E+00	1.26E-05	3.46E-04	2.71 Ë-05	6.17E-04	3.76E+04		1.06E+00		3.93E+00 3.78E+00	3.84E+00 3.70E+00	8.75E+06 8.81E+06	8.86E-01 9.09E-01	8.67E+06 8.65E+06	6.59E-01 4.08E-06	6.85E+04 6.95E+04	5.20€+04 1.96E+04
	own-dip	1	2	79 11		3.83E+05 8.02E+06	3.83E+05 8.02E+06	1.10E+01 2.88E+00	4.74E-06	4.59E+00	4.74E-06	1.70E+D1	6.20E-01	0.00E+00	1.40E+04	6.44E+06	3.99E+00	3.88E+00	1.08E+07	5.39E-01	1.14E+07	8.94E-07		1.96E+04 2.41E+04
	lown-dip	i	2	98				1.10E+01	1.38E-05 1.79E-06	4.70E-05 8.83E-02	1.88E-05 1.08E-05	5.80E-05 2.59E+00	2.92E+06 1.30E+01	0.00E+00 0.00E+00	1.43E-01 2.70E+02		3.63E+00 2.61E+00	3.54E+00	8.54E+06	9.20E-01	8.55E+06	2.22E-05	6.73E+04	1.60€+04
	lown-dip	1	2	20			2.43E+05	1.10E+01	1.24E-06	1.13E-01	6.46E-06	2.60E+00	7.17E+00	0.00E+00		2.46E+05	1.76E+00	2.61E+00 1.75E+00	3.36E+06 3.81E+06	4.12E-01 4.27E-01	8.41E+06 9.20E+06	3.70E-06 1.19E-07	6.61E+04 7.20E+04	6.89E+03 7.77E+03
	own-dip Jown-dip	1	2	42 41		3.15E+05 3.08E+05	3.15E+05 3.08E+05	1.10E+01 1.10E+01	4.99E-07 1.46E-07	2,57E-01 1.86E-01	3.49E-06	1.11E+01	1.23E+00			5.78E+05	7.09E-01	6.69E-01	4.08E+06	5.44E-01	1.31E+07	8.01E-07	8.87E+04	1.23E+04
364 D	Nown-dip	i	2	77	0.00E+00	2.97E+05	2.97E+05	1.10E+01	1.46E-07	1.89E-01	1.37E-06 1.10E-06	1.30E+01 9.05E+00	4.06E-01 4.19E-01	0.00E+00 0.00E+00		6.11E+05 5.59E+05	2.48E-01 2.34E-01	2.40E-01 2.28E-01	3.22E+06	2.71E-01	1.26E+07	1.57E-02	8.64E+04	1.09E+04
	kown-dip	1	2	84 06			2.72E+05	1.10E+01	2.81E-08	1.52E-01	2.53E-07	9.79E+00	9.81E-02	0.00E+00	4.66E+02	4.B0E+05	4.71E-02	4.71E-02	3.49E+06 2.81E+06	2.58E-01 1.50E-01	1.21E+07 1.01E+07	2.29E-05 0.00E+00	8.42E+04 7.60E+04	5.35E+03 5.29E+03
	Nown-dip Nown-dip	i	2	85 6				1.10E+01 1.10E+01	4.99E-09 6.85E-10	2.35E-01 1.64E-01	4.77E-08 7,46E-09	1.84E+01	1.09E-02	0.00E+00		7.75E+05	8.45E-03	8.13E-03	2.96E+06	3.33E-01	1.27E+07	3.12E-02	8.69E+04	9.24E+03
368 C	lown-dio	1	2	47	0.00E+00	4.09E+05	4.09E+05	1.10E+01	2.07E-11	2.65E-01	1.75E-10	1.55E+01 1.87E+01	2.01E-03 4.16E-05	0.00E+00	5.00E+02 8.07E+02	8.18E+05 8.12E+05	1.24E-03 3.38E-05	1.21E-03	2.58E+06 3.10E+06	2.06E-01 1.97E-01	1.15E+07	8.70E-03	8.21E+04	1.11E+04
	Hown-dip	1	3	22 51		3.90E+06		1.10E+01	7.58E-05	5.43E-02	1.36E-04	1.80E-01	1.52E+03	4.02E-05	1.66E+02	5.25E+04	7.98E+01	7.58E+01	9.07E+06	1.97E-01	1.24E+07 1.02E+07	2.97E-02 2.25E-02	8.57E+04 7.65E+04	1.00E+04 2.84E+04
	lown-dip lown-dip	1	3	46	_			1.10E+01 2.88E+00	4.11E-05 5.53E-05	6.43E-01 5.72E-05	5.22E-05 1.88E-04		5.92E+01 1.12E+06	9.71E-05			3.91E+01	3.69E+01	1.11E+07	6.82E-01	1.27E+07	2.36E-01	8.87E+04	3.33E+04
372 D	lown-dlp	1	3	78	8.01E+06	8.01E+06	1.17E+07	2.88E+00	6.00E-05	2.13E-05	1.42E-04	2.13E-05	1.12E+06 3.66E+06	1.39E-05 1.04E-05		1,54E+01 4,76E+00	1.74E+01 1.74E+01	1.70E+01 1.70E+01	1.10E+07 1.10E+07	9.65E-01 9.45E-01	9.32E+06	1.21E-02	7.50E+04	2.13E+04
	kown-dlp kown-dlp	1	3	69 52	8.00E+06 8.00E+06			2.88E+00	6.15E-05	0.00E+00	1.23E-04		1.74E+22	6.54E-06	0.00E+00	0.00E+00	1.74E+01	1.70E+01	1.10E+07	9.45E-01	1.09E+07 1.10E+07	6.03E-01 7.99E-01		6.00E+04 6.84E+04
	lown-dip	1	3	5	0.00E+00			2.88E+00 2.88E+00	5.84E-05 5.02E-05	2.66E-05 6.53E-04	1.44E-04 1.22E-04		2.89E+06 1.11E+05			5.87E+00	1.69E+01	1.66E+01	1.12E+07	9.60E-01	1.03E+07	6.00E-01	7.82E+04	5.94E+04
		٠	-	- 1					J.VLE-VO	J.002*04	. 222-04	J.00E-04	1.112+05	£.41E-U6	1.99E+00	1.47E+02	1.62E+01	1.59E+01	1.17E+07	8.55E-01	9.56E+06	4.32E-04	7.60E+04	1.84E+04

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					Ercavated Waste	0-4-0								naz													
ľ	•	•	•	•	Potosity (fraction)	Sal. (fraction)	Plesidual Brini Sat. (fiscilion)	Crushed Panel Height (m)	Pressure (Pa)	Up-dip Avg Sal. (fraction)	Down-dip Avg Pressure (Pa)	Down-dip Avg Sat. (fraction)	DRZ Porceity (Fraction)	Parmasbility (m/2)	Selt Piller Percently (Frantism)	Sell Pillar Permesbility	Intrusion Time (Years)	Skin factor	Well Productivity		Total Area solide released	Castile Reservoir	Castile Beservoir Permashlity	Up dip Srine Relative	Noistre	Down-dip Brine Relative	Down-dip Out
No. II		Replic.	Scen.	Vector	POROSITY	SAT_RGAS	SAT_RORN	HEIGHT	PRESPAN2	BSATPAN2	PRESPAN4	BSATPAN4	POROSITY	ų., L)	POROSITY	PERM X	INTR THE	SKIN	Index (1/Pa)	(m*2)	(m*2)	Pressure (Pa)	(m/5)	Permeability (fraction)	Permeability (fraction)	Permeability (fraction)	Permosbility (traction)
	vn-dip vn-dip	1	3	44 45	5.31E-01 5.27F-01	1.12E-01 5.05E-02		1.28E+00 1.27E+00	1.02E+07 9.88E+06	5.79E-01 9.82E-01	1.02E+07 9.97E+08	B.85E-01	1 29E-01	1.18E-13	1.34E-01	1.18E-13	1.20E+03	-1.17E+00	1.22E-13	PRM_SAND 3.80E-15	7.83E-01	1.38E+07	1.12F.12	1.27E-01	KRG2 6.57E-02	6.3 (E-01	KRG4 9.69E-0A
378 Doi		1	3	54	4.92E-01	1.25E-01	2.39E-02	1.19E+00	6.76E+06	2.33E-06	9.97E+08 1.20E+07	9.84E-01 8.47E-01	7.63E-02 3.07E-02	5.13E-14 5.01E-18	8.96E-02 5.37E-02	5.13E-14 2.57E-18	1,20E+03 1,20E+03	-9.31E-01 -1.16E+00	1.11E-13 1.13E-13	1.74E-15	4.89E-01	1.36E+07	4.57E-13	9.18E-01	0.00E+00	9.26E-01	0.00E+00
	wn-địp wn-địo	1	3	41 31	4.94E-01 5.43E-01	3.40E-02 5.2BE-02	8.64E-02 5.93E-02	1.19E+00 1.32E+00	7.00E+06 1.12E+07	7.55E-02	1.12E+07	9.40E-01	1.42E-01	1.70E-19	1.64E-01	1.70E-19	1.20E+03	-1.22E+00	1.13E-13	4.68E-12 3.24E-16	7.76E-01 8.64E-01	1.56E+07 1.48E+07	1.66E-12 3.47E-12	0.00E+00 0.00E+00	1.00E+00 1.00E+00	5.34E-01 7.76E-01	5 68E-05
381 Do	wn-dlp	1	3	16	4.84E-01	5.75E-02	2.76E-01	1.17E+00	6.33E+06	8.27E-04 5.91E-05	1.12E+07 1.17E+07	8.59E-01 9.17E-01	7.70E-02 9.07E-02	1.66E-15 2.24E-19	8.88E-02 1.33E-01	1,66E-15 2,14E-19		-1.27E+00		3.31E-14	9.73E-01	1.48E+07	6.31E-13	0.00E+00	1.00E+00	5.48E-01	4.60E-05 1.62E-03
	vn-dip vn-dio	1	3	43 23	4,73E-01 5,16E-01	5.88E-02 7.29E-02	_,,,,	1.15E+00 1.24E+00	5.67E+06 8.60E+06	8.08E-03	1.15E+07	9.15E-01	1.65E-01	2.87E-19	2.05E-01	9.77E-20	1.20E+03 1.20E+03	-1.29E+00 -1.26E+00	1.18E-13 1.14E-13	1.91E-14 3.63E-13	1.01E+00 9.52E-01	1.53E+07 1.51E+07	1.86E-12 9.55E-12	0.00E+00 0.00E+00	1.00E+00	6.40E-01 6.58E-01	8.87E-05
384 Dov	₩n-dip	i	3	7	5.20E-01	7.76E-03		1.24E+00 1.25E+00	9.39E+06	3.37E-02 6.14E-01	1.16E+07 9.44E+06	9.23E-01 9.90E-01	3.18E-02 1.42E-01	1.18E-16 2.29E-13	4.90E-02 1.63E-01	1.18E-16 2.29E-13	1.20E+03	-1.18E+00	1.19E-13	7.94E-17	8.09E-01	1.52E+07	6.03E-13	0.00E+00	1.00E+00	5.54E-01	7.70E-05 1.28E-06
	wn-dip wn-din	1	3	72 39	4.97E-01 5.40E-01	2.36E-02 1.50E-01		1.20E+00	7.34E+08	7.21E-06	1.07E+07	9.37E-01	5.96E-02	4.62E-18	8.58E-02	1.82E-18	1.20E+03 1.20E+03	-6.15E-01 -6.26E-01	9.80E-14 9.39E-14	7.94E-14 5.37E-12	2.60E-01 2.66E-01	1.30E+07 1.43E+07	1.35E-12 5.75E-13	1.08E-02 0.00E+00	4.31E-01 1.00E+00	9.49E-01 7.85E-01	3.90E-08
	wn-dip	i	3	73	5.30E-01	5.61E-02		1.31E+00 1.28E+00	1.09E+07 1.01E+07	3,36E-01 6,53E-02	1.09E+07 1.02E+07	8.47E-01 9.37E-01	1.89E-02 9.23E-02	3.02E-15 3.72E-16	2.93E-02 1.11E-01	3.02E-15 3.72E-16		-1.23E+00		2.40E-13	8.82E-01	1.45E+07	1.78E-13	2 07E-05	8.59E-01	4.02E-01	1.11E-04 5.28E-07
	vn-dip vn-dio	1	3	97	5.04E-01 4.47E-01	8.37E-02 1.07E-01	4.34E-01	1.21E+00	7.60E+06	4.86E-01	1.07E+07	9.13E-01	1.46E-01	5.63E-16	1.73E-01	5.62E-16	1.20E+03 1.20E+03	-8.01E-01 -8.88E-01	1.06E-13 1.04E-13	6.17E-15 4.57E-13	3.77E-01 4.49E-01	1.37E+07 1.43E+07	9.77E-12 3.02E-11	0.00E+00 1.48E-04	1.00E+00 7.78E-01	7.05E-01	2.17E-06
390 Dov	vn-dip	i	3	80	4.74E-01	6.43E-02	3.28E-01 2.68E-01	1.10E+00 1.15E+00	4.31E+06 5.90E+06	1.15E-01 2.84E-03	1.13E+07 1.06E+07	8.83E-01 9.15E-01	1.27E-01 3.92E-02	6.31E-19 1.59E-18	1.64E-01 6.33E-02	6.31E-19 5.01E-19	1.20E+03	-7.31E-01	8.93E-14	8.32E-16	3.28E-01	1.49E+07	2.53E-14	0.00E+00	1.00E+00	5.38E-01 4.93E-01	8.46E-07 1.03E-05
	vn-dip vn-din	1	3	6 34	4.27E-01 5.17E-01	6.58E-02	1.45E-01	1.06E+00	3.49E+06	1.23E-01	1.04E+07	9.20E-01	5.65E-02	5.76E-19	9.47E-02	5.75E-19	1.20E+03 1.20E+03	-8.21E-01 -1.18E+00	9.62E-14 1.02E-13	2.09E-12 6.46E-17	3.93E-01 8.02E-01	1.42E+07 1.40E+07	2.04E-13 3.09E-12	0.00€+00 0.00E+00	1.00E+00	6.34E-01	5.03E-05
393 Day	m-dip	i	3	68	4.86E-01	2.76E-02 6.78E-04	3.26E-01 5.01E-01	1.24E+00 1.17E+00	8.94E+06 6.68E+06	2.38E-03 5.96E-08	9.95E+06 1.03E+07	9.56E-01 9.91E-01	1.98E-02 1.69E-02	2.30E-17 9.12E-17	3.24E-02 3.55E-02	2.29E-17 9.12E-17	1.20E+03	-1.07E+00	1.14E-13	7.08E-14	6.47E-01	1.35E+07	4.68E-14	0.00E+00	1.00E+00 1.00E+00	6.96E-01 7.79E-01	9.78E-06 2.82E-05
	vn-dip vn-dio	1	3	53 60	4.48E-01 5.01E-01	4.46E-02	2.52E-01	1.10E+00	4.52E+06	2.97E-01	1.02E+07	8,43E-01	1.54E-01	9.23E-18	2.01E-01	8.51E-18	1.20E+03 1.20E+03	-1.32E+00 -1.23E+00	1.19E-13 1.07E-13	4.57E-16 1.38E-12	1.06E+00 8.92E-01	1.39E+07 1.38E+07	3.02E-13 4.57E-12	0.00E+00	1.00E+00	9.32E-01	9.27E-06
396 Dov	vn-dip-⊓v	i	3	21	4.62E-01	6.13E-02 7.93E-02	4.70E-02 4.09E-01	1.20E+00 1.12E+00	7.82E+06 5.35E+06	1.34E-01 7.35E-03	9.67E+08 9.96E+08	9.17E-01 9.05E-01	1.94E-01 1.70E-01	6.10E-18	2.14E-01 2.02E-01	5.75E-18	1.20E+03	-1.17E+00	1.15E-13	6.61E-13	7.91E-01	1.33E+07	234E-14	3.07E-05 1.44E-04	8.68E-01 7.99E-01	7.47E-01 7.13E-01	9.14E-06 2.56E-05
397 Dov 398 Dov	m-dip	1	3	57 90	4.36E-01 4.57E-01	7.43E-02	2.79E-01	1.07E+00	4.01E+06	1.14E-01	9.71E+06	9.07E-01	5.90E-02	5.52E-18	9.25E-02	8.32E-20 1.29E-18	1.20E+03 1.20E+03	-1.64E+00 -1.19E+00	1.26E-13 1.04E-13	1.45E-13 8.13E-12	1.65E+00 6.25E-01	1.35E+07 1.33E+07	4.90E-13 7.94E-14	0.00E+00	1.00E+00	5 22E-01	5 22E-05
399 Doy	··· – p	ì	3	90	5,17E-01	1.28E-02 1.35E-01	2.86E-01 5.34E-01	1.11E+00 1.24E+00	5.16E+06 8.75E+06	4.33E-02 3.32E-03	9.48E+06 1.07E+07	9.72E-01 8.51E-01	1.23E-02 1.51E-02	1.20E-17 2,36E-19	4.05E-02 2.91E-02	1.20E-17 2.34E-19	1.20E+03	-8.48E-01	9.41E-14	2.09E-14	4.15E-01	1.31E+07		0.00E+00	1.00E+00	5.99E-01 8.84E-01	4 34E-05 1.63E-05
	m-dip m-din	1	3	76 100	4.80E-D1	1.38E-01	3.34E-01	1.16E+00	6.43E+06	2.27E-06	9.79E+06	8.47E-01	3.21E-02	3.16E-18	5.59E-02	3.16E-18	1,20E+03 1,20E+03	-1.24E+00 -1.33E+00	1.22E-13 1.18E-13	2.63E-15 5.50E-16	9.00E-01 1.09E+00	1.43E+07 1.34E+07		0.00E+00	1.00E+00	2.42E-01	1.18E-04
	uu-qiip uu-qiip	i	3	1	4.90E-01 4.74E-01	1.14E-01 9.81E-02	3.43E-01 2.56E-01		7.22E+06 6.18E+06	9.09E-01 9.29E-01	9.20E+06 9.16E+06	9.36E-01 9.53E-01	6.67E-02 6.25E-02	9.12E-16 7.24E-16	9.21E-02 9.61E-02	9.12E-16 7.24E-16	1.20E+03	-1.26E+00	1.17E-13	2.51E-14	9.43E-01	1.28E+07	2.09E-12 1.29E-13	0.00E+00 5.77E-01	1.00E+00 0.00E+00	3.82E-01 6.84E-01	3.98E-05 0.00E+00
403 Dow 404 Dow	m-dip	!	3	65 70	5.16E-01	1.27E-01	8.96E-02		9.14E+06	8.00E+00	9.16E+06	8.01E-01	1.88E-02	8.71E-16	3.15E-02	8.71E-16	1.20E+03	-1.28E+00 -1.16E+00	1.14E-13 1.18E-13	1.66E-14 4.17E-15	9.73E-01 7.73E-01	1.28E+07 1.27E+07	7.08E-14 3.72E-12	6.92E-01 0.00E+00	0.00E+00	7.87E-01	0.00E+00
	m-dip	1	3	2	4.67E-01 5.28E-01	4.63E-02 8.22E-02	4.24E-01 4.02E-01	1.13E+00 1.27E+00	5.74E+06 9.94E+06		9.30E+06 9.95E+06	9.36E-01 6.07E-01	2.29E-01 1.67E-01	6.17E-20 4.47E-14	2.58E-01 1.78E-01	6.17E-20	1.20E+03	-1.28E+00	1.13E-13	1.00E-16	9.91E-01	1.29E+07		0.00E+00	1.00E+00 1.00E+00	4.02E-01 6.47E-01	1.30E-03 6.42E-05
406 Dow 407 Dow	-	1	3	67	4.91E-01	1.21E-01	6.61E-02	1.1BE+00	7,30E+06	1.10E-01	9.16E+06	8.46E-01	1.71E-01	3.55E-18	1.78E-01 1.96E-01	4.47E-14 3.55E-18	1.20E+03 1.20E+03	-1.29E+00 -1.27E+00	1.27E-13 1.17E-13	5.01E-14 7.24E-15	9.98E-01 9.65E-01	1.36E+07 1.27E+07	7.24E-11 1.15E-14	3.29E-03	5.15E-01	1.92E-02	2.87E-01
408 Daw		1	3	95 20	5.21E-01 5.13E-01	1.46E-01 1.23E-DI	3.69E-01 1.27E-01	1.25E+00 1.23E+00	9.38E+06 8.83E+06		9.59E+06 9.28E+06	8.45E-01 8.57E-01	1.56E-01 1.95F-02	6.03E-17	1.74E-01	6.03E-17	1,20E+03	-9.54E-01	1.10E-13	1.10E-16	5.13E-01	1.32E+07		1.27E-05 0.00€+00	8.88E-01 1.00E+00	5 14E-01 3.52E-01	1.17E-04 1.18E-05
409 Dow 410 Dow		1	3	13	3.88E-01	1.83E-02	4.86E-01	9.99E-01	1.72E+06	6.84E-01	9.33E+06	9.80E-01	5.38E-02	1.35E-17 1.69E-18	3.77E-02 9.75E-02	1.35E-17 1.62E-18	1.20E+03 1.20E+03	-6.04E-01 -1.31E+00	9.61E-14 1.01E-13	3.31E-15 1.23E-13	2.55E-01 1.03E+00	1.29E+07 1.29E+07	1.20E-12	0.00E+00	1.00E+00	5.16E-01	3.35E-05
410 Dow		1	3	84 19	4.50E-01 5.13E-01	1.44E-01 1.42E-01	6.88E-03 2.97E-02	1.10E+00 1.23E+00	4.83E+06 8.91E+06		9.16E+06 8.95E+06	8.34E-01 8.51E-01	1.46E-02 2.01F-01	4.91E-20	4.02E-02	4.90E-20	1.20E+03	-1.40E+00	1.16E-13	2.95E-16	1.25E+00		2.69E-12 3.55E-11	2.96E-02 1.36E-07	2.84E-01 9.67E-01	8.65E-01 5.08E-01	4.63E-08 3.28E-05
412 Dow		1	3	10	5.00E-01	3.17E-02	1.73E-01	1.20E+00	8.20E+06	2.89E-01	8.20E+06	4.84E-01	4.89E-02	1.41E-15 3.72E-14	2.21E-01 7.38E-02	1.41E-15 3.72E-14	1.20E+03 1.20E+03	-1.23E+00 -1.33E+00	1.21E-13 1.22E-13	2.00E-16 1.86E-16	8.94E-01 1.08E+00	1.25E+07 1.18E+07	1.45E-12	4.30E-04 7.08E-04	7.06E-01	5.40E-01	1.03E-06
414 Dow	··	1	3	55 50	5.10E-01 4.81E-01	7.03E-02 1.09E-01	2.38E-01 5.44E-01	1.23E+00 1.16E+00	8.75E+06 6.60E+06		8.74E+06 9.40E+06	9.26E-01 8.76E-01	9.27E-02 2.12E-01	8.71E-15 8.73E-19	1.11E-01	8.71E-15	1.20E+03	-8.68E-01	1.04E-13	6.03E-12	4.31E-01	1.24E+07	1.35E-11 1.62E-11	7.08E-04 0.00E+00	7.02E-01 1.00E+00	2.70E-02 6.85E-01	2.95E-01 3.26E-07
415 Dow		1	3	29	4.52E-01	7.66E-02	4.76E-01	1.10E+00	4.99E+06	3.27E-01	8.92E+06	9.17E-01	1.76E-01	8.73E-19 3.85E-17	2.44E-01 2.20E-01	2.88E-19 3.72E-17	1.20E+03 1.20E+03	-1.27E+00 -1.52E+00	1.16E-13 1.22E-13	1.12E-12 2.63E-12	9.68E-01 1.58E+00	1.30E+07 1.25E+07		0.00E+00	1.00E+00	3.11E-01	1.26E-04
416 Dow 417 Dow		1	3	32 66	4.51E-01 5.00E-01	1.00E-01 9.43E-02	5.29E-01 5.49E-01	1.10E+00 1.20E+00	4.86E+06 7.96E+06		9.19E+06 8.99E+06	8.96E-01 8.91E-01	3.96E-02	1.10E-16 6.23E-18	7.10E-02	1.10E-18	1.20E+03	-9.74E-01	9.74E-14	5.62E-13	5.33E-01	1.28E+07	7.94E-12 2.00E-12	0.00E+00 0.00E+00	1.00E+00 1.00E+00	5.27E-01 3.97E-01	5.94E-06 1.87E-06
418 Dow		1	э	77	4.91E-01	1,48E-01	6.84E-02	1.18E+00	7.43E+06			8.14E-01	8.45E-02 2.04E-01	6.23E-18 8.13E-19	1.11E-01 2.34E-01	5.37E-18 8.13E-19	1.20E+03	-1.37E+00 -7.13E-01	1.25E-13 9.54E-14	1.66E-12 2.75E-16	1.18E+00 3.17E-01	1.26E+07 1.24E+07		0.00E+00	1.00E+00	3.61E-01	1.10E-04
419 Dow 420 Dow		1	3 3	88 64	4.82E-01 4.66E-01	1.19E-01 1.33E-01	2.88E-01 1.78E-02	1.16E+00 1.13E+00	6.85E+06 5.87E+06			8.73E-01 8.59E-01	2.00E-02 4.96E-02	2.61E-16	4.25E-02	2.57E-16	1.20E+03	-1.19E+00	1.12E-13	7.59E-12	8.14E-01			0.00E+00 0.00E+00	1.00E+00	4.38E-01 4.85E-01	1.93E-04 4.40E-06
421 Dow	··P	1	3	47	4.45E-01	6.75E-02	1.61E-01	1.09E+00	4.70E+06			9.14E-01	1.47E-01	3.41E-16 6.92E-18	8.15E-02 1.81E-01	3.39E-16 6.92E-18		-1.53E+00 -1.09E+00	1.26E-13 1.01E-13	3.63E-12 2.19E-16	1.62E+00 6.75E-01		2.24E-12	5.35E-05	8.34E-01	5.64E-01	1.85E-06
422 Dow 423 Dow		1	3	71 96	4.80E-01 4.99E-01	1.57E-02 2.90E-03	1.06E-01 2.47E-01		6.80E+06 8.16E+06		8.41E+06 8.28E+06	9.43E-01 9.92E-01	3.97E-02	2.19E-18	6.99E-02	2.19E-18	1.20E+03	-1.37E+00	1.20E-13	5.25E-17	1.18E+00	1.20E+07	1.55E-12 6.76E-13	1.44E-05 0.00E+00	8.91E-01 1.00E+00	6.71E-01 7.84E-01	2.33E-05 1.73E-04
424 Dow		1	3	27	4.93E-01	1.18E-01	4.62E-01	1.18E+00	7.62E+06				3.74E-02 2.61E-02	3.55E-16 1.86E-18	5.66E-02 4.51E-02	3,55E-15 1,86E-16		-1.16E+00 -1.24F+00	1,14E-13 1,16E-13	1.07E-13 2.40E-15	7.79E-01 9.09E-01	1.19E+07 1.20E+07	4.79E-12	0.00E+00	1.00E+00	9.63E-01	4.56E-07
425 Dow 426 Dow		1	3	35 24	5.03E-01 4.97E-01	9.57E-02 9.01E-02	4.39E-01 1.37E-01		8.35E+06 8.04E+06			9.02E-01 9.08E-01	5.14E-02	7.24E-15	6.83E-02	7.24E-15	1.20E+03	-8.97E-01	1.04E-13	1.38E-13	4.57E-01		1.26E-12 3.98E-11	0.00E+00 4.65E-01	1.00E+00 1.38E-05	3.87E-01 4.93E-01	1.12E-06 1.97E-07
427 Dow		1	3	86	4.40E-01	6.86E-02	9.61E-02	1.08E+00	4.49E+06		8.24E+06	9.19E-01	1.98E-01 1.55E-01	2.82E-13 3.04E-17	2.26E-01 1.98E-01	2.82E-13 3.02E-17		-1.29E+00 -1.26E+00	1.20E-13 1.07E-13	2.63E-14 4.07E-13	9.94E-01 9.43E-01		7.41E-13	6.59€-01	3.43E-08	6.59E-01	3.36E-08
428 Dow 429 Dow		† T	3	98 37	4.74E-01 5.09E-01	3.56E-02 4.07E-02	5.00E-02 2.28E-01		6.45E+06 6.74E+06			9.15E-01 4.08E-01	5.69E-02	4.19E-19	9.04E-02	4.17E-19	1.20E+03	-1.23E+00	1.12E-13	4.79E-15	8.82E-01	1.17E+07	2.04E-11 3.98E-14	5.23E-02 0.00E+00	1.88E-01 1.00E+00	7.23E-01 7.06E-01	4.61E-06 2.70E-04
430 Dow	n-dip	1	3	62	5.27E-01	8.52E-02	4.53E-01	1.27E+00	9,89E+06	1.16E-01		4.08E-01 5.74E-01	1.14E-01 1.30E-01	3.98E-16 2.14E-15	1.27E-01 1.39E-01	3.98E-16 2.14E-15		-1.19E+00 -1.39E+00	1.18E-13 1.33E-13		8.19E-01 1.22E+00	1.22E+07	6.17E-12	0.00E+00	1.00E+00	4.64E-03	5.15E-01
431 Dow 432 Dow	·· p	1	3	33 94	5.12E-01 5.45E-01	1.31E-01 4.58E-03	1.22E-01 1.85E-01		8.88E+06 1.13E+07				2.95E-02	1.12E-14	4.09E-02	1.12E-14	1.20E+03	-1.24E+00	1.21E-13		9.16E-01		8.13E-13 1.26E-13	0.00E+00 1.64E-02	1.00E+00 3.01E-01	3.74E-03 2.42E-03	4.90E-01 5.44E-01
433 Dow		1	3	99	5.19E-01	1.28E-01	5.15E-01	1.25E+00	9.32E+06	1.64E-D1	9,33E+06	5,52E-01	2.04E-01 1.72E-01	6.31E-15 5.89E-17	2.11E-01 1.92E-01	6.31E-15 5.89E-17	1.20E+03 1.20E+03	-1.29E+00 -7.63E-01	1.32E-13 1.03E-13	9.77E-16 6.17E-17	9,95E-01	1.44E+07	1.785-12	6.13E-05	8.50E-01	2.47E-04	7.81E-01
434 Down 435 Down		1	3	56 58	5.02E-01 5.68E-01	4.66E-02 2.96E-02	3.20E-01 1.14E-01		8.33E+06 1.32E+07				8.25E-02	1.05E-15	9.99E-02	1.05E-15	1.20E+03	-7.21E-01	9.77E-14		3,50E-01 3,22E-01			0.00E+00 0.00E+00	1.00E+00 1.00E+00	7.48E-05 1.04E-05	7.86E-01 9.01E-01
436 Down	n-dip	1	3	49	5.61E-01	3.07E-02	7.64E-02	1.37E+00	1.26E+07				2.10E-01 4.01E-02	2.52E-16 4.27E-15	2.07E-01 4.19E-02	1.45E-16 4.27E-15		-1.18E+00 -1.26E+00	1.33E-13 1.36E-13		8.11E-01 9.52E-01	1.32E+07	1.07E-13	1.14E-07	9.72E-01	4.67E-06	9.23E-01
437 Down		1	3		5.50E-01 5.70E-01	1.16E-01 9.72E-02	4.16E-02 1.79E-01	1.33E+00 1.40E+00	1.17E+07 1.35E+07	5.30E-02		5.85E-02	3.51E-02	2.75E-14	4.16E-02	2.75E-14	1.20E+03	-6.49E-01	1.05E-13	2.19E-13	9,52E-01 2,79E-01			0.00E+00 7.83E-08	1.00E+00 9.73E-01	3.18E-06 3.35E-07	9.31E-01 9.59E-01
439 Down	n-dip	1	3	10	5.12E-01	3.17E-02	1.73E-01	.,,00,00				1.88E-01 7.24E-01	2.10E-01 5.02E-02	5.59E-17 3.72E-14	2.11E-01 7.19E-02	4.79E-17 3.72E-14		-1.08E+00 -1.33E+00	1.29E-13 1.25E-13	9.55E-12	6.64E-01	1.48E+07	9.55E-14	2.65E-10	9.94E-01	5.94E-08	9.75E-01
440 Down		1	3	78 44	5.58E-01 5.42E-01	4.93E-02 1.12E-01	1.51E-01 1.61E-02			7.80E-01	1.24E+07		1.14E-01	3.55E-15	1.11E-01	2.46E-15	1.40E+03	-1.06E+00	1.25E-13 1.24E-13		1.08E+00 6.28E-01			0.00E+00 3.30E-01	1.00E+00 1.53E-02	2.24E-01 7.81E-01	4.34E-02 6.07E-07
442 Down	n-dilp	1	3	18	5.08E-01	1.06E-01	3.40E-01	1.22E+00	8.66E+06			8.85E-01 6.81E-01	1.30E-01 5.11E-02	1.30E-13 3.31E-14	1.31E-01 7.38E-02	1.18E-13 3.31E-14		-1.17E+00 -1.09E+00		3.80€-15	7.83E-01	1.38E+07	1.12E-12	3.65E-02	2.13E-01	6.31E-01	8.69E-08
443 Down 444 Down		1	3	69	5.44E-01 5.29E-01	8.98E-02 5.05E-02	4.08E-01 2.04E-01				1.12E+07	9.17E-01	7.90E-02	1.26E-14	B.74E-02	1.26E-14		-1.09E+00 -1.29E+00	1.13E-13 1.32E-13					4.87E-03 5.40E-01	4.61E-01 1.72E-08		8.31E-02
445 Down	n-dip	i	3	52	5.39E-01	3.68E-02				9.69E-01 9.58E-01		9.71E-01 9.60E-01	7.65E-02 1.10E-01	5.13E-14 1.70E-15	8.93E-02 1.26E-01	5.13E-14 1.70E-15		-9.31E-01		1.74E-15	4.89E-01	1.36E+07	4.57E-13	8.64E-01	0.00E+00		0.00E+00 0.00E+00
446 Down 447 Down		1	3	31 73				1.29E+00	1.05E+07	5.60E-06	1.05E+07	8.56E-01	7.60E-02	1.66E-15	9.04E-02	1.66E-15		-9.48E-01 -1.27E+00	1.14E-13 1.29E-13						2.19E-06 1.00E+00	7.57E-01 5.41E-01	4.33E-07
448 Dowi	1-dip	1	3		5.29E-01	5.61E-02 1,29E-01	3.03E-01 1.21E-01			5.49E-02 6.40E-05			9.28E-02 1.33E-01	3.72E-16 1.91E-17	1.10E-01 1.48E-01	3.72E-16 1.82E-17		-8.01E-01		8.17E-15	3.77E-01	1.37E+07	9.77E-12	0.00E+00	1.00E+00		1.79E-03 2.11E-06
449 Down 450 Down		1	3		5.25E-01	2.03E-02			9.68E+06	6.72E-03	1.00E+07	9.64E-01	4.68E-02	1.59E-17	6.30E-02	1.59E-17		-1.37E+00 -1.41E+00	1.32E-13 1.33E-13								3.95E-05
-00 LOW	, up	•	3	90	5.18E-01	1.27E-01	8.96E-02	1.25E+00	9.21E+06 I	0.00E+00	9.23E+06	7.38E-01	1.89E-02	8.71E-16	3.14E-02		1.40E+03 ·						3.72E-12	0.00E+00		8.36E-01 2.85E-01	1.60E-05 8.21E-03

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	J

			•		•	Uo dia Flowina	Down-dip	BC well	Manager					Produced	Cum Brine					Aug Brian	Avg Brine		Ava Bane	100	
1	•		•	•	•	Battern-hole	Flowing Bolern-hole	Injection	Duralion	Brime Rate (m^3/s)	Ges Bete (ref m^3/a)	Max Brine Flate (m^3/s)	Max Gas Rate (ref m^3/s)	Linux/Gas	from Boundary Condition Well		Cum Gas Produced (ref	Cum Brine Produced	Curn Bring Raingses	Avg Brine Proseure	Saturation Panel 5	Avg Brins Prossum	Saturation Pared 0	Exceveled	Total Exception
١						Pressure (Pa)	Presente (Pa)	Pressure (Pa)	(Days)	1		, mw (iii 32)	hat in Oral	(e/t/m has	(m/g)	(mac//day)	M/3)	(m^3)	(D^m)	Panel 5 (Pa) after Blowout	(Anction) after	Panel 0 (Pa)	(kaction) after	Waste Porc Volume	Prime Volume
97/	1D Down		aplic.	Scan.	Vector	5BHP2 3.60E+05	F8HP4 7 99F+06	1.07E+07	time	BRINEFLW			MAX_GAS		BRINE_BC	GAS_RATE	GASOUT	BRINEOUT	BRIN_REL	BRNPRES5	SATBRNS	BANPRESO	blowoul SATBRING	(traction)	/ TOT_8RIN
37			i	3	45	B.00E+06	8.00E+06		2.88E+00 2.88E+00	5.93E-05 5.67E-05	4.52E-06 0.00E+00	8.12E-05 9.65E-05	4.52E-06 0.00E+00	1.73E+07 1.54E+22	1.61E-05 1.48E-05	1.38E-02		1.55E+01	1,51E+01	1.02E407	8.87E-01	1.02E+07	3.32E-01	7.63E+04	
374			1	3	54	0.00E+00	8.04E+06	1.25E+07	2.88E+00	4.81E-05	7.63E-04	1.14E-04	8.05E-04	8.33E+04	8.51E-06	0.00E+00 2.33E+00			1.51E+01 1.60E+01	9,78E+08 1,19E+07	9.84E-01 8.50E-01	9.80E+00 6.76E+06	8.81E-01	7.52E+04	7.38E+04
37%			1	3	41 31	0.00E+00	8.04E+06 7.70E+06	1,18E+07 1,15E+07	2.88E+00 2.88E+00	4.78E-05 4.80F-05	1.74E-04	1.37E-04	2.18E-04	3.13E+05	1.05E-05	5.31E-01	4.74E+01	1.48E+01	1,48E+01	1.10E+07	9.40E-01	7.00E+08	2.33E-08 7.56E-02	6.59E+04	
381			i	3	16	0.00E+00	8.04E+06	1.15E+07	2.88E+00	4.80E-05	4.11E-03 5.40E-04	1.20E-04 1.31E-04	8.55E-03 6.61E-04	1.16E+04 9.92E+04	7.91E-06	1.25E+01	1.27E+03	1.47E+01	1.44E+01	1.10E+07	8.61E-01	1.12E+07	6.38E-04	B.02E+04	1.89E+04
382		-,	1	3	43	0.00E+00	8.04E+06	1.21E+07	2.88E+00	4.47E-05	4.25E-04	1.24E-04	5.05E-04	1.23E+06		1.65E+00 1.30E+00	1.48E+02 1.15E+02	1.47E+01 1.41E+01	1.44E+01 1.38E+01	1.14E+07 1.13E+07	9.18E-01 9.16E-01	6.33E+06 5.67E+06	6.91E-05 8.08E-03	6.37E+04	
383			1	3	23 7	0.00E+00 2.41E+05	8.02E+06		2.88E+00	4.29E-05	1.89E-04	1.13E-04	1,90E-04	3.35E+05	6.07E-06	5.77E-01	4.02E+01	1.35E+01	1.32E+01	1.14E+07	9.24E-01	8.50E+06	3.39E-02	6.09E+04 7.20E+04	_,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
386			i	3	72	0.00E+00	7.99E+06 8.04E+06	9.99E+06 1.12E+07	2.88E+00	5.03E-05 3.86E-05	6.56E-08 2.11E-04	6.45E-05 9.51E-05	6.66E-08 3.15E-04	8.13E+08 1.99E+05	2.12E-05	2.00E-04	1.60E-02	1.30E+01	1.27E+01	9.34E+06	9.91E-01	9.39E+06	4.04E-01	7.32E+04	
386		7	1	3	39	3.25E+05	8.01E+06		2.88E+00	3.50E-05	1.93E-04	7.03É-05	1.93E-04	3.28E+05		6.43E-01 5.89E-01	5.88E+01 3.28E+01	1.17E+01 1.07E+01	1.14E+01 1.05E+01	1.05E+07 1.08E+07	9.37E-01 8.50E-01	7.34E+06 1.09E+07	7.24E-06	6.67E+04	
387			1	3	73 97	0.00E+00	8.02E+06 8.01E+06	1.08E+07 1.14E+07	2.88E+00	3.26E-05	1.94E-05	7.69E-05	1.94E-05	2.23E+06	1.08E-05	5.92E-02	4.39E+00	9.77E+00	9.58E+00	1.01E+07	9.38E-01	1.09E+07	2.09E-01 6.57E-02	7.90E+04 7.59E+04	4.12E+04 2.24E+04
389			i	3	14		8.04E+06		2.88E+00 2.88E+00	3.20E-05 3.06E-05	7.26E-05 2.43E-04	7.24E-05 6.84E-05	7.26E-05 2.43E-04	6.84E+05 1.84E+05	1.03E-05 0.00E+00	2.22E-01 7.41E-01	1.43E+01	9.74E+00	9.55E+00	1.06E+07	9.14E-01	7.80E+06	3.69E-01	0.86E+04	4.36E+04
390			1	3	80		8.04E+06		2.88E+00	3.05E-05	1.80E-04	7.33E-05	1.935-04	2.05E+05	2.58E-06	5.50E-01	5.17E+01 4.60E+01	9,48E+00 9,40E+00	9.30E+00 9.22E+00	1.11E+07 1.04E+07	9.85E-01 9.16E-01	4.31E+06 5.90E+06	1.15E-01 2.85E-03	5.52E+04	
391 392			1	3	6 34		8.04E+06 8.04E+06		2.88E+00 2.88E+00	2.96E-05 2.86E-05	5.00E-05	7.90E-05	5.13E-05	7.51E+05	8.71E-06	1.53E-01	1.22E+01	9.18E+00	9.00E+00	1.02E+07	9.21E-01	3.49E+06	1.23E-01	6.10E+04 5.10E+04	1.86E+04 2.59E+04
393			i	3	68	0.00E+00	8.03E+06		2.88E+00	2.80E-05	4.85E-05 9.14E-06	8.09E-05 1.18E-04	6.52E-05 2.63E-05	6.61E+05 3.20E+06	0.00E+00 1.15E-05	1,48E-01 2,79E-02	1.33E+01	8.81E+00	8.64E+00	9.71E+06	9.56E-01	8,94E+06	2.39E-03	7.21E+04	1.89E+04
394			1	3	53	0.00E+00	8.03E+06	1.08E+07	2.88E+00	2.83E-05	3.08E-05	8.11E-05	3.33E-05	1.11E+06		9.41E-02	2.74E+00 7.90E+00	8.76E+00 8.75E+00	8.60E+00 8.58E+00	9.67E+06 9.99E+08	9.90E-01 9.44E-01	6.68E+06 4.52E+06	5.96E-08 2.80E-01	6.38E+04	2.14E+04
395			1	3	60 21	0.00E+00 0.00E+00	8.04E+06 8.04E+06	8.89E+06 1.04E+07	2.885+00	2.53E-05	4.73E-05	6,40E-05	5.44E-05	6.30E+05	0.00E+00	1.44E-01	1.25E+01	7.87E+00	7.72E+00	9.55E+08	9.18E-01	7.82E+06	1.24E-01	5.51E+04 6.76E+04	
397			i	3	57		8.04E+08		2.88E+00 2.88E+00	2.20E-05 1.96E-05	1.91E-04 9.01E-05	6.01E-05 4.95E-05	2.16E-04 9.95E-05	1.42E+05 2.63E+05	6.44E-06 0.00E+00	5.83E-01	5.00E+01	7.08E+00	6.95E+00	9.87E+06	9,06E-01	5.35E+06	7.36E-03	5.B3E+04	1.78E+04
398			ţ	3	90	0.00E+00	8.03E+06	1,01E+07	2.88E+00	1.90E-05	1.16E-05	5.63E-05	2.21E-05	1.74E+06	9.84E-06	2,75E-01 3,54E-02	2.34E+01 3.31E+00	8.15E+00 5.77E+00	6.03E+00 5.66E+00		9.08E-01 9.73E-01	4.01E+06 5.16E+06	1,15E-01 4,31E-02	5.26E+04 5.71E+04	
399 400	Down Down		1	3	9 76	0.00E+00 0.00E+00	7.99E+06 8.04E+06	1.14E+07 1.04E+07	2.88E+00 2.88E+00	1.75E-05 1.75E-05	1.02E-03	3.85E-05	1.17E-03	2.23E+04	8.83E-06	3.12E+00	2.56E+02	5.71E+00	5.61E+00	1.07E+07	8.55E-01	8.75E+06	3.33E-03	7.21E+04	1.72E+04
	Down		i	3	100	0.00E+00	8.00E+06	9.44E+06	2.88E+00	1.75E-05	2.16E-04 0.00E+00	3.78E-05 4.58E-05	2.18E-04 0.00E+00	1.14E+05 5.53E+21	8.59E-06 4.02E-06	6.59E-01 0.00E+00	4.89E+01 0.00E+00	5.56E+00	5.46E+00	9.77E+06	8.51E-01	6,43E+06	2.27E-06	6.24E+04	1.56E+04
	Down		1	3	1	0.00E+00	8.00E+06	9.21E+06	2.88E+00	1.82E-05	0.00E+00	4.97E-05	0.00E+00	5.46E+21	1.22E-06	0.00E+00	0.00E+00	5.53E+00 5.46E+00	5.42E+00 5.35E+00	9.13E+06 9.04E+06	9.37E-01 9.54E-01	7.19E+06 6.15E+06	8.52E-01 9.28E-01	6.49E+04 6.08E+04	5.75E+04 5.69E+04
	Down Down		1	3	65 70		7.63E+06 8.03E+06		2.88E+00 2.88E+00	1.63E-05	1.35E-03	3.47E-05	2.25E-03	1.27E+04	1.17E-05	4.13E+00	4.02E+02	5.09E+00	4.99E+00	9.13E+06	8.06E-01	9.14E+06	0.00E+00	7.20E+04	1.50E+04
405			i	3	'n		2.63E+05		1.10E+01	1.61E-05 4.94E-06	6.59E-05 2.62E-01	4.41E-05 1.13E-05	9.08E-05 3.68E+00	2.74E+05 1.11E+01	0.00E+00 1.80E-04	2.01E-01 8.00E+02	1.84E+01 4.60E+05	5.03E+00	4.93E+00	9.18E+08	9.37E-01	5.74E+06	2.77E-05	5.93E+04	1.69E+04
406			1	3	67	0.00E+00	6.02E+06	8.42E+06	2.88E+00	1.51E-05	1.35E-04	3.27E-05	1.57E-04	1.32E+05		4.13E-01	3.62E+01	5.08E+00 4.75E+00	4.84E+00 4.66E+00	4.54E+06 9.11E+06	8.30E-01 8.50E-01	9.94E+06 7.30E+06	3.75E-01 1.06E-01	7.53E+04	4.22E+04
407 408	Down-		1	3	95 20	0.00E+00 0.00E+00	8.04E+06 8.04E+06	1.02E+07 9.84E+06	2.88E+00	1.54E-05		2.87E-05		2.57E+05	9.91E-06	2.89E-01	1.84E+01	4.71E+00	4.62E+00	9.58E+06	8.49E-01	9.38E+06	1.54E-01	6.51E+04 7.33E+04	2.21E+04 2.47E+04
409			1	3	13		7.99E+06		2.88E+00 2.75E+00	1.56E-05 1.51E-05	5.54E-05 2.24E-07	2.94E-05 5.57E-05	5.55E-05 2.34E-07	3.57E+05 8.36E+07	9.50E-06 9.29E-06	1.69E-01 6.84E-04	1.32E+01	4.71E+00	4.61E+00	9.27E+08	8.61E-01	8.83E+06	3.22E-03	7.10E+04	1.64E+04
	Down-		1	3	84		8.04E+06	9.78E+06	2.88E+00	1.43E-05	5.49E-05	3.14E-05	5.64E-05	3.34E+05	9.41E-06	1.6BE-01	5.38E-02 1.35E+01	4.49E+00 4.52E+00	4.47E+00 4.44E+00	9.14E+06 9.15F+06	9.80E-01 8.38E-01	1.72E+06 4.83E+06	4.85E-01 1.94E-02	4,35E+04 5,54E+04	3.14E+04 1.65E+04
	Down-		1	3	19		8.01E+06 2.34F+05	9.52E+06 8.77E+06	2.88E+00 1.10E+01	1.44E-05 3.02E-06	4.76E-06 1.94E-01	2.92E-05 1.25E-05	4.76E-06	4.54E+06	1.07E-05	1.45E-02	9.75E-01	4.42E+00	4.33E+00	8.95E+06	8.55E-01	8.91E+06	1.24E-01		3.19E+04
413			i	3	55		6.00E+06	9.40E+06	2.88E+00	1.36E-05	5.98E-07	2.52E-05	2.49E+00 5.98E-07	1.14E+01 2.79E+07	1.51E-04 1.40E-05	5.93E+02 1.82E-03	3.61E+05 1.37E-01	4.13E+00 3.81E+00	4.10E+00 3.72E+00	3.41E+06 8.74E+06	5.07E-01 9.28E-01	8.19E+06	1.71E-01		2.95E+04
	Down-		1	3	50		7.99E+06	9.78E+06	2.88E+00	1.09E-05	2.81E-04	2.41E-05	3.09E-04	4.88E+04	5.26E-06	8.58E-01	7.18E+01	3.50E+00	3.44E+00	9.37E+06	8.79E-01	8.75E+06 6.60E+06	1.59E-01 1.23E-04	7.01E+04 6.27E+04	3.79E+04
,	Down-		1	3	29 32		8.03E+06 8.02E+06		2.88E+00 2.88E+00	1.04E-05 1.03E-05	1.16E-05 1.84E-05	2.73E-05 2.16E-05	1.19E-05 1.84E-05	1.18E+06 8.88E+05	9.55E-06 7.87E-06	3.53E-02	2.82E+00	3.31E+00	3.24E+00	6.92E+06	9.19E-01	4.99E+06	3.27E-01	5.58E+04	3.28E+04
417			1	3	66		8.00E+06	8.45E+06	2.88E+00	9.34E-06		2.11E-05	1.56E-04	8.17E+04	0.00E+00	5.60E-02 4.24E-01		3.17E+00 2.98E+00	3.11E+00 2.93E+00	9.19E+06	8.99E-01 B.94E-01	4.86E+06 7.96E+06	7.84E-02 1.79E-05	5.56E+04	2.38E+04
418			1	3 3	77 88				2.88E+00	9.04E-06	1.1BE-04	1.61E-05	1.37E-04	8.64E+04	1.04E-05	3.61E-01	3.15E+01	2.72E+00	2.67E+00	8.79E+06	8.19E-01	7.43E+06	8.27E-03	6,74E+04 6,51E+04	1.56E+04
420			1	3	64		8.02E+06 8.01E+06		2.88E+00 2.88E+00	7.88E-06 7.61E-06	5,18E-08 1.66E-06	1.64E-05 1.74E-05	5.16E-06 1.68E-06	2.04E+06 6.00E+06	0.00E+00 9.91E-06	1.57E-02 5.05E-03	1.20E+00	2.44E+00	2.39E+00	8.64E+06	8.76E-01	6.85E+06	1.79E-07	6.28E+04	1.83E+04
421	Down-		1	3	47	0.00E+00	8.03E+06	9.14E+06	2.88E+00	6.74E-06	6.59E-06	1.61E-05	1.05E-05	1.11E+06	8.72E-06	2.01E-02		2.40E+00 2.07E+00	2.36E+00 2.03E+00	8.54E+06 8.55E+06	8.63E-01 9.16E-01	5.87E+06 4.70E+06	6.06E-02 1.97E-01		2.72E+04
422 423	Down-		1	3	71		8.00E+06		2.88E+00 2.88F+00	6.45E-06	2.89E-05	1.80E-05		2.26E+05	8.90E-06	8.82E-02	8.68E+00	1.97E+00	1.93E+00	8.43E+06	9.45E-01	6.80E+06	4.65E-06	5.42E+04 6.23E+04	2.71E+04 1.59E+04
424			i	3	27		8.01E+06		2.88E+00	6.17E-06 4.86E-06	5.73E-08 1.63E-06	1.47E-05 9.69E-06	1.27E-07 1.63E-06	1.08E+08 4.39E+06	1.07E-05 8.89E-06	1.75E-04 4.97E-03	1.51E-02 3.43E-01	1.63E+00	1.59E+00	8.33E+06	9.93E-01	8.16E+06	7.16E-07	6.73E+04	3.27E+04
425			1	3	35		8.00E+06	8.98E+06	2.88E+00	5.19E-06	2.18E-07	9.11E-06	2.16E-07	3.19E+07	1.20E-05	6.58E-04	4.65E-02	1.50E+00 1.48E+00	1.47E+00 1.45E+00	8.49E+06 8.39E+06	8.81E-01 9.05E-01	7.62E+06 8.35E+06	5.07E-02 5.48E-01	6.55E+04 6.81E+04	1.87E+04 4.81E+04
426 427	Down-		1	3	24		7.99E+06 8.02E+06		2.88E+00 2.88E+00	4.47E-06 3.28E-06	5.29E-09 5.02E-07	5.12E-06		8.41E+08	1.78E-05	1.61E-05	1.32E-03	1.11E+00	1.08E+00	8.14E+06	9.10E-01	8.02E+06	9.07E-01	6.66E+04	6.05E+04
42B	Down-	dip	1	3	98		7.98E+06		2.88E+00	2.66E-06	1.92E-05	8.15E-06 6.59E-06	9.46E-07 4.54E-05	6.89E+06 1.40E+05	9.13E-06 3.83E-06	1.53E-03 5.87E-02	1.45E-01 5.87E+00	9.98E-01 8.20E-01	9.78E-01 8.04E-01	8.28E+06	9.21E-01	4.49E+06	3.02E-01		3.19E+04
	Down-		1	3	37	0.00E+00	2.27E+05	9.22E+06	1.10E+01	3,65E-07	1.49E-01	2.22E-06	4.75E+00	1.55E+00	1.32E-04	4.53E+02	3.43E+05	5.30E-01	5.04E-01	8.16E+06 3.34E+06	9.17E-01 4.36E-01	6.45E+06 8.74E+06	1,40E-05 1,60E-02	6.07E+04 7.00E+04	1.50E+04 8.44E+03
430	Down-		1	3	82 33		2.49E+05 2.32E+05	9.98E+06 7.15E+06	1.10E+01 1.10E+01	3.40E-07 2.34E-07	1.44E-01 2.32E-01	2.28E-06 1.21E-06	6.45E+00	1.38E+00	1.50E-04	4.41E+D2	3.59E+05	4.95E-01	4.73E-01	3.22E+06	5.99E-01	9.86E+06	1.17E-01	7.51E+04	1.78E+04
432	Down-	dip	i	3	94	3.22E+05	3.04E+05	1.12E+07	1.10E+01	3.14E-08	4.99E-01	1.21E-06 1.70E-07	5.30E+00 1.32E+01	6.63E-01 4.13E-02	1,04E-04 2,04E-04	7.08E+02 1.52E+03	4.94E+05 1.04E+06	3.27E-01 4.32E-02	3.27E-01 4.26E-02	3.08E+06 3.94E+06	3.19E-01 3.05E-01	8.88E+06	2.30E-01		2.78E+04
433 434	Down-		1	3	99	0.00E+00	2.75E+05	9.71E+08	1.10E+01	3.94E-09	9.84E-02	3.32E-08	7.14E+00	2.10E-02	7.23E-05	3.00E+02	3.01E+05	6.32E-03	4.26E-02 6.18E-03	3.94E+06 2.33E+06	3.05E-01 5.76E-01	1.12E+07 9.31E+06	2.23E-01 1.64E-01		2.84E+04 1.95E+04
434	Down-		1	3	56 58	_	2.72E+05 4.03E+05	8.64E+06 7.37E+06	1.10E+01 1.10E+01	5.80 E-1 0 5.17 E-1 0		3.89E-09 3.82E-09		2.28E-03			3.94E+05	8.97E-04	8.85Ë-04	2,51E+06	3.82E-01	B.30E+06	7.90E-06		
436	Down-	dip	1	3	49		3.91E+05	9,71E+06	1.10E+01	4,03E-10		2.52E-09	2.01E+01	6.79E-04 4.67E-04		1.38E+03 1.80E+03	1,16E+06 1,19E+06	7.89E-04 5.43E-04	7.48E-04 5.19E-04	4.06E+06 3.87E+06	1.70E-01 1.41E-01	1.32E+07	1.27E-01		1.21E+04
437 438	Down-		!	3	30 j	–	3.85E+05	9.39E+06	1.10E+01	5.45E-11		1.90E-10	1.37E+01	3.56E-05	1.48E-04	3.69E+03	1.79E+06	6.38E-05	6.30E-05	4.61E+06	9.02E-02	1.23E+07 1.05E+07	4.98E-02 5.31E-02		5.94E+03 4.76E+03
438	Down-		1	3	10		4.44E+05 9.36E+05	8.22E+06 9.36E+05	1.10E+01 1.10E+01	7.11E-12 4.35E-05	4.01E-01 7.19E-02	4.70E-11 1.07E-04		1.02E-05 5.57E+02		1.22E+03	1.04E+06	1.07E-05	1.02E-05	3.79E+06	2.12E-01	1.35E+07	1.81E-01	8.93E+04	1.66E+04
440	Down-	dip	1	3	78	4,58E+06	8.01E+06	8.01E+08	2.88E+00	8,35E-05		2.01E-04		2.44E+06	0.00E+00	2.19E+02 1.39E-01	8.81E+04 9.97E+00	4.91E+01 2.43E+01	4.68E+01 2.38E+01	6.40E+06 1.20E+07	7.33E-01 9.45E-01	8.89E+06 1.23E+07	9.35E-02 4.99E-01		3.11E+04
	Down-		1	3	44		8.00£+06		2.88E+00	8.30E-05	1.13E-05	1.15E-04	1.13E-05	9.99E+06	0.00E+00	3.44E-02	2.19E+00	2.18E+01	2.13E+01	1.09E+07	8.86E-01	1.23E+07	4.99E-01 2.37E-01		6.00E+04 4.40E+04
	Down-		1	3	69		8.94E+05 8.00E+06	8.94E+05 8.00E+06	1.10E+01 2.88E+00	1.66E-05 5.93E-05	9.01E-02 3.41E-06	3.66E-05 1.16E-04		1.41E+02 4.11E+07	0.00E+00 0.00E+00	2.75E+02	1.27E+05	1.79E+01	1.70E+01	5.63E+06	6.92E-01	8,66E+06	4.11E-01	6.96E+04	4.13E+04
444	Down-	dip	1	3	45	8.00E+06	8.00E+06	8.00E+08	2.88E+00			9.70E-05		4.17E+07 1.69E+22		1.04E-02 0.00E+00	4.16E-01 0.00E+00	1.68E+01 1.59E+01	1.65E+01 1.55E+01	1.11E+07 9.86E+06	9.18E-01 9.71E-01	1.11E+07	7.94E-01	8.03E+04	6.81E+04
445 446	Down-		!	3	52 31				2.88E+00	4.83E-05		1.18E-04	1.54E-05	4.10E+06	0.00E+00	4.69E-02	3.42E+00	1.40E+01	1,37E+01	1.06E+07	9.60E-01	9.99E+06 1.08E+07	9.68E-01 6.05E-01		7.34E+04 6.01E+04
	Down-		' 1	3	73		7.65E+06 8.02E+06			3.86E-05 3.68E-05		9.53E-05 8.78E-05		1.13E+04 1.90E+06		1.04E+01	1.05E+03	1.19E+01	1.16E+01	1.03E+07	8.58E-01	1.05E+07	1.15E-05		1.80E+04
44B	Down-	dip	1	3	5	0.00E+00	8.04E+06	8.07E+06	2.88E+00	3,44E-05		7.90E-05		1.90E+06				1.11E+01 1.10E+01	1.09E+01	1.03E+07 1.05E+07	9.38E-01 8.52E-01	1.04E+07 9.84E+06	5.54E-02 6.44E-05		2.21E+04
	Down-		1	3			8.04E+06			3.18E-05		1.04E-04	4.39E-05	1.27E+06	0.00E+00	8,46E-02	7.86E+00	9.99E+00	9.81E+00		9.64E-01	9.68E+06	6.44E-05 5.76E-03		1.77E+04 2.10E+04
1 450	Down-	пŧр	•	3	05	U.UUE+00	5.53E+06	5.53E+06	2.88E+00	2.47E-05	1.35E-02	6.96E-05	3.47E-02	1.80E+03	0.00E+00	4.10E+01	4.19E+03	7,52E+00	7.37E+00		7.44E-01	9.21E+06	0.00E+00		1.39E+04

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					Excepted																						
ļ	•	•	•	•	Waste Parasily	Finaldural Grau Saf Utacalos	Residual Brine Set (fraction)	Crushed Panel Helsty (m)	Up dip Avg	Up-dip Avg	Down-dip Avg Pressure (Ps)	Down-dip Avg	DRZ Porosity	DRZ Permeability	Sali Pillar Porosity	Soil Pilter Permenhille	Intrusion Time (Years)	Chin lent-	Wetl Productivity	BC well Sand	Total Area	Castle	Castile Passevoir	Up-dip Brine	Up-dāp Gas Rečitiva	Down-dp Bring Bolation	Down dip Gras
1					(fraction)		out. (anderso)	1 to Gut his	LIBSENG (L.S)	SAL (TACON)	LIBRACK® (INR)	SAL (Iraction)	(Fraction)	(m^2)	(Fraction)	(m/2)	(Years)	SIUI) IBUTO!	Index (1/Pa)	Parmeability (m/2)	Policis raleasect (m*2)	Reservoir Pressure (Pa)	Permeability	Permeabley	Permeability	Permenbally	Permeability
No.	Ю	Replic.	. Scen	Vector	POROSITY	SAT_ROAS	SAT_RBRN	HEIGHT	PRESPAN2	BSATPAN2	PRESPAN4	BSATPAN4	POROSITY	PERM X	POROSITY	PERM X	INTR TME	SKIN	WELL PI	PO14 04400			(m/c)	(fraction)	(haction)	(Irraction)	(fraction)
451	Down-dip	1	3	24	5 10E 01	9.01E-02		1.23E+00	8.77E+06	9.08E-01	8.87E+06	9.08E-01	1.90E-01	2.82E-13	2.20E-01	2.82E-13		-1.29E+00	1.23F-13	2 63E-14	9.94E-01	CAST RE	PRM CAST	KRW2	KRG2	KRW4	KRG4
	Down-dip	1	3	2 19	5.16E-01 5.20E-01	8.22E-02	4.02E-01 2.97E-02	1.24E+00 1.25E+00	9.09E+06	4.01E-01	9.14E+06	9.16E-01	1.66E-01	4.47E-14	1.83E-01	4.47E-14		-1.29E+00	1.24E-13	5.01E-14	9.94E-01	1.17E+07 1.35E+07	7.41E-13	6.59E-01 0.00E+00	3.00E-08 1.00E+00	6.59E-01 5.71E-01	2.97E-08
1	Down-dip	i	3	54	4.95E-01	1.42E-01 1.25E-01	2.97E-02 2.39E-02	1.25E+00 1.19E+00	9.37E+06 7.48E+06	1.36E-01 1.55E-06	9.40E+06	8.48E-01	2.01E-01	1.41E-15	2.17E-01	1.41E-15	1.40E+03	-1.23E+00	1.22E-13	2.00E-16	8.94E-01	1.25E+07	1.45E-12		7.36E-01	5.33E-01	2.71E-06
455	Down-dip	1	3	39	5.21E-01	1.50E-01	2.09E-02	1.26E+00	9.46E+06	4.17E-01	9.54E+06 9.57E+06	8.35E-01 8.47E-01	3.20E-02 1.54E-02	5.01E-18	5.36E-02 3.04E-02	2.57E-18	1.40E+03	-1.16E+00	1.13E-13	4.68E-12	7.76E-01	1.54E+07	1.86E-12	0.00E+00	1.00E+00	5.05E-01	1.71E-04
456	Down-dip	1	3	9	5.18E-01	1.35E-01	5.34E-01	1.25E+00	9.17E+06	1.55E-05	9.42E+06	7,97E-01	1.58E-02	3.02E-15 2.36F-19	3.04E-02 2.91F-02	9.02E-15 2.34E-19	1.40E+03 1.40E+03	-1.23E+00 -1.24E+00	1.23E-13	2.40E-13	8.82E-01	1.45E+07	1.78E-13	1.45E-03	5.68E-01	4.03E-01	4.66E-07
457	Down-dip	1	3	95	5.27E-01	1.46E-01	3.69E-01	1.27E+00	9.87E+06	1.36E-01	9.99E+06	8.43E-01	1.56E-01	6.03E-17	1.72E-01	6.03E-17	1.40E+03	-9.54E-01	1.22E-13 1.12E-13	2.63E-15 1.10E-16	9.00E-01 5.13E-01	1.43E+07	4.90E-11	0.00E+00	1.D0E+00	1.22E-01	1.33E-02
	Down-dip	!	3	28	5.15E-01	9.72E-02		1.24E+00	8.98E+06	2.12E-01	9.21E+06	8.92E-01	2.15E-01	5.28E-17	2.38E-01	4.79E-17	1.40E+03	-1.08E+00	1.14E-13	9.55E-12	6.64E-01	1.32E+07 1.45E+07	1,70E-11 9.55E-14	0.00E+00 7.22E-06	1.00E+00 9.05E-01	3.46E-01	2.07E-05
	Down-dip	1	3	23 34	5.14E-01 5.13E-01	7.29E-02 2.76E-02	4.80E-01 3.26E-01	1.24E+00 1.23E+00	8.91E+06	2.28E-02	9.20E+06	9.23E-01	3,26E-02	1.18E-16	4.93E-02	1.18E-18	1.40E+03	-1.18E+00	1.19E-13	7.94E-17	8.09E-01	1.52E+07	6.03E-13	0.00E+00	1.00E+00	5.94E-01 5.51E-01	5.83E-06 1.85E-06
1	Down-dip	i	3	77	4.99F-01	1.48E-01	3.26E-01 6.84E-02	1.23E+00 1.20E+00	6,96E+06 B,09E+06	3.87E-04 2.66E-03	8.98E+06 8.51E+06	9.34E-01 7.33E-01	1.98E-02	2.30E-17	3.26E-02	2.29E-17	1.40E+03	-1.07E+00	1.13E-13	7.08E-14	6.47E-01	1.35E+07	4.68E-14	0.00E+00	1.00E+00	6.84E-01	3.48E-04
	Down-dip	ì	š	72	5.02E-01	2.36E 02	4 74F-03	1.21F+00	B.14E+06	5.07E-06	8.99E+06	7.33E-01 9.22E-01	2.04E-01 6.13E-02	8.13E-19 4.62E-18	2.30E-01 8.49E-02	8.13E-19	1.40E+03	-7.13E-01	9.69E-14	2.75E-16	3.17E-01	1.24E+07	1.20E-11	0.00E+00	1.00E+00	2.88E-01	5.56E-03
463	Down-one	1	3	43	4.76E-01	5.88E-02	2.07E-01	1.15E+00	6.43E+06	3.82E-03	8.99E+06	8.96E-01	1.67E-01	2.87E-19	2.05F-01	1.82E-18 9.77F-20	1.40E+03 1.40E+03	-6.26E-01 -1,26E+00	9.47E-14 1.14E-13	5.37E-12 3.63E-13	2.66E-01	1.42E+07	5.75E-13	0.00E+00	1.00E+00	7.39E-01	2.98E-04
464	Down-dip	1	9	20	5.15E-01	1.23€-01	1.27E-01	1.24E+00	9,01E+06	1.14E-03	9.09E+06	8.13E-01	1.98E-02	1.35E-17	3.76E-02	1.35E-17	1.40E+03	-6.04E-01	9.64E-14	3.83E-13	9.52E-01 2.55E-01	1.51E+07 1.29E+07	9.55E-12 1.20E-12	0.00E+00	1.00E+00	5.96E-01	3.81E-04
465	Down-dip	1	3	48	5.01E-01	1.02E-01	2.11E-01	1.20E+00	B.26E+06	2.02E-01	8.29E+06	8.19E-01	4.68E-02	7.76E-14	6.37E-02	7.76E-14	1.40E+03	-1.29E+00	1.21E-13	2.19E-15	1.01E+00	1.10E+07	3.80E-12	0.00E+00 0.00E+00	1.00E+00 1.00E+00	4.11E-01 3.83E-01	1.03E-03
,,,,	Down-dip		3	16 67	4.85E-01 4.97E-01	5.75E-02 1.21E-01	2.76E-01 6.61E-02	1.17E+00	7.16E+06	4.78E-05	8.31E+06	8.51E-01	1.01E-01	2.24E-19	1.33E-01	2.14E-19	1.40E+03	-1.29E+00	1.17E-13	1.91E-14	1.01E+00	1.53E+07	1.866-12		1.00E+00	4.28E-01	2.42E-03 4.14E-03
1 /**	Down-dip	i	3	41	4.90E-01	3.40E-02	8.64F-02	1.20E+00 1.18E+00	7.98E+06 7.44E+06	9.42E-02 6.95E-02	8.42E+06 8.60E+06	7.84E-01 9.01E-01	1.71E-01 1.44E-01	3.55E-18	1.94E-01	3.55E-18	1.40E+03	-1.27E+00	1.19E-13	7.24E-15	9,65E-01	1.27E+07	1.15E-14	2.41E-06	9.29E-01	3.78E-01	2.65E-03
469	Down-dio	1	3	97	5.07E-01	8.37E-02	4.34E-01	1.22E+00	8.54E+06	5.30E-01	8.70F+06	9.12E-01	1.48E-01	1.70E-19 5.63E-16	1.65E-01 1.73E-01	1.70E-19 5.62E-16	1.40E+03	-1.22E+00	1.15E-13	3.24E-16	8.54E-01	1.48E+07	3.47E-12	0.00E+00	1.00E+00	6.53E-01	6.82E-04
	Down-dip	1	3	76	4.83E-01	1.38E-01	3.34E-01	1.16E+00	7.09E+06	1.55E-06	8.13E+06		3.35E-02	3.16E-18	5.57E-02	3.16F-18	1.40E+03 1.40E+03	-8.88E-01 -1.33E+00	1.05E-13 1.19E-13	4.57E-13	4.49E-01	1.43E+07	3.02E-11	1,40E-03	8.02E-01	5.37E-01	1.00E-06
	Down-dip	1	3	60	5.00E-01	6.13E-02	4.70E-02	1.20E+00	8.16E+06	1.24E-01	8.51E+06	9.10E-01	1.95E-01	6.10E-18	2.14E-01	5.75E-18	1.40E+03	-1.17E+00	1.19E-13 1.15E-13	5.50E-16 6.61E-13	1.09E+00 7.91E-01	1.34E+07 1.33E+07	2.09E-12 2.34E-14	0.D0E+00 9.07E-05	1.00E+00 8.23E-01	2.70E-01	2.56E-03
	Down-dip Down-dip	1	3	66 80	4.97E-01	9.43E-02 6.43E-02	5.49E-01	1.19E+00	8.05E+06	1,64E-05	8.18E+06	8.73E-01	8.51E-02	B.23E-18	1,11E-01	5.37E-18		-1.37E+00	1.24E-13	1.66E-12	1.18E+00	1.26E+07	1.48E-14	9.07E-05 0.00E+00	8.23E-01 1.00E+00	6.94E-01	5.51E-05
	Down-dip	i	3	50	4.75E-01 4.84E-01	1.09E-01	2.68E-01 5.44E-01	1.14E+00 1.17E+00	6.49E+06 7.22E+06	1.96E-04 1.15E-04	8.40E+06	9.11E-01	4.04E-02	1.69E-18	6.35E-02	5.01E-19	1.40E+03	-8.21E-01		2.09E-12	3.93E-01	1.41E+07	2.04E-13	0.00E+00	1.00E+00	6.20E-01	8.46E-05
	Down-dip	i	ä	94	5,45E-01	4.58E-03	1.85E-01	1.32E+00		2.32F-01	8.05E+06 1.12E+07	8.69E-01 3.34E-01	2.14E-01 2.04E-01	6.31E-15	2.43E-01 2.11E-01	2.88E-19 6.31F-15		-1.27E+00	1.16E-13	1.12E-12	9.68E-01	1.30E+07	2.75E-13	0.00E+00	1.00E+00	2.B7E-01	4.07E-04
	Down-dip	1	3	15	5.20E-01	4.22E-02	5.21E-01	1.25E+00	9.39E+06	4.85E-01	9.39E+06		5.41E-02	1.32E-14	7.03E-02	0.31E-15 1.32E-14	1.40E+03 1.40F+03	-1,29E+00 -9,48E-01	1.32E-13 1.10E-13	9.77E-16 1.32E-14	9.95E-01	1.44E+07	1.78E-12	2.56E-05	8.81E-01	1.85E-03	6.30E-01
	Down-dip	1	9	37	5.13E-01	4.07E-02	2.28E-01		8.97E+06	B.98E-03	8.97E+06	3.60E-01	1.14E-01	3.98E-16	1.25E-01	3.98E-16	1.40E+03	-1.19E+00	1.10E-13	1.32E-19 1.35E-15	5.06E-01 8.19E-01	1.15E+07 1.22E+07	4.47E-13 6.17E-12	0.00E+00	1.00E+00	1.89E-03	5.97E-01
1 ",	Down-dip Down-dip	!	3	99 58	5.24E-01 5.72E-01	1.28E-01 2.96F-02	5,15E-01	1.26E+00	9.67E+06	1.51E-01			1.72E-01	5,89E-17	1.90E-01	5.89E-17	1.40E+03	7.63E-01	1.04E-13	6.17E-17	3.50E-01	1.27E+07	2.296-11	0.00E+00	1.00E+00 1.00E+00	1.47E-03 2.97E-08	6.35E-01
	Down-dip	;	3	78	5.72E-01 5.89E-01	4.93E-02	1.14E-01 1.51E-01	1.40E+00 1.46E+00	1.36E+07 1.51E+07	1.01E-01 1.13E-01	1.35E+07		2.11E-01	4.63E-16	2.06E-01	1.45E-16		-1.18E+00	1.35E-13	3.09E-15	8.11E-01	1.32E+07	1.07E-13	0.00E+00	1.00E+00	1.33E-08	9.85E-01
	Down-dip	i	š	16	5.66E-01	1.06E-01	3.40E-01	1.39E+00		1.82F-01	1.51E+07 1.30E+07		2.22E-01 6.20E-02	3.45E-11 3.31E-14	1.03E-01 6.51E-02	2.46E-15 3.31E-14			1.34E-13	8.32E-17	6.28E-01	1.48E+07	1.07E-12	0.00E+00	1.00E+00	3.55E-01	1.23E-02
	Down-dip	1	3	94	5,45E-01	4.58E-03	1.85E-01	1.32E+00	1.12E+07	1.92E-01			2.04E-01	6.31F-15	2.11E-01				1.28E-13 1.32F-13	6.17E-16	6.69E-01	1 12E+07	5.25E-12	0.00E+00	1.00E+00	1 76E-01	2.60E-02
1	Down-dip	ŧ	3	10	5.60E-01	3,17E-02	1.73E-01	1.36E+00	1.25E+07	4.31E-03	1.25E+07	6.87E-01	5.91E-02	3.72E-14	6.49E-02	3.72E-14		• •	1,39E-13	9.77E-16 1.86E-16	9.95E-01 1.08E+00	1.44E+07 1.18E+07	1.78E-12 1.35E-11	1.55E-08 0.00F+00	9.84E-01 1.00F+00	2.61E-01	4.13E-02
	Down-dip Down-dip	1	3	19	5.55E-01	1.426-01	2.97E-02	1.35E+00		5.54E-02		6.10E-01	1.98E-01	1.41E-15	2.01E-01	1.41E-15			1.32E-13	2.00E-16	8.94E-01	1.25E+07		1.51E-06	9.36E-01	1.73E-01 1.50E-01	6.55E-02 4.05E-02
1	Down-dia	ì	3	73	5.61E-01 5.57E-01	1.12E-01 5.61E-02	1.61E-02 3.03E-01	1.37E+00 1.36E+00		2.55E-05 8.40E-06		B.87E-01	1.45E-01	4.82E-13	1.25E-01	1.1BE-13	_		1.31E-13	3.80E-15	7.83E-01	1.38E+07		0.00E+00	1.00E+00	6.39E-01	2.45E-10
	Down-dip	1	3	48	5.52E-01	1.02E-01				6.44E-02			9.62E-02 5.68E-02	3.72E-16 7.77E-14	1.04E-01 5.72E-02	3.72E-16 7.76E-14			1.13E-13	6.17E-15	3.77E-01	1.37E+07		0.00E+00	1.00E+00	1.59E-01	5.81E-02
	Down-dip	1	3	45	5.41E-01		2.04E-01	1.31E+00		9.49E-01			7.86E-02	5.13E-14	8.70E-02	5.13E-14			1.35E-13 1.14E-13	2.19E-15 1.74E-15	1.01E+00			0.00E+00	1.00E+00	5.67E-01	5.58E-06
	Down-dip	1	3	69	5.44E-01	8.98E-02	.,	1.32E+00		9.09E-01			7.90E-02	1.26E-14	8.73E-02				1.32E-13		4.89E-01 9.99E-01	1.36E+07 1.47E+07	4.57E-13 4.07E-13	7.81E-01 5.40E-01	4.05E-09 1.85E-08	7.81E-01 5.40E-01	4.02E-09 1.83E-08
	Down-dip Down-dip	1	3	27	5.12E-01 5.28E-01	1.18E-01 9.01E-02	4.62E-01 1.37E-01		9.01E+06	1.12E-03			2.96E-02	1,86E-16	4.33E-02	1.86E-16	3.00E+03	-1.24E+00	1.21E-13	2.40E-15	9.09E-01	1.20E+07	1.26E-12	0.00E+00	1.00E+00	1.40E-01	2.33F-02
	Down-dip	í	3	46	5.33E-01	2.036-02	2.35E-01		9,74E+08 1,03E+07	9.08E-01 2.68E-06		9.08E-01 8.46E-01	1.85E-01 4.85E-02	2.82E-13 1.59E-17	2.13E-01 6.20F-02	2.82E-13			1.27E-13	2.63E-14	9.94E-01	1 17E+07	7.41E-13	6.59E-01	3.36E-08	6.59E-01	2.89E-08
	Down-dip	1	3	90	4.97E-01	1.28E-02	2.86E-01			2.68E-06			1.69E-02	1.20E-17	3.77E-02	1.59E-17 1.20E-17			1.36E-13 1.01E-13	1.45E-14 2.09E-14	1.26E+00 4.15F-01	1.51E+07	1.15E-11	0.00E+00	1.00E+00	4.35E-01	9.26E-03
	Down-dlp	1	3	23	5.33E-01	7.29E-02	4.80E-01	1.29E+00		5.36E-07	1.04E+07	8.49E-01	3.64E-02	1.18E-16	4.73E-02	1.18E-16			1.01E-13	2.09E-14 7.94E-17	9.15E-01 8.09E-01	1.31E+07 1.52E+07		0.00E+00 0.00E+00	1.00E+00 1.00E+00	9.59E-02	1.37E-01
	Down-dip Down-dip	!	3	31	5.19E-01 5.16E-01	3.40E-02 5.28E-02	8.64E-02			3.B9E-02		5.17E-01	1.44E-01	1.70E-19	1.56E-01			-1.22E+00	1,21E-13	3.24E-16	8.64E-01	1.48E+07		0.00E+00	1.00E+00	2.82E-01 6.22E-02	8.46E-03 1.83E-01
100	Down-dip	;	3	60	5.02E-01	6.13E-02	5,93E-02 4,70E-02			8.35E-06 7.72E-02			7.37E-02	1.66E-15	9.41E-02				1.24E-13	3.31E-14	9.73E-01	1.48E+07		0.00E+00	1.00E+00	7.02E-01	8.80E-05
,	Down-dip	i	š	67	5.32E-01	1.21E-01		,,_,,		2.60E-02		7.84E-01 4.40E-01	1.97E-01 1.70E-01	6.05E-18 3.55E-18	2.13E-01 1.81E-01	5.75E-18 3.55E-18			1.15E-13	6.61E-13	7.91E-01	1.32E+07	2.34E-14	2.90E-06	9.31E-01	3.88E-01	8.24E-03
	Down-dip	1	3	52	5.07E-01	3.68E-02	4.49E-01	1.22E+00		B.01E-01		9.60E-01	1.09E-01	1.70E-15	1.81E-01				1.28E-13 1.07E-13	7.24E-15	9.65E-01	1.27E+07		0.00E+00	1.00E+00	3.42E-02	2.13E-01
	Down-dip	1	3	20	5.20E-01	1.23E-01			9,39E+06	1.19E-07	9.41E+06	4.67E-01	2.07E-02	1,35E-17	3.71E-02	1.35E-17			9.76E-14	4.17E-14 3.31E-15	6.07E-01 2.55E-01	1.51E+07 1.29E+07	2.63E-13 1.20E-12	1.90E-01 0.00E+00	4.75E-02 1.00E+00	7.56E-01 3.08E-02	5.28E-07
	Down-dip Down-diio	:	3	47 53	5.04E-01	6.75E-02				9.84E-02			1.48E-01	6.92E-18	1.62E-01			-1.09E+00	1.12E-13	2.19E-16	6.75E-01	1.21E+07		0.00E+00	1.00E+00	2 80E-02	2.21E-01 2.67E-01
	Jown-dip	i	3	100	5.06E-01	4.46E-02 1.14E-01	2.52E-01 3.43E-01	1.20E+00 1.22E+00		2.28E-01 8.83E-01			1.56E-01 6.93E-02	9.13E-18	1.83E-01				1.18E-13	1.38E-12	8.92E-01	1.34E+07		0.00E+00	1.00E+00	4.98E-01	2.77E-03
	Down-dip	1	š	2	4.98E-01	8.22E-02			8.28E+06	1.51E-01		9.16E-01		9.12E-16 4.47E-14	8,94E-02 1,90E-01				1.20E-13	2.51E-14	9.43E-01	1.28E+07	1.29E-13	4,86E-01	1.66E-07	4.86E-01	1.61E-07
505	Down-dip	1	3	65	5.30E-01	1.27E-01	8.96E-02	1.28E+00		5.96E-08			- · · -	8.71E-16	3.07E-02				1.20E-13 1.21E-13	5.01E-14 4.17E-15	9.98E-01 7.73E-01			0.00E+00	1.00E+00	5.70E-01	1.37E-07
	Down-dip	1	3	71	5.14E-01	1.57E-02			9.03E+08	1.37E-08			4.42E-02	2.19E-18	6.54E-02				1.28E-13	5.25E-17	7.73E-01 1.18E+00			0.00E+00 0.00E+00	1.00E+00 1.00E+00	9.36E-03 1.04F-02	3.B3E 01 4.33E-01
	Down-dip Down-dip	;	3	95	5.59E-01 5.01E-01	1.46E-01 3.56E-02		1.36E+00 1.20E+00		4.87E-02			_	8.03E-17	1.60E-01			·9.54E·01	1.20E-13	1.10E-18	5.13E-01	1.32E+07		0.00E+00	1.00E+00	5.39E-03	4.33E-01 4.01E-01
~~~	Jown-dip	í	3	97	4.94E-01	8.37E-02				5.13E-08 3.35E-01		2.96E-01 9.12E-01		4.19E-19 5.63E-16	8.57E-02				1.18E-13	4.79E-15	8.82E-01	1.17E+07	3.98E-14	0.00E+00	1.00E+00	6.82E-03	4.78E-01
	Down-dlp	ŧ	3	77	5.30E-01	1.48E-01				8.08E-05			2.01E-01	5.636-16 8.13E-19	1.77E-01 2.16E-01				1,02E-13	4.57E-13	4.49E-01			0.00E+00	1.00E+00	5.36E-01	1.11E-06
511	Down-dip	ŧ	3	15	5.46E-01	4.22E-02		1.32E+00		2.22E-01				1.32E-14	6.66E-02		0.000.00		1.03E-13 1.16E-13	2.75E-16 1.32E-14	3.17E-01 5.06E-01	1.24E+07 1.15E+07		0.00E+00	1.00E+00	4.95E-03	4.54E-01
	Down-dip	1	3	11	4.91E-01	9.81E-02				8.99E-01			6.77E-02	7.24E-16	9.32E-02	7.24E-16			1.17E-13	1.66E-14	5.06E-01 9.73E-01		4.47E-13 7.08E-14	0.00E+00 5.84E-01	1.00E+00 1.42E-07	1.32E-03 5.84E-01	6.32E-01
	Down-dip Down-dip	1	3	16	5.10E-01 5.07E-01	5.75E-02 4.63E-02								2.22E-19	1.27E-01		3.00E+03	1.29E+00	1.23E-13	1.91E-14	1.01E+00	1.53E+07		0.00E+00	1.00E+00	3.71E-04	1.38E-07 7.37E-01
	Jown-dip	i	3	76	5.07E-01 5.15E-01				8.77E+06 9.08E+06	1,89E-05 4,17E-07				6.17E-20	2.39E-01				1.22E-13		9.91E-01		5.50E-14	0.00E+00	1.00E+00	4.43E-06	9.21E-01
	Down-dip	1	š	78	5.91E-01	4.93E-02				3.42E-02				3.16E-18 7.83E-11					1.26E-13	5.50E-16				0.00E+00	1.00E+00	2.84E-07	9.57E-01
517	Down-dip	1	3	10	5,78E-01	3.17E-02		1.42E+00		2.38E-07		_,,,,		4.36E-14					1.34E-13 1.45E-13	8.32E-17 1.86E-16	5.28E-01			0.00E+00	1.00E+00	1.59E-01	6.61E-02
	Down-dip	1	3	18	5,89E-01		3.40E-01	1.46E+00		8.62E-02	1.50E+07			1.49E-13					1.45E-13 1.35E-13	1.86E-16 6.17E-16	1.08E+00 6.69F-01			0.00E+00 0.00E+00	1.00E+00 1.00F+00	1.36E-01	8 86E 02
	Down-dip Down-dip	1	3	45	5.53E-01 5.70E-01	5.05E-02 1.42E-01				9,49E-01				5.13E-14		5.13E-14	5.00E+03	-9.31E-01	1.17E-13		4.89E-01			0.00E+00 7.81E+01	1.00E+00 3.78E-09	7.11E-02 7.81E-01	1.05E-01 3.75E-09
	Jown-dip	1	3	48	5.62E-01				1.33E+07 1.26E+07	1.61E-02 4.05F-06				3,47E-15	1.95E-01			1,23E+00	1.37E-13	2.00E-16	8.94E-01	1.25E+07		0.00E+00	1.00E+00	1.02E-01	7.37E-02
	Jown-dip	i	3	46	5.26E-01					-,,,,,,			6.22E-02 4.72E-02	1,30E-13 1,59E-17	5.59E-02 6.29E-02				1.38E-13				3.80E-12	0.00E+00	1.00E+00		3.13E-04
	Down-dip	1	š	44	5.45E-01									1.59E-17 1.19E-13	6.29E-02 1.30E-01				1.34E-13 1.26E-13	1.45E-14 3.80E-15				0.00E+00	1.00E+00	1.57E-01	7.69E-02
	Down-dip	1	3	94	5.46E-01	4.58E-03													1.26E-13 1.32E-13	0.002 10	7.83E-01 9.95E-01	1.38E+07 1.44E+07		0.00E+00		6.38E-01	6.27E-10
525	Jown-dip	1	3	69	5.40E-01	8.98€-02	4.08E-01	1.31E+00	1.09E+07	9.09E-01	1.10E+07	9.09E-01	7.B3E-02	1.26E-14			5.00E+03 -		1.31E-13		0.00L 0 I			0.00E+00 5.40E-01		9.71E-01 5.40E-01	1.87E-08
																								2.406*01	2.010700	5.40E-01	1.000-08

		-

					Up-dip Flowing	Down-dip	BC well	Blowout					Produced	Cum Brine						Avg Srine		Avo Britis	lotsi	
	•	•	•	•	Battom-hole Pressure (Pn)	Patters by to	Injection	Ouration	Brine Rate (m/9/a)	Gas Rate (ref	Max Brine Rate (mr/3/a)	Max Gas Rate (ref m/G/s)	Uquid/Gas	from Boundary Condition Well	Gas Rale (mac//day)	Cum Gas Produced (rei	Cum Brine Produced	Cum Brine Releases	Avg Brine Pressure	Seturation Panel 5	Avg Brine Pressure	Saturation Panel 0	Exceveted Waste Pore	Total Expansional
	íD	٠. ١	_		1 '	Pressure (Pa)	Pressure (Pa)	(Oays)		41.4	ran jiii say	her in Orth	ref m^3/s)	(m/3)	(mact/day)	m^3)	(m*3)	(m/3)	Panel 5 (Pa) after Blowoul	(Irection) elter	Panel 0 (Pa)	(kaction) after	Vokene .	Brire Volume
451	Down-dip	Hapte	Scen.	Vector 24	7.99E+06	7.99E+06	7.99E+06	time 2.88E+00	2.74E-05	GASFLW 1 42F-07		MAX GAS	LGR_MET	BRINE_BC			BRINEOUT	BRIN_REL	BRNPRESS	SATBRINS	9ANPRESO	blowaut SATBRNO	(fraction) WASTE PV	fot Bain.
	Down-dip	1	3	2	0.D0E+00	7.99E+06		2.88E+00	2.74E-05 2.53E-05	1.42E-07 1.84E-06	3.39E-05 3.87E-05	1.42E-07 1.84E-06	2.37E+08 1.82E+07	0.00E+00 0.00E+00	4.32E-04 5.61E-03	2.98E-02 3.72E-01	7.06E+00 6.78E+00	6.89E+00	B.B3E+06	9.10E-01	8.75E+06	B.45E-01	7.03E+04	
453 454	Down-dip		3	19	2.61E+05	8.02E+06		2,88E+00	2.11E-05	2.03E-05	4.30E-05	2.03E-05	1.56E+06		6.20E-03	4.15E+00		6.62E+00 6.34E+00	9.09E+06 9.36E+06	9.18E-01 8.51E-01	9.09E+06 9.37E+06	2.96E-01		4 32E+04
	Down-dip Down-dip	1	3	54 39	0.00E+00 2.46E+05	8.00E+06 8.01E+06	8.08E+06 8.01E+06	2.88E+00 2.88E+00	1.98E-05	2.85E-04	4.20E-05	3.22E-04	B.20E+04	0.00E+00	8.68E-01	7.55E+01		6.07E+00	9.48E+06	8.39E-01	7.48E+06	1.12E-01 1.55E-06	7.30E+04 6.61E+04	3.16E+04 1.87E+04
1	Down-dip	1	3	9	0.00E+00	2.22E+06	V.V.C.100	2.88E+00	1.94E-05	3.01E-05 3.12E-02	3.69E-05 5.11E-05	3.01E-05 1.16E-01	1.16E+06 5.92E+02	0.00E+00 0.00E+00	9.17E-02	5.10E+00	5.87E+00	5.75E+00	9.53E+06	8.50E-01	9.45E+06	2.54E-01	7.35E+04	3.99E+04
457	Down-dip	1	3	95	0.00E+00	8.04E+06	8.04E+06	2.88E+00	1.89E-05	2.08E-04	3.60E-05	2.08E-04	1.41E+05	0.00E+00	9.51E+01 6.35E-01	9.91E+03 4.15E+01	5.86E+00 5.83E+00	5.75E+00 5.71E+00	8.70E+06 9.94E+06	8.02E-01 8.46E-01	9.17E+06	1.55E-05		1.62E+04
458 459	Down-dip	1	3	28 23	2.90E+05 0.00E+00	8.03E+06 8.02E+06	U. FOL IDO	2.88E+00 2.88E+00	1.72E-05 1.54E-05	1.55E-05	3.83E-05	1.55E-05	1,48E+06	0.00E+00	4.74E-02	3.60E+00	5.34E+00	5.23E+00	9.15E+06	8.94E-01	9.87E+06 8.98E+D6	1.36E-01 2.16E-01		2.43E+04 2.81E+04
460	Down-dip	1	3	34		7.97E+06		2.88E+00	1.46E-05	1.11E-05 1.84E-04	3.69E-05 3.74E-05	1.11E-05 3.76E-04	1.97E+06 8.24E+04	0.00E+00 0.00E+00	3.38E-02 5.61E-01	2.43E+00	4.78E+00	4.69E+00	9.13E+06	9.24E-01	8.91E+06	2.29E-02	7.12E+04	2.39E+04
461	Down-dip Down-dio	1	3 3	77	0.00E+00	6.18E+06	6.1BE+06	2.88E+00	1.46E-05	5,44E-03	3.10E-05	1.12E-02	2.69E+03	0.00E+00	1.66E+01	5.45E+01 1.66E+03	4.49E+00 4.46E+00	4.40E+00 4.37E+00	8.89E+06 8.39E+06	9.35E-01 7.40E-01	8.96E+06 8.09E+06	3.94E-04 2.65E-03	7.11E+04 6.72E+04	
463	Down-dla	1	3	72 43	0.00E+00	7.99E+06 7.95E+06	8.05E+06 7.96E+06	2.88E+00 2.88E+00	1.46E-05 1.35E-05	1,39E-04 2,32E-04	3.34E-05 3.36E-05	2.66E-04	1.09E+05	0.00E+00	4.25E-01	4.07E+01	4.43E+00	4.34E+00	8.91E+06	9.23E-01	8.14E+08	5.09E-08	6.80E+04	
464	Down-dlp	1	3	20	0.00E+00	7.71E+06	7.71E+06	2.88E+00	1.37E-05	8.87E-04	2.61E-05	4.24E-04 1.30E-03	6.19E+04 1.64E+04	0.00E+00 0.00E+00	7.09E-01 2.71E+00	8,88E+01 2.54E+02	4.25E+00 4.16E+00	4.17E+00 4.08E+00	8.92E+06	8.98E-01	6.43E+06	3.82E-03	6.12E+04	
465 466	Down-dip Down-dip	1	3	48 16		7.29E+06		2.88E+00	1.46€-05	1.26E-03	2.21E-05	2.\$6E-03	9.75E+03		3.85E+00	3.92E+02		3.74E+00	9.05E+06 8.25E+06	8.18E-01 8.24E-01	9,01E+06 8,26E+06	1.15E-03 1.30E-01	7.14E+04 6.76E+04	1.55E+04 3.18E+04
467	Down-dip	j	3	57		6.97E+06 7.22E+06		2.88E+00 2.88E+00	1.21E-05 1.13E-05	2.24E-03 1.64E-03	3.19E-05 2.58E-05	5.66E-03 3.36E-03	5.42E+03	0.00E+00	6,84E+00	6.99E+02		3.71E+00	8,20E+06	8.55E-01	7.16E+06	4.78E-05	6.34E+04	1.83E+04
468	Down-dip	1	3	41	0.00E+00	7.89E+06	7.89E+06	2.88E+00	1.01E-05	2.28E-04	2.52E-05	4.99E-04	7.03E+03 4.57E+04	0.00E+00 0.00E+00	5.02E+00 6.94E-01	5.08E+02 6.92E+01	3.57E+00 3.16E+00	3.50E+00 3.10E+00	8.37E+06 8.55E+06	7.89E-01 9.03E-01	7.98E+06	9.07E-02	6.67E+04	
469 470	Down-dip	1	3	97 76	2.29E+05 0.00€+00	0.01E+06 6.98E+06	8.02E+06	2.88E+00	8.77E-06	1.98E-06	1.84E-05	1.98E-06	6.08E+06	0.00E+00	5.05E-03	4.37E-01	2.65E+00	2.60E+00	8.66E+06	9.03E-01 9.14E-01	7.44E+06 8.54E+06	6.95E-02 3.83E-01	6.48E+04 6.92E+04	
471	Down-dip	i	3	60	2.48E+05	6.98E+06	8.98E+06 8.04E+06	2.88E+00 2.88E+00	7.60E-06 7.67E-06	1.48E-03 1.49E-05	1.75E-05 1.84E-05	2.99E-03 2.75E-05	5.29E+03 5.47E+05		4.50E+00	4.57E+02	2.42E+00	2.37E+00	8.08E+06	8.06E-01	7.09E+06	1.55 <b>E-08</b>	6.29E+04	
	Down-dip	1	3	66	0.00E+00	7.51E+08	7.53E+06	2.88E+00	4.98E-06	4.48E-04	1.17E-05	8.67E-04	5.4/E+05 1.16E+04	0.00E+00	4.63E-02 1.37E+00	4.36E+00 1.37E+02	2.38E+00 1.59E+00	2.34E+00 1.58E+00	8.48E+06 8.15E+08	9.12E-01 8.77E-01	8.18E+08 8.05E+08	1,15E-01	6.75E+04	2.72E+04
473 474	Down-dip Down-dip	1	3	80 50		8.02E+06 7.83E+06	8.05E+06 7.84E+06	2.88E+00	4.84E-06	1.52E-05	1.06E-05	2.89E-05	3.34E+05	0.00E+00	4.65E-02	4.43E+00	1.48E+00	1.45E+00	8.38E+06	9.13E-01	8.05E+08 8.49E+06	1.84E-05 1.97E-04	6.66E+04 6.09E+04	
	Down-dlp	i	3	94		7.83E+06 2.82E+05	7.84E+06 2.82E+05	2.88E+00 1.10E+01	1.73E-06 2.43E-07	5.12E-05 4.41E-01	3.44E-06 1.28E-06	8.68E-05 1.06E+01	3.55E+04 3.69E-01	0.00E+00 0.00E+00	1.56E-01 1.35E+03	1.52E+01	5.39E-01	5.29E-01	8.04E+06	8.73E-01	7.22E+06	1.15E-04	6.33E+04	1.55E+04
	Down-dip	1	3	15	0.00E+00	2.44E+05	2.44E+05	1.10E+01	2.60E-07	1.46E-01	9.06E-07	5.89E+00	8.20E-01	0.00E+00	1,35E+03 4,46E+02	9.05E+05 3.41E+05	3.34E-01 2.79E-01	3.15E-01 2.77E-01	4.08E+06 2.76E+06	3.52E-01 6.22E-01	1.12E+07	2.16E-01	8.06E+04 7.31E+04	
	Down-dip Down-dip	1	3	37 99	0.00E+00 0.00E+00	2.38E+05	2.38E+05 3.44E+05	1.10E+01 1.10E+01	1.09E-07	1.62E-01	7.26E-07	6.19E+00	4.05E-01	0.00E+00	4.94E+02	4.05E+05	1.64E-01	1.59E-01	3.07E+06	3.77E-01	9.36E+06 8.96E+06	2.96E-01 8.99E-03	7.31E+04 7.11E+04	0.0
479	Down-dip	i	3	58		4.59E+05	4.59E+05	1.10E+01	3.52E-12 1.78E-12	1.14E-01 5.00E-01	1.40E-11 1.12E-11	9.54E+00 2.40E+01	1.45E-05 2.08E-06	0.00E+00 0.00E+00	3,48E+02 1.53E+03	3,59E+05		5.05E-06	2.19E+06	5.33E-01	9.66E+06	1.51E-01	7.42E+04	1.84E+04
	Down-dip	1	3	78		5.33E+06	5.33E+06	1.10E+01	9.53E-05	9.57E-02	2.22E-04	2.45E-01	9.70E+02	0.00E+00	2.92E+02	1.28E+06 1.02E+05	2.66E-06 9.92E+01	2.56E-06 9.34E+01	4.06E+06 1.43E+07	1.44E-01 7.97E-01	1.35E+07 1.50E+07	1.04E-01 7.97E-02	8.99E+04	1.01E+04
	Down-dip	1	3	18 94		1.44E+06 1.30E+06	1.44E+06 1.30E+06	1,10E+01	6.208-05	1.12E-01	1.25E-04	5.17E-01	5.71E+02	0.00E+00	3.42E+02	1.20E+05	6.83E+01	6.40E+01	1.01E+07	7.62E-01	1.30E+07	1.67E-01		
	Down-dip	i	3	10	-,	2.53E+05	2.53E+05	1.10E+01 1.10E+01	5.28E-05 5.38E-05	8.07E-02 2.26E-01	1.63E-04 1.40E-04	6.31E-01 1.43E+00	5.64E+02 2.18E+02		2.46E+02	1.05E+05		5.82E+01	8 19E+06	7.62E-01	1.12E+07	1.93E-01	8.07E+04	3,78E+04
	Down-dlp	1	3	19		4.35E+05	4.35E+05	1.10E+01	3.11E-05	1.29E-01	1.10E-04		2.33E+02	0.00E+00	3.92E+02	2.76E+05 1.66E+05	6.03E+01 3.87E+01	5.61E+01 3.80E+01	7.84E+06 9.16E+06	6.90E-01 6.17E-01	1.23E+07 1.21E+07	2.41E-03 4.67E-02	8.57E+04	2.39E+04
	Down-dip	1	3	44 73		8,00E+06 2,63E+05	8.00E+06 2.63E+05	2.88E+00 1.10E+01	1.32E-04 2.37E-05	1.77E-05 8.46E-02	1.85E-04		1.07E+07	0.00E+00	5.39E-02	3.25E+00	3.46E+01	3.38E+01	1.25E+07	8.88E-01	1.26E+07	1.71E-05	8.41E+04 8.63E+04	2.42E+04 3.52E+04
487	Down-dlp	1	3	48		8.04E+06	8.04E+06	2.88E+00	9.07E-05	1.62E-04	1.03E-04 1.37E-04	9.95E-01 1.62E-04	2.27E+02 6.65E+05	0.00E+00 0.00E+00	2.58E+02 4.96E-01	1.38E+05 3.65E+01	3.14E+01 2.42E+01	2.94E+01	6.90E+06	7.33E-01 8.89E-01	1.23E+07	6.49E-05	8.49E+04	1.61E+04
	Down-dip Down-dip	1	3	45 69		7.99E+06	7.99E+06	2.88E+00	8.02€-05	2.27E-06	1.29E-04	2.27E-06	5.20E+07	0.00E+00	6.92E-03	4.19E-01		2.37E+01 2.12E+01	1.16E+07 1.08E+07	8.89E-01 8.49E-01	1.18E+07 1.09E+07	3.64E-02 9.49E-01	8.29E+04 7.95E+04	2.57E+04   7.54E+04
	Down-dip	i	3	27		7.99E+06 1.22E+06	7.99E+06 1.22E+06	2.88E+00 8.00E+00	5.73E-05 1.76E-05		1.11E-04 6.31E-05	7.01E-05 2.08E-01	1.24E+06 5.02E+02	0.00E+00	2.14E-01	1.32E+01	1.63E+01	1.60E+01	1.11E+07	9.10E-01	1.12E+07	7.58E-01	8.05E+04	6.64E+04
	Down-dip	1	3	24	7.99E+06	7.99E+06	7.99E+06	2.88E+00	5.88E-05		7.35E-05	9.35E-07	8.28E+07	0.00E+00 0.00E+00	9.91E+01 2.85E-03	3.13E+04 1.83E-01	1.57E+01 1.52E+01	1.48E+01 1.48E+01	7.01E+06 9.75E+06	7.83E-01 9.09E-01	9.01E+06 9.72E+06	1.18E-03	7.08E+04	1.56E+04
	Down-dip Down-dia	1	3 3	46 90		6.08E+06 3.09E+05	6.09E+06 3.09E+05	2.88E+00	3.88E-05		1.18E-04		2.30E+03	0.00E+00	5.06E+01	5.23E+03	1.20E+01	1.18E+01	9.74E+06	8.46E-01	1.03E+07	8.78E-01 2.68€-06	7.47E+04 7.69E+04	6.83E+04 1.69E+04
	Down-dip	1	3	23			5.48E+06	1.10E+01 2.88E+00	7.00E-06 2.91E-05		3.69E-05 8.09E-05	9.69E-01 5.49E-02		0.00E+00 0.00E+00	1.52E+02	1.00E+05	1.00E+01	9.57E+00	3.83E+06	6.73E-01	8.29E+06	2.66E-06	6.67E+04	1.51E+04
	Down-dip	1	3	41				1.10E+01	5.86E-06	B.65E-02	3.29E-05		4.68E+01	0.00E+00	5.39E+01 2.64E+02	5.50E+03 1.80E+05		8.68E+00 B.22E+00	9.81E+06 4.23E+06	6.52E-01 5.30E-01	1.03E+07 9.26E+06	5.36E-07 3.89E-02		2.16E+04
	Down-dip	1	3	31 60		8,03E+06 6.03E+06	8.03E+06 6.04E+08	2.88E+00 2.88E+00	2.03E-05		4.78E-05	1.21E-04	2.70E+05	0.00E+00	2.40E-01	2.20E+01	6.11E+00	5.99E+00	9.11E+06	9.16E-01	9.16E+06	5.92E-05	7.28E+04 7.19E+04	1.63E+04 1.70E+04
	Down-dip	1	3	67			2.92E+05	1.10E+01	1.93E-05 3.82E-06		4.93E-05 2.05E-05		2.64E+03 2.12E+01	0.00E+00 0.00E+00	2.20E+01 3.83E+02	2.25E+03 2.49E+05			8.16E+06	7,90E-01	8.60E+06	7.85 <b>E-</b> 02	6.80E+04	2.15E+04
	Down-dip	1	3	52		8.00E+06	8.00E+06	2.88E+00	1.40E-05	B.00E-07	3.30E-05		2.07E+07	0.00E+00	2.44E-03	1.96E-01		5.01E+00 3.98E+00	4.63E+06 8.78E+06	4.56E-01 9.60E-01	1.02E+07 8.76E+06	2.41E-02 4.70E-01	7.65E+04 6.94E+04	1.19E+04
	Down-dip	1	3	20		2,70E+05 2,47E+05	2.70E+05 2.47E+05	1.10E+01 1.10E+01	2.78E-06		1.31E-05		1.82E+01	0.00E+00	3.22E+02	2.10E+05	3.82E+00	3.63E+00	4.35E+06	4.82E-01	9.39E+06	1.19E-07	7.32E+04	
502	Down-dip	1	3	53				2.88E+00	2.28E-06 1.04E-05	9.27E-02 1.13E-03	1.27E-05 2.65E-05	2.31E+00 2.70E-03	1.66E+01 9.31E+03	0.00E+00 0.00E+00	2.83E+02 3.45E+00	1.94E+05 3.49E+02		3.19E+00 3.19E+00	3.69E+06	4.94E-01	8.58E+06	9.42E-02	6.84E+04	1.87E+04
~~~	Down-dlp Down-dlp	1	3 3	100			8.00E+06	2.88E+00	1.05E-05	2.03E-06	2.21E-05	2.03E-06	8.44E+06	0.00E+00	6.20E-03	3.84E-01		3.19E+00	8.24E+06 8.76E+06	8.74E-D1 8.86E-01	8.55E+06 8.68E+06	1.84E-01 7.24E-01	6.78E+04 6.90E+04	3.45E+04 5.49E+04
	Down-dip	i	3	65 E			7.99E+06 2.54E+05	2.88E+00 1.10E+01	7.05E-06 9.03E-07		1,06E-05 5,33E-06			0.00E+00 0.00E+00	3.00E-04	2.25E-02	1.89E+00	1.84E+00	8.31E+06	9.18E-01	8.28E+06	8.90E-02	6.67E+04	2.85E+04
506	Down-dlp	1	3	71	0.00E+00	2.36E+05	2.36E+05	1.10E+01	7.77E-07					0.00E+00 0.00E+00		3.74E+05 2.85E+05	1.31E+00 1.20E+00	1.26E+00 1.18E+00	3.82E+06 3.10E+06	3.65E-01 3.83E-01	1.00E+07 9.03E+06	5.96E-08 1.37E-06		6.96E+03
	Down-dip Down-dip	1	3 3	95 98			3.00E+05	1.10E+01	5.41E-07		3.74E-06	7.46E+00	1.82E+00	0.00E+00	5.46E+02	4.47E+05		7.93E-01	4.00E+06	5.37E-01	9.03E+06 1.24E+07	1.37E-06 5.14E-02		6.87E+03
	Down-dip	1	3	98			2.24E+05 8.01E+06	1.10E+01 2.88E+00	4.58E-07 2.26E-06		3,20E-06 4,67E-06		2.58E+00 1.67E+07	0.00E+00 0.00E+00	3.19E+02 4.73E-04	2.73E+05	7.05E-01	6.78E-01	2.94E+06	3.15E-01	8.46E+06	5.13E-06		5.34E+03
	Down-dip	1	3	77	0.00E+00	2.54E+05	2.54E+05	1.10E+01	3.79E-07				1.57E+07	0.00E+00	4.73E+04 4.37E+02	4.09E-02 3.67E+05	6.83E-01 5.77E-01	6.69E-01 5.72E-01	8.18E+06	9.14E-01		2.34E-01		3.75E+04
	Down-dip Down-dip	1	3	15		2.86E+06 7.99E+06	2.86E+05	1.10E+01	2.99€-07	2.85E-01	8.03E-07	9.44E+00	5.14E-01	0.00E+00	8.71E+02	5.31E+05	2.73E-01	2.60E-01	3.50E+06 3.51E+06	3.09E-01 6.15E-01	1.00E+07 1.11E+07	8.09E-05 1.31E-01		5.86E+03
	Down-dip	i	3	16			7.99E+06 2.48E+05	2.88E+00 1.10E+01	2.19E-07 1.82E-08		4.84E-07 1.87E-07	2.03E-09 7.23E+00	2.21E+08 1.06E-01	0.00E+00 0.00E+00	3.10E-06	3.05E-04	6.73E-02	6.60E-02	8.01E+06	9.02E-01	7.90E+06	8.56E-01	6.49E+04	5.68E+04
	Down-dip	1	3	70	0.00E+00	2.93E+05	2.93€+05	1.10E+01	1.79E-10	6.07E-02		9.01E+00	1.26E-03	0.00E+00	2.59E+02 1.85E+02	3:05E+05 2:82E+05	3.23E-02 3.55E-04	3.22E-02 3.42E-04	2.12E+06 1.63E+06	3.79E-01 4.61E-01	8.93E+06 B.77E+06	2.89E-05 1.89E-05	7.01E+04	
	Down-dip Down-dip	1	3 3	76 78	0.00E+00 0.00E+00		3.20E+05 2.00E+05	1.10E+01 1.10E+01	1,58E-11		1.52E-10	1.03E+01	7.85E-05	0.00E+00	2.89E+02	3.61E+05	2.83E-05	2.80E-05	1.98E+06	3.64E-01	9.08E+06	1.89E-05 4.17E-07		8.11E+03 6.54E+03
	Down-dip	i	3	10				1.10E+01 1.10E+01	6.21E-05 4.87E-05			2.07E+00 2.52E+00	1.08E+02 1.13E+02	0.00E+00 0.00E+00	1.71E+03 1.19E+03	8.20E+05 4.75E+05		6.38E+01	1.36E+07	6.80E-01	1.47E+07	2.18E-02	9.74E+04	3.83E+04
	Down-dip	1	3	18		5.04E+05	5.04E+05	1.10E+01	3.73E-05	6.54E-01								5.29E+01 3.43E+01	8.44E+06 1.05E+07	6.65E-01 6.75E-01	1.38E+07 1.44E+07	1.60E-07		1.88E+04
	Down-dip Down-dip	1	3	45 19					1.07E-04		1.74E-04	5.63E-06	2.90€+07	0.00E+00	1.69E-02	1.01E+00	2.91E+01	2.84E+01	1.16E+07	9.48E-01	1.44E+07 1.19E+07	7.60E-02 9.49E-01		2.52E+04 7.91E+04
	Down-dip	1	3	48				1.10E+01 2.88E+00	2.28€-05 9.99€-05		8.48E-05 1.47E-04	1.75E+00 3.20E-03						2.75E+01	9.17E+06	5.62E-01	1.33E+07	1.53E-02	8.93E+04	2.11E+04
	Down-dip	1	3	46	0.00E+00	3.55E+05	3.55E+05	1.10E+01	1.70E-05	5.87E-02	9.43E-05	1.02E+00							1.25E+07 5.07E+06	8.60E-01 7.05E-01	1.26E+07 9.82E+06	2.40E-06 3.52E-06		2.06E+04
	Down-dip Down-dip	1	3	44				2.88E+00 2.88E+00	9.06E-05 7.46E-05				2.09E+07	0.00E+00	1.96E-02	1.15E+00	2.38E+01	2.32E+01	1.12E+07	8.89E-01	9.82E+06 1.12E+07	6.27E-06	7.48E+04 8.07E+04	1.36E+04 3.46E+04
	Down-dip	i	3	69					7.46E-05 5.19E-05		2.05E-04 1.00E-04					3.98E-02		2.12E+01		9.93E-01	1.13E+07	1.83E-01	8.10E+04	4.25E+04
	•			'								17E-03	1.016100	V.UUC+00	1.576-01	9.59E+00	1.48E+01	1.44E+01	1.08E+07	9.10E-01	1.08E+07	7.48E-01	7.926+04	6.49E+04

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					Excevated Wests	Basidual Gas	Residual Bria	e Crushed Pane	i Up⊹dip Avg	Up-dip Avg	Down-dip Avg	Controle Ave	DB7 Paranthe	DRZ	Sali Piliar	Sali Pila	hannel Y		Well	BC well Sand	Total Area	Coelila	Castile	Up-dip Brins	Up-dip Gas	Down-skp	Down-die Ga
					Parcetty (fraction)	9at. (fraction)) Sal. (hacilon) Heighl (m)	Pressure (Pa)	6at (fraction)	Репякте (Ра)	Sal. (fraction)	(Fraction)	Permeability (m/2)	Peresity (Fraction)	Permeability (m*2)	Intrusion Time (Years)	Sidn lactor	Productivity India (1/2a)	Permeability (te22)	notids released	Reservoir	Reservois Permenhillo	Relative Permeabling	Relative Remembra	Brine Relative	Rolative Permeability
No.	ID E	Replic.	Scen.	Vector	POROSITY	SAT_RGAS	SAT_RBR	N HEIGHT	PRESPAN2	BSATPAN2	PRESPANA	RSATPANA	POGOGITY	DCDM V	POROSITY	, ,	(L)YO 2			(27	(m²2)	Ргеззила (Ра)	(m*2)	(Iraction)	(fraction)	(fraction)	(fraction)
	own-dip	4	3	73	5.58E-01	5.61E-02	5.40E-01		1.23E+07	6.38E-06	1.23E+07	6.42E-01	9.62E-02	3.72E-16	1.04E-01	3.72E-16	NTA_TME	-8.0(E-0)	WELLPI 1,13E-13	6.17E-15	3.77E-01		PRM_CAST	KRW2	KAG2	KAW4	KRG4
	own-dip own-dip	1	3	24 23	5.17E-01 5.48E-01	9.01E-02 7.29E-02	, _ , ,			7.49E-01	9.27E+06	9.08E-01	1.96E-01	2.82E-13	2.17E-01	2.82E-13		U.U.L.U.	1.13E-13	2.63E-14	9.94E-01	1 37E+07	9.77E 12 7.41E-13	0.00E+00 2.82E-01	1.00E+00 1.41E-02	7.01E-02 0.59E-01	1.46E-01 3.07E-08
	own-dip	i	3	1	5.09E-01	9.81E-02		1.33E+00 1.22E+00	1.15E+07 8.87E+06	2.38E-07 8.99E-01	1.15E+07 8.96E+06	7.19E-01 8.99E-01	3.98E-02	1.18E-16	4.59E-02	1.18E-16	5.00E+03		1.27E-13	7.94E-17	8.09E-01	1.52E+07	6.03E-13	0.00E+00	1.00E+00	5.67E-02	1.42F-01
	own-dip	1	3	27	5.19E-01	1.18E-01	4.62E-01	1.25E+00	9.28E+06	4.17E-07	9.29E+06	6.74E-01	8.91E-02 3.02E-02	7.24E-16	8.99E-02 4.28E-02	7.24E-16 1.86E-16	5.00E+03 5.00E+03	-1.28E+00 -1.24E+00	1.22E-13	1.66E-14	9.73E-01	1.28E+07	7.08E-14	5.84E-01	1.38E-07	5.84E-01	1.34E-07
1	own-dip	!	3	31 100	4.97E-01 5.00E-01	5.28E-02	5.93E-02		B.43E+06	1.05E-05	8.53E+06	9.47E-01	7.36E-02	1.66E-15	9.78E-02	1.66E-15	5.00E+03	-1.27E+00	1.23E-13 1.19E-13	2.40E-15 3.31E-14	9.09E-01 9.73E-01	1.20E+07 1.48E+07	1.26E-12 6.31E-13	0.00E+00 0.00E+00	1.00E+00	3.22E-02	1.68E-01
	own-diip own-diip	i	3	71	5.17E-01	1.14E-01 1.57E-02	3.43E-01 1.06E-01	1.20E+00 1.24E+00	8.52E+06 9.18E+06	8.83E-01 1.19E-06	8.61E+06	8.83E-01	6,96E-02	9.12E-16	9.05E-02	9.12E-16	5.00€+03	-1.26E+00	1.19E-13	2.51E-14	9.43E-01	1.28E+07	1.29E-13	4.85E-01	1.00E+00 1.95E-07	8.06E-01 4.86E-01	8.14E-10 1.70E-07
534 D	own-dip	1	3	67	5.30E-01	1.21E-01	6.61E-02		1.02E+07	1.19E-06 1.51E-04	9.21E+06 1.01E+07	3.87E-01 3.48E-01	4.44E-02 1.70E-01	2.19E-18 3.55E-18	6.50E-02 1.81E-01	2.19E-18	5.00E+03		1.29E-13	5.25E-17	1.18E+00	1.20E+07	6.76E-13	0.00E+00	1.00E+00	1.40E-02	3.95E-01
	own-dip	1	3	41	5.38E-01	3.40E-02	8.64E-02	1.30E+00	1.07E+07	1.65E-02	1.08E+07	3.50E-01	1.45E-01	1.70E-19	1.50E-01	3.55E-18 1.70E-19	5.00E+03 5.00E+03	-1.27E+00 -1.22E+00	1.27E-13 1.27E-13	7.24E-15 3.24E-16	9.65E-01 8.64E-01	1.27E+07	1.15E-14	0.00E+00	1.00E+00	1.20E-02	3.56E-01
	own-dlp own-dla	1	3	6 65	5.01E-01 5.27E-01	6.58E-02 1.27E-01	1.45E-01	1.20E+00	8.57E+06	1.85E-02	B.69E+06	4.00E-01	6.67E-02	5.76E-19	8,36E-02	5.75E-19	5.00E+03	-1.18E+00	1.15E-13	6.46E-17	8.02E-01	1.48E+07	3.47E-12 3.09E-12	0.00E+00 0.00E+00	1.00E+00 1.00E+00	1.02E-02 1.14F-02	4.28E-01
1	own-dip	i	3	20	5.15E-01	1.23E-01	8.96E-02 1.27E-01	1.27E+00 1.24E+00	9.91E+06 9.13E+06	2.38E-07	9.91E+06 9.10E+06	3.39E-01 3.69E-01	2.09E-02	8.71E-18	3.08E-02	8.71E-16	5.00E+03	-1.18E+00	1.21E-13	4.17E-15	7.73E-01	1.27E+07	3.72E-12	0.00E+00	1.00E+00	8.42E-03	3.91E-01
	QID-mwo	1	3	98	4.96E-01	3.56E-02	5.00E-02		8.41E+06	4.36E-06	8.35E+06	2.98E-01	2.01E-02 6.13E-02	1.35E-17 4.19E-19	3.75E-02 8.67E-02	1.35E-17 4.17E-19	5.00E+03 5.00E+03		9.65E-14	3.31E-15	2.55E-01	1.29E+07	1.20E-12	0.00E+00	1.00E+00	8.80E-03	3.91E-01
540 D	own-dip	1	3	90	5.12E-01	1.28E-02	2.86E-01	1.23E+00	9.02E+06	1.49E-06	8.97E+06	4.70E-01	1,83E-02	1.20E-17	3.66E-02	1.20E-17	5.00E+0.3	-1.23E+00 -8.48E-01	1.16E-13 1.04F-13	4.79E-15 2.09E-14	8.82E-01 4.15E-01	1.17E+07 1.31E+07	3 98E-14 3.02E-12	0.00E+00	1.00E+00	7.04E-03	4.72E-01
542 D		1	3	84 77	4.95E-01 5.37E-01	1.44E-01 1.48E-01	6.88E-03 6.84E-02	1.19E+00 1.30E+00	8.34E+06 1.06E+07	5.96E-08 4.73E-05	8.45E+06	2.44E-01	2.14E-02	4.91E-20	3.72E-02	4.90E-20	5.00E+03	-1.40E+00	1.25E-13	2.95E-16	1.25E+00	1.27E+07	3.55E-11	0.00E+00 0.00E+00	1.00E+00 1.00E+00	6.77E-03 5.04E-03	4.86E-01
543 D		i	3	15	5.31E-01	4.22E-02	5.21E-01	1.28E+00	1.00E+07	9.73E-05 9.56E-02	1.07E+07 1.02E+07	2.38E-01 5.93E-01	2.00E-01 5.60E-02	8.13E-19 1.32E-14	2.13E-01 6.88E-02	8.13E-19	5.00E+03	-7.13E-01	1.05E-13	2.75E-16	3.17E-01	1.24E+07	1.20E-11	0.00E+00	1.00E+00	1.84E-03	5.69E-01
	own-dip	1	3	47	5.34E-01	6.75E-02	1.61E-01	1.29E+00	1.04E+07	5.07E-02	1.04E+07	3.01E-01	1.48E-01	6.92E-18	1.53E-01	1.32E-14 6.92E-18	5.00E+03	-9.48E-01 -1.09E+00	1.12E-13 1.19E-13	1.32E-14 2.19E-16	5.06E-01	1.15E+07	4.47E-13	0.00E+00	1.00E+00	9.20E-04	6.64E-01
545 D 546 D		1	3	14 10	5.18E-01 5.77E-01	1.07E-01	3.28E-01	1.25E+00	9.21E+06	2.13E-02	9.31E+06	3.79E-01	1.31E-01	8,31E-19	1.45E-01	6.31E-19	5.00E+03	-7.31E-01	1.19E-13	8.32E-16	6.75E-01 3.28E-01	1.21E+07 1.49E+07	1.55E-12 2.63E-14	0.00E+00 0.00E+00	1.00E+00	1.36E-03 7.34E-05	6.31E-01
547 D		i	3	78	5.77E-01 6.93E-01	3.17E-02 4.93E-02	1.73E-01 1.51E-01	1.42E+00 1.48E+00	1.39E+07 1.51E+07	1.79E-07 9.90E-03	1.39E+07 1.51E+07	7.78E-01 7.36F-01	8.33E-02	3.93E-14	6.23E-02	3.72E-14	1.00E+04	-1.33E+00	1.45E-13	1.86E-16	1.08E+00	1.18E+07	1.35E-11	0.00E+00	1.00E+00	7.34E-05 3.15E-01	8.14E-01 2.12E-02
54B D		1	3	45	5.73E-01	5.05E-02	2.04E-01	1.41E+00	1.35E+07	9.49E-01	1.36E+07	7.36E-01 9,49E-01	2,20E-01 8,92E-02	3.53E-11 1.01F-13	1.02E-01 6.09E-02	2.46E-15 5.13E-14	1.00E+04 1.00E+04	-1.06E+00 -9.31E-01	1.35E-13 1.23E-13	8.32E-17	6.28E-01	1.48E+07	1.07E-12	0.00E+00	1.00E+00	2.53E-01	2.96E-02
549 D		1	3	18	5.98E-01	1.06E-01	3.40E-01	1.49E+00	1.54E+07	3.28E-06	1.54E+07	8.61E-01	8.72E-02	3.62E-13	6.04E-02	3.31E-14	1.00E+04	-9.31E-01 -1.09E+00	1.23E-13 1.38E-13	1.74E-15 6.17E-16		1.36E+07 1.12E+07	4.57E-13	7.82E-01	2.68E-09	7 82E-01	2.66E-09
	own-dip own-dip	1	3	94 48	5.50E-01 5.44E-01	4.58E-03 1.02E-01	1.85E-01 2.11E-01	1.33E+00 1.32E+00	1.16E+07 1.11E+07	1.55E-01 2.68E-06			2.03E-01	6.31E-15	2.09E-01	6.31E-15	1.00E+04	-1.29E+00	1.34E-13	9.77E-16		1.44E+07	5.25E-12 1.78E-12	0.00E+00 0.00E+00	1.00E+00 1.00E+00	6.97E-02 9.72E-01	1.07E-01 1.66E-08
552 D		í	3	19	5.76E-01	1.42E-01	2.97E-02	1.42E+00	1.11E+07 1.38E+07	2.68E-06 8.30E-05	1.12E+07 1.38E+07	8.97E-01 7.57E-01	5.47E-02 2.05E-01	7.76E-14	5.82E-02	7.76E-14	1.00E+04	-1.29E+00	1.32E-13	2.19E-15		1.10E+07	3.80E-12	0.00E+00	1.00E+00	5.98E-01	3.67E-10
	wn-dip	1	3	73	5.51E-01	5.61E-02	3.03E-01	1.34E+00	1.17E+07	4.29E-06	1.17E+07	9.43E-01	9.50E-01	9.48E-15 3.72E-16	1.92E-01 1.06E-01	1.41E-15 3.72E-16	1.00E+04 1.00E+04	-1.23E+00 -8.01E-01	1.39E-13 1.11E-13	2.00E-16 6.17E-15		1.25E+07		0.00E+00	1.00E+00	3.46E-01	2.88E-03
554 Do 555 Do	wn-dip	1	3	69 44	5.37E-01 5.19E-01	8.98E-02 1.12E-01	4.08E-01	1.30E+00	1.05E+07	9.09E-01		9.09E-01	7.76E-02	1.26E-14	8.87E-02	1 26E-14	1.00E+04	-1.29E+00	1.30E-13	9.33E-15	3.77E-01 9.99E-01	1.38E+07 1.47E+07	9.77E-12 4.07E-13	0.00E+00 5.40E-01	1.00E+00 2.84E-08	7.31E-01 5.40E-01	1.23E-09 1.90E-08
556 C		i	3	71	5.19E-01	1.57E-01	1.61E-02 1.06E-01		9.28E+06 9.32E+06	3.27E-04 1.19E-06		8.88E-01	1.28E-01	1.18E-13	1.38E-01	1.18E-13		-1.17E+00	1.19E-13	3.80E-15		1.38E+07	1.12E-12	0.00E+00	1.00F+00	6.39E-01	1.90E-08
557 Do	wn-dip	1	3	46	4.96E-01	2.03E-02	2.35E-01		8.43E+08	8.05E-06		5.24E-01 8.54E-01	4.46E-02 4.47E-02	2.19E-18 1.59E-17	6.47E-02 6.69E-02	2.19E-18 1.59E-17	1.00E+04 1.00E+04	-1.37E+00	1.30E-13	5.25E-17	1.18E+00	1.20E+07	6.76E-13	0.00E+00	1.00E+00	6.03E-02	1 97E-01
	wn-dip	!	3	1	5.15E-01	9.81E-02	2.56E-01	1.24E+00	9.09E+06	B.99E-01	9.18E+06		6.93E-02	7.24E-16	8.89E-02	7.24E-16		-1.41E+00	1.26E-13	1.45E-14 1.66E-14	1.26E+00 9.73E-01	1.51E+07 1.28E+07	1.15E-11 7.08E-14	0.00E+00	1.00E+00	4.58E-01	7.60€-03
	wn-dip wn-din	1	3	67 20	4.98E-01 4.95F-01	1.21E-01 1.23E-01	6.61E-02 1.27E-01	1.20E+00 1.19E+00	8.52E+06	9.23E-05		4.21E-01	1.74E-01	3.55E-18	1.94E-01	3.55E-18	1.00E,+04	-1.27E+00	1.19E-13	7.24E-15		1.27E+07	1.15E-14	5.84E-01 0.00E+00	1.57E-07 1.00E+00	5.84E-01 2.80E-02	1.36E-07 2.40E-01
, - .	wn-dip	i	3	65	5.21E-01	1.27E-01	6.96E-02		8.37E+06 9.45E+06	1.79E-07 1.31E-06		4.39E-01 3.85E-01	1.88E-02 1.96F-02	1.35E-17 8.71E-16	3.91E-02 3.12E-02	1.35E-17		-6.04E-01	9.26E-14	3.31E-15		1.29E+07	1.20E-12	0.00E+00	1.00E+00	2.24E-02	2.64E-01
	wn-dip	1	3	56	4.88E-01	4.66E-02	3.20E-01		8.13E+06	1.37E-06		5.39E+01	B.40E-02	1.05E-15	1.03E-02	8.71E-16 1.05E-15	1.00E+04 1.00E+04	-1.16E+00 -7.21E-01	1.19E-13 9.50E-14	4.17E-15 1.05E-14		1.27E+07		0.00E+00	1.00E+00	1.57E-02	3.14E-01
	wn-dip wn-dip	1	3	77	5.45E-01	1.48E-01	6.84E-02	1.32E+00	1.12E+07	2.25E-05	1.12E+07	2.63E-01	1.99E-01	8.13E-19	2.10E-01	8.13E-19		-7.13E-01	1.07E-13	2.75E-16	·	1.17E+07 1.24E+07		0.00E+00 0.00E+00	1.00E+00 1.00E+00	1.54E-02 3.06E-03	3.56E-01 5.12E-01
, _,	wn-dio	1	3	84	5.56E-01 5.15E-01	3.40E-02 1.44E-01	8.64E-02 6.88E-03		1,21E+07 9,13E+06	4.86E-03 0.00E+00		2.36E-01	1.48E-01	3.35E-19	1.44E-01	1.70E-19	1.00E+04	-1.22E+00	1.31E-13	3.24E-16		1.48E+07		0.00E+00	1.00E+00	1.25E-03	6.55E-01
566 De	wn-dip	1	3	58	5.54E-01	2.96E-02	1.14E-01		1.19E+07	1.73E-06		1.34E-01 2.11E-01	2.31E-02 2.09E-01	4.91E-20 1.45E-16	3.57E-02 2.14E-01	4.90E-20 1.45E-16		-1.40E+00 -1.18E+00	1.30E-13	2.95E-16		1.27E+07	3.55E-11	9.00E+00	1.00E+00	5.07E-04	6.94E-01
	wn-dip	1	3	12	5.27E-01	7.06E-02	1.02E-01		9.89E+06	8.35E-07	9.89E+06		3.00E-02	1.78E-13	4.57E-02	1.78E-13		-1.18E+00	1.29E-13 1.32E-13	3.09E-15 5.50E-15		1.32E+07 1.44E+07		0.00E+00	1.00E+00	2.81E-04	7.67E-01
	wn-dip wn-dip	1	3	6	5.35E-01 5.50E-01	6.58E-02 6.75E-02	1.45E-01 1.61E-01	1.29E+00 1.34E+00	1.04E+07	1.09E-05			7.01E-02	5.76E-19	7.80E-02	5.75E-19	1.00E+04	-1.18E+00	1.24E-13	6.46E-17		1.40E+07		0.00E+00 0.00E+00	1.00E+00 1.00E+00	1.32E-04 7.99E-05	8.01E-01 B.26E-01
570 Do		i	3	27	5.19E-01	1 18E-01	4.62F-01		1.16E+07 9.32E+06	5.20E-03 3.58E-07		1.96E-01 4.74E-01	1.50E-01 3.03E-02	1.08E-17 1.86E-16	1.47E-01 4.27E-02	6.92E-18		-1.09E+00	1.24E-13	2.19E-16		1.21E+07		0.00E+00	1.00E+00	8.04E-06	9.07E-01
571 Do	wn-dip	1	4	40	5.58E-01	1.02€-01	3.54E-01	1.36E+00	8.68E+06	1.36E-01		7.37E-01	1.22E-01	1.50E-16	1.35E-01	1.86E-16 1.51E-13		-1.24E+00 -1.32E+00	1.23E-13 1.38E-13	2.40E-15 3.02E-13		1.20E+07 1.47E+07		0.00E+00	1.00€+00	7.53E-07	9.42E-01
572 Do 573 Do		1	4	51	5.96E-01 5.50E-01	1.34E-01 3.07E-02	3.63E-01	1.49E+00	1.15E+07	2.47E-01			1.67E-01	6.31E-14	1.67E-01	6.17E-14		-1.16E+00	1.42E-13	1.00E-12	7.77E-01			0.00E+00	1.00E+00 1.00E+00	1.45E-01 3.12E-01	3.97E-02 7.42E-04
574 Do		1	4	58	6.01E-01	2.96E-02	7.64E-02 1.14E-01	1.33E+00 1.51E+00	8.15E+06 1.19E+07	6,98E-02 1,72E-01	_		2.45E-02	4.27E-15	4.30E-02	4.27E-15	5.50E+02	-1.26E+00	1.32E-13	8.91E-13				0.00E+00	1.00E+00	4.22E-04	7.41E-01
575 Do		1	4	28	5.93E-01	9.72E-02	1.79E-01		1.12E+07	1.99E-01	.,,	2.06E-01	1.87E-01 1.89E-01	1.45E-16 5.21E-17	1.91E-01 1.99E-01	1.45E-16 4.79E-17		-1.18E+00 -1.08E+00	1.45E-13 1.36E-13	3.09E-15		1.26E+07	1.07E-13	4.41E-05	8.59E-01	1.16E-04	8.16E-01
576 Do		1	4	94	5.35E-01	4.58E-03	1.85E-01	1.29E+00	8.60E+06	2.90E-01	B.61 E+06	5.97E-01	1.96E-01	6.31E-15	2.15E-01	6.31E-15		-1.29E+00	1.36E-13	9.55E-12 9.77E-16		1.48E+07 1.43E+07	9.55E-14	1.05E-06 5.19E-04	9.44E-01 7.34E-01	3.31E-06	9.24E-01
577 Do		1	4	79 31	5.36E-01 5.34E-01	1.23E-01 5.28E-02	3.88E-01 5.93E-02		8.68E+06 8.55E+06				1.69E-01	2.67E-13	1.92E-01	2.57E-13	7.50E+02	-1.10E+00	1.20E-13	1.51E-16			1.78E-12 4.37E-15	5.19E-04 0.00E+00	7.34E-01 1.00E+00	8.03E-02 2.89E-01	1.65E-01 1.94E-03
579 Do	wn-dip	į.	4	73	5.29E-01	5.61E-02	3.03E-01		8.21E+06				6.78E-02 8.48E-02	1.66E-15 3.72E-16	9.05E-02 1.11E-01	1.66E-15 3.72E-16	7.50E+02 7.50E+02	-1.27E+00	1.29E-13	3.31E-14	9.73E-01	1.49E+07	6.31E-13	0.00€+00	1.00E+00	3.46E-02	2.52E-01
580 Do		1	4	58	5.90E-01	2.96E-02	1.14E-01	1.47E+00	1.28E+07	1.58E-01			1.97E-01	3.72E-16 3.58E-16	1.11E-01 1.97E-01	3.72E-16 1.45E-16		-8.01E-01 -1.18E+00	1.06E-13 1.41E-13	6.17E-15 3.09E-15		1.39E+07 1.26E+07		0.00E+00	1.00E+00	8.35E-04	6.75E-01
_	wn-dip wn-dip	1	4	94	5.47E-01 5.14E-01	4.58E-03 5.28E-02	1.85E-01		1.14E+07	2.21E-01			2.04E-01	6.31E-15	2.10E-01	6.31E-15	2.00E+03	-1.29E+00	1.33E-13			1.43E+07	1.07E-13 1.78F-12	1.51E-05 9.97E-06	6.95E-01 9.08E-01	5.78E-05 4.59E-01	8.48E-01 1.01E-02
583 Do		i	4	19	5.14E-D1 6.29E-01	5.28E-02 1.42E-01	5.93E-02 2.97E-02		9.02E+06 1.00E+07	8.88E-06 9.67E-02			7.28E-02 2.00F-01	1.66E-15	9.45E-02			-1.27E+00	1.23E-13	3,31E-14	9.73E-01	1.49E+07		0.00E+00	1.00E+00	6.57E-02	1.66E-01
584 Do	wn-dip	1	4	44	5.07E-01	1.12E-01	1.61E-02		8.65E+06				1.28E-01	1.41E-15 1.18E-13	2.13E-01 1.41E-01	1.41E-15 1.18E-13		-1.23E+00 -1.17E+00	1.25E-13 1.16E-13	2.00E-16 3.80E-15			1.45E-12	5.16E-05	8.33E-01	2.82E-02	2.29E-01
	wn-dip	1	4	79	5.74E-01	1.23E-01	3.88E-01	1.41E+00	1.97E+07	2.98E-06	1.37E+07	5.28E-01	1.78E-01	3.22E-13	1.76E-01	*****		-1.17E+00	1.16E-13 1.31E-13	3.80E-15 1.51E-16		1.45E+07 1.31E+07			1.00E+00	6.29E-01	1.65E-07
	wn-dip wn-dip	t	4	73 58	5.37E-01 5.86E-01	5.61E-02 2.96E-02	3.03E-01 1.14E-01			3.02E-02 6.33E-02			9.32E-02	3.72E-16	1.09E-01		2.00E+03	-8.01E-01	1.08E-13	6.17E-15					1.00E+00 1.00E+00	4.27E-03 1.84E-04	4.49E-01 7.82E-01
	wn-dip	í	4	58	5.92E-01	2.96E-02	1.14E-01			6.33E-02 1.12E-04			2.27E-01 2.41E-01	2.70E-14 4.30E-13	1.99E-01 1.96E-01			-1.18E+00	1.39E-13		B.11E-01	1.26E+07	1.07E-13	0.00E+00	1.00E+00	2.18E-06	9.38E-01
	wn-dip	1	4	94	5.47E-01	4.58E-03	1.85E-01	1.33E+00	1.14E+07	1.90E-01	1.15E+07		2.04E-01	6.31E-15	2.10E-01		4.00E+03 4.00E+03	-1.18E+00 -1.29E+00	1.41E-13 1.33E-13					0.00E+00	1.00E+00	1.48E-01	8.24E-02
	wn-dip wn-dip	1	4	44	5.10E-01 5.57E-01	1.12E-01 1.42E-01	1.61E-02				8.95E+06	8.87E-01	1.28E-01	1.18E-13	1.40E-01	1.18E-13	4.00E+03	-1.17E+00	1.17E-13	9.77E-16 3.80E-15		1.43E+07 1.45E+07			9.87E-01 1.00E+00	9.72E-01 6.39E-01	1.57E-08 2.73E-10
	wn-dip wn-dio	i	4	31	5.5/E-01 4.96E-01	1.42E-01 5.28E-02	2.97E-02 5.93F-02		1.23E+07 8.37E+06				1.98E-01	1.41E-15	2.00E-01		4.00E+03	-1.23E+00	1.33E-13	2.00E-16	8.94E-01	1.27E+07		0.00E+00	1.00E+00	6.39E-01 1.38E-02	3.27E-01
593 Do	wn-dlp	1	4	79	5.75E-01	1.23E-01	3.88E-01		1.38E+07				7.28E-02 1.79E-01	1.66E-15 3.46E-13	9.79E-02 1.76E-01			·1.27E+00	1.19E-13		9.73E-01	1.49E+07	6.31E-13	0.00E+00	1.00E+00	5.91E-01	8.76E-04
594 Do		1	4	78	5.21E-01	4.93E-02	1.51E-01	1.25€+00	9.41E+06	3.13E-05				2.46E-15	1.76E-01	2.46E-15		-1.10E+00 -1.06E+00	1.32E-13 1.14E-13	1.51E-16 8.32E-17				0.00E+00	1.00E+00	2.38E-03	5.20E-01
595 Do 596 Do		1	4	41 12		3.40E-02	8.64E-02				8.36E+06	2.09E-01	1.46E-01	1.70E-19	1.64E-01	1,70E-19	4.00E+03	-1.22E+00	1.16E-13							4.87E-04 5.99E-04	7.24E-01 7.15E-01
	wu-dab wu-dab	i	4			7.06E-02 2.96E-02	1.02E-01 1.14E-01		9.77E+06 1.39E+07				2.97E-02	1,78E-13	4.69E-02				1.32E-13	5.50E-15	1.19E+00	1.44E+07			1.00E+00		8.60E-01
598 Do	wn-dip	i	4				2.97E-02						2.13E-01 1.99E-01	1.05E-15 2.54E-15	2.03E-01 1.95E-01	1.45E-16 1.41E-15		-1.18E+00	1.36E-13			1.26E+07	1.07E-13	0.00E+00	1.00E+00	4.30E-01	8.79E-03
599 Do		1	4	94	5.51E-01	4.58E-03	1.85E-01	1.34E+00	1.17E+07	1.57E-01	1.17E+07				2.0BE-01			-1.23E+00 -1.29E+00	1.36E-13 1.34E-13								8.11E-02
600 Do	wn-dip	1	4	73	5.49E-01	5.61E-02	3.03E-01	1.33E+00	1.15E+07	4.17E-06	1.15E+07															9.72E-01 8.64E-02	1.54E-08 1.21E-01
																						· ····································	U.114-12	v.vvc+00	VC+VV	0.046-02	1.21E-U1

_					1	Down-dip							Produced							Avii Brue				
		•		•	Up-dip Flowing Bottom-hole	Flowing Bottom-hole	BC well Injection	Plowout Duration	Brine Rais (m^3/s)	Gas Rete (ref	Max Brine		Liquid/Gas	Cum Brine from Boundary		Cum One Produced (ref	Com Bring Produced	Cum Brine	Avg Brine Pressure	Sakuration	Avg Brine Preseure	Avg Bane Seturation	Total Excavated	Total Excession
					Pressure (Pa)	Pressure (Pa)	Pressure (Pa)	(Days)	(m-(1/a)	m^3/a)	Rate (m*3/s)	(ref m/3/a)	Ratio (m^3/s / ref m^3/s)	Condition Well (m^3)	(macMdny)	m/3)	m^3	(m/3)	Panel 5 (Pa) after Shwoul	Panel 5 (kaction) after	Penal 0 (De)	Panel 0 (#action) after	Waste Pore Volume	Brine Volume
No.	ID Down-de		c. Scen	. Vector	FBHP2 0.00E+00	FOHP4	HP_ABAN	time		GASFLW		MAX_GAS	LOR_MET		GAS_RATE		BRINEOUT	BRIN_REL	BANPAES5	SATBRNS	BANPRESO	SATERNO	(fraction) WASTE PV	(m^3) TOT BRIN
527	,		3	24	4.31E+06	4.03E+05 7.99E+06	4.03E+05 7.99E+06	1.10E+01 2.88E+00	8.85E-06 4.03E-05	1.32E-01 3.62E-07	4.50E-05 5.00E-05	2.48E+00 3.62E+07	4.85E+01 1.42E+08	0.00E+00 0.00E+00	4.01E+02			1.22E+01	5.64E+06	6.52E-01	1.23E+07	6.25E-05	B.50E+04	1.42E+04
528	Down-dir		3	23	0.00E+00	3.69E+05		1.10E+01	6.54E-06	6.90E-02	3,83E-05	2.37E+00	5.05E+01	0.00€+00				1.01E+01 B.54E+00		9.10E-01 7.28E-01	9.16E+06 1.15E+07	4.70E-01	7.22E+04	
529 530	Down-dig		3 3	1 27	7.99E+06 0.00E+00	7.99E+06 2.79E+05		2.88E+00 1.10E+01	1.45E-05 2.86E-06	1.97E-06 6.33E-02	3.29E-05	1.97E-06	1.14E+07	0.00E+00	6.01E-03	3.92E-01	4.46E+00	4.37E+00	8.91E+06	9.01E-01	8.85E+06	2.38E-07 7.62E-01	8.16E+04 6.99E+04	
531	Down-dir	1	3	31	0.00E+00	7.99E+06	7.99E+06	2.88E+00	9.BOE-06	1.04E-08	1.70E-05 2.45E-05	1.80E+00 1.04E-08	2.95E+01 1.30E+09	0.00E+00 0.00E+00						6.B4E-01	9.28E+06	4.17E-07	7.27E+04	1.32E+04
532 533	W-0.111		3	100 71	8.00E+D6	B.00E+06		2.88E+00	8.14E-06	1.00E-06	1.70E-05	1.00E-06	1.28E+07	0.00E+00		1,96E-01		2.45E+00	8.48E+06 8.59E+06	9.48E-01 8.86E-01	8.43E+06 8.50E+06	7.01E-05 7.13E-01	6.66E+04 6.73E+04	
534			3	67	0.00E+00 0.00E+00	2.40E+05 2.57E+05		1.10E+01 1.10E+01	1,09E-06 1,15E-06	1.08E-01 1.47E-01	7.71E-06 7.13E-06	4.41E+00 4.67E+00	6.05E+00	0.00E+00				1.64E+00	3.22E+06	4.04E-01	9.18E+06	1.19E-06	7.21E+04	7.38E+03
535	Down-dip		3	41	0.00€+00	2.69E+05	2.69E+05	1.10E+01	8.40E-07	1.32E-01	8.50E-06	6.40E+00	5.01E+00 3.57E+00	0.00E+00 0.00E+00	4.50E+02 4.03E+02			1,61E+00 1,31E+00	3.90E+06 3.37E+06	3.66E-01 3.68E-01	1.02E+07	6.95E-04	7.61E+04	
536 537	Down-dip		3	6 65	0.00E+00 0.00E+00	2.28E+05 2.50E+05	2.28E+05 2.50E+05	1.10E+01	7.77E-07	9.05E-02	5.31E-06	3.49E+00	5.12E+00	0.00E+00	2.76E+02	2.33E+05	1.19E+00	1.14E+00		4.16E-01	1.07E+07 8.57E+06	1.65E-02 1.12E-02	7.86E+04 6.77E+04	1.15E+04 1.59E+04
538			3	20		2.35E+05	2.36E+05	1.10E+01 1.10E+01	7.92E-07 6.42E-07	1.63E-01 1.19E-01	4.69E-06 3.60E-06	4.80E+00 3.19E+00	3.09E+00 3.40E+00	0.00E+00 0.00E+00		3.71E+05	1.15E+00		3.73E+06	3.58E-01	9.87E+06	2.12E-07	7.52E+04	
539	Down-dip	1	3	98		2.19E+05	2.20E+05	1.10E+01	4.61E-07	9.99E-02	3.18E-06	3.93E+00	2.74E+00			2.75E+05 2.57E+05		9.11E-01 6.89E-01	3.50E+06 2.90E+08	3.87E-01 3.18E-01	9.13E+06 8.41E+05	1.19E-07 4.35E-06	7.16E+04 6.62E+04	6.98E+03
540 541	Down-dip	1	3	90 84		2.31E+05 2.21E+05	2.31E+05 2.21E+05	1.10E+01 1.10E+01	3.88E-07	8.67E-02	2.94E-06	4.17E+00	2.48E+00	0.00E+00	2.65E+02	2.52E+05	6.25E-01	6.18E-01	2.67E+06	4.86E-01	9.02E+06	1.46E-06	7.07E+04	5.25E+03 1.01E+04
542	Down-dip	ì	3	77		2.70E+05		1.10E+01	3.59E-07 1.34E-07	1.07E-01 1.61E-01	2.47E-06 9.61E-07	4.20E+00 6.93E+00	2.01E+00 4.68E-01	0.00E+00 0.00E+00		2.71E+05 4.54E+05		5.33E-01	3.03E+06	2.65E-01	8.34E+06	5.96E-08	6.60E+04	6.51E+03
543	Down-dip	1	3	15		2.66E+05	2.66E+05	1.10E+01	1.71E-07	2.45E-01	4.88E-07	7.81E+00	3.54E-01	0.00E+00		4.55E+05		2.08E-01 1.61E-01	3.28E+06 3.19E+08	2.59E-01 6.07E-01	1.06E+07 9.95E+06	4.73E-05 5.46E-02	7.82E+04 7.62E+04	4.99E+03 1.76E+04
544 545	Down-dip Down-din	1	3	47 14		2.66E+05 2.75E+05		1.10E+01 1.10E+01	1.04E-07	1.72E-01	7.85E-07	8.22E+00	3,53E-01	0.00E+00	5.23E+02	4,51E+05	1.59E-01	1.58E-01	3.18E+06	3.21E-01	1.04E+07	4.94E-02	7.71E+04	1.27E+04
546		· i	3	10		3.62E+06	3.62E+06	1.10E+01	3.28E-09 9.33E-05	8,86E-02 1.05E-01	3.21E-08 2.25E-04	7.26E+00 4.49E-01	1.77E-02 9.71E+02	0.00E+00 0.00E+00	2.70E+02 3.21E+02	3.32E+05 1.09E+05		5.65E-03 9.97E+01	2.10E+06	3.97E-01	9.21E+06	2.13E-02	7.24E+04	1.46E+04
547	Down-dlp	1	3	7B	0.00E+00			1.10E+01	8.74E-05	3.17E-01	2.13E-04	7,99E-01	3.12E+02	0.00E+00	9.66E+02		9.50E+01	9.97E+01	1.10E+07 1.41E+07	7.86E-01 7.41E-01	1.39E+07 1.48E+07	1.53E-07 5.55E-03	9.20E+04 9.82E+04	2.06E+04 3.83E+04
548 549	Down-dip Down-dip	1	3	45 18	7.99E+06 0.00E+00	7.99E+06 5.16E+05	7.99E+06 5.16E+05	2.BBE+00 1.10E+01	1.59E-04 4.09E-05	1.54E-05 8.83E-01	2.57E-04 6.86E-05	1.54E-05	1.52E+07	0.00E+00	4.70E-02			4.17E+01	1.31E+07	9.48E-01	1.35E+07	9.49E-01	9.05E+04	
550	Down-dip	1	3	94		7.99E+06	7.99E+06	2.88E+00	8.14E-05	1.77E-07	2.24E-04	3.45E+00 1.79E-07	4.61E+01 5.36E+08	0.00E+00 0.00E+00	2.69E+03 5.40E-04		4.07E+01 2.36E+01	3.87E+01 2.31E+01	1.17E+07 1.09E+07	6.73E-01	1.46E+07	2.73€-06		1.94E+04
551 552	Down-dip Down-dip	1	3	48 19		8.00E+06	8.D0E+06	2.88E+00	7.94E-05	1.33E-05	1.20E-04	1.33E-05	9.04E+06	0.00E+00	4.06E-02	2.36E+00		2.07E+01	1.10E+07	9.94E-01 8.98E-01	1.16E+07 1.11E+07	1.57E-01 1.95E-06	8.23E+04 8.04E+04	4.13E+04 1.98E+04
553	Down-dip	÷	3	73		7.23E+06 7.99E+06	7.23E+06 7.99E+06	2.88E+00 2.88E+00	6.28E-05 5.87E-05	1.82E-02 2.04E-05	1.51E-04 1.45E-04	3.70E-02 2.04E-05	3.43E+03 4.58E+06	0.00E+00	5.55E+01		1.92E+01	1.89E+01	1.35E+07	7.62E-01	1.38E+07	B.54E-05	9.15E+04	
554	Down-dip	1	3	69	7.99E+06	7.99E+06	7.99E+06	2.88E+00	4.63E-05	3.57E-05	8.86E-05	3.57E-05	1.99E+06	0.00E+00 0.00E+00	6.21E-02 1.09E-01	3.86E+00 6.62E+00	1.76E+01 1,31E+01	1.73E+01 1.29E+01	1.14E+07 1.05E+07	9.43E-01 9.11E-01	1.17E+07	3.98E-05	8.27E+04	2.02E+04
555 556	Down-dip	1	3	44 71		B.00E+06	8.00E+06	2.88E+00	3.62E-05	2.50E-07	4.93E-05	2.50E-07	2.14E+08	0.00E+00	7.62E-04	4.45E-02		9.26E+00	9.31E+06	8.90E-01	1.05E+07 9.28E+08	6.53E-01 1.84E-04	7.80E+04 7.27E+04	5.98E+04 3.25E+04
557	Down-dip	i	3 3	46		3.01E+05 6.39F+06	3.01E+05 6.39E+06	1.10E+01 2.88E+00	5.66E-06 1.88E-05	8.72E-02 5.56E-03	3.38E-05 5.54E-05		4.44E+01 3.36E+03	0.00E+00	2.66E+02	1.84E+05		7.98E+00	4.06E+06	5.37E-01	9.32E+06	1.19E-06	7.28E+04	9.97E+03
558	Down-dip	1	9	1		B.00E+06	8.00E+06	2.88E+00	1.79E-05	3.71E-06	4.08E-05	3,71E-08	7.66E+06	0.00E+00	1.70E+01 1.13E-02	1,74E+03 7.22E-01	5.85E+00 5.51E+00	5.74E+00 5.40E+00	8.18E+06 8.12E+08	8.58E-01 9.01E-01	8.43E+06 9.07E+08	7.97E-06 6.98F-01	6.64E+04	1.47E+04
559 560	Down-dip Down-dip	1	3	67 20	0.00E+00 0.00E+00			1.10E+01	2.50E-06	9.53E-02		2.09E+00	1.84E+01	0.00E+00	2.91E+02	1.86E+05	3.42E+00	3.26E+00	3.94E+06	4.36E-01	8.52E+06	1.64E-04	7.14E+04 6.69E+04	5.63E+04 7.49E+03
561	Down-dip	i	3	65		2,30E+05	2.49E+05	1.10E+01 1.10E+01	1.68E-06 1.52F-06	9.04E-02 1.41E-01	8.05E-06 8.22E-06	1.75E+00 3.41E+00	1.27E+01 7.19E+00	0.00E+00 0.00E+00	2.76E+02 4.30E+02	1.82E+05 2.98E+05		2.28E+00	3.78E+06	4.55E-01	8.37E+06	1.79E-07	6.59E+04	7.60E+03
562	Down-dip	1	3	56			2.21E+05	1.10E+01	1.06E-06	9.78E-02	5.52E-06		7.12E+00	0.00E+00	2.98E+02	2.10E+05	2.14E+00 1.49E+00	2.06E+00 1.48E+00	3.96E+06 3.32E+06	4.02E-01 5.53E-01	9,43E+06 8,12E+06	1.29E-06 5.91E-06	7.33E+04 6.42E+04	7.44E+03 9.05E+03
563 564	Down-dip Down-dip	1	3	77 41		2.75E+05 3.02E+05	2.75E+05 3.02E+05	1.10E+01 1.10E+01	2,43E-07 9,54E-08	1.68E-01 1.70E-01	1.70E-06	6.86E+00	8.22E-01		5.12E+02	4.64E+05	3.81E-01	3.65E-01	3.51E+06	2.83E-01	1.12E+07	2.25E-05	8.06E+04	5.66E+03
565	Down-dip	i	3	84			2.50E+05	1.10E+01	9.54E-08 3.30E-08	1.70E-01 1.33E-01	9,19E-07 2,79E-07	1.25E+01 7.67E+00	2.84E-01 1.35E-01	0.00E+00 0.00E+00	5.19E+02 4.07E+02	5.81E+05 4.00E+05	1.65E-01 5.41E-02	1.68E-01 5.22E-02	3.03E+06	2.57E-01	1.21E+07	5.00E-03	B.43E+04	6.91E+03
566	Down-dip	1	3	58	0.00E+00		3.18E+05	1.10E+01	2.98E-08	3.62E-01	2.02E-07	1.42E+01	5.06E-02	0.00E+00	1.11E+03		4.41E-02	4.33E-02	2.70E+06 4.03E+06	1.58E-01 2.32E-01	9.13E+06 1.19E+07	0.00E+00 4.41E-06	7.16E+04 8.38E+04	
567 568	Down-dip Down-dip	T E	3 3	12 8		2.81E+05 3.01E+05	2.81E+05 3.01E+05	1.10E+01 1.10E+01	3.06É-08 4.79E-09	1.63E+00 1.42E-01	7.99E-08 4.82E-08	1.05E+01	1.53E-02	0.00E+00	4.99E+03	2.31E+06	3.53E-02	3.48E-02	4.42E+06	2.03E-01	7.44E+06	8.35E-07	7.52E+04	3,71E+03
569	Down-dip	1	3	47	0.00E+00		3.54E+05	1.10E+01	5,99E-10	2.24E-01	5.34E-09	1.14E+01 1.51E+01	1,69E-02 1.45E-03	0.00E+00 0.00E+00	4.32E+02 6.84E+02	4.99E+05 6.73E+05	8.42E-03 9.73E-04	8.32E-03 9.35E-04	2.53E+06 2.99E+06	2.33E-01 2.18E-01	1.04E+07 1.16E+07	1.09E-05	7.75E+04	9.56E+03
570 571	Down-dip Down-dip	t	3	27 40	0.00E+00		3.17E+05	1.10E+01	4.17E-11	7.87E-02	3.97E-10	1.01E+01	2.30E-04	0.00E+00	2.40E+02	3.36E+05	7.74E-05	7.46E-05	1.82E+06	4.89E-01	9.31E+06	1.10E-02 6.42E-06	8.24E+04 7.28E+04	8.10E+03 9.04E+03
572	Down-dip	1	4	51	0.00E+00		0.00E+00 0.00E+00	1.10E+01 2.88F+00	6.07E-05 5.75E-05	1.22E-01 2.48E-03	7.82E-05 7.94E-05		5.47E+02 1.68E+04	0.00E+00 0.00E+00	3.71E+02	1.16E+05	6.35E+01	6.02E+01	7.1BE+06	7.49E-01	8.61E+06	1.37E-01	8.51E+04	
573	Down-dip	1	4	49	0.00E+00	2.32E+05	0.00E+00	1.10E+01	3.95E-08	2.69E-01	2.10E-07	6.65E+00	9.98E-02	0.00E+00	7.66E+00 8.21E+02	8.91E+02 5.32E+05	1.48E+01 5.31E-02	1.44E+01 5.16E-02	1.14E+07 3.01E+06	8.32E-01 2.11E-01	1.15E+07 8.01E+06	2.50E-01 7.02E-02		4.13E+04
574 575	Down-dip Down-dip	1	4	58 28		3.30E+05 3.51E+05	0.00E+00 0.00E+00	1.10E+01	1.34E-08	4.13E-01	9.30E-08	1.69E+01	1.97E-02	0.00E+00	1.26E+03	1.02E+06	2.02E-02		3.95E+00	2.12E-01	1.19E+07	1.71E-01	8.22E+04	8.57E+03
	Down-dip	i	4	94		3.05E+05	0.00E+00	1.10E+01 1.10E+01	3.32E-10 1.07E-05	3.47E-01 1.51F-01	2.32E-09 4.11E-05	1.56E+01 1.60E+00	5.76E-04 5.85E+01	0.00E+00 0.00E+00		8.58E+05	4.94E-04 1.34E+01	4.85E-04	3.49E+06	2.28E-01	1.12E+07	1.99E-01	9.82E+04	1.99E+04
577	Down-dip	1	4	79	0.00E+00	7.26E+06	0.00E+00	2.88E+00	2.1BE-05	1.18E-03	2.40E-05	3.08E-03	1.20E+04	0.00E+00	4.41E+02 3.61E+00	2.30E+05 4.38E+02	1.34E+01 5.27E+00		5.10E+06 8.67F+06	6.07E-01 8.30E-01	8.59E+06 8.68E+06	2.59E-01 1.78E-01	7.75E+04 7.78E+04	3.46E+04 2.92F+04
578 579	Down-dip Down-dip	1	4	31 73		2.51E+05 2.27E+05	0.00E+00 0.00E+00	1.10E+01	3.88E-06	1.50E-01	1.76E-05	2.42E+00	1.92E+01	0.00E+00	4.58E+02	2.67E+05	5.13E+00	4.92E+00	4.35E+06	4.52E-01	8.53E+06	3.30E-02	7.78E+04 7.73E+04	1.11E+04
	Down-dip	1	4	58			0.00E+00	1.10E+01 1.10E+01	5.26E-08 6.82E-09	1.36E-01 4.55E-01	3.38E-07 4.82E-08	4.95E+00 1.94E+01	2.29E-01 9.04F-03	0.00E+00 0.00E+00	4.16E+02 1.39E+03	3.49E+05 1.13E+06	7.98E-02	7.59E-02	2.76E+06	4.22E-01	8.21E+06	8.87E-02	7.57E+04	1.30E+04
581	Down-dip	1	4	94				2.88E+00	6.47E-05	2.35E-02	1.55E-04	8.42E-02	2.38E+03	0.00E+00	7.16E+01	7.50E+03	1.02E-02 1.79E+01	1.01E-02 1.75E+01	4.09E+06 1.09E+07	1.99E-01 8.49E-01	1.28E+07 1.14E+07	1.57E-01 2.09E-01	9.72E+04 8.13E+04	1.61E+04 4.07E+04
582 583	Down-dip Down-dip	1	4	31 19	0,00E+00 2.95E+05		0.00E+00 0.00E+00	1.10E+01 1.10E+01	7.69E-06 4.07E-06	1.25E-01 2.31E-01	3.37E-05	1.69E+00	4.84E+01	0.00E+00	3.61E+02	2.09E+05	1.01E+01	9.68E+00	4.99E+06	5.22E-01	9 01E+06	5.42E-05		9.50E+03
584	Down-dip	i	4	44	0.00E+00	7.99E+06	0.00E+00	2.88E+00	1.76E-05	3.27E-07	1.64E-05 2.38E-05		1.37E+01 8.38E+07	0.00E+00 0.00E+00	7.04E+02 9.96E-04	3.81E+05 7.24E-02	5.22E+00 4.61E+00	5.19E+00 4.50E+00	5.68E+06 8.65E+06	4 15E-01	1.00E+07	8.04E-02	7.57E+04	2.06E+04
	Down-dip	1	4	79		3.28E+05	0.00E+00	1.10E+01		2.44E+00	3.58E-06	1.10E+01	9.52E-01	0.00E+00	7.44E+03	2.99E+06	2.84E+00	2.82E+00		8.87E-01 5.42E-01	8.65E+06 1.17E+07	7.93E-06 3.03E-06	6.94E+04 9.08E+04	1.96E+04 1.27E+04
586 587	Down-dip Down-dip	1	4	73 58		2.93E+05 4.57E+05	0.00E+00 0.00E+00	1.10E+01 1.10E+01	1.25E-08 5.36E-10	1.78E-01 1.92E+00	9.75E-08 2.08E-09	9.57E+00 2.81E+01	3.78E-02 2.32E-04	0.00E+00	5.42E+02	5.39E+05	2.04E-02	1.96E-02	2.89E+06	3.89E-01	1.06E+07	3.10E-02	7.80E+04	9.42E+03
588	Down-dip	í	4	58	0.00E+00	3.09E+05	0.00E+00	1.10E+01	5.31E-05	6.79E-01	1.50E-04		8.90E+01	0.00E+00 0.00E+00	5.85E+03 2.07E+03	2.62E+06 6.53E+05	6.06E-04 5.81E+01		7.07E+06 1.24E+07	1.63E-01 6.47E-01	1.40E+07 1.50E+07	6.45E-02	9.53E+04	9.95E+03
	Down-dip	1	4	94 44			0.00E+00	2.88E+00	7.82E-05	1.56E-07	2.15E-04	1.58E-07	5.84E+08	0.00E+00	4.75E-04	3.69E-02	2.27E+01	2.22E+01	1.24E+07	9.94E-01	1.505+07 1.14E+07	1.02E-04 1.90E-01	9.79E+04 8.15E+04	1.68E+04 4.41E+04
590 591	Down-dip Down-dip	i	4	19			0.00E+00 0.00E+00	2.88E+00 1.10E+01	2.52E-05 2.22E-06	7.99E-08 3.64E-01	3.42E-05 1.04E-05		4.57E+08 4.35E+00	0.00E+00 0.00E+00	2.44E-04 1.11E+03	1.45E-02	6.60E+00	6.45E+00	8.92E+06	8.90E-01	8.93E+06	5.13E-06	7.02E+04	1.85E+04
592	Down-dip	i	4	31	0.00E+00	7.83E+06	0.00E+00	2.88E+00	8.35E-06	2.53E-04	1.91E-05		3.36E+04	0.00E+00	7.72E-01	6.85E+05 7.62E+01	2.98E+00 2.56E+00	2.98E+00 2.61E+00	5.77E+06 B.37E+06	3.52E-01 8.78E-01	1.22E+07 8.37E+06	2.55E-02	8.49E+04	1.53E+04
	Down-dip Down-dip	1	4	79 ·			0.00E+00	1.10E+01			2.01E-06	1.30E+01	4.31E-01	0.00E+00	8.54E+03	3.48E+08	1.50E+00	1.47E+00	7.87E+06	5.22E-01	1.14E+07	1.25E-04 2.05E-06	6.64E+04 9.13E+04	1.51E+04 1.22E+04
	Down-dip	i	4	41			0.00E+00 0.00E+00	1.10E+01 1.10E+01	4.31E-08 3.21E-08	2.67E-01 1.04E-01	2.44E-07 2.69E-07	7.48E+00 5.92E+00	1.04E-01 1.67E-01		8.14E+02 3.17E+02	5.80E+05	6.05E-02		3.35E+06	2.79E-01	9.35E+06	2.11E-03	7.32E+04	5.61E+03
596	Down-dip	1	4	12		2.93E+05	0.00E+00	1.10E+01	7.97E-09	1.64E+00	2.11E-08	1.09E+01	3.94E-03			3.16E+05 2.34E+08	5.29E-02 9.23E-03	5.29E-02 9.14E-03	2.42E+06 4.31E+06	2.31E-01 1.80E-01	8.30E+06 7.29E+06	3.26E-02	6.82E+04	5.34E+03
	Down-dip Down-dip	1	4	58 19		6.25E+06 7.32E+05	0.00E+00 0.00E+00	7.00E+00	6.22E-05		2.15E-04	1.31 E-0 1	1.87E+03	0.00E+00	1.01E+02	2.52E+04	4.71E+01	4.39E+01	1.23E+07	8.20E-01	1.39E+05	1.19E-07 5.20E-07	7.47E+04 9.20E+04	3.23E+03 1.95E+04
	Down-dip	1	4	94				1.10E+01 2.88E+00	2.00E-05 8.47E-05	2.27E-01 1.83E-07	7.62E-05 2.54E-04				6.92E+02	3,20E+05	2.53E+01	2.46E+01	8.87E+06	5.52E-01	1.31E+07	1.36E-04	8.87E+04	1.88E+04
	Down-dip	1	4	73					1.07E-05					0.00E+00	3.36E+02	2.00E+05	2.46E+01 1.45E+01	2.41E+01 1.38F+01	1.11€+07 5.70€±0€	9.94E-01 6.71E-01	1.17E+07 1.15E+07	1.57E-01 5.45E-05	8.28E+04 8.20F+04	4.26E+04
																			J., ULTUU	2115	·	- 10E U0	D.ZUCTU4	1.415.404



			_	Excreated	Desire 14								n	G.6.5							_	0				
•	•	•	•	Waste Porosity	Residual Clas Sat. (fraction)	Residual Brine Sat (fraction)	Crushed Panel Height (m)	Pressure (Pa)	Up-dip Avg Set. (fraction)	Down-dip Avg Pressure (Pe)	Down-dip Avg Sal. (fraction)	DRZ Porceity (Fraction)	Permanbility	Salt Pillar Porosity	Selt Piller Permeability	Intrusion Time (Years)	Skin lactor	Well Productivity	BC well Sand Permeability	Folsi Area solida released	Castile Peservoir	Castile Reservoir	Up-dip Brine Relative	Up-dip Gas Flatstve	Down-risp Brine Relative	Clown-d Refe
ID:	Reolic	Scen	Vector	(fraction)	SAT_RGAS	CAT DOON							(m^2)	(Fraction)	(m^2)			Index (I/Pa)	(m,5)	(m^2)	Pressure (Pa)	Permeability (m*2)	Permeability (haction)	Permeability (Itaction)	Permonbility (fraction)	Perme (fraci
Down-dip	1	4	79	5.75E-01	1.23E-01	3.88E-01	1.41E+00	1.37E+07	8.35E-07	PRESPAN4 1.37E+07	6.13E-01	1.78E-01	РЕЯМ_X 3.18E-13	1.76E-01	PERM_X 2.57E-13	INTR THE	SKIN +1,10€+00	WELLPI 1,31E-13			CAST_RE			KRG2	KRW4	KRG
own-dip	1	4	69 44	4.94E-01 4.91E-01	8.98E-02 1.12E-01	4.08E-01 1.61E-02		B.33E+06		8.36€+06	9.09E-01	7.48E-02	1.26E-14	9.70E-02	1.26E-14	1.00E+04	-1.29E+00	1.19E-13	9.33E-15	6.89E-01 9.99E-01	1.91E+07 1.62E+07	4.37E-15 4.07E-13		1.00E+00	2.87E-03 5.39E-01	4.98
own-dip	i	4	12	5.23E-01	7.06E-02	1.02E-01		8.23E+06 9.56E+06	2.80E-06 8.94E-07	8.26E+08 9.56E+06	B.BBE-01 3.D4E-01	1.30E-01 2.92E-02	1.18E-13 1.78E-13				-1,17E+00	1.12E-13	3.80E-15		1.45E+07	1.12E-12	0.00E+00	1.00E+00	6.39E-01	1.6
own-dip	1	4	78	5.29E-01	4.93E-02	1.51E-01	1.28E+00	1.00E+07	1.04E-05	1.00E+07	3.69E-01	1.09E-01	2.46E-15		2.46E-15		-1.38E+00 -1.06E+00	1.31E-13 1.16E-13	5.50E-15 8.32E-17	1.19E+00 6.28E-01	1.44E+07 1.61E+07	1.86E-13 1.07E-12	0.00E+00	1.00E+00	4.05E-03	5.1
own-dip own-dip	1	4	41 56	5.24E-01 4.85E-01	3.40E-02 4.66E-02	8.64E-02 3.20E-01	1.26E+00 1.17E+00	9.63E+06 8.04E+06	8,45E-03 1,43E-06		2.46E-01	1.44E-01	1.70E-19		1.70E-19		-1.22E+00	1.23E-13	3.24E-16		1.51E+07	3.47E-12		1.00E+00 1.00E+00	6.61E-03 1.61E-03	4.7 6.3
own-dip	i	5	79	5.51E-01	1.23E-01	3.88E-01	1.34E+00	1.18E+07	7.07E-02		3.75E-01 7.49E-01	8.40E-02 1.78E-01	1.05E-15 2.67E-13		1.05E-15 2.57E-13	1.00E+04	-7.21E-01	9.45E-14	1.05E-14		1.18E+07	2.82E-12	0.00E+00	1.00E+00	9.49E-05	8.2
own-dip	1	5	26	5.34E-01	7.60E-02	4.97E-01	1.29E+00	1.04E+07	2.18E-01	1.04E+07	8.05E-01	1.81E-01	2.00E-14		2.00E-14	1.20E+03 1.20E+03	-1.10E+00 -1.33E+00	1.24E-13 1.32E-13	1.51E-16	6.89E-01 1.10E+00	1.31E+07 1.19E+07	4.37E-15 6.76E-12	0.00E+00	1.00E+00	1 42E-01	2.7
own-dip cih-nwo	1	5 5	94 51	5.47E-01 5.69E-01	4.58E-03 1.34E-01	1.85E-01 3.63E-01	1.33E+00 1.39E+00	1.15E+07	2.41E-01	1.15E+07	6.63E-01	2.04E-01	6.31E-15		6,31E-15		-1,29E+00	1.33E-13	9.77E-16		1.43E+07	1.78E-12	0.00E+00 4.90E+05	1.00E+00 6.59E-01	1.63E-01 1.39E-01	3.3 9.9
own-dip	i	5	40	5.49E-01	1.02E-01	3.54E-01	1.33E+00	1.34E+07 1.16E+07	2.35E-01 6.42E-02	1.34E+07 1.16E+07	8.60E-01 6.35E-01	2.09E-01 1.38E-01	9.34E-13 1.54E-13	1.79E-01 1.38E-01	6.17E-14 1.51E-13		-1.16E+00	1.33E-13	1.00E-12		1.68E+07	6.92E-12	0.00E+00	1.00E+00	4.00E-01	3.4
own-dip	1	5	22	5.28E-01	2.51E-02	8.22E-02	1.27E+00	9.99E+06	2.28E-02	1.00E+07	9.72E-01	1.35E-01	7.41E-14	1.46E-01	7.41E-14	1.20E+03 1.20E+03		1.35E-13 1.32E-13	3.02E-13 1.74E-13		1.47E+07 1.39E+07	2.57E-11 1.59E-12	0.00E+00	1.00E+00	4.64E-02	1.5
own-dip own-dip	1	5 5	2 19	5.03E-01 5.06E-01	8.22E-02 1.42E-01	4.02E-01 2.97E-02	1.21E+00 1.22E+00	8.38E+06 8.56E+06	1.90E-01	8,40E+06	8.25E-01	1.69E-01	4.47E-14	1,68E-01	4.47E-14	1.20E+03	-1.29E+00	1.21E-13	5.01E-14	9.98E-01	1.41E+07	7.24E-11	0.00E+00 0.00E+00	1.00E+00 1.00E+00	8.91E-01 2.77E-01	7.3 9.3
own-dip	i	5	30	5.52E-01	1.16E-01	4.16E-02	1.24E+00	1.19E+07	1.52E-01 5.26E-02	8.57E+06 1.19E+07	4.62E-01 4.08E-01	2.02E-01 3.58E-02	1.41E-15 2.75E-14			1.20E+03 1.20E+03	-1.23E+00	1.19E-13	2.00E-16		1.27E+07	1.45E-12	4.77E-04	6.98E-01	4.64E-02	1.6
own-dip	1	5	31	5.36E-01	5.28E-02	5.93E-02	1.29E+00	1.05E+07	9,12E-04				1.66E-15				-6.49E-01 -1.27E+00	1.06E-13 1.29E-13	2.19E-13 3.31E-14	2.79E-01 9.73E-01	1.47E+07 1.49E+07	1.59E-13 6.31E-13	6.69E-08	9.74E-01	2.8BE-02	2.4
own-dip own-dio	1	5 5	79 49	5.23E-01 5.61E-01	5.61E-02 3.07E-02	3.03E-01 7.64E-02	1.26E+00 1.37E+00	9.56E+06 1.27E+07	6.72E-02	-,			3.72E-16		3.72E-16	1.20E+03	-8.01E-01	1.05E-13	6.17E-15	3.77E-01	1.39E+07	9.77E-12	0.00E+00 0.00E+00	1.00E+00 1.00E+00	2.26E-02 1.21E-03	3,1 6,4
chp-use	i	5	58	5.81E-01	2.96E-02	1.14E-01	1.43E+00	1.45E+07	4.93E-02 1.24E-01		1.55E-01 1.45E-01	4.03E-02 2.22E-01	4.27E-15 6.89E-15	4.19E-02 2.01E-01	4.27E-15 1.45E-16		-1.26E+00	1.36E-13	8.91E-13	9.52E-01	1.31E+07	9.77E-13	0.00E+00	1,00E+00	1.13E-04	8,1
wn-dip	1	5	5	5.10E-01	1.29E-01	1.21E-01		0.79E+D6			1.53E-01	1.33E-01	1.90E-17	1.54E-01	1.82E-17		-1,18E+00 -1,37E+00	1.38E-13 1.27E-13	3.09E-15 1.82E-12		1.26E+07 1.57E+07	1.07E-13 3.31E-13	7.79E-08 0.00E+00	9 75E-01 1 00E+00	4.55E-06	9 2
wn-dip wn-dip	1	5 5	28	5.70E-01 6.48E-01	9.72E-02 4.58E-03	1.79E-01 1.85E-01	1.40E+00 1.33E+00	1.35E+07 1.15E+07	1.81E-01			2.10E-01	5.51E-17		4.79E-17	1.20E+03	-1.08E+00	1.29E-13	9.55E-12		1.48E+07	9.55E-14	2.81E-10	9.94E-01	4.97E-06 8.56E-08	9,1 9,7
wn-dip	i	5	79	5.63E-01	1.23E-01	3.88E-01	1.37E+00	1.28E+07	2.28E-01 2.90E-02		7.05E-01 6.69E-01	2.04E-01 1.78E-01	6.31E-15 2.61E-13	2.10E-01 1.81E-01	0.31E-15 2.57E-13	1.40E+03 1.40E+03	-1.29E+00	1.33E-13	9.77E-18		1.43E+07	1.78E-12	1.92E-05	8.91E-01	1.90E-01	6.7
own-dip	t	5	19	5.13E-01	1.42E-01	2.97E-02	1.23E+00	8.96E+06	1.37E-01		4.41E-01	2.01E-01	1.41E-15		1.41E-15		-1.10E+00 -1.23E+00	1.28E-13 1.21E-13	1.51E-16 2.00E-16		1.31E+07 1.27E+07	4.37E-15 1.45E-12	0.00E+00 2.96E-04	1.00E+00 7.33E-01	5.63E-02 4.21E-02	1,1
own-dip own-dip	1	5 5	31 73	5.26E-01 5.26E-01	5.28E-02 5.61E-02	5.93E-02 3.03E-01		9.84E+06 9.81E+06			4.15E-01	7.44E-02	1.66E-15	9.21E-02	1.66E-15	1.40E+03	-1.27E+00	1.26E-13	3.31E-14	9.73E-01	1.49E+07	8.31E-13	0.00E+00		2.77E-02	1.7 2.6
wn-dip	i	5	58	5.83E-01	2.96E-02	1.14E-01	1.44E+00	1.46E+07	5.69E-02 1.10E-01		4.08E-01 1.50E-01	9.19E-02 2.25E-01	3.72E-16 1,82E-14	1.12E-01 2.00E-01	3.72E-16 1.45E-16	1.40E+03 1.40E+03		1.06E-13	6.17E-15		1.39E+07	9.77E-12	0.00E+00	1.00E+00	9.18E-04	6.6
cilb-nwi	1	5	58	5.93E-01	2.96E-02	1.14E-01	1.48E+00	1.55E+07	1.83E-02	1.55E+07	7.72E-01	2.44E-01	8.33E-13	1.95E-01			-1.18E+00 -1.18E+00	1.38E-13 1.42E-13	3 09E-15 3.09E-15	8.11E-01 8.11E-01	1.26E+07 1.26E+07	1.07E-13 1.07E-13	0.00E+00 0.00E+00		7.34E-06 3.34E-01	9.1
wn-dip wn-dip	1	5 5	94	5.06E-01 5.48E-01	5.28E-02 4.58E-03	5.93E-02 1.85E-01	1.22E+00 1.33E+00	8.71E+06 1.15E+07	9.95E-06			7.29E-02	1.66E-15		1.66E-15	3.00E+03	-1.27E+00	1.21E-13	3.31E-14	9.73E-01	1.49E+07	6.31E-13	0.00E+00	1.00E+00	1.95E-01	1.9 4.8
wn-dip	i	5	44	5.14E-01	1.12E-01		1.23E+00	9.06E+06	2.03E-01 5.72E-06		9.94E-01 8.87E-01	2.04E-01 1.28E-01	6.31E-15 1.18E-13	2.09E-01 1.39E-01	6.31E-15 1.18E-13		-1.29E+00	1.33E-13	9.77E-16	9.95E-01	1.43E+07	1.78E-12	8.88E-07	9.56E-01	9.72E-01	1.8
wn-dip	1	5	19	5.46E-01		2.97E-02	1.32E+00	1.14E+07			3.58E-01	1.99E-01	1.41E-15	2.05E-01		3.00E+03	-1.17E+00 -1.23E+00	1.18E-13 1.30E-13	3.80E-15 2.00E-18	7 83E-01 8 94E-01	1.45E+07 1.27E+07	1.12E-12 1.45E-12	0.00E+00 1.37E-06	1 00E+00 9 38E-01	8.38E-01	4.4
wn-dip wn-dip	1	5	79 78	5.75E-01 5.12E-01		3.88E-01 1.51E-01	1.41E+00 1.23E+00	1.38E+07	2.44E-06		5.02E-01		3.49E-13	1.76E-01	2.57E-13	3.00E+03	-1.10E+00	1.32E-13	1.51E-16	6.89E-01	1.31E+07	4.37E-15	0.00E+00		1.R3E-02 2.02E-03	2.8 5.3
wn-dip	i	5	73	5.49E-01		3.03E-01	1.33E+00	9.00E+06 1.15E+07	8.60E-03 9.72E-06			1.08E+01 9.48E+02	2.46E-15 3.72E-16	1.22E-01 1.06E-01		3.00E+03 3.00E+03		1.12E-13	8.32E-17		1.61E+07	1.07E-12	0.00E+00	t.00E+00	2.11E-04	7,7
wn-dip	1	5	12	5.25E-01	7.06E-02	1.02E-01	1.26E+00	9.71E+06				2.96E-02	1.78E-13	4.59E-02		3.00E+03		1.11E-13 1.31E-13	6.17E-15 5.50E-15	3.77E-01 1.19E+00	1.39E+07 1.44E+07	9.77E-12 1.86E-13	0.00E+00 0.00E+00	1.00E+00 1.00E+00	1.88E-08 3.94E-09	9.8
own-dip own-dip	1	5 5	58 94	5.93E-01 5.48E-01	2.96E-02 4.58E-03	1.14E-01 1.85E-01	1.48E+00 1.33E+00	1.55E+07					7.30E-13	1.95E-01	1.45E-16	5.00E+03	-1.18E+00	1.42E-13	3.09E-15	8.11E-01	1.26E+07	1.07E-13			2.88E-01	9.8
wn-dip	i	5	69	4.88E-01	8.98E-02	4.08E-01	1.17E+00	1.15E+07 8.08E+06					6.31E-15 1.26E-14	2.09E-01 9.81E-02		5.00E+03		1.33E-13	9.77E-16	9.95E-01	1.43E+07	1.78E-12	0.00E+00		9.72E-01	1.5
wn-dip	1	5	19	5,60E-01		2.97E-02	1.37E+00	1.25E+07				1.98E-01	1.44E-15	1.99E-01	_	5.00E+03 5.00E+03		1.17E-13 1.34E-13	9.33E-15 2.00€-16	9.99E-01 8.94E-01	1.62E+07 1.27E+07	4.07E-13 1.45E-12	0.00E+00 0.00E+00		2.50E-01	1.0
wn-dip wn-dip	1	5	31	5.03E-01 4.92E-01	1.12E-01 5,28E-02	1.61E-02 5.93E-02	1.21E+00 1.18E+00					1.29E-01	1.18E-13	1.42E-01	1.18E-13	6.00E+03	-1.17E+00	1.15E-13	3.80€-15	7.83E-01	1.45E+07	1.12E-12	0.00E+00		2.19E-02 6.39E-01	2.6
wn dip	i	5	79	5.75E-01		3.88E-01	1.41E+00				9.45E-01 5.10E-01	7.31E-02 1,78E-01	1.66E-15 3.37E-13	9.87E-02 1.76E-01		5.00E+03		1.18E-13		9.73E-01	1.49E+07	6.31E-13	0.00E+00	1.00E+00	7.99E-01	4.5
wn-dlp	1	5	78	5.24E-01			1.26E+00	9.66E+06			2.87E-01		2.48E-15	1.19E-01		5.00E+03 5.00E+03		1.31E-13 1.15E-13	1.51E-16 8.32E-17	6.89E-01 6.28E-01	1.31E+07 1.61E+07		0.00E+00 0.00E+00		2.59E-03	5.1
wn-dip wn-dip	1	5 5	41 12	5.05E-01 5.32E-01			1.21E+00 1.28E+00	8.72E+06 1.03E+07			2.01E-01		1.70E-19	1.61E-01				1.18E-13	3.24E-16			3.47E-12	0.00E+00		1.16E-03 4.76E-04	6.5 7.3
wn-dip	i	5	73	5.50E-01			1.34E+00					3.10E-02 9.51E-02	1.78E-13 3.72E-16	4.52E-02 1.06E-01				1.34E-13	5.50E-15	1.19E+00	1.44E+07	1.86E-13	0.00E+00	1.00E+00	5.12E-05	8.4
wn-dip	•	5	47	4.93E-01				8.31E+06	5.43E-02	8.34E+06			6.92E-18	1.66E-01	6.92E-18			1.11E-13 1.10E-13	6.17E-15 2.19E-16	3.77E-01 6.75E-01	1.39E+07 1.24E+07		0.00E+00 0.00E+00	1.00E+00 1.00E+00	7.64E-08 1.82E-11	9.0
wn-dip wn-dio	1	5 5	58 19	5.79E-01 5.68E-01	2.96E-02 1.42E-01	1.14E-01 2.97E-02		1.41E+07 1.31E+07					1.B4E-15	2.02E-01	1.45E-16	1.00E+04	-1.18E+00	1.37E-13	3.09E-15	B.11E-01	1.26E+07	1.07E-13	0.00E+00		4.52E-01	9.9 7.2
wn-dip	i	5	94	5.52E-01	4.58E-03	1.85E-01							2.36E-15 6.31E-15	1.96E-01 2.08E-01			-1.23E+00	1.36E-13	2.00E-16	8.94E-01	1.27E+07	1.45E-12	0.00E+00	1.00E+00	9.53E-02	8.0
wn-dip	1	5	73	5.49E-01		3.03E-01	1.33E+00		4.17E-06			9.48E-02	3.72E-16	1.06E-01	3.72E-16		-1,29E+00 -8.01E-01	1.34E-13 1.11E-13	9.77E-16 6.17E-15	9.95E-01 3.77E-01	1.43E+07 1.39E+07		0.00E+00 0.00E+00		9.72E-01 7.97E-02	1.5
wn-dip wn-dip	1	5 5	79 69	5.74E-01 4.94E-01		3.88E-01 4.08E-01	1.41E+00 1.19E+00	1.37E+07 8.33E+06	8.35E-07 5.52E-02		5.14E-01		3.08E-13	1.76E-01	2.57E-13	1.00E+04	-1.10E+00	1.31E-13	1.51E-16	6.89E-01	1.31E+07	4.37E-15	0.00E+00		2.95E-03	1.3 4.9
wn-dip	i	5	44	4.88E-01							9.09E-01 8.88E-01	7,48E-02 1,30E-01	1.26E-14 1.18E-13	9.70E-02 1.46E-01	1.26E-14 1.18E-13			1.19E-13 1.12E-13	9.33E-15		1.62E+07	4.07E-13	0.00E+00		5.39E-01	4.3
wn-dip	1	5	78	5.29E-01		1.51E-01	1.28E+00	1.00E+07			3.69E-01	-	2.46E-15	1.18E-01				1.18E-13	3.80E-15 8.32E-17		1.45E+07 1.61E+07	1.12E-12 1.07E-12	0.00E+00 0.00E+00	1.00E+00 1.00E+00	6.39E-01	1.5 4.7
wn-dip wn-dip	1	5 5	12 41	5.22E-01 5.24E-01				9.65E+06 9.62E+06				2.92E-02 1.44E-01	1.78E-13	4.82E-02	1.78E-13	1.00E+04	-1.38E+00	1.31E-13	5.50E-15	1.19E+00	1.44E+07	1.86E-13	0.00E+00		6.57E-03 2.83E-03	5.5
wn-dip	i	5	56	4.85E-01				8.05E+06				8.40E-02	1.70E-19 1.05E-15	1.54E-01 1.03E-01				1.23E-13 9.46E-14	3.24E-16 1.05E-14		1.51E+07	3.47E-12	0.00E+00	1.00E+00	1.59E-03	8.3
≻dip	1	1	58	6.36E-01	2.96E-02		1.65E+00	1.01E+07	1.70E-01	1.01E+07	1.B1E-01	1.64E-01	1.45E-16	1.75E-01					0.00E+00	3,22E-01 8,11E-01	1.18E+07 1.26E+07	2.82E-12 1.00E-12	0.00E+00 3.76E-05	1.00E+00 B.65E-01	9.34E-05 7.53E-05	8.2
rdip rdio	1	1		5.02E-01 5.44E-01	1.42E-01 4.58E-03			8.04E+06 1.09E+07					1.41E-15	2.26E-01			-1.23E+00	1.18E-13	0.00E+00	8.94E-01	1.27E+07	1.00E-12	7.78E-04		4.84E-02	8.3 1.5
-dip	1	1	58	5.B0E-01	2.96E-02	1.14E-01	1.43E+00	1.40E+07	1.37E-01	1.40E±07	1.55E-01	2 145-01	6.31E-15 1.59E-15	2 M2E 04	1 455 46	1.00E+03	4 30	4 075 44				1.00E-12			1.06E-01	1.3
-dlp	1	1	28	5.70E-01	9.72E-02	1.79E-01	1.40E+00	1.31E+07	1.94E-01	1.31F+07	1.99E-01	2 08F-01	4 70E.17	2 11E-01	4 70E-17	4 AAE - AA	4 005 - 00	4 005 40	* ***		1.26E+07 1.48E+07	1.00E-12 1.00E-12	1.49E-06 3.92E-07		1.18E-05	9.0
ı -dip ı-dip		1	30 19	5.47F-01	1.16E-01 1.42F-01	4.16E-02 2 97F-02	1.35E+00 1.33E+00	1.18E+07	5.30E-02	1.18E+07	3.99E-01	3.52E-02	2.75E-14	4.11E-02	2.75E-14	1.00E+03	-6,49E-01	1.07E-13	0.00E+00	2.79E-01	1.47E+07	1.00E-12	7.74E-08	9.73E-01	2.62E-02	2.5
-dip		;	60	5.21 E- 01	6.13E-02	4.70E-02	1.25E+00	9.44E+06	6.74E-02	9.48E+06	1.98E-01															
-dip	1	1	30	5.53E-01	1.16E-01	4.16E-02	1.34E+00	1.19E+07	4.82E-02	1.19E+07	4.39E-01	3.58E-02	2.75E-14	4.13E-02	2.75E-14	3.00E+03	-1.1/E+00 -6.49E-01	1.20E-13	0.00E+00	7.91E-01	1.35E+07	1.00E-12	6.77E-07	9.53E-01	1.10E-03	6.5
o-dip ≻dip		1	94	5.52E-01	4.68E-03	1.85E-01	1.34E+00	1.18E+07	1.91E-01	1.18E+07	9.94E-01	2.03E-01	6.31E-15	2 ORF 01	6 31F 15	3 00F±03	1,29E+00	1.34±•13	U.00E+00	9.95E-01	143F+07	1 00€.19	RAIE no	6 P7E_01	B 71E-01	2.00
o-dip	i	i	30	5.56E-01	1.16E-01	4.16E-02	1.35E+00	1.21E+07	4.18E-02	1.20E+07 1.21E+07	4.67E-01					5.00E+03 1.00E+04	*0.49E*U	1.U0E-13	D.UOE+00	2.79E-01	1.47E+07	1 00F-12	2 17F_00	a one ni	4 455 03	1 0
p-dip		2	30	5.96E-01	1.16E-01	4 16F-02	1 49F400	1 15F±07	9.38E_01	1.165.07	1 095.01						-6.49E-01	1.076-13	0.00E+00	2.79E-01	1.47E+07	1.00E-12	5.53E-15	1.00€+00	4.97E-02	1.6
p-dip p-dip		2	69	5.87E-01	8.98E-02	4.08E-01	1.45E+00	1 08€+D7	9 22E-01	1.075+07	7 13E-01	6.98E-02	1.26E-14	7.91E-02	1.26E-14	5.50E+02 5.50E+02	1.29E+00	1.46E-13	9.33E-15	9.99E-01	1.42E+07	4.07E-13	5.94F-01	2.725+04 0.00E±06	8.62F-03	5.24 g p
·+	•	_	344	J., UL-U1	7.006703	1.000-01	1,425+00	a.03E+00	5.51E-U1	9.81E+0 0	4.50E-01	1.84E-01	6.31E-15	1.96E-01	6.31E-15	5.50E+02	1,29E+00	1.42E-13	9.77E-16	9.95E-01	1.31E+07	1.78E-12	9.58E-01	3 81F-07	1.57E-02	3.4

4	

-					Up-dip Flowing	Down-dip	BC well	Slowout			-		Produced	Cum Brine					Ava Brine	Ave Hime		Ava Hane	Tolki	
	•	•	•	•	Bottom-hole Pressure (Pa)	Flowing Bottom-hole	Injection	Duration	Brime Flate (m°3/si	Gas Plate (ref m/3/s)	Max Brine Rate (m^3/s)	Max Gas Pate (rel m^3/s)	Uquid/Gea Ratio (m/3/s /	from Boundary Condition Well		Cum Bns Produced (ref	Cum Brine Prorkload	Com Brine Releases	Prendure	Saturation Panel 5	Avg Brine Pressure	Saturation Page 0	Executated Waste Pore	Total Exceveled
						Ргозакле (Ра)	Prosoure (Pa)	(Clays)					ref (n/3/s)	(m^3)	(mac reasy)	m^3)	(m^3)	(m^3)	Panel 5 (Pa) after Slowoul	(Asction) after	Panel 0 (Pa)	(haction) after	Volume	Brine Volume : (mr3)
6D	Down-dip	Replic	c. Scon.	Vector 70	FBHP2 0.00E+00	FBHP4 3.30€±05	0.00E+00	time	BRINEFLW			MAX_QAS		CIMIC DO				BRIN_REL	BRNPRES5	blowout SATBRN5	BRNPRESO	Mowout SATBRNO	Itraction) WASTE PV	TOT BRIN
602		i	4	69	0.00E+00	7.99E+06		1.10E+01 2.88E+00	2.20E-06 8.23F-06	2.63E+00 9.14E-08	2.41E-06 1.12E-05	1.22E+01 9.14E-08	5.58E-01 9.11E+07	0.00E+00 0.00E+00	8.01E+03 2.79E-04	3.25E+06		1,76E+00		5.28E-01	1.15E+07	8.61E-07	9.12E+04	
60:		1	4	44	0.00E+00	B.00E+06	0.00C+00	2.88E+00	6.65E-06	9.79E-10	8.93E-06	9.79E-10	9.22E+09		2.79E-04 2.99E-06	1.93E-02 1.89E-04	1.78E+00 1.74E+00		8.34E+06 8.25E+06	9.11E-01	8.33E+06	5.40E-02	6.57E+04	
604		1	4	12 78	0.00E+00	2.43E+05			9.48E-07	1.28E+00	2.35E-06	6.33E+00	6.55E-01	0.00E+00	3.90E+03	1.68E+06	1.10E+00	1.03E+00	4.72E+06	8.90E-01 3.22E-01	8.23E+06 7.72E+06	2.91E-06 9.47E-07	6.50E+04 7.38E+04	1.93E+04 5.94F+03
606	Down-dip	i	4	41	0.00E+00	2.51E+05 2.52E+05	0.00E+00 0.00E+00	1.10E+01	6.89E-07 1.04E-07	2.41E-01 1.26E-01	3.59E-06 8.90E-07	5.59E+00	1.92E+00		7.34E+02		9.50E-01	9.31E-01	3.94E+06	3.87E-01	9.96E+06	1.06E-05	7.57E+04	7.38E+03
607	Down-dip	1	4	56	0.00E+00	2.45E+05		1.10E+01	5.00E-09	1.28E-01	3.34E-08	7.46E+00 5.12E+00	4.42E-01 2.27E-02	0.00E+00 0.00E+00	3.85E+02 3.89E+02		1.73E-01 7.69E-03	1.69E-01 7.31E-03	2.75E+06	2.67E-01	9.62E+06	8.44E-03	7.42E+04	
608	Down-dip	1	5	79		8.75E+05		1.10E+01	8.45E-05	1.67E-01	1.07E-04	4.61E-01	6.41E+02		5.09E+02			8.50E+01	2.46E+06 1.04E+07	3.93E-01 7.61E-01	8.02E+06 1.17E+07	6.50€-06 7.09E-02	6.35E+04 B.28E+04	
610	Down-dip Down-dip	1	5 5	26 94	0.00E+00 3.30E+05	8.25E+05 5.73E+05	0.00E+00 0.00E+00	1.10E+01 1.10E+01	6.69E-05 2.51E-05	4.39E-02 1.68E-01	9.84E-05	4.57E-01	1.22E+03	0.00E+00	1.34E+02		6.62E+01	6.27E+01	8.52E+06	8.23E-01	1.04E+07	2.22E-01	7.73E+04	2.18E+04 3.08E+04
611		i	5	51		8.04E+06	0.00E+00	2.88E+00	9.22E-05	4.67E-04	9.64E-05 1.35E-04	1.72E+00 5.03E-04	1.25E+02 2.27E+05	0.00E+00 0.00E+00	5.13E+02 1.42E+00	2.47E+05 1.08E+02	3.10E+01		7.03E+06	6.71E-01	1.15E+07	2.21E-01	8.15E+04	3.67E+04
612		ţ	5	40		3.55E+05	0.00E+00	1.10E+01	2.58E-05	8.24E-01	3.37E-05	2.86E+00	3.44E+01	0.00E+00	1.91E+03	7.13E+05		2.39E+01 2.25E+01	1.33E+07 7.61E+06	8.62E-01 6.48E-01	1.34E+07 1.11E+07	2.35E-01 6.42E-02	8.90E+04 8.19E+04	3.72E+04 1.75E+04
613	Down-dip	1	5	22		7.99E+06 5.19E+06	0.00E+00 0.00E+00	2.88E+00 2.88E+00	6.84E-05 3.74E-05	8.07E-07	1.14E-04	6.07E-07	1.38E+08	0.00E+00	1.85E-03	1.36E-01	1.87E+01		9.78E+06	9.72E-01	9,99E+08	2.28E-02	7.55E+04	2.75E+04
615	Down-dip	1	5	19		2.79E+05	0.00E+00	1.10E+01	6.05E-06	6.97E-03 1.51E-01	5.13E-05 2.19E-05	3.21E-02 1.45E+00	3.18E+03 3.31E+01	0.00E+00 0.00E+00	2.13E+01 4.62E+02	2.74E+03 2.27E+05	8.73E+00		8.23E+06	8.31E-01	8.3BE+06	1.93E-01	6.82E+04	2.63E+04
618	Down-dip	1	5	30		3.20E+05	0.00E+00	1.10E+01	5.40E-08	5.62E-01	1.69E-05	3.63E+00	8.57E+00	0.00E+00	1.71E+03	7.69E+05	7.53E+00 6.59E+00	7.21E+00 6.30E+00	5.56E+06 5.95E+06	4.66E-01 4.23E-01	8.56E+06 1.14E+07	1.27E-01 5.26E-02	6.92E+04 8.31E+04	2.36E+04
617	Down-dip Down-dip	1	5 5	31 73		2.78E+05 2.51E+05	0.00E+00	1.10E+01	2.75E-06	2.11E-01	1.43E-05	4.51E+00	9.09E+00	0.00€+00	6.45E+02	4.17E+05	3.79E+00	3.72E+00	4.59E+06	4.13E-01	1.05E+07	7.43E-04	8.31E+04 7.77E+04	1.22E+04 8.39E+03
619	Down-dip	1	5	49		3.47E+05	0.00E+00 0.00E+00	1.10E+01 1.10E+01	8.16E-08 1.46E-08	1.49E-01 5.45E-01	5.65E-07 9.03E-08	6.26E+00 1.78E+01	3.13E-01 1.79E-02	0.00E+00	4.55E+02		1.27E-01	1.23E-01	2.97E+06	4.33E-01	9.55E+06	6.76E-02	7.38E+04	1.18E+04
620	Down-dip	1	5	58		4.38E+05	0.00E+00	1.10E+01	8.32E-10	1.11E+00	4.20E-09	2.62E+01	5.56E-04	0.00E+00 0.00E+00	1.66E+03 3.39E+03	1.10E+06 1.86E+06	1.97E-02 1.04E-03	1.89E-02 9.71E-04	3.90E+06 5.64E+06	1.78E-01 1.69E-01	1.23E+07	4.97E-02	8.63E+04	6.93E+03
621	Down-dip Down-dip	1	5	5 28		2.89E+05 4.42E+05	0.00E+00	1.10E+01	3.31E-10	1.80E-01	2.57E-09	9.12E+00	1.10E-03	0.00E+00	5.48E+02		5.01E-04		2.76E+06	1.76E-01	1.42E+07 8.79E+06	1.24E-01 4.59E-04	9.35E+04 7.03E+04	1.28E+04 2.98E+03
623	Down-dip	i	5	94		2.85E+05	0.00E+00 0.00E+00	1.10E+01 1.10E+01	9.96E-12 3.89E-05	3.95E-01 1.31E-01	6.78E-11 1.35E-04	2.19E+01 1.20E+00	1.45E-05 2.55E+02	0.00E+00 0.00E+00	1.21E+03	1.04E+06	1.51E-05		3.73E+06	2.11E-01	1.35E+07	1.81E-01	8.94E+04	1.66E+04
	Down-dip	1	5	79		4.21E+05	0.00E+00	1.10E+01	4.33E-05	6.42E-01	4.70E-05	2.28E+00	6.28E+02	0.00E+00	3.98E+02 1.96E+03	1.81E+05 6.74E+05	4.61E+01 4.23E+01	4.52E+01 4.00E+01	7.55E+06 9.80E+06	7.13E-01	1.15E+07	2.14E-01		
625	Down-dip Down-dip	1	5	19 31	_,	2.80E+05	0.00E+00 0.00E+00	1.10E+01	5.70E-06	1.70E-01	2.11E-05	1.73E+00	2,75E+01	0.00E+00	5.17E+02	2.60E+05	7.14E+00		5.64E+06	6.82E-01 4.56E-01	1.23E+07 8.96E+06	2.91E-02 1.14E-01	8.68E+04 7.11E+04	1.79E+04 2.29E+04
627	Down-dip	i	5	73		2.70E+05 2.58E+05		1.10E+01 1.10E+01	3.23E-06 6.21E-08	1.83E-01 1.56E-01	1.60E-06 4.41E-07	3.51E+00	1.27E+01	0.00E+00	5.57E+02	3.47E+05	4.40E+00	4.28E+00	4.54E+06	4.31E-01	9.81E+06	2.77E-05	7.49E+04	B.29E+03
628	Down-dip	1	5	58	0.00E+00	4.37E+05	0.00E+00	1.10E+01	1,64E-09	1.60E+00	6.89E-09	6.88E+00 2.67E+01	2.26E-01 8.25E-04	0.00E+00 0.00E+00	4.75E+02 4.89E+03	4.33E+05 2.30E+06	9.77E-02 1.90E-03		2.97E+06 6.62E+06	4.25E-01	9.80E+06	5.75E-02	7.48E+04	1.12E+04
629 630	Down-dip	1	5	58			0.00E+00	1.10E+01	9.12E-05	1.97E-01	2.58E-04	4.89E-01	5.64E+02	0.00E+00	6.01E+02	1.77E+05	1.00E+02	9.58E+01	1.37E+07	1.73E-01 7.72E-01	1.40E+07 1.54E+07	1.11E-01 1.79E-02	9.44E+04 9.84E+04	1.26E+04 2.17E+04
631	Down-dip		5	31 94		5.83E+05 7.99E+06	0.00E+00 0.00E+00	1.10E+01 2.88E+00	2.45E-05 7.83E-05		9.19E-05	4.40E-01	3.86E+02	0.00E+00	1.77E+02	7.91E+04		2.92E+01	6.26E+06	6.70E-01	8.71E+06	8.01E-05	6.90E+04	1.19E+04
632	Down-dip	1	5	44				2.88E+00	2.89E-05	1.72E-07 1.35E-07	2.16E-04 3.92E-05	1.75E-07 1.35E-07	5.29E+08 3.10E+08	0.00E+00 0.00E+00	5.25E-04 4.10E-04	4.30E-02 2.45E-02	2.27E+01 7.55E+00	2.23E+01 7.38E+00	1.08E+07 9.04E+06	9.93E-01	1.15E+07	1.98E-01		4.37E+04
633	Down-dip	1	5	19		2.92E+05	0.00E+00	1.10E+01	2.83E-06	3.09E-01	1.25E-05	4.86E+00	6.76E+00		9.41E+02	5.53E+05			5.75E+06	8.90E-01 3.75E-01	9.06E+06 1.14E+07	5.96E-06 4.66E-02	7.11E+04 8.12E+04	1.84E+04 1.75E+04
634	Down-dip Down-dlp	1	5 5	79 78		3.35E+05 2.57E+05	0.00E+00 0.00E+00	1.10E+01 1.10E+01	1.50E-06 1.75E-08	2.87E+00	1.71E-06	1.35E+01	3.50E-01	0.00E+00	6.77E+03	3.59€+06	1.25E+00	1.23E+00	7.80E+06	5.17E-01	1.14E+07	2.52E-06	9.13E+04	1.20E+04
636	Down-dip	1	5	73	-,	3.98E+05	0.00E+00	1.10E+01	2.03E-12	2.57E-01 2.11E-01	9.90E-08 1.11E-11	7.23E+00 1.45E+01	4.40E-02 4.64E-06		7.83E+02 6.43E+02	5.57E+05 7.06E+05	2.45E-02 3.27E-06		3.20E+06	2.58E-01	8.94E+06	1.17E-02	7.07E+04	5.81E+03
637	Down-dip	1	5	12		3.51E+05	0.00E+00	1.10E+01	9.52E-13	1.71E+00	2.31E-12	1.23E+01	4.38E-07		5.21E+03	2.50E+06	1.09E-06		2.78E+06 4.18E+06	3.28E-01 1.30E-01	1.15E+07 7.10E+06	7.17E-05 5.96E-08	8.19E+04 7.45E+04	6.72E+03 2.24E+03
638	Down-dip Down-dip	1	5 5	58 94		2.63E+06 7.99E+06	0.00E+00 0.00E+00	1.10E+01 2.88E+00	8.70E-05	2.82E-01	2.51E-04	7.81E-01	3.77E+02	0.00E+00	8.60E+02	2.56E+05	9.64E+01	9.51E+01	1.34E+07	7.47E-01	1.53E+07	1.37E-05	9.84E+04	1.90E+04
640	Down-dip	1	5	69		4.62E+06		2.88E+00	8.00E-05 2.45E-05	1.63E-07 1.04E-02	2.20E-04 4.88E-05	1.65E-07 3.82E-02	5.71E+0B 1.81E+03	0.00E+00 0.00E+00	4.99E-04 3.18E+01	4.07E-02 3.55E+03			1.09E+07	9.94E-01	1.15E+07	1.83E-01	8.18E+04	4.42E+04
641	Down-dip	1	5	19	0.00E+00	3.24E+05		1.10E+01	3.77E-06	3.46E-01		5.54E+00	B.05E+00	0.00E+00	1.05E+01	6.23E+05			7.84E+06 6.25E+06	8.20E-01 3.91E-01	8.08E+06 1.25E+07	9.61E-02 1.55E-02	6.42E+04 8.59E+04	1.81E+04
642 643	Down-dip Down-dip	1	5 5	44 31		8.00E+06 7.99E+06		2.88E+00 2.88E+00	1.84E-05		2,48E-05	2.71E-08	9.71E+08	0.00E+00	8.26E-05	4.97E-03	4.81E+00		8.68E+06	8.90E-01	8.67E+06	4.63E-06	6.83E+04	1.57E+04 1.85E+04
644	Down-dip	i	5	79		3.32E+05	0.00E+00	2.00E+00 1.10E+01	6.41E-06 1.99E-06	2.30E-08 2.73E+00	1.59E-05 2.19E-06	2.41E-08 1.27E+01	3.27E+08 4.84E-01	0.00E+00 0.00E+00	7.00E-05 B.33E+03	5.79E-03 3.39E+06	1.89E+00	1.85E+00	8.31E+06	9.46E-01	8.27E+06	1.07E-04	6,54E+04	1.63E+04
645	Down-dip	1	5	78	0.00E+00	2.53E+05	0.00E+00	1.10E+01	1.08E-07	2.65E-01		7.17E+00	2.64E-01		8.07E+02	5.71E+05	1.64E+00 1.51E-01		7.88E+06 3.49E+06	5.25E-01 3.07E-01	1.15E+07 9.60E+06	1.70E-06 9.13E-05	9.12E+04 7.42E+04	1.22E+04 5.85E+03
646	Down-dip	1	5 5	41 12		2.44E+05 3.01E+05	0.00E+00 0.00E+00	1.10E+01 1.10E+01	2.65E-08	1.12E-01	2.29E-07	6.82E+00	1.25E-01	0.00E+00	3.43E+02		4.42E-02		2.46E+06	2.23E-01	8.72E+06	2.19E-02	6.87E+04	5.85E+03 4.86E+03
64B	Down-dip	i	5	73		3.57E+05	0.00E+00	1.10E+01 1.10E+01	1.22E-08 5.58E-10		3.25E-08 4.59E-09	1.21E+01 1.38E+01	5.52E-03 1.37E-03		5.45E+03 6.35E+02	2.56E+06	1.42E-02		4.50E+06	1.85E-01	7.60E+06	1.79E-07	7.67E+04	3.43E+03
649	Down-dip	1	5	47		3.12E+05	0.00E+00	1.10E+01	2.62E-15	1.37E-01		7.72E+00	9.70E-09			6.88E+05 3.83E+05	9.40E-04 3.71E-09		2,86E+06 2,38E+06	3.50E-01 1.85E-01	1.17E+07 8.30E+06	6.44E-05 5.31E-02		7.25E+03
650	Down-dip Down-dip	1	5 5	58 19		6.60E+06		4.00E+00	7.66E-05		2.23E-04	1.07E-01	2.27E+03	0.00E+00	1.00E+02	1.39E+04	3.16E+01	2.84E+01	1.31E+07	8.31E-01	1.41E+07	4.60E-07	6.56E+04 9.28E+04	6.08E+03
652	Down-dip	i	5	94		7.11E+05 7.99E+06	0.00E+00 0.00E+00	1.10E+01 2.88E+00	2.01E-05 8.53E-05		7.66E-05 2.36E-04	1.81E+00 1.87E-07	8.12E+01 5.38F+08	0.00E+00 0.00E+00	6.79E+02				8.84E+06	5.53E-01	1.91E+07	1.45E-04	8.85E+04	1.88E+04
653	Down-dip	1	5	73	0.00E+00	3.95E+05	0.00E+00	1.10E+01	9.74E-06	1.15E-01	4.71E-05	1.93E+00	6.31E+01		5.67E+04 3.49E+02	4.60E-02 2.11E+05	2.47E+01 1.33E+01		1.11E+07 5.60E+06	9.94E-01 6.64E-01	1.17E+07 1.15E+07	1.58E-01 5.81E-05	8.29E+04	4.26E+04
654	Down-dip	1	5 5	79 69	0.00E+00 0.00E+00		0.00E+00	1,10E+01	2.25E-06		2.47E-06	1.21E+01	5.82E-01	0.00E+00	7,85E+03	3.18E+06	1.85E+00		7.B1E+06	5.29E-01	1.15E+07 1.15E+07		8.21E+04 9.10E+04	1.40E+04 1.23E+04
656	Down-dip Down-dip	1	5	44		7.99E+06 8.00E+06		2.88E+00 2.88E+00	6.21E-06 4.43E-06		1.12E-05 6.95E-06	9.08E-08 3.02E-10	9.14E+07 1.94E+10	0.00E+00 0.00E+00	2.77E-04	1.92E-02	1.75E+00	1.71E+00	8.34E+06	9.11E-01	8.33E+06	5.52E-02	6.57E+04	1.82E+04
657	Down-dip	1	5	78	0.00E+00	2.51E+05		1.10E+01	6.B4E-07			5.59E+00	1.94E+10 1.91E+00		9.20E-07 7.34E+02	6.00E-05 4.95E+05	1.16E+00 9.43E-01	1.13E+00 9.24E-01	8.16E+06 3.94E+06	8.90E-01 3.86E-01	8.14E+06 9.96E+06	2.97E-06	6.43E+04	1.93E+04
658	Down-dip	1	5 5	12 41		2.44E+05	0.00E+00	1.10E+01	6.63E-07	1.32E+00	1.64E-06	6.79E+00	4.36E-01	0.00E+00	4.03E+03	1.75E+06	7.64E-01		4.64E+06	3.86E-01	9.96E+06 7.63E+06	1.06E-05 9.80E-07	7.57E+04 7.37E+04	7.37E+03 5.59E+03
660	Down-dip	1	5	56		2.52E+05 2.45E+05		1.10E+01 1.10E+01	1.03E-07 4.93E-09			7.47E+00	4.36E-01			3.93E+05	1.71E-01			2.67E-01	9.62E+06	8.44E-03	7.42E+04	5.35E+03
661	Up-dlp	1	1	58	3.00E+05	2.92E+05	0.00E+00	1.10E+01	5.21E-09		3.29E-08 2,76E-08	5.14E+00 1.39E+01	2.23E-02 6.50E-03	0.00E+00 0.00E+00	3.90E+02 1.71E+03	3.40E+05 1.05E+06	7.58E-03 6.85E-03		2.47E+06 1.01E+07	3.93E-01	8.03E+06	6.46E-06	6.36E+04	6.29E+03
662	Up-dip Ua-dia	1	1	19 94		2.70E+05	0.00E+00	1.10E+01	9.23E-08	4.27E-01	3.41E-07	5.11E+00	1.69E-01	0.00E+00	1.30E+03	6.65E+05	1.13E-01		8.05E+06	1.81E-01 4.57E-01	3.73E+06 4.22E+06	1.70E-01 1.42E-01	1.18E+05 6.78E+04	2.03E+04 2.43E+04
664	Up-dip	í	í	58		3.77E+05 4.14E+05	0.00E+00 0.00E+00	1.00E+01 1.10E+01	2.74E-08 3.16E-10			1.26E+01	1.93E-02		3.54E+03	1,49E+06	2.88E-02	2.88E-02	1.09E+07	6.29E-01	5.83E+06	2.33E-01	8.03E+04	3.56E+04
665	Up-dlp	1	1	28	4.24E+05	4.14E+05		1.10E+01	5.28E-11			2.49E+01 2.06E+01	1.63E-04 6.24E-05		4.51E+03 1.77E+03	2.36E+06 1.09E+06	3.84E-04 6.79E-05	3.83E-04 6.52E-05	1.39E+07 1.31E+07	1.55E-01	6.18E+06	1.37E-01	9.31E+04	1.34E+04
666	Up-dip	1	1	30				1.10E+01	1.65E-11	1.99E+00	4.48E-11	1.43E+01	6.73E-06	0.00E+00	6.07E+03	2.84E+06	1.91E-05			1,99E-01 3,99E-01	3.98E+06 6.46E+06	1.95E-01 5.31E-02	8.82E+04 8.40E+04	1.75E+04 1.20E+04
667	Up-dip Up-dip	1	1	19 60	3.66E+05 . 3.21E+05 .			1.10E+01 1.10E+01	2.13E-10 4.46E-11			1.56E+01	1.66E-04		2.94E+03	1.58E+06	2.63E-04	2.59E-04	1.14E+07	3.73E-01	5.18E+06	4.66E-02	8.13E+04	1.75E+04
669	Up-dip	i	i	30	4.11E+05	3.40E+05		1.10E+01				1.02E+01 1.47E+01	1.31E-04 9.03E-07			5.07E+05 2.89E+06	6.63E-05 2.61E-06		9.48E+06 1.04E+07	1.98E-01	2.4BE+06	6.36E-02	7.34E+04	1.02E+04
670	Up-dip	1	1	94	4.08E+05	7.99E+06	0.00E+00	1.10E+01	2.23E-12	1.38E+00	6.26E-12	1.81E+01					2.55E-06	2.49E-06		4.39E-01 9.94E-01	6.46E+06 5.79E+06	4.83E-02 1.91E-01	8.35E+04 8.30E+04	1.25E+04 4.39E+04
671	Up-dip Up-dip	1	1	30 30		3.53E+05 3.67E+05	0.00E+00 0.00E+00	1.10E+01 1.10E+01				1.49E+01	1.92E-07				5.62E-07	5.23E-07	1.04E+07	4.54E-01	6.47E+06	4.60E-02	8.36E+04	1.27E+04
673	Up-dip	i	2	30				2.88E+00	9.01E-18 6.36E-05							3.00E+06 6.04E+02				4.67E-01	6.48E+06	4.18E-02	8.43E+04	1.28E+04
674	Up-dip	1	2						5.97E-05	0.00E+00	1.14E-04	0.00E+00		0.00E+00				1.6/£+01 1.59E+01		2.20E-01 7.21E-01	1.14E+07 1.06E+07	5.35E-01 9.15E-01		5.15E+04
675	Up-dip	1	2	94 🕴	8.00€+06	2.53E+05	9.85E+06	2.88E+00	6.05E-05	7.89E-07	1.20E-04	1.03E-06	7.84E+07	1.21E-06	2.41E-03			1.64E+01		4.65E-01	9.70E+06	8.08E-01	'	8.33E+04 6.88E+04

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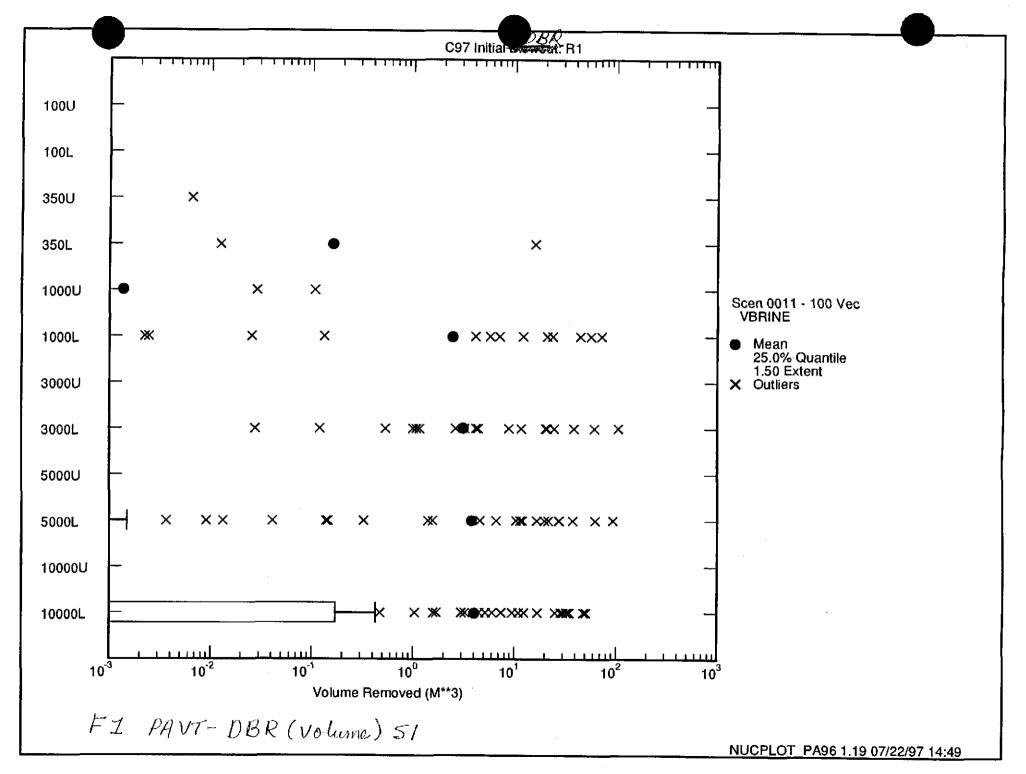
					Excepted																						
	•	•	•	•	Waste Porgelly		 Residual Brins Sat. (kaction) 	Crushed Panel Height (m)		Up-dip Avg	Down-dip Avg Pressure (Pe)	Down-dip Avg	DRZ Parasity	Permeability	Ball Pille Porpally	Salt Pillur Permeability	intrusion Time	Skin factor	Well Productivity	BC well Sand		Castle	Casile Reserveir	Up dip Briga Relativa	Up din Gas Flataire	Down dip Brine Relative	Down dip Gree Relative
					(fraction)		,			our (second	revalue (re)	Sat (raction)	(Fraction)	(m^2)	(Fraction)	(nt^2)	(Years)	Diviti (acux	Index (1/Pa)	(uv,5)	acids released (m^2)	Pressure (Pa)	Permeability	Permemberly	Permeability	Permenbility	Permanbility
No.	, ID	Replic.	Scen.	Vector				HEIGHT	PRESPAN2	BSATPAN2	PRESPANA	BSATPAN4	POROSITY	PERM_X	POROSITY	PERM X	INTO THE	SKIN	WELLPI	0014 01410	AREA_TOT		(m*2)	(fraction)	(fraction)	[kaction]	(fraction)
676 677	Up-dip Up-din	1	2	78	5.84E-01	4.93E-02		1.44E+00	1.04E+07	0.44E-01		9.44E-01	9.79E-02	2.46E-15	1.04E-01	2.46E-15	5.50E+02	-1.06F+00		8.32E-17	6.28E-01	1.40E+07	1 07F-12	7.79E-01	KRGZ	KRW4	KRG4
678	Up-dip	1	2	45 22	5.72E-01 5.70F-01	5.05E-02 2.51E-02	2.04E-01 8.22E-02		9.55E+06	9.85E-01	9.61E+06	9.84E-01	6.78E-02	5.13E-14	8.12E-02	5.13E-14	5.50E+02	-9.31E-01	1.22E-13	1.74E-15	4.89E-01	1.32E+07	4.57E-13	9.30E-01	7 96E-07 0.00E+00	7.78E-01 9.27E-01	8.42E-07
679	Up-dlo	i	2	79	5.63E-01	1.23E-01		1.40E+00 1.37E+00	9.43E+06 6.97E+06	9.12E-01 6.30E-01	9.42E+06 8.98E+06	6.34E-01 6.96E-01	1.21E-01	7.41E-14	1.33E-01	7.41E-14	5.50E+02	-1.37E+00		1.74E-13	1.17E+00	1.30E+07	1.59E-12	6.90E-01	5.75E-04	1.52E-01	8.15F-02
680	Up-dlp	1	2	44	5.69E-01	1.12E-01	1.61E-02	1.39E+00	9.40E+06	0.30E-01	9.40E+06	8.84E-01	1.61E-01 1.15E-01	2.57E-13 1.18E-13	1.81E-01 1.23E-01	2.57E-13	5.50E+02	-1.10E+00		1.51E-16	6.89E-01	1.22E+07	4 37E-15	3.23E-02	1.78E-01	7.91E-02	7.45E-02
681	Up-dlp	1	2	39	5.78E-01	1.50E-01	2.98E-01	1.42E+00	1.01E+07	8.47E-01	9.85E+06	8 19F-01	1.49E-02	3.02E-15	2.68E-02	1.18E-13 3.02E-15	5.50E+02 5.50E+02	-1.17E+00 -1.23E+00		3.80E-15	7.83E-01	1.29E+07	1.12E-12	6.30E-01	1.08E-07	6.31E-01	1.05E-07
682	Up-dip	1	2	52	5.73E-01	3.68E-02	4.49E-01	1,41E+00	9.36E+06	9.60E-01	1.07E+07	9.60E-01	9.67E-02	1.70E-15	1.17E-01	1.70E-15	5.50E+02	·9.48E-01	1,39E-13 1,24E-13	2.40E-13 4.17E-14	B.82E-01 5.07E-01	1.34E+07	1.78E-13	4.03E-01	3.76E-07	3.33E-01	2.92E-04
683 684	Up-dip Up-dip	!	2	7 33	5.81E-01	7.76E-03	3.12E-01	1.37E+00	8.82E+06	9.90E-01	8.88E+06	9.90E-01	1.28E-01	2.29E-13	1,49E-01	2.29E-13	5.50E+02	-6.15E-01	1.07E-13	7.94E-14	2.60E-01	1.43E+07 1.24E+07	2.63E-13 1.35E-12	7.57E-01 9.46E-01	4.27E-07 9.52E-08	7.56E-01	4.64E-07
685	Up-dip	;	2	15	5.65E-01	1.31E-01 4.22E-02	1.22E-01 5.21E-01		9.26E+06 9.15E+06	8.65E-01	9.22E+06	3.22E-01	2.74E-02	1.12E-14	3,63E-02	1.12E-14	5.50E+02	-1.24E+00	1.36E-13	8.32E-13	9.16E-01	1.15E+07	1.26E-13	5.40E-01	3.23E-07	9.49E-01 4.22E-03	4.16E-08 4.79E-01
686	Up-dip	i	2	2	5.62F-01	6 22E 02		1.38E+00	9.15E+06 8.95E+06	9.52E-01 9.16E-01	9.13E+06 B.91E+06	5.74E-01 9.16E-01	4.81E-02 1.51E-01	1,32E-14	6.37E-02	1.32E-14	5.50E+02	-9.48E-01	1.21E-13	1.32E-14	5.06E-01	1.06E+07	4.47E-13	6.75E-01	4.76E-06	3.08E-04	7.48E-01
687	Up-dip	1	2	55	5.54E-01	7.03E-02			8.42E+06	9.27E-01	8.36E+06	4,56E-01	8.29E-02	4.47E-14 8.71E-15	1.65E-01 1.01E-01	4.47E-14 8.71E-15	5.50E+02 5.50E+02	-1.29E+00	1.37E-13	5.01E-14	9.98E-01	1.24E+07	7.24E-11	5.71E-01	1.19E-07	5.71E-01	1.25E-07
688	Up-dip	1	2	40	5.85E-01	1.02E-01	3.54E-01	1.45E+00	1.06E+07	4.83E-01	1,06E+07	3.71E-01	1.22E-01	1.51E-13	1.27E-01	1.51E-13	5.50E+02	-8.68E-01 -1.32E+00	1.15E-13 1.47E-13	6.03E-12 3.02E-13	4.31E-01 1.07E+00	1.18E+07	1.62E-11	6.88E-01	1.52E-07	9.84E-03	4.03E-01
689 690	Up-dip	1	2	51	6.10E-01	1.34E-01	3.63E-01	1,54E+00	1.27E+07	4.24E-01	1.27E+07	5.63E-01	1.75E-01	2.36E-13	1.62E-01	6.17E-14		-1.16E+00		1,00E-12	7.77E-01	1.59E+07	2.57E-11 6.92F-12	2.66E-03 1.67E-04	5.30E-01 7.53E-01	1.67E-06	9.34E-01
691	Up-dip Up-dip	1	2	91 31	5.60E-01 5.82E-01	5.46E-02 5.28E-02		1.38E+00 1.44E+00	8.76E+06	3.62E-01	8.76E+06	4.80E-01	1.74E-01	5.01E-15	1.95E-01	5.01E-15	5.50E+02	-7.73E-01		2.82E-13	3.57E-01	1.18E+07	4.17E-14	9.00E-05	8.20E-01	1.40E-02 6.01E-03	2.86E-01 4.72E-01
692	Up-dip	i	2	58	6.01E-01	2 96F-02	1.14E-01	1.44E+00	1.03E+07 1.19E+07	1.31E-01 1.72E-01	1.04E+07 1.19E+07	9.39E-01 1.84E-01	6.71E-02	1.66E-15	8.12E-02	1.66E-15	5.50E+02			3.31E-14	9.73E-01	1.40E+07	6.31E-13	7.44E-05	8.33E-01	7.B1E-01	1.29E-06
693	Up dip	1	2	28	5.95E-01	9.72E-02	1.79E-01	1.48E+00	1.15E+07	1.96E-01	1.12E+07	1.84E-01	1.87E-01	1.45E-16 5.28E-17	1.92E-01	1.45E-16 4.79E-17		-1.18E+00		3.09E-15	8.11E-01	1.26E+07	1.07E-13	4.42E-05	8.59E-01	8.83E-05	B.29E-01
694	Up-dip	1	2	94	5.83E-01	4.58E+03	1.85E-01	1.44E+00	1,22E+07	9.91E-01	1.22E+07	6.96E-01	1.92E-01	7.82E-15	1.93E-01	6.31E-15	5.50E+02 7.50E+02	-1.08E+00 -1.29E+00		9.55E-12 9.77E-10	6.64E-01	1.475+07	9.55€-14	6.66E-07	9.51E-01	2,92E-02	2.41E-01
695	Up-dip	1	2	7B	5.89E-01	4.93E-02		1.46E+00	1.27E+07	9.46E-01	1.27E+07	9.46E-01	1.19E-01	4.24E-14	1.03E-01	2.46E-15		-1.06E+00		8.77E-18 8.32E-17	9.95E-01 6.28E-01	1.31E+07 1.40E+07	1.78E-12 1.07E-12	9.59E-01 7.85E-01	2.93E-07	1,78E-01	7.44E-02
696 697	<i>Up-dlp</i> Up-dlo	1	2	44 45	5.78E-01	1.12E-01	1.81E-02	1.12E+00	J. 16E+07	8.85E-01	1.16E+07	8.85E-01	1.24E-01	1.52E-13	1.21E-01	1.18E-13	7.50E+02	-1.17E+00	1.35E-13	3.80E-15	7.83E-01	1.40E+07	1.0/E-12 1.12E-12	6.31E-01	3.35E-07 7.78E-08	7.85E-01 6.31F-01	3.39E-07 7.72E-08
698	Up-dip	1	2	15	5.67E-01 5.72E-01	5.05E-02 4.22E-02	2.04E-01 5.21E-01	1.39E+00 1.40E+00	1.08E+07 1.13E+07	9.76E-01 7.53E-01		9.75E-01 7.95E-01	7.38E-02	5.13E-14	8.21E-02	5.13E-14	7.50E+02	9.31E-01	1.21E-13	1.74E-15	4.89E-01	1.32E+07	4.57E-13	8.92E-01	0.00E+00	8.89E-01	0.00E+00
699	Up-dlp	- í	2	69	5.75E-01	8.98E-02	4.08E-01	1.41E+00	1.15E+07	7.53E-01 9.10E-01		7.95E-01 9.13E-01	5.56E-02 7.49E-02	1.32E-14 1.26E-14	6.27E-02 8.13E-02	1.32E-14 1.26E-14	7.50E+02	-9.48E-01	1.23E-13	1.32E-14	5.06E-01	1.06E+07	4.47E-13	6.94E-02	1.44E-01	1.27E-01	7.61E-02
700	Up-dip	1	2	52	5.71E-01	3.68E-02	4.49E-01	1.40E+00	1.12E+07	9.60E-01		9.60E-01	1.04E-01	1.70E-15	8.13E-02 1.17E-01	1.26E-14 1.70E-15	7.50E+02 7.50E+02	-1.29E+00 -9.48E-01	1.42E-13 1.23E-13	9,33E-15 4,17E-14	9.99E-01 5.07E-01	1.42E+07 1.43E+07	4.07E-13	5.42E-01	4.53E-09	5.58E-01	0.D0E+00
701	Up-dip	1	2	2	5.65E-01	8.22E-02	4.02E-01	1.38E+00	1.07E+07	9.16E-01	1.08E+07	9.16E-01	1.58E-01	4.47E-14	1.64E-01	4.47E-14		-1.29E+00		5.01E-14	9.98E-01	1.43E+07 1.24E+07	2.63E-13 7.24E-11	7.57E-01 5.71E-01	4.04E-07 9.13E-08	7.57E-01	4.00E-07
702	Up-dip Up-dip	1	2	39 10	5.73E-01 5.46F-01	1.50E-01	2.98E-01	1.41E+00	1.13E+07	8.47E-01		B.47E-01	1.90E-02	3.02E-15	2.71 E-02	3.02E-15		-1.23E+00		2.40E-13	8.82E-01	1.34F+07	1.78E-13	4.04E-01	9.13E-08 3.35E-07	5.71E-01 4.04E-01	9.05E-08 3.28E-07
704	Up-dip	i	2	19	5.49E-01	3.17E-02 1.42E-01	1.73E-01 2.97E-02	1.32E+00 1.33F+00	9.38E+06 9.51E+06	9.65E-01 7.93E-01		6.55E-01	4.85E-02	3.72E-14	6.69E-02	3.72E-14		·1.33E+00	1.35E-13	1.86E-16	1.08E+00	1.09E+07	1.35E-11	8.52E-01	1.31E-07	1.36E-01	8.91E-02
705	Up-dip	i	2	24	5.40E-01	9.01E-02	1.37E-01	1.30E+00	8.91E+06	9.08E-01	9.62E+06 9.00E+06	8.51E-01 9.08E-01	1.89E-01 1.85E-01	1.41E-15 2.82E-13	2.04E-01 2.07E-01	1.41E-15 2.82E-13	7.50E+02	1.23E+00		2.00E-16	8.94E-01	1.18E+07	1.45E-12	4.13E-01	7.78E-04	5.41E-01	7.43E-07
706	Up-dip	1	2	18	5.46E-01	1.06E-01	3.40E-01		9.32E+06	8.92E-01	9.35E+06	7.80F-01	4.95E-02	3.31E-14	6.82E-02	3.31E-14		-1.29E+00 -1.09E+00		2.63E-14	9.94E-01	1.09E+07	7.41E-13	6.59E-01	2.82E-08	6.59E-01	2.79E-08
707	Up-dip	1	2	30	5.42E-01	1.16E-01	4.16E-02		9.07E+06	8.80E-01	9.16E+06	8.80E-01	2.61E-02	2.75E-14	4.23E-02	2.75E-14	7.50E+02	-6.49E-01	1.22E-13 1.04E-13	6.17E-16 2.19E-13	8.69E-01 2.79E-01	1.05E+07 1.34E+07	5.25E-12 1.59E-13	5.17E-01	1.10E-07	2.24E-01	1.38E-02
708	Up-dip Un–dia	1	2	48 35	5.40E-01	1.02E-01	2.11E-01		8.90E+06	8.42E-01		8.95E-01	4.55E-02	7.76E-14	5.88E-02	7.76E-14		-1.29E+00	1.31E-13	2.19E-15	1.01E+00	1.03E+07	3.80F-12	6.10E-01 4.38E-01	2.22E-07 8.82E-04	6.10E-01 5.91E-01	2.20E-07 8.41E-08
710	Up-dip	1	2	31	5.42E-01 5.77F-01	9.57E-02 5.28E-02	4.39E-01 5.93E-02		9.09E+06 1.17E+07	9.03E-01 1.11E-01	9.17E+06 1.17E+07	9.03E-01	5.00E-02	7.24E-15	6.29E-02	7.24E-15	7.50E+02	-8.97E-01	1.13E-13	1.38E-13	4.57E-01	1.12E+07	3.98E-11	4.94E-01	1.05E-07	4.94E-01	1.04E-07
	Up-dip	Ì	2	28	5.49E-01	9.72E-02	1.79E-01		9.52E+06	2.26E-01		9.40E-01 8.90E-01	7.33E-02 2.02E-01	1.66E-15 5.28E-17	8.22E-02 2.21E-01			-1-27E+00	1.42E-13	3.31E-14	9.73E-01	1.40E+07	6.31E-13	2.22E-05	8.80E-01	7.82E-01	1.13E-06
712	Up-dip	1	2	58	5.90E-01	2.96E-02	1.14E-01		1.29E+07	1.58E-01	1.28E+07	1.71E-01	1.96E-01	1.67E-16	1.97E-01			-1.08E+00 -1.18E+00	1.23E-13 1.41E-13	9.55E-12 3.09E-15	6.64E-01	1.45E+07	9.55E-14	2.55E-05	8.66E-01	5.88E-01	9.58E-06
713	Up-dip	1	2	79	5.70E-01	1.23E-01	3.88E-01		1.11E+07	4.12E-01		7.76E-01	1.67E-01	2.57E-13	1.78E-01			-1.10E+00		1.51E-16	8.11E-01 6.89E-01	1.26E+07 1.23E+07	1.07E-13 4.37E-15	1.53E-05 6.18E-06	8.94E-01 9.00E-01	4.09E-05 1.86E-01	8.62E-01
714	Up-dip Un-dip	1	2	78	5.95E-01 5.84E-01	4.93E-02 4.58E-03	1.51E-01 1.85E-01	1.48E+00	1.57E+07	6.49E-01			2.78E-01	6.27E-10	1.02E-01	2.46E-15		-1.06E+00	1.36E-13	8.32E-17	6.28E-01	1.40E+07	1.07E-12	1.39E-01	7.87E-02	1.86E-01 5.18E-01	1.38E-02 2.25E-03
716	Up-dip	í	2	24	5.78E-01	9.01E-02	1,37E-01	1.44E+00 1.42E+00	1.46E+07 1.40E+07	9.95E-01 9.08E-01	1.47E+07 1.41E+07	9.95E-01	2.24E-01 1.94E-01	3.88E-13 4.31E-13	1.93E-01	6.31E-15		-1.29E+00	1.44E-13	9.77E-16	9.95E-01	1.31E+07	1.78E-12	9.75E-01	2.34E-09	9.75E-01	2.24E-09
717	Up-dip	t	2	45	5.65E-01	5.05E-02	2.04E-01	1.38E+00	1.29E+07	9.49E-01		9.08E-01 9.49F-01	8.38E-02	4.31E-13 5.57E-14	1.90E-01 8.25E-02			-1.29E+00 -9.31F-01	1.42E-13	2.63E-14	9.94E-01		7.41E-13	6.60E-01	1.82E-08	6.60E-01	1.81E-08
718	Up-dip	1	2	44	5.73E-01	1.12E-01	1.61E-02	1.41E+00	1.36E+07	5.27E-01	1.37E+07	8.86E-01	1.80E-01	5.30E-12	1.22E-01	1.18E-13		-1.17E+00	1.20E-13 1.34E-13	1.74E-15 3.80E-15	4.89E-01 7.83E-01	1.32E+07 1.29E+07	4.57E-13	7.81E-01	3.41E-09	7.81E-01	3.38E-09
719	Up-dip	1	2	52 69	5.63E-01	3,68E-02	4.49E-01	1.38E+00	1.28E+07	9.60E-01		9.60E-01	1.13E-01	1.70E-15	1.19E-01	1.70E-15		-9.48E-01	1.21E-13	4.17E-14	5.07E-01		1.12E-12 2.63E-13	8.92E-02 7.57E-01	1.02E-01 3.95E-07	6.34E-01 7.58E-01	2.17E-08 3.73E-07
720 721	Up-dip Up-dip	1	2	39	5.70E-01 5.56E-01	8,98E-02 1,50E-01	4.08E-01 2.98E-01	1.40E+00 1.35E+00	1.33E+07 1.21E+07	9.09E-01			8.52E-02	1.65E-14	8.23E-02	1.26E-14		-1.29E+00	1.40E-13	9.33E-15	9.99E-01	1.42E+07	4.07E-13	5.41E-01	1.30F-08	5.41E-01	1.29E-08
722	Up-dip	i	2	2	5.36F-01	8.22E-02	4.02E-01	1.33E+00 1.29E+00	1.21E+07	8.47E-01 9.16E-01		8.47E-01 9.16E-01	2.24E-02 1.67E-01	3.02E-15	2.83E-02			-1.23E+00	1.32E-13	2.40E-13	8.82E-01	1.35E+07	1.78E-13	4.03E-01	3.55E-07	4.04E-01	3.51E-07
723	Up dlp	1	2	100	5.34E-01	1.14E-01	3.43E-01	1.29E+00	1.04E+07	8.84E-01	1.05E+07		7.15E-02	4.47E-14 9.12E-16	1.75E-01 8.43E-02			-1.29E+00 -1.26E+00		5.01E-14	9.98E-01	1.25E+07	7.24E-11	5.71E-01	1.15E-07	5.71E-01	1.00E-07
724	Up dlp	,	2	35	5.34E-01	9.57E-02	4.39E-01	1,29E+00	1.04E+07	9.03E-01	1.05E+07	9.03E-01	5.65E-02	7.24E-15	6.40E-02			-8.97E-01	1.11E-13	2.51E-14 1.38E-13	9.43E-01 4.57E-01	1.25E+07 1.12F+07	1.29E-13 3.98E-11	4.86E-01	1.30E-07	4.86E-01	1.27E-07
725 726	Up-dlp	!	2	30	5.26E-01	1.16E-01	4.16E-02		9.77E+08				2.94E-02	2.75E-14	4.38E-02			6.49E-01	f.00E-13	2.19E-13	2.79E-01	1.34E+07		4.94E-01 6.19E-01	1.08E-07 1.55E-09	4.94E-01 6.19E-01	1 07E-07 1.54E-09
726	Up-dip Up-dip	i	2	97	5.86E-01 5.15E-01	3.17E-02 8.37E-02	1.73E-01 4.34E-01		-	4.19E-01 9.04E-01		7.92E-01	7.28E-02	1.12E-13	6.10E-02			-1.33E+00	1.48E-13	1.86E-16	1.08E+00	1.09E+07	1.35E-11	1.13E-02	4.12E-01	3.42E-01	1.71E-02
728	Up-dip	i	2	19	5.75E-01	1.42E-01	2.97E-02	1.41E+00	1.37E+07	3.21E-01		9.12E-01 6.53E-01	1.48E-01 2.05E-01	5.63E-16 8.99E-15	1.706-01 1.93E-01	5.62E-16 1.41E-15		-8.88E-01	1.06E-13	4.57E-13	4.49E-01		3.02E-11	5.03E-01	2.77E-05	5.37E-01	9.93E-07
729	Up-dip	1	2	53	4.96E-01	4.46E-02	2.52E-01			5.28E-01		9.33E-01	1.56E-01	9.13E-18	1.93E-01			-1.23E+00 -5.58E-01	1.38E-13 9.15E-14	2.00E-16 1.38E-12	8.94E-01	1.18E+07	1.45E-12	1.17E-02	3.49E-01	5.44E-01	4.12E-07
730	Up-dip	Ţ	2	18	5.87E-01	1.06E-01	3.40E-01		1.49E+07		1.49E+07	8.93E-01	7.53E-02	1.16E-13	6.20E-02	3.31E-14		-1.09E+00	9.15E-14 1.34E-13	7.38E-12 8.17E-16	2.32E-01 6.69F-01	1.33E+07 1.05E+07	4.57E-12 5.25E-12	2.52E-02 3.55E-04	2.94E-01	7.05E-01	5.75E-05
731 732	Up-dip Up-dip	1	2	60 47	5.19E-01 4.98F-01	6.13E-02	4.70E-02		9.41E+06			7.87E-01	1.94E-01	6.05E-18	2.06E-01	5.75E-18	2.00E+03	1.17E+00	1.19E-13	8.61E-13	7.91E-01	1.30E+07	2.34E-14	4.47E-05	7.16E-01 8.53F-01	5.19E-01 3.92E-01	4.54E-08 7.91E-03
	Up-dip	i	2	94	4.98E-01 5.83F-01	6.75E-02 4.58E-03	1.61E-01 1.85E-01	1.20E+00 1.44E+00	8.13E+06 1.44E+07			5.57E-01 9.95E-01	1.48E-01	6.92E-18	1.64E-01	6.92E-18		1.09E+00	1.11E-13	2.19E-16	6.75E-01	1.20E+07	1.55E-12	3.78E-09	9.89E-01	6.24E-02	1.61E-03
734	Up-dip	1	2	24	5.77E-01	9.01E-02	1.37E-01			9.08E-01		9.95E-01 9.08E-01	2.21E-01 1.95E-01	2.51E-13 4.73E-13	1.93E-01 1.90E-01			1.29E+00	1.44E-13	9.77E-16	9.95E-01	1.31E+07	1.78E-12	9.75E-01	2.65E-09	9.75E-01	2.53E-09
735	Up-dip	1	2	45	5.72E-01	5.05E-02	2.04E-01	1.40E+00				9.49E-01	8.92E-02	1.01E-13	8.11E-02	2.82E-13 5.13E-14	4.00E+03	-1.29E+00 -9.31F-01	1.42E-13 1.22E-13	2.63E-14 1.74E-15	9.94E-01 4.89E-01	1.09E+07 1.32E+07	7.41E-13	6.60E-01	1.99E-08	6.60E-01	1.97E-08
736	Up-dip	1	2	69	5.79E-01	8.98E-02	4.08E-01	1.43E+00		9.09E-01			9.47E-02	4.77E-14	8.07E-02			-1.29E+00	1.43E-13	9.33E-15	4.89E-01 9.99E-01		4.57E-13 4.07E-13	7.82E-01 5.41E-01	2.64E-09 7.74E-09	7.82E-01	2.63E-09
737 738	Up-dip Up-dio	1	2	100	5.64E-01 5.38E-01	1.12E-01 1.14E-01	1.61E-02 3.43E-01	1.38E+00 1.30E+00		4.04E-01		8.87E-01	1.50E-01	7.98E-13	1.25E-01	1.18E-13	4.00E+03	-1.17E+00	1.31E-13	3.80E-15	7.83E-01		1.12E-12		7.74E-09 2.29E-01	5.41E-01 6.39E-01	7.70E-09 2.57E-10
739	Up-dip	i	2	52	5.30E-01	3.68E-02	3.43E-01 4.49E-01	1.30E+00 1.28E+00		8.83E-01 9.58E-01		9.60E-01	7.21E-02 1.10E-01	9.12E-16				-1.26E+00	1.29E-13	2.51E-14	9.43E-01	1.25E+07	1.29E-13	4.86E-01	1.39E-07	4.86E-01	1.36E-07
740	Up-dip	1	2	1	5.20E-01		2.56E-01						1.10E-01 6.96E-02	1.70E-15 7.24E-16	1.28E-01 8.79E-02				1.12E-13		5.07E-01	1.43E+07	2.63E-13	7.43E-01	2.31E-06	7.56E-01	4.65E-07
741	Up-dip	1	2	30	5.19E-01	1.16E-01	4.16E-02						2.81E-02	2.75E-14	4.45E-02			-1.28E+00 -6.49E-01	1.25E-13 9.87E-14	1.66E-14 2.19E-13		1.25E+07	7.08E-14	5.84E-01	1.29E-07	5.84E-01	1.26E-07
	Up-dip	1	2	39	5.25E-01	1.50E-01	2.98E-01	1.27E+00	9.73E+06	8.4BE-01	9.82E+06	8.48E-01	1.60E-02	3.02E-15	3.02E-02			-0.49E-01 -1.23E+00	9.87E-14 1.24E-13	2.19E-13 2.40E-13	2.79E-01 B.82E-01	1.34E+07 1.35E+07	1.59E-13 1.78E-13	6.19E-01 4.05E-01	1.39E-09 2.05E-07	6.19E-01	1.33E-09
	Up-dip Up-dip	1	2	78 35	6.04E-01	4.93E-02	1.51E-01						2.85E-01	1.00E-09		2.46E-15	4.00E+03	1.06E+00	1.39E-13	8.32E-17		1.40E+07	1.78E-13 1.07E-12	4.05E-01 6.78E-03	2.05E-07 4.67E-01	4.05E-01 7.56E-02	2.02E-07
	up-dip Up-dip	i	2	35 86	5.05E-01 4.95E-01	9,57E-02 6,86E-02	4.39E-01 3.61E-02		B.72E+06 B.29E+06				5.26E-02	7.24E-15	6.80E-02			8.97E-01	1.05E-13	1.38E-13	4.57E-01	1.12E+07	3.98E-11	4.94E-01	1.28E-07	4.94E-01	1.4BE 01 1.27E-07
	Up-dip	1	2	19	5.96E-01	1.42E-01	3.01E-02 2.97E-02					9.18E-01 8.34E-01	1.56E-01 2.54E-01	3.04E-17 2.28E-11	1.79E-01 1.83E-01			1.26E+00	1.18E-13	4.07E-13			2.04E-11	9.02E-04	6.72E-01	7.21E-01	5.50E-06
747	Up-dlp	1	2	60	4.91E-01	6,13E-02	4.70E-02			*.**			1.99E-01	6.05E-18	2.18E-01			1.23E+00 -3.73E-01	1.46E-13 B.55E-14	2.00E-16 6.61E-13		1.18E+07	1.45E-12	5.19E-05	8.33E-01	4.99E-01	4.15E-05
	Up-dip	!	2	53	4.97E-01	4.46E-02	2.52E-01			2.53E-01	8.18E+06	8.36E-01	1.57E-01	9.13E-18					1.17E-13	6.61E-13 1.38E-12			2.34E-14 4.57E-12	3.84E-06	9.25E-01	3.88E-01	8.24E-03
	Up-dip Up-dip	1	2	94	6.80E-01	4.58E-03	1.85E-01						2.15E-01	9.08E-14		6.31E-15	1.00E+04		1.43E-13				1.78E-12	1.38E-11 9.75E-01	9.98E-01 3.88E-09	4.00E-01 9.75E-01	7.88E-03 3.63E-09
130	ob-ob	•	-	70	5.85E-01	5.05E-02	2.04E-01	1.45E+00	1.45E+07	9.49E-01	1.46E+07	9.49E-01	1.11E-01	0.10E-13	7.87E-02		1.00E+04		1.26E-13					7.82E-01	1.60E-09	7.82F-01	1.59E-09
																										01	

						Down-dio																		
					Up-dip Flowing Bottom-hole	Flowing	BC well Injection	Blowout	Brine Rate	Gau Rate (raf	Max Grice	May Guy Rutu	Produced Liquid/Ges	Cum Brine from Boundary	One Date	· Com Gas	Cum Brine	Cum Brine	Avg Brine	Avg Brine Saturation	Avp Britis	Avg Brime Saturation	Total Excavated	Total
					Pressure (Pa)	Pressure (Pal	Diameter (Da)	Duration Days)	(m*3/s)	m^3/a)	Rate (m/3/s)	(rel m/3/s)	Ratio (m^3/s /	Condition Wall		Produced (ref	Produced	Paleases	President Panel 5 (Pa)	Panel 5	Pressure Panel 0 (Pa)	Panel0	Waste Pore	Excavaled
No.	ın	Repli		Vector	FBHP2	FRMP4	BHP ABAN						ref mr3/s)	{m^3}		uvaj	(m^3)	(m^3)	atter Blowout	(fraction) alte	after blowout	(fraction) after		Brine Volume (m/3)
676	Up-dip	Lebik	. acen.	VIICTOR 70	8.01E+06	8.01E+06	1.10F+07	2.88E+00	BRINEFLW						GAS RATE		BRINEOUT	ORIN_REL	BANPAESS	SATERNS	BRNPRESO	SATBANO	(Iraction) WASTE PV	/ TOT BRIN
677	Up-dip	i	,	45	8.00E+06	8.00E+06	.,		5.54E-05 4.87E-05	1.09E-05 0.00E+00		1.09E-05	6.17E+06	1.04E-05	3.31E-02	2.53E+00	1.56E+01	1.52E+01	1.05E+07	9.46E-01	1.02E+07	9.43E-01	9.45E+04	
678	Up-dip	1	2	22	7.93E+06	3.90E+05		2.88E+00	4.54E-05	1.10E-03	8.39E-05 7.14E-05	0.00E+00 1.23E-03	1.28E+22	1.08E-05	0.00E+00	0.00E+00	1.28E+01	1.25E+01	9.67E+06	9.84E-01	9.39E+08	9.83E-01	8.99E+04	8.85E+04
679	Up-dip	1	2	79	2.70E+05	8.77E+05	1.63E+06	1.10E+01	1.27E-05	5.56E-01	1.71E-05	1.86E+00	4.67E+04 1.72E+01	1.17E-05 0.00E+00	3.37E+00	2.51E+02	1.17E+01	1.14E+01	9.43E+06	6.44E-01	9.39E+06	5.50E-01		5.85E+04
680	Up-d#p	1	2	44	7.99E+06	7.99E+06	9.89E+06	2.88E+00	3.89E-05	1.48E-05	5.61E-05	1.48E-05	8.20E+06	1.65E-05	1.70E+03 4.53E-02	6.95E+05 1.35E+00	1.20E+01 1.01E+01	1.13E+01		7.04E-01	6.96E+06	5.09E-01	8.68E+04	5.53E+04
681	Up-dip	1	2	39	8.01E+06	7.93E+06		2.88E+00	3.13E-05	5.62E-05	5.54E-05	5.62E-05	8.02E+05	1.86E-06	1.72E-01	1.08E+01	8.60E±00	9.83E+00 8.41E+00	9.42E+06 9.86E+06	8,88E-01 8.24E-01	9.35E+06	8.10E-01	8.91E+04	
682	Up-dlp	. !	S	52	8.00E+06	B.01E+06		2.88E+00	2.77E-05	2.28E-06	6.08E-05	2.28E-06	1.46E+07	3.17E-06	6.94E-03	5.37E-01	7.80E+00	7.64E+00	1.07F+07	9.61E-01	1.00E+07 9.20E+06	8.46E-01 9.59E-01	9.24E+04	
683 684	Up-dip Up-dio	1	2	7 33	7.99E+06	7.99E+06		2.88E+00	3.02E-05	7.51E-08	4.02E-05	7.88E-08	4.05E+08	1.66E-05	2,29E-04	1.87E-02	7.56E+00	7.37E+00	8.98E+06	9.91E-01	8.20E+06	7.19E-01	9.06E+04 8.60E+04	
685	∪p-dip Up-dip	1	2	15	8.00E+06 B.02E+06	2.36E+05 2.56E+05		2.88E+00	2.67E-05	6.22E-06	4.41E-05	6.22E-06	5.75E+06	0.00E+00	1.90E-02	1.24E+00	7.10E+00	6.93E+00	9.22E+06	3.40E-01	9.21E+06	7.33E-01	8 83F+04	
686	Up-dip	i	2	2	7.99E+06	7.99E+06		2.88E+00 2.88E+00	2.57E-05 2.23E-05	8.95E-06	4.40E-05	8.98E-06	3.05E+06	0.00E+00	2.73E-02	2.22E+00	6.75E+00	6.59E+00	9.13E+06	5.86E-01	9.09E+06	8.24E-01	8.77E+04	0.172707
687	Up-dip	- 1	2	55	7.99E+06	2.21E+05		2.88E+00	9.4BE-06	1.77E-06 1.26E-07	3.59E-05 1.62E-05	1.77E-06 1.26E-07	1.72E+07	1.68E-05	5.41E-03		5.85E+00		8.94E+06	9.18E-01	8.91E+06	9.15E-01	8.66E+04	
688	Up-dip	1	2	40	2.64E+05	3.43E+05		1.10E+01	7.91E-07	1.31E+00	1.91E-06	8.71E+00	8.39E+07 4.37E+01	1.31E-05 1.85F-05	3.83E-04	3.01E-02	2.52E+00	2.46E+00	8.37E+06	4.71E-01	8.39E+08	6.05E-01	8.37E+04	5.25E+04
689	Up-dip	1	2	51	3.42E+05	3.16E+05		1.10E+01	5.05E-08	2.00E+00	1.44E-07	1.76E+01	1.75E-02	3.68E-05	4.00E+03 6.09E+03	2.06E+06 3.67E+06	8.99E-01	8.50E-01	1.05E+07	3.89E-01	5.88E+06	3.34E-01	9.51E+04	
690	Up-dip	1	2	91	2.61E+05	2.27E+05	4.41E+06	1.10E+01	1.22E-08	6.60E-01	4.09E-08	7.15E+00	1.48E-02	0.00E+00	2.01E+03	9.63E+05	6.41E-02 1.43E-02	6.26E-02 1.36E-02	1.23E+07 8.76E+06	5.76E-01	5.88E+06	3.61E-01		5.49E+04
691	Up-dip	1	2	31	2.97E+05	8.01E+06	1.09E+07	1.10E+01	1.08E-08	6.53E-01	5.06E-08	1.27E+01	1.22E-02	6.87E-06	1.99E+03	1.10E+06	1.34E-02	1.28E-02	1.05E+08	4.94E-01 9.41E-01	4.52E+06	2.87E-01		4.22E+04
692	Up-dip	1	2	58	3.425+05	3.33E+05		1.10E+01	6.42E-09	6.60E-01	3.52E-08	1.75E+01	6.81E-03	0.00E+00	2.01E+03	1.23E+06	8.41E-03	8.27E-03	1.03E+07	2.06E-01	4.29E+06 4.26E+06	9.57E-02 1.71E-01	9.40E+04 1.02E+05	4.87E+04
693 694	Up-dīp	1	2	28		3.06E+05	7.96E+06	1.10E+D1	8.38E-11	5.08E-01	4.80E-10	1.69E+01	1.12E-04	0.00E+00	1.55E+03	9.73E+05	1.09E-04	1.07E-04	1.12E+07	5.08E-01	3.62E+06	1.97E-01	9.90E+04	
695	Up-dip Up-dip	•	2	94 78	8.00E+06 8.01E+06	2.59E+05 8.01E+06	2.59E+05 8.01E+06	2.88E+00	1.42E-04	2.49E-06	2.77E-04	2.55E-06	5.95E+07	0.00E+00	7.5BE-03	6.20E-01	3.69E+01	3.60E+01	1.22E+07	7.04E-01	1.19E+07	7.58E-01	9.42E+04	
696	Un-dlp	- 1	2	44	8.00E+06	8.00E+06	8.00E+06	2.88E+00 2.88E+00	1.42E-04 8.61E-05	4.10E-05	2.34E-04	4.10E-05	5.02E+06	0.00E+00	1.25E-01		3.68E+01	3.59E+01	1.27E+07	9.47E-01	1.25E+07	8.31E-01		8.52E+04
697	Up-dlp	i	2	45	8.00E+08	8.00E+06		2.88E+00 2.88E+00	8.61E-05 8.52E-05	2.01E-03 0.00E+00	1.44E-04 1.46E-04	2.01E-03	1.31E+06	0.00€+00	8.14E+00		2.41E+D1	2.36E 401	1.16E+07	8.88E-01	1.15E+07	8.79E-01	9.14E+04	
698	Up-dlp	i	2	15	3.75E+05	4.30E+05		1.10E+01	1.98E-05	3.33E-01	1.40E-U4 4.43E-05	0.00E+00 2.24E+00	2.24E+22 4.62E+01	0.00E+00 0.00E+00	0.00E+00 1.02E+03			2.19E+01	1.09E+07	9.76E-01	1.08E+07	9.74E-01	8.81E+04	8.59E+04
699	Up-dip	1	2	69	7.99E+06	8.00E+06	8.00E+06	2.88E+00	6.75E-05	1.36E-04	1.29E-04	1.36E-04	9.64E+05	0.00E+00	1.02E+03 4.16E-01	4.32E+05 1.95E+01	1.99E+01 1.85E+01	1.89E+01 1.81E+01	1.13E+07	8.00E-01	7.14E+08	6.60E-01	9.01E+04	
700	Up-dip	- 1	2	52	8.01E+06	8.01E+06		2.88E+00	6.33E-05	1.81E-05	1.42E-04	1.81E-05	4.25E+06	0.00E+00	5.51E-02	4.19E+00	1.85E+01 1.78E+01	1.81E+01 1.74E+01	1.16E+D7 1.13E+07	9.16E-01 9.61E-01	1.13E+07	9.07E-01	9.13E+04	8.34E+04
701	Up-dip	1	2	2	B.00E+06	8.00E+06		2.88E+00	6.05E-05	1.43E-04	1.02E-04	1.43E-04	1.10E+06	D.00E+00	4.36E-01		1.61E+01	1.74E+01 1.58E+01	1.13E+07	9.61E-01 9.18F-01	1.08E+07 1.06E+07	9.59E-01 8.55E-01	8.98E+04 8.75E+04	
702	Up-dip	1	2	39	8.01E+06	8.01E+06	B.01E+06	2.88E+00	4.68E-05	2.14E-04	8.62E-05	2.14E-04	3.48E+05	0.00E+00	6.52E-01	3.75€+01	1.30E+01	1.27E+01	1.13E+07	8.10E-01	1.12E+07	8.45E-01	9.05E+04	7.73E+04 7.67E+04
703 704	Up-dip Up-dip	1	2	10 19		5.26E+05		2.88E+00	4.44E-05	5.73E-07	7.59E-05	5.73E-07	B.24E+07	0.00E+00	1.75E-03	1.39E-01	1.14E+01	1.12E+01	9.40E+06	6.64E-01	9.31E+06	7.30E-01	8.12E+04	6.13E+04
705	Up-dip	1	2	24	7.79E+06 7.99E+06	8.01E+06 7.99E+06	8.01E+06 7.99E+06	2.88E+00	2.62E-05	1.44E-03	4.42E-05	1.74E-03	1.97E+04	0.00E+00	4.39E+00	3.56E+02	7.02E+00	6.86E+00	9.62E+06	8.55E-01	9.47E+06	5.00€-01	8.20E+04	
706	Up-dio	- 1	5	18		3.77E+06		2.88E+00 2.88E+00	2.70E-05 2.60E-05	1.22E-06	3.79E-05	1.22E-06	5.61E+07	0.00€+00	3.72E-03		6,92E+00	6.75E+00	9.00E+06	9.10₹-01	8.87E+06	9.07E-01	7,90E+04	
707	Up-dip	i	2	30	8.00E+06	8.00E+06	8.00E+06	2.88E+00	2.19F-05	7.72E-06 1.43E-06	4.01E-05 3.23E-05	7.72E-06 1.43E-06	6.13E+06 1.91E+07	0.00E+00	2.36E-02		6.77E+00	6.61E+00	9.35E+06	7.86E-01	9.28E+06	7.42E-01	8.09E+04	6.32E+04
708	Up-dlp	1	2	48		7.99E+06	7.99E+06	2.88E+00	2.07E-05	1.66E-03	3.09E-05	1.66E-03	1.64E+04	0.00E+00 0.00E+00	4.36E-03 5.05E+00		5.67E+00	5.53E+00	9.16E+06	8.83E-01	9.03E+06	6.38E-01	7.98E+04	
709	Up-dlp	1	2	35	7.99E+06	7.99E+06	7.99E+06	2.88E+00	1.71E-05	2.96E-06	2.91E-05	2.96E-06	7.76E+06		9.04E-03	3.32E+02 5.97E-01	5.45E+00 4.62E+00	5.32E+00	8.97E+06	8.98E-01	8 87 E +06	5.77E-01	7.90E+04	
710	Up-dip	1	2	31		8.02E+06	8.02E+06	1.10E+01	3.49E-09	8.12E-01	1.69E-08	1.68E+01	3.18E-03				4.02E+00	4.51E+00 4.24E-03	9.17E+06 1.17E+07	9.05E-01 9.41E-01	9.03E+06 4.72E+06	9.00E-01	7.99E+04	7.20E+04
711	Up-dip	1	2	28			8.15E+06	1.10E+01	2.40E-09	3.31E-01		9.70E+00	5.06E-03		1.01E+03	.,	3.11E-03	3.02F-03	9.45E+06	8.93E-01	3.21E+06	7.51E-02 2.27E-01	9.20E+04 8.21E+04	
712 713	Up-dip	1	2	58		3.65E+05	3.66E+05	1.10E+01	2.30E-09	7.45E-01		2.04E+01	2,15E-03		2,27E+03		3.02E-03	2.85E-03	1.28E+07	1.93E-01	4.50E+06	1.57E-01	9.70E+04	3.29E+04
714	Up-dip Up-dip	1	2	79 78		3.29E+06	3.29E+06	1,10E+01	1.47E-09	1.51E+00	4.09E-09	1.42E+01	6.56E-04			2.90E+06	1.90E-03	1.B2E-03	1.08E+07	7.86E-01	4.97E+06	3.70E-01	8.93E+04	
715	Up-dip	1	2	94		7.64E+06 8.00E+06	7.64E+06 8.00F+06	1.10E+01 2.88E+00	1.23E-04			2.58E+00	1.50E+02		3.69E+03		1,49E+02	1.44E+02	1.41E+07	8.60E-01	1.39E+07	4.38E-01	9.91E+04	
716	Up-dip	- 1	2	24		8.00E+06	8.00E+06	2.88E+00	3.24E-04 1.57E-04	1.16E-07 5.28E-03	4.42E-04	1.16E-07	2.86E+09	0.00E+D0	3.54E-04	2.83E-02		7.91E+01	1.47E+07	9.95E-01	1.44E+07	7.59E-01	9.45E+04	8.17E+04
717	Up-dip	i	2	45		7.99E+06	7.99E+06	2.88E+00	1.31E-04		2.71E-04 2.19E-04		5.71E+04 1.15E+07	0.00E+00	1.61E+01		4.31E+01	4.21E+01	1.41E+07	9.11E-01	1.39E+07	8.85E-01	9.23E+04	
718	Up-dip	1	2	44		8.00E+06	8.00E+06	1.10E+01	2.52E-05		7.51E-05	2.49E+00	1.79E+01	0.00E+00 0.00E+00	6.07E-02 5.09F+03		3.45E+01 3.32E+01	3.37E+01	1.30E+07	9.50E-01	1.26E+07	9.47E-01	8.75E+04	
719	Up-dip	1	2	52	8.01E+06	8.01E+06	8.01E+06	2.88E+00	1.05E-04		2.07E-04		2.38E+06		2.9BE-01		2.81E+01	3.19E+01 2.74E+01	1.24E+07 1.28E+07	8.77E-01	1.02E+07	3.21E-01	9.05E+04	5.15E+04
720	Up-dip	1	2	69			7.99E+0 6	2.88E+00	9.76E-06	7.48E-04	1.93E-04		2.77E+05		2.28E+00		2.71E+01	2.65E+01	1.34E+07	9.61E-01 9.12E-01	1.24E+07 1.31E+07	8.34E-01 9.03E-01	8.70E+04	
721	Up-dip	1	2	39		8.01E+06	8.01E+06	2.88E+00	5.62E-05	3.98E-04	1.04E-04	3.98E-04	2.31E+05				1.54E+01	1.51E+01	1.22E+07	8.51E-01	1.20E+07	7.60E-01	8.94E+04 8.43E+04	8.11E+04 6.74E+04
722 723	Up-dip Up-dio	- !	2	2		8.00E+06	8,00E+06	2.88E+00	5.33E-05	1.13₹-04	8.86E-05	1.13E-04	1.24E+06	0.00E+00	3,44E-01		1.41E+01	1.38E+01	1.06E+07	9.18E-01	1.04E+07	7.40E-01	7.78E+04	
724	Up-dip	1	2	100 35		8.00E+06	8.00E+06	2.88E+00	3.56E-05		7.04E-05	4.00E-05	1.20E+06	0.00E+00	1.22E-01	8.35E+00	9.97E+00	9.75E+00	1.05E+07	B.B7E-01	1.03E+07	8.53E-01	7.72E+04	
725	Up-dip	i	2	30		7.99E+06	7.99E+06	2.88E+00 2.88E+00	3.63E-05 3.52E-05	3.16E-05	6.20E-05		1.69E+06	0.00E+00			9.71E+00	9.48E+00	1.05E+07	9.05E-01	1.03E+07	8.16E-01	7.72E+04	B.B0E+04
726	Up-dip	i	2	10		4.44E+06	4.44E+06	1.10E+01	3,52E-05 3,48E-06		5.28E-05 1.15E-05		2.61E+07	0.00E+00	7.08E-03		9.14E+00		9.86E+06	8.86E-01	9.71E+06	6.74E-01	7.48E+04	5.74E+04
727	Up-dip	1	2	97			8.01E+06	2.88E+00	1.48E-05	3.52E-05	1.10E-05 2.62E-05		1.58E+00 4.52E+05	0.00E+00 0.00E+00	5.19E+03 1.07E+01		4.59E+00	4.37E+00	1.46E+07	7.98E-01	7.38E+06	3.00E-01	9.56E+04	5.39E+04
728	Up-dip	1	2	19	3.34E+05	8.02E+06	8.02E+06	1.10E+01	3.46E-06		1.03E-05		2.18E+00		4.41E+03		4.02E+00 4.00E+00		9.13E+06	9.15E-01	9.01E+06	7.03E-01	7.16E+04	5.71E+04
729	Up-dip	1	2	53	2.31E+05	0.00E+00	5.65E+03	1.10E+01	1.73E-06			1.80E+00	1.20E+01		3.04E+02		4.00E+00 2.46E+00		1.38E+07 7.96E+06	8.57E-01 9.34E-01	8.77E+06 3.03E+06	2.11E-01		4.81E+04
730	Up-dip	1	2	18		8.00E+06	8.00E+06	1.10E+01	9.01E-08	1.52E+00		2.08E+01	3.80E-02			3.26E+06	1.24E-01	1.22E-01	7.96E+06 1.48F+07	9.34E-01 8.94E-01	3.03E+06 5.80E+06	3.72E-01 3.75E-01	6.64E+04 9.58E+04	
731	Up-dip		2	60		6.13E+06	6.13E+06	1.10E+01	2.94E-09			9.08E+00	9.45E-03	0.00E+00	5.53E+02	4.67E+05	4.41E-03	4.40E-03	9.12E+06	7.92E-01	2.48E+06	3.75E-01	9.58E+04 7.28E+04	5.87E+04
732 733	Up-dip	1	2	47		2.86E+05	2.86E+05	1.10E+01	2.40E-13			7.26E+00	1.02E-06				3.57E-07		8.26E+08	5.68E-01	2.05E+06	1.51E-01	6.68E+04	
733 734	Up-dip Up-dip	1	2	94		7.99E+06	7.99E+06	2.88E+00	3.06E-04	1.30E-07	4.32E-04		2.42E+09			3.17E-02			1.45E+07	9.95E-01	1.43E+07	7.57E-01	9.41E+04	8.12E+04
734	∪p-dep Up-dep	- 1	2	24 45		8.00E+06 7.99E+06	8.00E+06 7.99E+06	2.88E+00 2.88E+00	1.55E-04		2.67E-04		4.62E+04					4.17E+01	1.40E+07	9.11E-01	1.39E+07	6.80E-01	= -	7.21E+04
736	Up-dip	i	2	69		7.99E+06		2.88E+00	1.58E-04 1.21E-04		2.53E-04		7.21E+06	0.00E+00		5.97E+00		4.05E+D1		9.50E-01	1.32E+07	9.46E-01	9.02E+04	
737	Up-dip	i	2	44		8.00E+06	8.00E+06	1.10E+01	8.72E-06				1.09E+05 5.26E+00				3.31E+01	3.24E+01	1.42E+07	9.12E-01	1.39E+07	B.25E-01	9.26E+04	8.00E+04
	Up-dip	1	2	100		8.00E+06	8.00E+08	2.88E+00	4.23E-05		8.07E-05		1.02E+06	0.00E+00 0.00E+00			1.19E+01	1.15E+01	1.23E+07	8.85E-01	8.36E+06	2.53E-01	8.70E+04	4.72E+04
739	Up-dip	1	2	52	8.02E+06	8.00E+06	8.00E+06	2.88E+00	4,35E-05		8.27E-05		3.64E+06	0.00E+00			1.16E+01 1.16E+01	1.13E+01 1.13E+01	1.08E+07 1.02E+07	8.87E-01	1.06E+07	7.65E-01	7.86E+04	6.43E+04
740	Up-dip	1	2	1		8.00E+06		2.88E+00	2.43E-05		4.73E-05		7.17E+06	0.00E+00			6.70E+00		1.02E+07 9.44E+06	9.61E-01	9.96E+06	7.25E-01	7.61E+04	6.32E+04
	Up-dip	1	2	30				2.88E+00	2.52E-05	5.60E-07	3.75E-05		6.49E+07	0.00E+00	1.71E-03		6.53E+00		9.44E+06 9.37E+06	9.02E-01 8.86E-01	9.27E+06 9.22E+06	8.06E-01	7.30E+04	6.19E+04
	Up-dip	1	2	39			8.00E+06	2.88E+00	2.39E-05	2.56E-05			1.31E+06	0.00E+00			6.47E+00		9.82E+06	8.52E-01	9.22E+06 9.67E+06	6.78E-01 6.85E-01	7.26E+04 7.46E+04	5.59E+04
743	Up-dip	1	2	78			5.32E+05	1.10E+01	3.67E-06	3.65E+00	7.13E-06	1.68E+01	6.39E-01	0.00E+00	1.11E+04		4.03E+00		9.40E+06	5.85E-01	9.07E+06	6.85E-01 2.48E-01		5.66E+04 4.91E+04
	Up-dip	!	2	35				2.88E+00	1.07E-05				1.57E+07	0.00E+00			2.86E+00		8.81E+06	9.05E-01	8.68E+06	7.40E-01		4.91E+04 5.59E+04
	Up-dip Up-dip	1	2	86 19		8.02E+06 8.04E+06	8.02E+06	1.10E+01	7.12E-08				2.40E-01	0.00E+00	6.17E+02		9.57E-02	9.02E-02	8.26E+06	9.20E-01	2.89E+06	1.22E-01		3.42E+04
	∪p-esp Up-ello	1	2	60			8.04E+06 2.66E+03	1.10E+01	1.90E-08				3.31E-03				2.66E-02	2.59E-02	1.03E+07	7.85E-01	6.76E+06	1.49E-01	9.94E+04	4.29E+04
	∪p-dip Up-dip	;	2	53			6.15E+06	1.10E+01	1.86E-10 4.51E-15	1.46E-01 1.37E-01			7.66E-04				2.74E-04	2.72E-04	7.88E+06	7.90E-01	2.32E+06	9.28E-02	5.49E+04	2.18E+04
1 10	Up-dlo	i	2	94		_			2.61E-04			8.42E+00 1.77E-07	1.61E-08				5.82E-09		8.18E+06	8.40E-01	2.07E406	2.02E-01	6,67E+04	3.21E+04
	Up-dip	1	2						2.08E-04									6.45E+01		9.95E-01		7.49E-01		7.99E+04
	, ,		-					_,_,_,			5.00E-04	5.05E*04		U.VVE+00	1.722400	5.02E+01	5.50E+01	5.37E+01	1.46E+07	9.50E-01	1.42E+07	9.46E-01	9.48E+04	9.00E+04

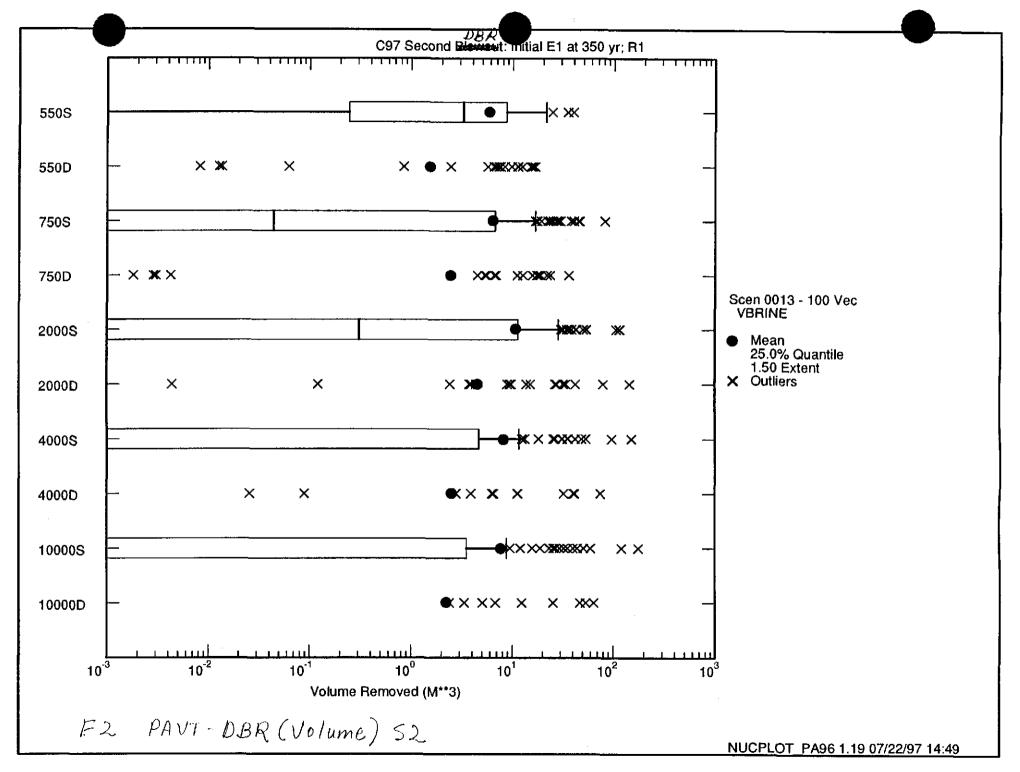
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					Excevates Waste		Residual Srive	e Carebed Boom	1 15- d- 4-	lle de boo	David de			DRZ	Sali Pilar	Saft Pitter			 -				0	11 - 4:			
1	•	•	•	•	Porceity	Set (fraction) Sat. (traction)	a Crushed Panel I Height (m)	Pressure (Pa)	Sat. (fraction)	Pressure (Ps)	Down-dip Avg Sat. (fraction)	DRZ Porosity (Fraction)	Permeability	Porceity (Fraction)	Permeability	Intrusion Time (Years)	Skin factor	Well Productivity	BC well Sand Permembility		Castile Flaservois	Castile Reservoir	Up-dip Brine Relative	Up-dip Gas Relative	Down-dip Brine Relative	Down-dip Gas Rabéve
Na	10	Reptic.	Scen	. Vactor	POROSIT	Y SAT_RGAS	SAT_REAN	HEIGHT	PRESPAN2	RSATPANS	PRESPAN4	DCATRANA	GO BOOKIEV	···>	(.,	(m*2)			Index (1/Pa)	(m°2)	(44,5)	Ртивите (Ра)	Permenbēty (m*2)	Permanblity (frantion)	Permentality (fraction)	Permenbility (fraction)	Permenbility (fraction)
751 752	Up-dip Up-dip	1	5	44	5.32E-0	1 1.12E-01	1.61E-02	1.28E+00	1.02E+07	6.50E-01	1.03E+07	8.87E-01	1.29E-01	1.18E-13	PORIOSITY 1.34E-01	1.18E-13	1.00E+04	-1.17E+00		9.80E-15			PRM_CAST	1311072	KRG2	KfIW4	KRG4
753	Up-dip	1	2	6 9	5.68E-0 5.36E-0			1.39E+00 1.30E+00	1.30E+07 1.05E+07	9.09E-01 8.99E-01	1.31E+07 1.06E+07	9.09E-01	8.35E-02	1.30E-14	8.28E-02	1.26E-14	1.00E+04	·1.29E+00		9.33E-15	7.83E-01 9.99E-01	1.29E+07 1.42E+07	1.12E-12 4.07E-13	1.98E-01	3,09E-02 1,64E-08	6.38E-01 5.41E-01	3.57E-10 1.62E-08
754	Up-dip	1	5	24	5.13E-0	9.01E-02	1.37E-01	1.23E+00	9.02E+06	9.10E-01	9.11E+06	8.99E-01 9.10E-01	7.21E-02 1.96E-01	7.24E-16 2.82E-13	8.49E-02 2.19E-01	7.24E-16 2.82E-13	1.00E+04 1.00E+04	-1.28E+00	1.29E-13	1.66E-14	9.73E-01	1.25E+07	7.08E-14	5.84E-01	1.20E-07	5.85E-01	1.02E-08
755 756	Up-dip Un-din	1	5	100 30	5.18E-0 5.04E-0		3.43E-01		9.22E+06	8.63E-01	9.32E+06	8.83E-01	6.96E-02	9.12E-16	8.72E-02	9.12E-16	1.00E+04	-1.29E+00 -1.26E+00	1.23E-13 1.23E-13		9.94E-01 9.43E-01	1.09E+07 1.25E+07	7.41E-13	6.66E-01	2.14E-13	6.66E-01	2.09E-13
757	Up-dip	i	ž	78	6.00E-0		4.16E-02 1.51E-01	1.21E+00 1.50E+00	8.69E+06 1.56E+07	8.83E-01 3.47E-01	8.78E+06 1.57E+07	8.83E-01 5.59E-01	2,70E-02 2,73E-01	2.75E-14	4.59E-02	2.75E-14	1.00E+04	-6.49E-01	9.57E-14	2.19E-13	2.79E-01	1.34E+07	1.29E-13 1.59E-13	4.85E-01 6.19E-01	1.83E-07 1.25E-09	4.86E-01 6 19E-01	1.59E-07 1.23E-09
758 759	Up-dip	1	3	44	6.31E-0		1.61E-02	1.28E+00	1.02E+D7	5.79E-01	1.02E+07	8.85E-01	1.29E-01	5.83E-10 1.18E-13	1.00E-01 1.34E-01	2.46E-15 1.18E-13		-1.06E+00 -1.17E+00	1.37E-13 1.22E-13	8.32E-17 3.60E-15	6.28E-01	1.40E+07	1.07E-12	4.42E-03	5.18E-01	6.68E-02	1.63E-01
760	Up-dlp Up-dlo	1	3	78 69	5.41E-0 5.42E-0		1.51E-01 4.08E-01	1.31E+00 1.31E+00	1.09E+07	9.44E-01	1.12E+07	9.45E-01	1.10E-01	2.46E-15	1.15E-01	2.46E-15	1.20E+03	-1.06E+00		8.32E-17	7.83E-01 6.28E-01	1.38E+07 1.48E+07	1.12E-12 1.07E-12	1.27E-01 7.79E-01	6 57E-02 8.41E-07	6.31E-01 7.79E-01	9.69E-08
761	Up-dlp	1	š	45	5.27E-0		2.04E-01			9.13E-01 9.82E-01	1.11E+07 9.97E+06	9.30E-01 9.84E-01	7.88E-02 7.63E-02	1,26E-14 5,13E-14	8.77E-02 8.96E-02	1.26E-14	1.20E+03	1.29E+00	1.31E-13	9.33E-15	9.99E-01	1.47E+07	4.07E-13	5.54E-01	0.00E+00	6.28E-01	7.82E-07 0.00E+00
762	Up-dip Up-dip	†	3	52 33	5.37E-01 5.12E-01	. 0.002 02		1.30E+00	1.04E+07	9.60E-01	1.15E+07	9.60E-01	1.09E-01	1.70E-15	1.27E-01	5.13E-14 1.70E-15	1,20E+03 1,20E+03	-9.31E-01 -9.48E-01	1,11E-13		4.89E-01 5.07E-01	1.36E+07 1.51E+07	4.57E-13 2.63E-13	9.18E-01	0.00E+00	9.26E-01	0.00E+00
764	Up-dip	i	3	7	5.20E-0		1.22E-01 3.12E-01		8.88E+06 9.39E+06	4.11E-01 5.14E-01	8.87E+06 9.44E+06	2.94E-01 9.90E-01	2.95E-02	1.12E-14	4.09E-02	1.12E-14	1.20E+03	-1.24E+00			9.16E-01	1.23E+07	1.26E-13	7.57E-01 1.64E-02	4.18E-07 3.01E-01	7.57E-01 2.42E-03	4.13E-07 5.44E-01
765	Up-dip	1	3	35	5.03E-0		4.39E-01	1.21E+00	8.35E+06	8.95E-01	8.37E+06	9.02E-01	1.42E-01 5.14E-02	2.29E-13 7.24E-15	1.63E-01 6.83E-02	2.29E-13 7.24E-15	1.20E+03 1.20E+03	-6.15E-01 -8.97E-01	9.80E-14 1.04E-13	7.94E-14 1.38E-13	2.60E-01	1.30E+07	1.35E-12	1.08E-02	4.31E-01	9.49E-01	3.90E-08
766 767	Up-dip Up-dip	1	3	2 15	5.28E-01 5.06E-01		4.02E-01 5.21E-01	1.27E+00 1.22E+00	9.94E+06 8.54E+06	5.29E-01 6.33E-01	9.95E+06	6.07E-01	1.67E-01	4.47E-14	1.78E-01	4.47E-14	1.20E+03	-1.29E+00	1.27E-13	1.38E-13 5.01E-14	4.57E-01 9.98E-01	1.19E+07 1.35E+07	3.98E-11 7.24E-11	4.65E-01 3.29E-03	1.38E-05 5.15E-01	4.93E-01 1.92E-02	1.97E-07
768	Up-dip	í	ă	24	4.97E-01		1.37E-01	1.19E+00	8.04E+06	9.08E-01	8.54E+06 8.12E+06	5.14E-01 9.08E-01	5.22E-02 1.98E-01	1.32E-14 2.82E-13	7.24E-02 2.26E-01	1.32E-14	1.20E+03	-9.46E-01	1.07E-13	1.32E-14	5.06E-01	1.15E+07	4.47E-13	4.69E-03	4.97E-01	0.00E+00	2.87E-01 1.00E+00
769 770	Up-dip Up-dio	1	3	10	5.00E-01	3.17E-02	1.73E-01	1.20E+00	8.20E+06	2.89E-01	8.20E+06	4.84E-01	4.89E-02	3.72E-14	7.38E-02	2.82E-13 3.72E-14	1.20E+03 1.20E+03	-1.29E+00 -1.33E+00	1.20E-13 1.22E-13	2.63E-14 1.86E-16	9.94E-01 1.08E+00	1.17E+07 1.18E+07	7.41E-13	8.59E-01	3.43E-08	6.59E-01	3.36E-08
771	Up-dip	i	3	19 94	5.13E-01 5.45E-01	1.42E-01 4.58E-03	2.97E-02 1.65E-01	1.23E+00 1.32E+00	8.91E+06 1.13E+07	1.49E-01 2.44E-01	8.95E+06 1.13E+07		2.01E-01	1.41E-15	2.21E-01	1.41E-15	1.20E+03	1.23E+00	1.21E-13	2.00E-16	8 04E-01	1.18E+07 1.25E+07	1.35E-11 1.45E-12	7.08E-04 4.30E-04	7.02E-01 7.06E-01	2.70E-02 5.40E-01	2.95E-01 1.03E-06
772	Up-dip	1	3	39	5.40E-01	1.50E-01	2.98E-01	1.31E+00	1.09E+07	3.36E-01		2.71E-01 8.47E-01	2.04E-01 1.89E-02	8.31E-15 3.02E-15	2.11E-01 2.93E-02	6.31E-15 3.02E-15			1.32E-13 1.27E-13	9.77E-16	9.95E-01	1.44E+07	1.78E-12	6.13E-05	8.50E-01	2.47E-04	7.81E-01
773 774	Up-dip Up-dip	1	3	58 30	5.68E-01 6.50E-01	2.96E-02 1.16E-01	1.14E-01 4.16E-02	1.39£+00 1.33£+00	1.32E+07	1.25E-01	1.32E+07	1.46E-01	2.10E-01	2.52E-16	2.07E-01	1.45E-16			1.27E-13 1.33E-13	2.40E-13 3.09E-15	8.82E-01 8.11E-01	1.45E+07 1.32E+07	1.78E-13 1.07E-13	2.07E-05 1.14E-07	8.59E-01 9.72E-01	4.02E-01	5.26E-07
775	Up-dip	i	3	28	5.70E-01	9.72E-02	1.79E-01	1.40E+00	1.17E+07 1.35E+07	5.30E-02 1.81E-01			3.51E-02 2.10E-01	2.75E-14 5.59E-17	4.16E-02 2.11E-01	2.75E-14		-6.49E-01		2.19E-13	2.79E-01	1.48E+07	1.59€ 13	7.83E-08	9.73E-01	4.67E-06 3.35E-07	9.23E-01 9.59E-01
776 777	Up-dip Up-dio	1	3	78	5.58E-01	4.93E-02	1.51E-01	1.36E+00	1.23E+07	7.80E-01	1.24E+07		1.14E-01	3.55E-15	1.11E-01	4.79E-17 2.46E-15	1.20E+03 1.40E+03	-1.08E+00 -1.06E+00	1.29E-13	9.55E-12 B.32€-17	6.64E-01 6.28E-01	1.48E+07 1.48E+07		2.65E-10	9.94E-01	5.94E-08	9.75E-01
	Up-dip	i	3 3	69 52	5.44E-01 5.39E-01	8.98E-02 3.68E-02	4.08E-01 4.49E-01	1.32E+00 1.30E+00	1.11E+07 1.08E+07	9.09E-01 9.58E-01		9.17E-01	7.90E-02	1.26E-14	8.74E-02	1.26E-14	1.40E+03	-1.29E+00	1.32E-13		9.99E-01			3.30E-01 5.40E-01	1.53E-02 1.72E-08	7.81E-01 5.72E-01	6.07E-07 0.00E+00
779	Up-dip	1	Э	45	5.29E-01	5.05E-02	2.04E-01	1.28E+00	1.00E+07	9.69E-01		9.60E-01 9.71E-01	1.10E-01 7.65E-02	1.70E-15 5.13E-14	1.26E-01 B.93E-02	1.70E-15 5.13E-14	1.40E+03 1.40E+03		1.14E-13		5.07E-01	1.51E+07	2.63E-13	7.44E-01	2.19E-06	7.57E-01	4.33E-07
780 781	Up-dip Un-din	1	3	44 24	5.42E-01 5.10E-01	1,12E-01 9.01E-02	1.61E-02 1.37E-01	1.31E+00		4.17E-01	1.11E+07	8.85E-01	1.30E-01	1.30E-13	1.31E-01	1.18E-13		-1.17E+00	1.11E-13 1.25E-13		4.89E-01 7.83E-01			8.64E-01 3.65E-02	0.00E+00 2.13E-01	8.72E-01	0.00E+00
782	Up-dlp	ì	3	18	5.08E-01	1.06E-01	3.40E-01			9.08E-01 4.95E-01		9.08E-01 6.81E-01		2.82E-13 3.31E-14	2.20E-01	2.82E-13	1.40E+03	-1.29E+00	1.23E-13	2.63E-14	9.94E-01			6.59E-01	3.00E-08	6.31E-01 6.59F-01	8.69E-08 2.97E-08
783 784	Up-dip	1	3	39	5.21E-01	1.50E-01	2.98E-01	1.26E+00	9.46E+06	4.17E-01		8.47E-01	1.54E-02	3.02E-15	7.38E-02 3.04E-02	3.31E-14 3.02E-15			1.13E-13 1.23E-13		6.69E-01 8.82E-01	1.12E+07 1.45E+07		4.67E-03	4.61E-01	B.72E-02	8.31E-02
785	Up-dip Up-dip	1	3	97 19	5.07E-01 5.20E-01	8.37E-02 1.42E-01	4.34E-01 2.97E-02	1.22E+00 1.25E+00	8.54E+06	5.30E-01 1.36E-01		9.12E-01	1.48E-01	5.63E-16	1.73E-01	5.62E-16	1.40E+03	-8.88E-01	1.05E-13		4.49E-01		1.78E-13 3.02E-11	1.45E-03 1.40E-03	5.68E-01 6.02E-01	4.03E-01 5.37E-01	4.66E-07 1.00E-06
786	Up-dip	1	3	60	5.00E-01		4.70E-02	1.20E+00		1.24E-01	8.51E+06			1.41E-15 6.10E-18	2.17E-01 2.14E-01	1.41E-15 5.75E-18		-1.23E+00	1.22E-13	2.00E-16	8.94E-01	1.25E+07	1.45E-12	2.85E-04	7.36E-01	5.33E-01	2.71E-06
787 788	Up-dip Un-dio	1	3	94	5.45E-01	4.58E-03	1.85E-01		1.12E+07	2.32E-01	1.12E+07	3.34E-01	2.04E-01	6.31E-15	2.11E-01	6.31E-15			1.15E-13 1.32E-13		7.91E-01 9.95E-01		2.34E-14 1.78E-12	9.07E-05	8.23E-01	6.94E-01	5.51E-05
789	Up-dip	i	3	28 52	5.15E-01 5.07E-01	9.72E-02 3.68E-02	1.79E-01 4.49E-01			2.12E-01 8.01E-01	9.21E+06 8.86E+06			5.28E-17 1.70E-15	2.38E-01	4.79E-17	1.40E+03	1.08E+00	1.14E-13		6.64E-01			2.56E-05 7.22E-06	8.81E-01 9.05E-01	1.85E-03 5.94E-01	6.30E-01 5.83E-06
	Up-dip	1	3	45	5.41E-01	5.05E-02	2.04E-01			9.49E-01	1.10E+07			5.13E-14	1.35E-01 8.70E-02	1.70E-15 5.13E-14	3.00E+03 3.00E+03	-9.48E-01 -9.31E-01	1.07E-13 1.14E-13	4.17E-14 1.74E-15	5.07E-01			1.90E-01	4.75E-02	7.56E-01	5.28E-07
791 792	Up-dip Up-dip	1	3	69 24	5.44E-01 5.26E-01	8.98E-02 9.01E-02	4.08E-01 1.37E-01	1.32E+00 1.27E+00		9.09E-01	1.13E+07	9.09E-01	7.90E-02	1.26E-14	8.73E-02	1.26E-14	3.00E+03	-1.29E+00	1.32E-13		4.89E-01 9.99E-01			7.B1E-01 5.40E-01	4.05E-09 1.85E-08	7.B1E-01 5.40E-01	4.02E-09
793	Up-dip	i	3	100	5.06E-01	1.145-01	3.43E-01			9.08E-01 8.83E-01	9.83E+06 8.79E+06			2.82E-13 9.12E-16	2.13E-01 8.94E-02	2.82E-13 9.12E-16	3.00E+03	-1.29E+00	1.27E-13	2.63E-14	9.94E-01	1.17E+07	7.41E-13	8.59E-01	3.36E-08	6.59E-01	1.83E-08 2.89E-08
	Up-dip Up-dip	1	3	19	5.55E-01	1.42E-01	2.97E-02	1.35E+00	1.21E+07	5.54E-02	1.21E+07		-,		2.01E-01				1.20E-13 1.32E-13	-	9.43E-01 8.94E-01	1.28E+07 1.25E+07		4.86E-01	1.66E-07	4.B6E-01	1.61E-07
796	Op-dip	1	3	94	5.02E-01 5.45E-01	6.13E-02 4.58E-03	4.70E-02 1.85E-01			7.72E-02 1.92E-01		7.84E-01 7.51E-01	1.97E-01		2.13E-01	5.75E-18	3.00E+03	·1.17E+00	1.15E-13		7.91E-01			1.51E-06 2.90E-06	9.36E-01 9.31E-01	1.50E-01 3.88E-01	4.05E-02 8.24E-03
	Up-dip	1	3	24	5.17E-01	9.01E-02	1.37E-01		9.17E+06				2.04E-01 1.96E-01	6.31E-15 2.82E-13	2.11E-01 2.17E-01			-1.29E+00 -1.29E+00			9.95E-01	1.44E+07	1.78E-12	1.55E-08	9.84E-01	2.61E-01	4.13E-02
	Up-dip Up-dip	1	3	45 69	5.53E-01 5.40E-01	5.05E-02 6.98E-02	2.04E-01 4.08E-01			9.49E-01	1.20E+07	9.49E-01	8.09E-02	5.13E-14	8.47E-02			-9.31E-01	1.24E-13		9.94E-01 4.89E-01			2.82E-01 7.81E-01	1.41E-02 3.78E-09	6.59E-01 7 A1F-01	3.07E-08
	Up-dip	i	3	1	5.09E-01	9.81E-02	2.56E-01			9.09E-01 8.99E-01				1.26E-14 7.24E-16	8.80E-02 8.99E-02	1.26E-14	5.00E+03	-1.29E+00	1.31E-13	9.33E-15	9.99E-01			5.40E-01	2.01E-08	7.01E-01 5.40E-01	3.75E-09 1.86E-08
	Up-dip Up-dip	!	3	100	5.00E-01	1.14E-01	3.43E-01		8.52E+06	8.83E-01	8.61E+06				9.05E-02	7.24E-16 9.12E-16		-1.28E+00 -1.26E+00			9.73E-01 9.43E-01			5.84E-01	1.38E-07	5.84E-01	1.34E-07
	up∙aip Up∙dip	1	3	86 45	4.86E-01 5.73E-01	6.86E-02 5.05E-02	3.61E-02 2.04E-01							3.04E-17	1.B2E-01	3.02E-17	5.00E+03	1.28E+00	1.16E-13	4.07E-13				4.85E-01 2.73E-06		4.86E-01 7.20E-01	1.70E-07 5.73E-06
804	Up-dip	1	3	69	5.37E-01	8.98E-02	4.08E-01	1.30E+00	1.05E+07	9.09E-01		-,		1.01E-13 1,26E-14	8.09E-02 8.87E-02	5.13E-14 1.26E-14			1.23E-13	1.74E-15	4.89E-01	1.36E+07	4 57E-13	7.82E-01	2.68E-09	7.82E-01	2.66E-09
	Up-dip Up-dio	1	3	1 58	5.15E-01 6.01E-01	9.81E-02 2.96E-02	2.56E-01				9.18E+06	8.99E-01	6,93E-02	7.24E-16	8.89E-02	7.24E-16			1.30E-13 1.23E-13		9.99E-01 9.73E-01			5.40E-01 5.84E-01		5.40E-01	1.90E-08
	Up-dip	i	4	28	5.93E-01	9.72E-02	1.14E-01 1.79E-01						1.87E-01 1.89E-01	1.45E-16 5.21E-17	1.91E-01		5.60E+02 -	1.18E+00	1.45E-13	3.09E-15	8.11E-01				8.59E-01	5.84E-01 1.16E-04	1.36E-07 B.16E-01
	Up-dip	!	4	94	5.35E-01	4.58E-03	1.85E-01	1.29E+00	B.60E+06	2.90E-01	8.61E+06	5.97E-01				4.79E-17 6.31E-15			1.36E-13 1.29E-13		6.64E-01					3.31E-06	9.24E-01
	Up-dip Up-dip	1	4	58 19	5.90E-01 5.29E-01	2.96E-02 1.42E-01				1.58E-01	1.28E+07	1.77E-01	1.97E-01	3.58E-16	1.97E-01	1.45E-16	7.50E+02 -	1.18E+00			9.95E-01 8.11E-01	1.43E+07 1.26E+07		5.19E-04 1.51E-05		8.03E-02 5.78E-05	1.65E-01
811	Up-dip	i	4	94	5.47E-01	4.58E-03				9.67E-02 2.21E-01					2.13E-01 2.10E-01	1.41E-15		1.23E+00	1.25E-13	2.00E-16	B.94E-01	1.27E+07	1,45E-12	5.16E-05		2.82E-02	8.48E-01 2.29E-01
	Up-dip Un-din	1	4	94	5.47E-01	4.58E-03	1.85E-01	1.33E+00	1.14E+07	1.90E-01	1.15E+07	9.94E-01	2.04E-01						1.33E-13 1.33E-13		9.95E-01 9.95E-01			9.97E-06	9.08E-01	4.59E-01	1.01E-02
	Up-dip Up-dip	1	5 5	19 94	5.06E-01 5.47E-01	1.42E-01 4.5BE-03	2.97E-02 1.85E-01						2.02E-01	1.41E-15	2.23E-01	1.41E-15	1.20E+03 -	1.23E+00	1.19E-13						9.87E-01 6.98E-01	9.72E-01 4.64E-02	1.57E-08 1.63E-01
815	Up-dip	1	5		5.81E-01	2.96E-02	1.14E-01												1.33E-13	9.77E-16	9.95E-01	1.43E+07	1.78E-12	4.90E-05	8.59E-01	1.39E-01	9.98E-02
	Up-dip Up-dio	1	5 5	30 28	5.52E-01	1.16E-01 9.72E-02			1.19E+07	5.26E-02	1.19E+07	4.08E-01	3.58E-02	2.75E-14	4.14E-02				1,38E-13 1,06E-13			1.26E+07 1.47E+07			_	4.55E-06	9.24E-01
	Up-dip	i	5		5.70E-01 5.13E-01					1.81E-01 1.37E-01					2.11E-01			1.08E+00	1.29E-13	9.55E-12	6.64E-01						2.41E-01 9.72E-01
	Up-dip	1	5		5.48E-01	4.58E-03	1.85E-01	1.33E+00	1.15E+07	2.28E-01			,								8.94E-01				7.33E-01	4.21E-02	1.76E-01
	Up-dip Up-dip	1	5		5.46E-01 5.48E-01							3.58E-01	1.99E-01	1.41E-15	2.05E-01	1.41E-15	3.00E+03 -	1.23E+00	1.30E-13						8.91E-01 9.38E-01	1.90E-01 1.83E-02	6.79E-02
	-r-27		_ - _	97	G. 10E-01	7.005-70	1.03E-01	1.030+00	1. 10E+U/	E.U3E-U1	1.15E+07	9.94E-01	2.04E-01	6.31E-15	2.09E-01	6.31E-15	3.00E+03 -	1.29E+00	1.33E-13							9.72E-01	1.81E-08
																											

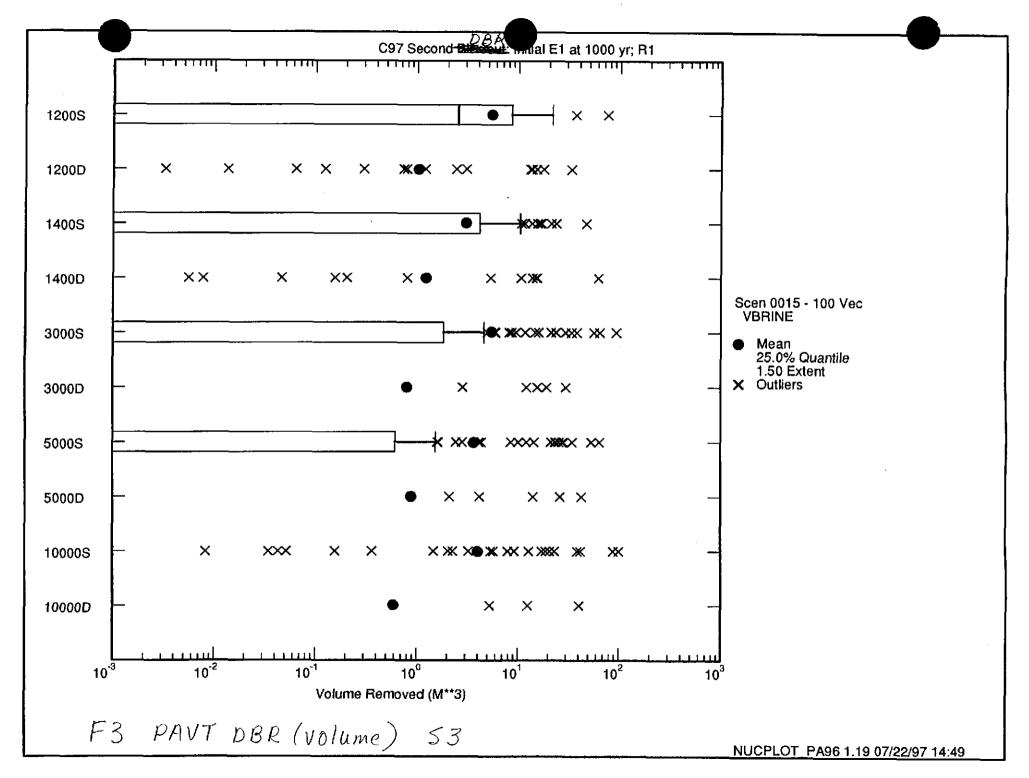
						Down-do		_																
	•		•	•	Up-dip Flowing Bottom-hole	Flowing Bottom-hole	BC well Injection	Blowout Duration	Brine Rate	Gas Role (ref	Max Brine	Max Gau Rain	Produced Liquid/Gas	Cum Brins from Boundary	Gas Plate	Cum Gas Produced for	Cum Brine Produced	Cum Brine Releases	Avg Brine Pressure	Saturation	Avg Brine Pressure	Avg Barre Saturation	Total Escavated	Total Excession
					Pressure (Pn)	Ргозамя (Ра)	Preserve (Pa)	(Days)	(m/3/s)	hr/G/s)	Plate (m^3/s)	rei m/3/s)	Relio (m^3/s / ref m^3/s)	Condition (Yell (m^3)	(macMday)	Lucinced Med	(m/3)	(m/3)	Primel 5 (Pin) after Blowout	Panel 5 (fraction) After	Panel 0 (Pa)	Panel D (Iraction) after	Waste Pore Volume	Brine Volume
No.	ID Um eller	Heplic.	Scen.	Vector	FBHP2	F8HP4	BHP ABAN	Lime				MAX GAS	LGR_MET	BRINE_BC	GAS_RATE	GASOUT	BRINEOUT	BRIN_REL		SATBRNS	BRNPRESO	blowed CaTBCAM	(kacton) WASTE PV	(m^3)
	Up-dip Up-dip	1	2	44 69	1.34E+06 7.99E+06	7.99E+06	7.99E+06 7.99E+06	1.10E+01 2.88E+00	4.25E-05 9.58E-05	3.41E-01	1.02E-04	3.54E-01	1.62E+02	0.00E+00	1.04E+03	3.04E+05	4.93E+01	4.71E+01	1.03E+07	8.90E-01	9.16E+08	3.53E-01	7.65E+04	
	Up-dip	Ť	2	1	1	8.00E+06	B.00E+06	2.88E+00	4.64E-05	5.29E-04 2.54E-05	1.81E-04 9.13E-05	5.29E-04 2.54E-05	3.79E+05 2.32E+06		1.62E+00 7.75E-02	6.98E+01 5.51E+00	2.60E+01	2.54E+01	1.31E+07	9.12E-01	1.29E+07	7.41E-01	8.85E+04	
	Up-dip	1	2	24		8.04E+06		2.88E+00	2.74E-05	6.45E-07	3.83E-05	6.45E-07	1.60E+08		1.97E-03	5,17E-02	1.28E+01 6.98E+00	1,25E+01 6,81E+00	1.06E+07 9.11E+06	9.02E-01 9.12E-01	1.04E+07 8.99E+06	7.20E-01 6.68E-01	7.80E+04 7.09E+04	
	Up-dip Uo-dio	1	2	100		8.00E+06 7.99E+06	8.00E+06 7.99E+06	2.88E+00 2.88E+00	1.90E-05 1.32E-05	5.96E-06	3.49E-05	5.96E-06	4.10E+06	0.00E+00	1.82E-02	1.27E+00	5.19E+00	5.07E+00		8.87E-01	9.16E+06	7.04E-01	7.09E+04 7.24E+04	
	Up-dip	i	2	78		4.91E+05	4.91E+05	1.10E+01	1.32E-05 1.86E-06	6.04E-08 3.71E+00	1.98E-05 4,39E-06	6.04E-08 1.69E+01	2.80E+08 3.81E-01	0.00E+00 0.00E+00	1.84E-04 1.13E+04	1.23E-02 6.27E+06	3.44E+00	3.35E+00		8.87E-01	8.65E+06	6.59E-01	6.85E+04	
	Up-dip	1	3	44		7.99E+06	1.07E+07	1.10E+01	2.92E-05	5.45E-01	7.26E-05	8.32E-01	6.52E+01	1.31E-05	1.66E+03	5.33E+05	2.39E+00 3.48E+01	2.39E+00 3.32E+01	8.89E+06 1.03E+07	5.72E-01 B.88E-01	8.53E+06 8.58E+06	2.39E-01 3.24E-01	1.01E+05	
	Up-dip Up-dio	1	3	78 69	8.00E+06	8.00E+06	1.17E+07 1.14E+07	2.88E+00	6.79E-05	1.43E-05	1.30E-04	1.43E-05	5.36E+06	9.46E-06	4.36E-02	3.39E+00	1.81E+01	1.77E+01	1.12E+07	9.46E-01	1.08E+07	8.00E-01	7.63E+04	4.52E+04 6.00E+04
	Up-dip	i	3	45		8.00E+06	1.04E+07	2.88E+00 2.88E+00	5.82E-05 5.32E-05	2.49E-05 0.00E+00	1.06E-04 9.12E-05	2.49E-05 0.00E+00	4.63E+06 1.40E+22	6.11E-06	7.61E-02	3.42E+00	1.56E+01	1.52E+01	1.11E+07	9.32E-01	1.09E+07	7.97E-01	7.98E+04	
	Up-dip	1	3	52	8.00E+06	8.01E+06	1.16E+07	2.88E+00	5.06E-05	7.02E-06	9.71E-05	7.02E-06	8.07E+06	9.97E-06 1.50E-06	0.00E+00 2.14E-02	0.00E+00 1.67E+00	1.40E+01 1.35E+01	1.37E+01 1.31E+01	1.00E+07	9.84E-01	9.70E+06	9.81E-01		7.38É+04
	Up-dip Up-dio	1	3	33		2.32E+05	7.15E+06	1.10E+01	2.81E-06	4.83E-01	8.20E+06	2.93E+00	5.33E+00	0.00E+00	1.47E+03		3.21E+00	3.06E+00	1.15E+07 8.87E+06	9.61E-01 3.13E-01	1.02E+07 5.72E+06	5.98E-01 2.30E-01		5.94E+04 2.77E+04
	Up-dip	i	3	7 35	2.41E+05 8.03E+06	7.99E+06 8.00E+06	9.99E+06 8.98E+06	1.10E+01 2.88E+00	2.37E-06 4.66E-06	8.40E-01 3.87E-06	4.60E-06 7.49E-06	3.77E+00	2.09E+00		2.56E+03	1.22E+06		2.43E+00	9.13E+06	9.90€-01	5.83E+06	4.18E-01	7.32E+04	
	Up-dip	i	ž	2		2.63E+05	1.05E+07	1.10E+01	7.67E-07	9.32E-01	1.93E-06	4.13E-06 6.52E+00	1.27E+06 6.40E-01	1.20E-05 1.88E-05	1.18E-02 2.84E+03	9.77E-01 1.30E+06	1.24E+00			9.05E-01	8.34E+06	5.48E-01	6.81E+04	
	Up-dip	1	3	15		0.00E+00	7.81E+06	1.10E+01	7.74E-07	4.41E-01	1.98E-06	3.92E+00	1.31E+00	0.00E+00	1.35E+03	5.94E+05	8.29E-01 7.78E-01	7,88E-01 7,37E-01	9.96E+06 8.54E+06	6.18E-01 5.27E-01	5.96E+06 4.86E+06	3.78E-01 3.90E-01		
	Up-dip Up-dip	1	3	24 10		7.99E+06 2.34E+05	8.69E+06 8.77E+06	2.88E+00 1.10E+01	1.18E-06	1.46E-09	1,92E-08	1.77E-09	8.26E+08	1.77E-05	4.44E-06	3.70E-04	3.06E-01	2.98E-01	8.15E+06	9.11E-01	8.02E+06	9.07E-01		
	Up-dip	í	3	19		8.01E+06	9.52E+06	1.10E+01	1.08E-07 5.55E-08	7.10E-01 5.25E-01	3.28E-07 2.14E-07	5.85E+00 6.86E+00	1.22E-01 8.16E-02	1.72E-05 8.95E-06	2.17E+03 1.60E+03	1.06E+08	1.30E-01	1,24E-01	8.21E+06	4.99E-01	4.47E+06	1.72E-01	8.73E+04	2.94€+04
	Up-dip	1	3	94	3.22€+05	3.04E+05	1.12E+07	1.10E+01	1.19E-08	1.19E+00	4.20E-08	1.41E+01	8.03E-03	0.00E+00	1.60E+03 3.64E+03	8.36E+05 1.72E+06	6.82E-02 1.38E-02	6,36E-02 1,35E-02	9.01E+06 1.12E+07	8.56E-01 2.91E-01	4.48E+08 5.78E+06	1.24E-01 2.24E-01	7.09E+04	
	Up-dip	1	3	39		8.01E+06	1.08E+07	1.10E+01	2.87E-09	6.09E-01	1.32E-08	1.28E+01	3.61E-03	0.00E+00	1.86E+03	9.52E+05	3.43E-03	3.26E-03	1.09E+07	8.51E-01	5.76E+06 4.36E+06	2.24E-01 2.09E-01	8.06E+04 7.90F+04	
	Up-dip Up-dip	1	3	58 30			7.37E+06 9.39E+06	1.10E+01 1.10E+01	1.B2E-11 1.67E-11	8.26E-01 2.01E+00	9.22E-11 4.43E-11	2.22E+01 1.38E+01	1.52E-05		2.52E+03	1.57E+06	2.38E-05	2.24E-05	1.32E+07	1.69E-01	4.69E+06	1.27E-01		1.21E+04
	Up-dip	1	3	28	4.64E+05	4.44E+05		1.10E+01	8.22E-14	6.44E-01		2.27E+01	6.82E-06 8.28E-08	0.00E+00 0.00E+00	6.14E+03 1.96E+03	2.80E+06 1.20E+06	1.91E-05 9.92E-08	1.80E-05	9.85E+06	8.38E-02	6.52E+06	5.31E-02	8.22E+04	4.71E+03
	Up-dip	f	3	78			8.01E+06	1.10E+01	5.48E-05	1.40E-01	1.51E-04	1.84E-01	5.76E+02	0.00E+00	4.29E+02	1.13E+05	6.48E+01	9.71E-08 6.19E+01	1.33E+07 1.24E+07	2.10E-01 9.47E-01	4.12E+06 1.10E+07	1.82E-01 4.91E-01	8.93E+04 8.49E+04	1.66E+04
	Up-dip Up-dip	1	3	69 52			8.00E+06 8.01E+06	2.88E+00	5.90E-05	9.12E-05	1.07E-04	9.12E-05	1.20E+06	0.00E+00	2.78E-01	1.33E+01	1.58E+01	1.55E+01	1.12E+07	9.19E-01	1.10E+07	7.92E-01		6.00E+04 6.81E+04
	∩b-qib ob-qib	í	3	45				2.88E+00 2.88E+00	5.84E-05 5.42E-05	2.29E-05 0.00E+00	1.11E-04 9.18E-05		.2.79E+06 1.43E+22	0,00E+00 0.00E+00	7.00E-02	5.56E+00	1.55E+01	1.51E+01	1.09E+07	9.61E-01	1.06E+07	6.03E-01	7.88E+04	6.01E+04
	Up-dip	1	3	44	3.13E+05		8.00E+06	1.10E+01	9.09E-06	1.10E+00					0.00E+00 3.36E+03	0.00E+00 1.33E+06	1.43E+01 1.13E+01	1.39E+01 1.08E+01	1.01E+07 1.10E+07	9.72E-01 B.B7E-01	9.84E+06 7.86E+06	9.68E-01	7.57E+04	
	Up-dip	!	3	24				2.88E+00	2.17E-05	5.66E-07	3.03E-05	5.66E-07	8.26E+07	0.00E+00	1.73E-03		5.53E+00	5.40E+00	8.86E+06	9.10E-01	8.74E+06	2.35E-01 8.45E-01	7.97E+04 7.03E+04	
	Up-dip Up-dip	i	3	16 39			8.94E+05 8.01E+06	1.10E+01 1.10E+01	7.30E-07 1.87E-07	5.22E-01 4.12E-01	2.12E-06 7.79E-07		1.13E+00			7.47E+05	B.47E-01	8.08E-01	8.67E+06	6.90E-01	4.89E+06	4.13E-01	6.96E+04	
784 (Jp-dip	1	3	97			8.02E+06	1.10E+01	1.23E-07	2.37E-01	5.75E-07	6.28E+00 4.65E+00	3.63E-01 3.68E-01	0.00E+00 0.00E+00	1.26E+03 7.24E+02	6.11E+05	2.22E-01 1.63E-01	2.06E-01 1.57E-01	9.57€+06	8.51E-01	4.32E+06	2.55E-01		3.99E+04
	Jp-dip	1	3	19			8.02E+06	1.10E+01	3.85E-08	5.86E-01		7.98€+00	5.03E-02		1.79E+03		4.74E-02	4.68E-02	8.70E+06 9.40E+06	9.15E-01 8.52E-01	3.35E+06 4.62E+06	3.84E-01 1.12E-01	6.92E+04 7.30E+04	4.44E+04 3.16E+04
	Up-dip Up-dip	1	3	60 94			8.04E+06 2.82E+05	1,10E+01 1,10E+01	5,30E-09 4,93E-09	1.43E-01		6.38E+00	2.20E-02				7.89E-03	7.82E-03	8.51E+06	9.13E-01		1.15E-01		2.72E+04
	Up-dip	i	3	28			8.15E+06	1.10E+01	6.06E-10	1.21E+00 2.91E+01		1.46E+01 8.39E+00	3.29E-03 1.47E-03		3.68E+03 8.87E+02	1.75E+06 5.29E+05	5.74E-03 7.78E-04	5.62E-03	1.12E+07	3.51E-01		2.17E-01		2.96E+04
	Jp-dip	1	3	52		B.00E+06	8.00E+06	1.10E+01	2.57E-05	1.45E-01					4.43E+02		3.12E+01	7.33E-04 2.98E+01	9.21E+06 8.86E+06	8.95E-01 9.61E-01	3.06E+06 6.71E+06	2.17E-01 4.68E-01	7.15E+04 6.94E+04	2.81E+04
	qib-qt Jp-qip	1	3	45 69				2.88E+00 2.88E+00	7.48E-05 5.97E-05	2.68E-06	1.25E-04				8.18E-03	5.10E-01	1.97E+01	1.92E+01	1.10E+07	9.50E-01	1.07E+07	9.47E-01	7.95E+04	
	Jp-dip	i	3	24				2.88E+00	5.97E-05 4.72E-05	9.44E-05 1.19E-04	1.08E-04 6.97E-05	9.44E-05 1.19E-04		0.00E+00 0.00E+00	2.88E-01 3.63E-01	1.38E+01	1.60E+01	1.57E+01	1.13E+07	9.12E-01	1.11E+07	7.56E-01	8.05E+04	6.64E+04
	Jp-dip	1	3	100			8.00E+06	2,88E+00	1.07E-05	1.21E-06	1.95E-05	1.21E-06		0.00E+00	3.69E-03	8.59E+00 2.61E-01	1.25E+01 2.93E+00	1.22E+01 2.86E+00	9.83E+06 8.79E+06	9,10E-01 8,87E-01	9.70E+06 8.65E+06	6.77E-01 7.24E-01	7.47E+04	5.83E+04
	Jp-dip Jo-din	1	3	19 60				1.10E+01	2.55E-10	1.06E+00	1.11E-09	1.77E+01	1.81E-04		3.23E+03	1.75E+06	3.16E-04	3.15E-04	1.21E+07	6.20E-01	5.38E+06	4.68E-02	6.90E+04 8.41E+04	5.49E+04 2.43E+04
	Jo-dio	ì	3	94	2.89E+05 3.90F+05		6.04E+06 1.30E+06	1.10E+01 1.10E+01	1.70E-10 3.58E-12	1.65E-01 1.26E+00		7.99E+00 1.62E+01		0.00E+00	5.02E+02	4.14E+05	2.54E-04	2.41E-04	8.35E+06	7.90E-01	2.32E+06	7.87E-02		
797 L	Jp-dip	1	3	24				1.10E+01	4.14E-05	1.10E-01	8.13E-05		4.79E+02	0.00E+00 0.00E+00	3.83E+03 3.35E+02	1.85E+06 9.31E+04	4.11E-06 4.46E+01	3.99E-06 4.24E+01	1.12E+07 9.25E+06	7.58E-01 9.10E-01	5.58E+06	1.93E-01		
	jp-dip	1	. 3	45				2.88E+00	1.01E-04	7.70E-06	1.70E-04	7.70E-06	2.01E+07	0.00E+00	2.35E-02		2.87E+01	2,60E+01	1.20E+07	9.50E-01	8.64E+06 1.16E+07	4,62E-01 9.47E-01	7.22E+04 8.34E+04	
	Jp-dip Jp-dip	1	3	69				2.88E+00 2.88E+00	5.40E-05 1.55E-05	6.39E-05 1.27E-06	9.69E-05 2.98E-05		1.51E+06			9.68E+00	1.44E+01	1.41E+01	1.10E+07	9.12E-01	1.08E+07	7.46E-01	7.92E+04	6.49E+04
801 L	Jp-dip	1	3	100	8.00E+06	B.00E+06		2.88E+00	7.84E-06	5.87E-07	1.43E-05		1.54E+07 1.66E+07		3.88E-03 1.79E-03			4.18E+00 2.10E+00		9.02E-01	8.81E+06	7.61E-01	6.99E+04	5.75E+04
	Jp-dip	1	3	86				1.10E+01	1.85 E -10	2.11E-01	1.18E-09	7.00E+00	5.83E-04	2.12E-07	6.44E+02		2.50E-04	2.10E+00 2.50E-04	8.61E+06 8.01E+06	8.86E-01 9.20E-01	8.48E+06 2.61E+06	7.13E-01 4.61E-02	6.73E+04 6.38E+04	5.31E+04 2.81E+04
	Jp-dip Jp-dlo	1	3	45 69				2.88E+00 2.88E+00	1.58E-04 4.81E-05	5.40E-05 4.15E-05				0.00E+00		5.92E+00	4.14E+01	4.05E+01	1.36E+07	9.50E-01	1.32E+07	9.46E-01		8.58E+04
805 L	Jp-dlp	1	3	1	8.00E+06			2,88E+00		2.43E-06	8.54E-05 3.75E-05	4.15E-05 2.43E-06		0.00E+00 0.00E+00	1.27E-01 7.42E-03	6.60E+00 5.29E-01		1.25E+01 5.26E+00		9.12E-01	1.05E+07	6.51E-01	7.80E+04	5.98E+04
	Jp-dip	1	4	58	3.42E+05	3.30E+05	0.00E+00	1.10E+01	6.40E-09	6.60E-01	3.51E-08	1.75E+01	6,80E-03	0.00E+00	2.02E+03	1.23E+06	6.38E+00 B.39E-03	8.25E-03		9.02E-01 2.12E-01	9.02E+D6 4.26E+D6	6.98E-01		5.63E+04 1.83E+04
	Jp-dip Jp-dio	1	4	28 94			0.00E+00 0.00E+00	1.10E+01 1.10E+01	1.28E-10 8.01E-08	4.89E-01		1.61E+01				9.34E+05	1.67E-04	1.67E-04		2.27E-01	3.57E+06	1.99E-01		1.99E+04
B09 L	lp-dlp	i	4	58			0.00E+00	1.10E+01	8.01E-08 2.40E-09	7.10E-01 8.26E-01					2.17E+03 2.52E+03		9.22E-02	8.80E-02		6.08E-01	4.80E+06	2.59E-01	7.75E+04	3.46E+04
	lp-dip	1	4	19		2.80E+05	0.00E+00	1.10E+01	7.32E-09	7.10E-01	2.9BE+08	1.05E+01	7.81E-03	0.00E+00	2.52E+03 2.17E+03		3.16E-03 9.03E-03	2,96E-03 8,56E-03	1.28E+07 1.00E+07	1.99E-01 4.15E-01	4.74E+06 4.76E+06	1.57E-01 8.06E-02	9.72E+04 7.57E+04	1.61E+04
	Jp-dip Jp-dlp	1	4	94 94				1,10E+01 1,10E+01		1.25E+00		1.55E+01	1.25E-03	0.00E+00	3.80E+03	1.82E+06	2.27E-03	2.20E-03		8.49E-01	5.73E+06	2.10E-01		2.06E+04 4.07E+04
) p-qi p	i	5	19				1.10E+01				1.69E+01 6.19E+00			3.93E+03 1.49E+03		2.11E-06	2.03E-06		9.94E-01	5.63E+06	1.90E-01	B.15E+04	4.41E+04
	lp-dlp	1	5	94	3.30E+05	5.73E+05	0.00E+00	1.10E+01	9.69E-09	1.25E+00					3.80E+03	1.80E+06	7.26E-02 1.13E-02	6.86E-02 1.10E-02	8.57E+06 1.15E+07	4.67E-01 6.72E-01	4.37E+06 5.86E+06	1.27E-01 2.21E-01		2.36E+04
	Jp-dip Jo∙dio	1	5	58	4.78E+05			1.10E+01			7.12E-11	2.72E+01	7.33E-06	0.00E+00	8.18E+03	3.62E+06	2.66E-05	2.53E-05	1.39E+07	1.68E-01	7.78E+06	1,25E-01		3.67E+04 1.28E+04
	∖b-q,βc ìb∙aib	i	5	26	4.02E+05 4.64E+05											2.86E+08	1.65E-05	1.55E-05	1.03E+07	4.24E-01	6.48E+06	5.26E-02		1.22E+04
318 U	lp-dip	1	5	19	2.52E+05												9.77E-08 4.70E-02	9.55E-08 4.37E-02		2.11E-01 4.56E-01	4.12E+06	1.82E-01	8.94E+04	1.66E+04
	lp-dlp	1	5	94			0.00E+00	1.10E+01	3.77E-09	1.26E+00	1.35E-08	1.54E+01	2.41E-03	0.00E+00	3.83E+03					4.56E-01 7.13E-01	4.48E+06 5.80E+06	1.14E-01 2.14E-01		2.29E+04 3.77E+04
	lp-dip lp-dip	i	5	19 94	3.65E+05 3.74E+05		0.00E+00 0.00E+00						1.71E-04	0.00€+00	2.93E+03	1.58E+06	2.69E-04	2.65E-04	1.14E+07	3.75E-01	5.16E+06	4.67E-02		1.75E+04
~ '	γ υψ	•		87	0.7 TETOU	r.984+00	0.006100	·	1.39E-10	1.28E+00	4.B1E-10	1.64E+01	8.59E-05	0.00E+00	3.92E+03	1.89E+06	1.62E-04	1.56E-04	1.15E+07	9.94E-01	5.69E+06	1.99E-01	8.16E+04	



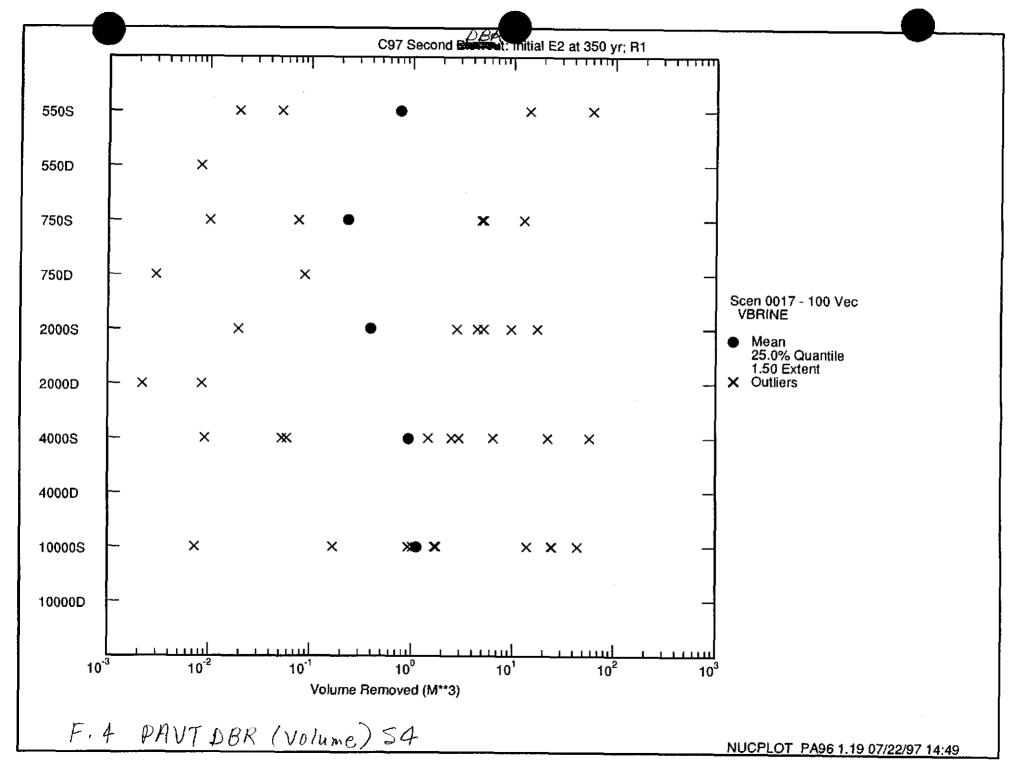
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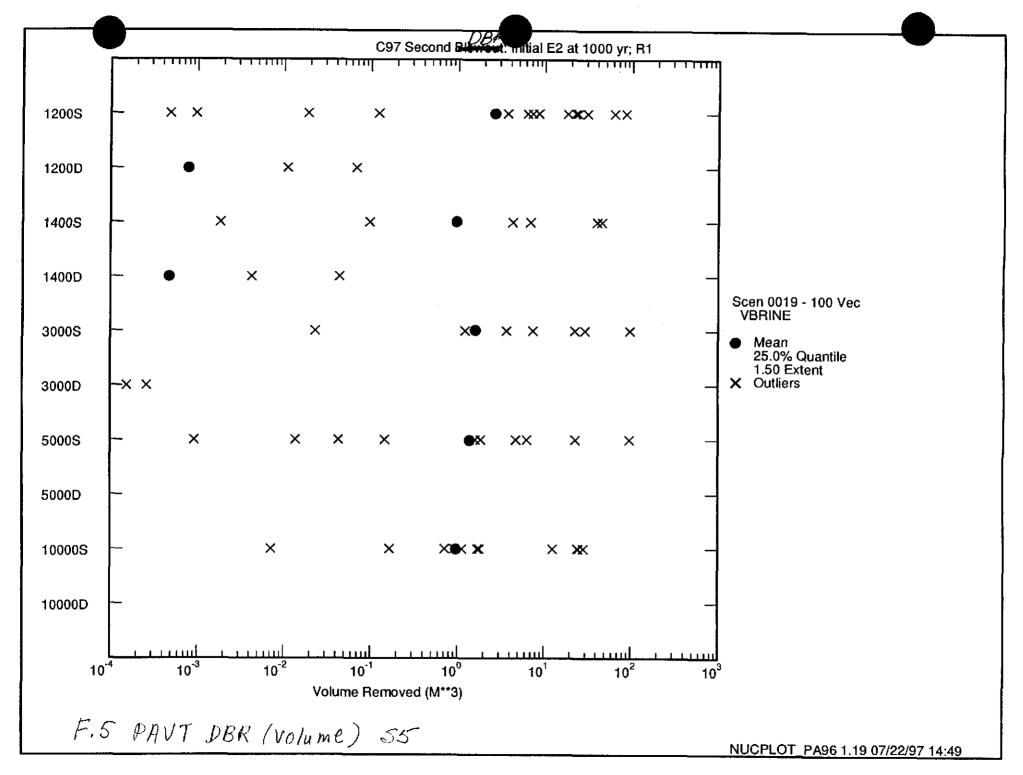
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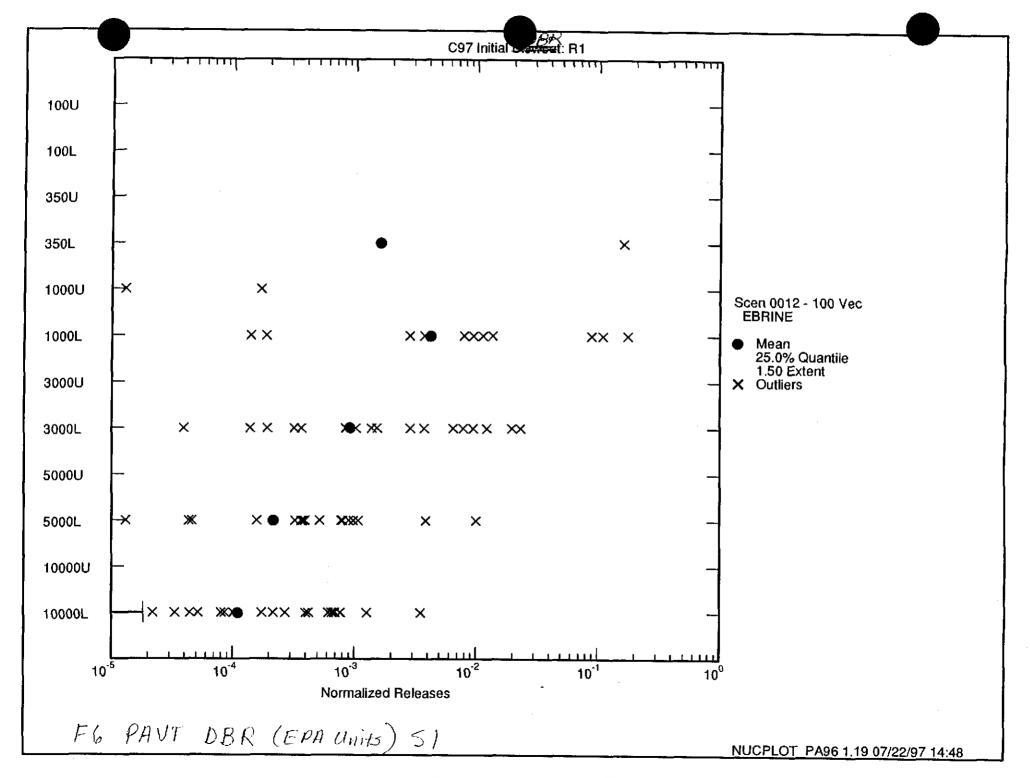
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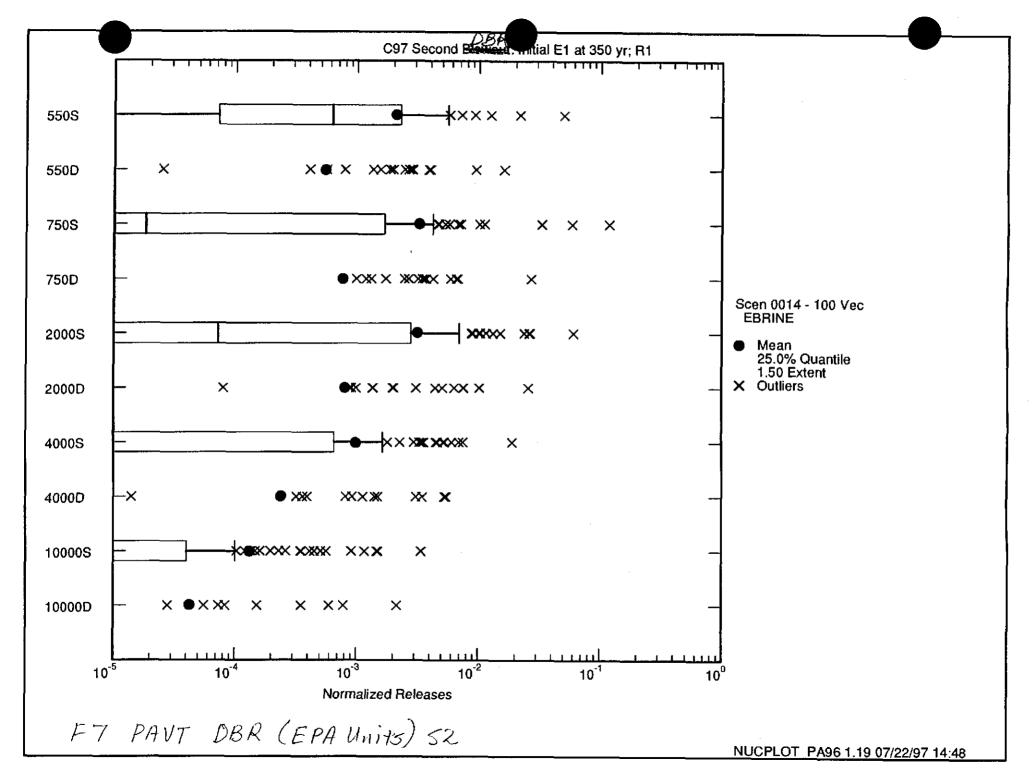
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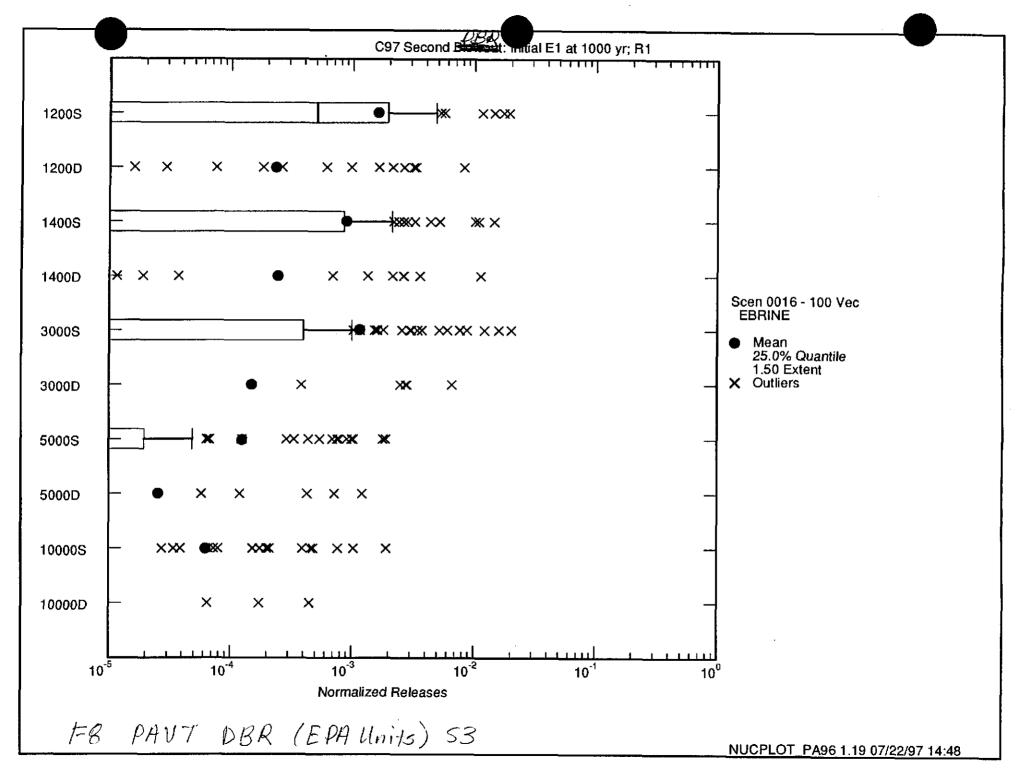
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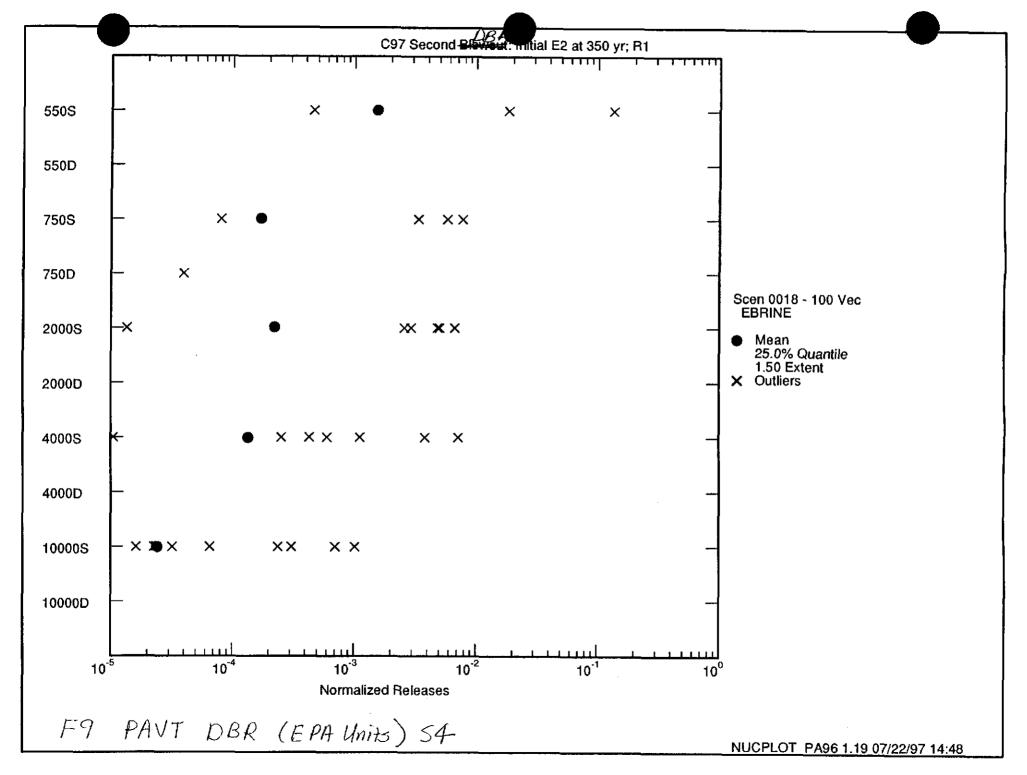
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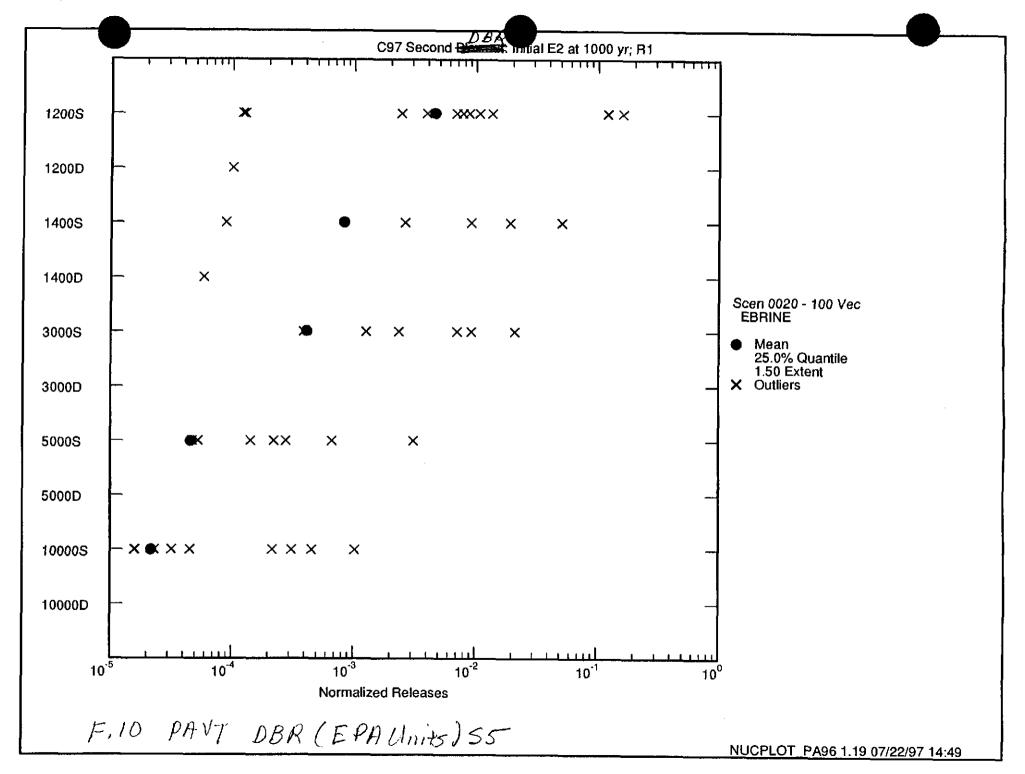
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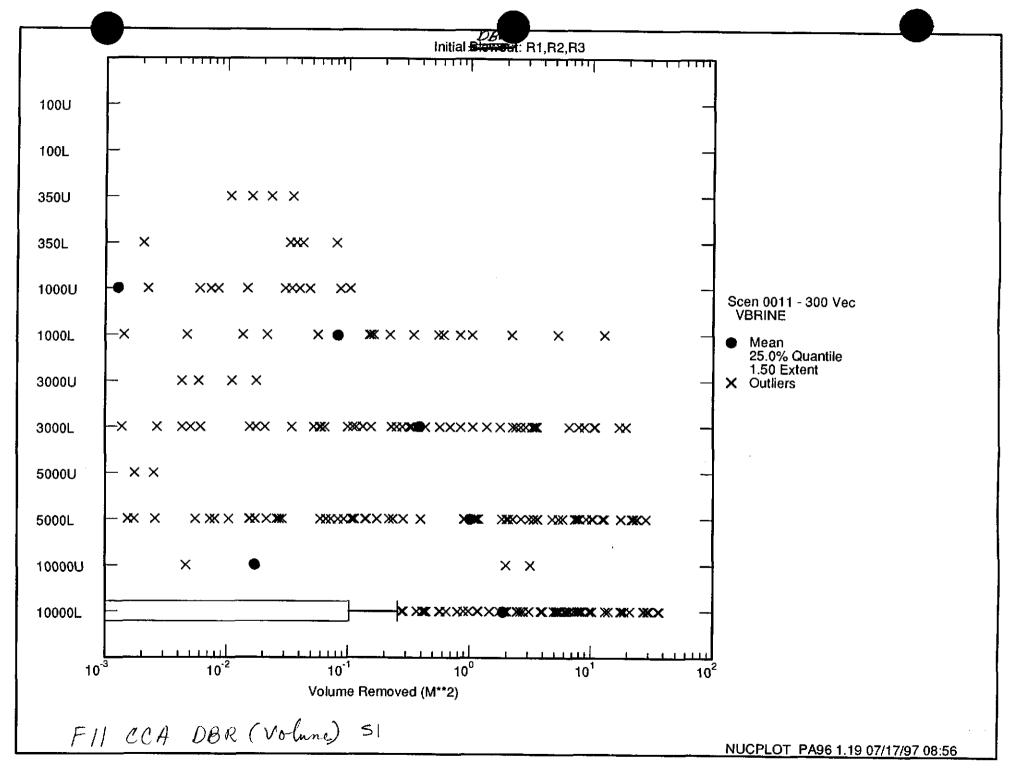
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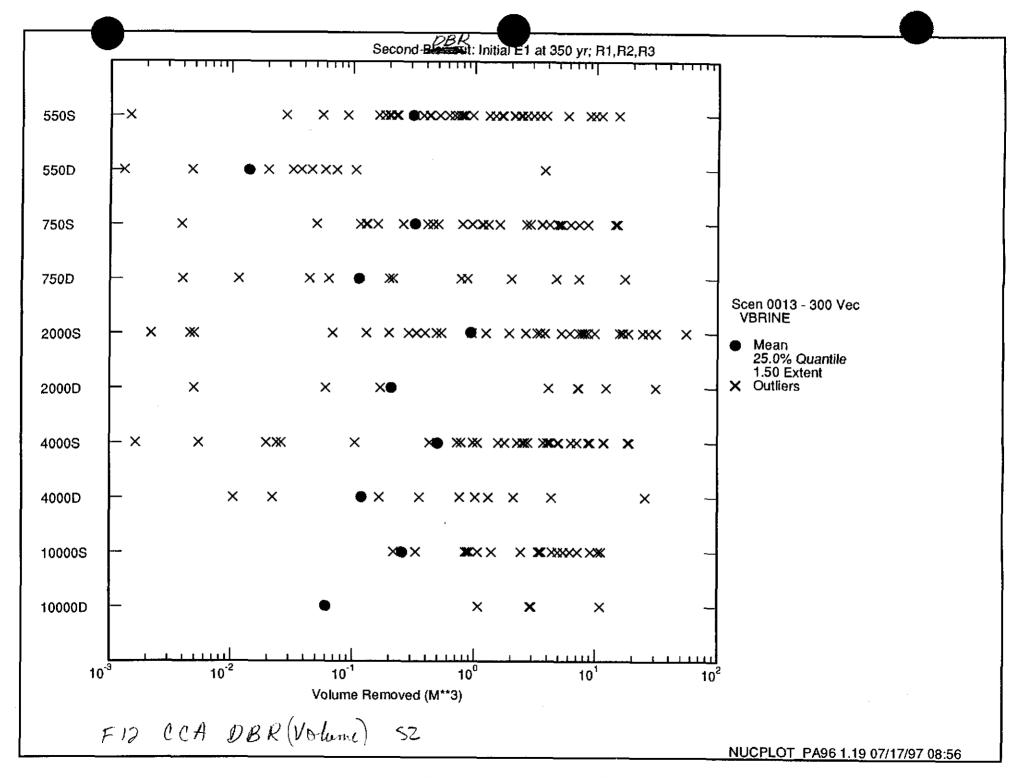
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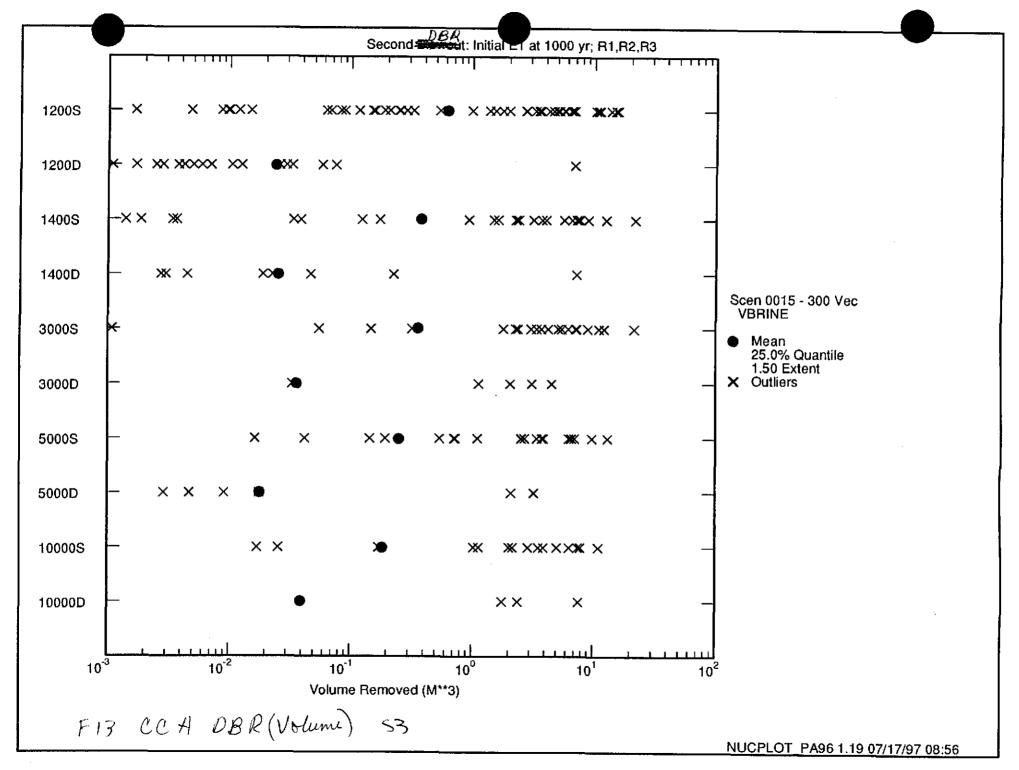
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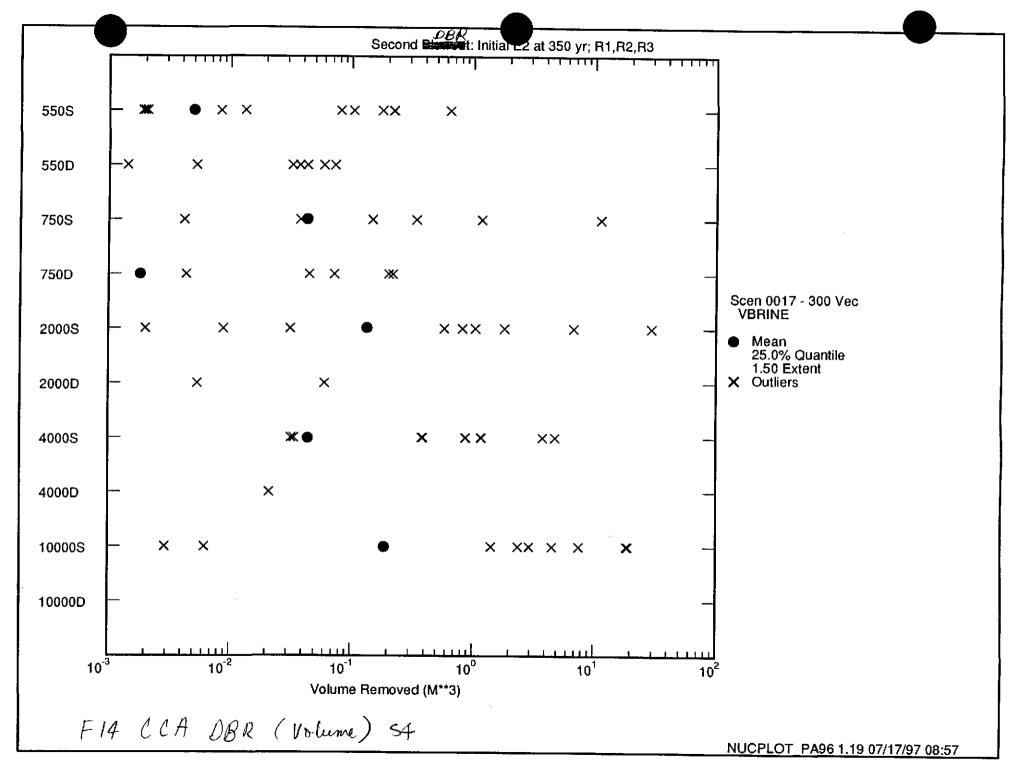
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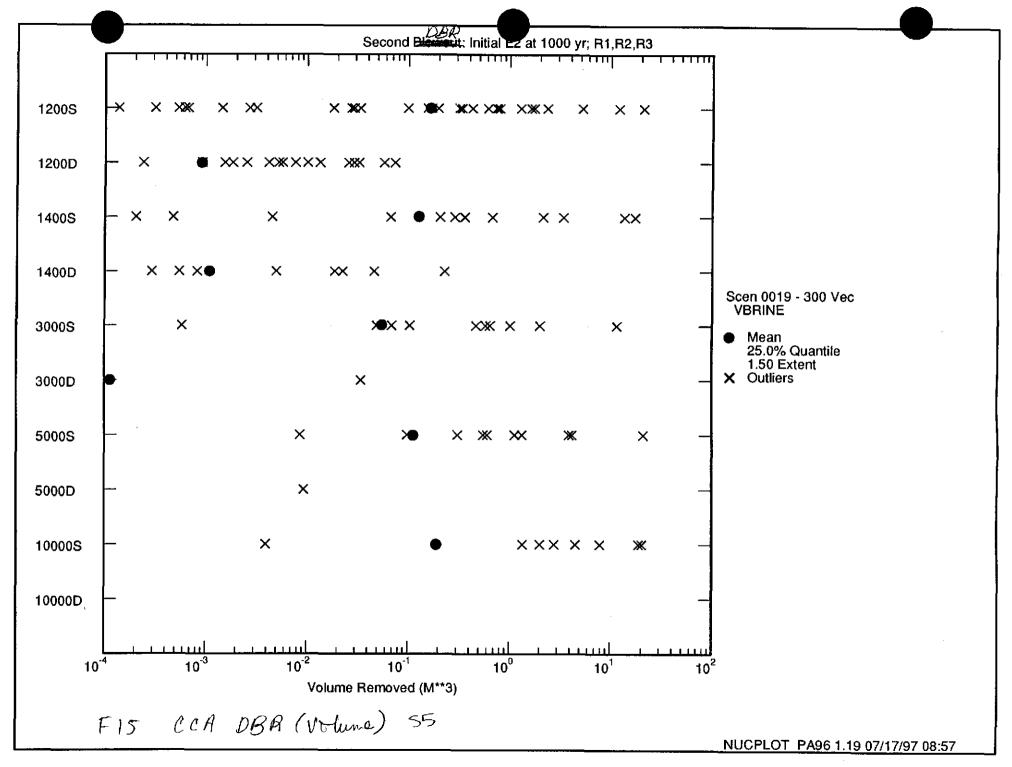
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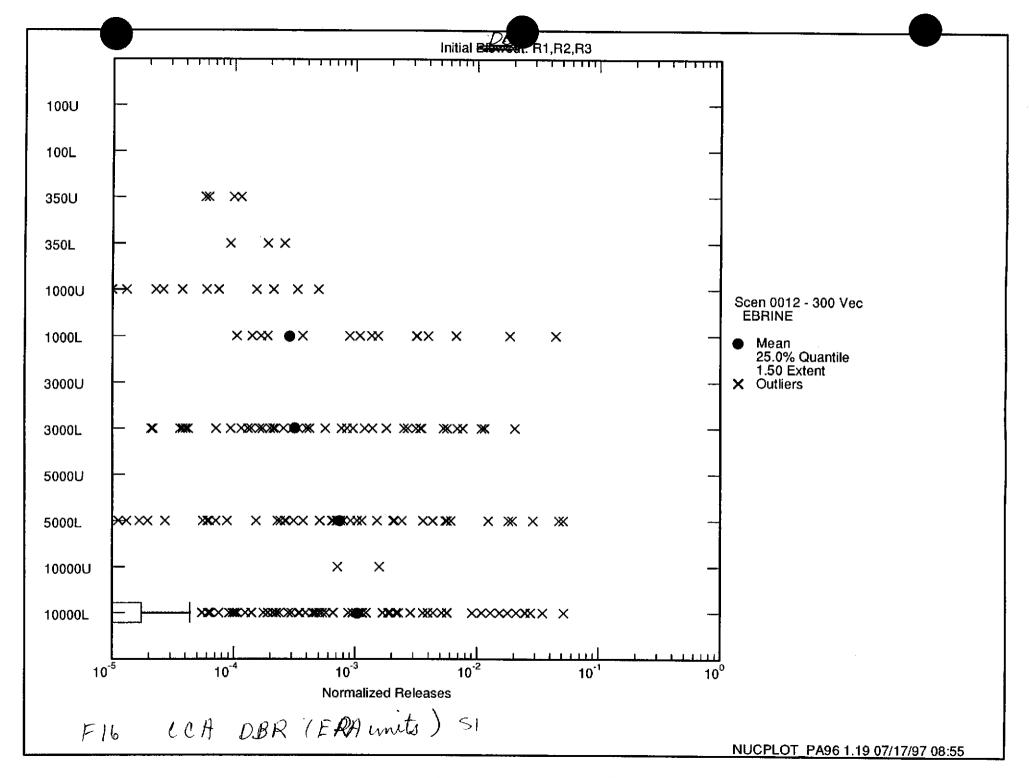
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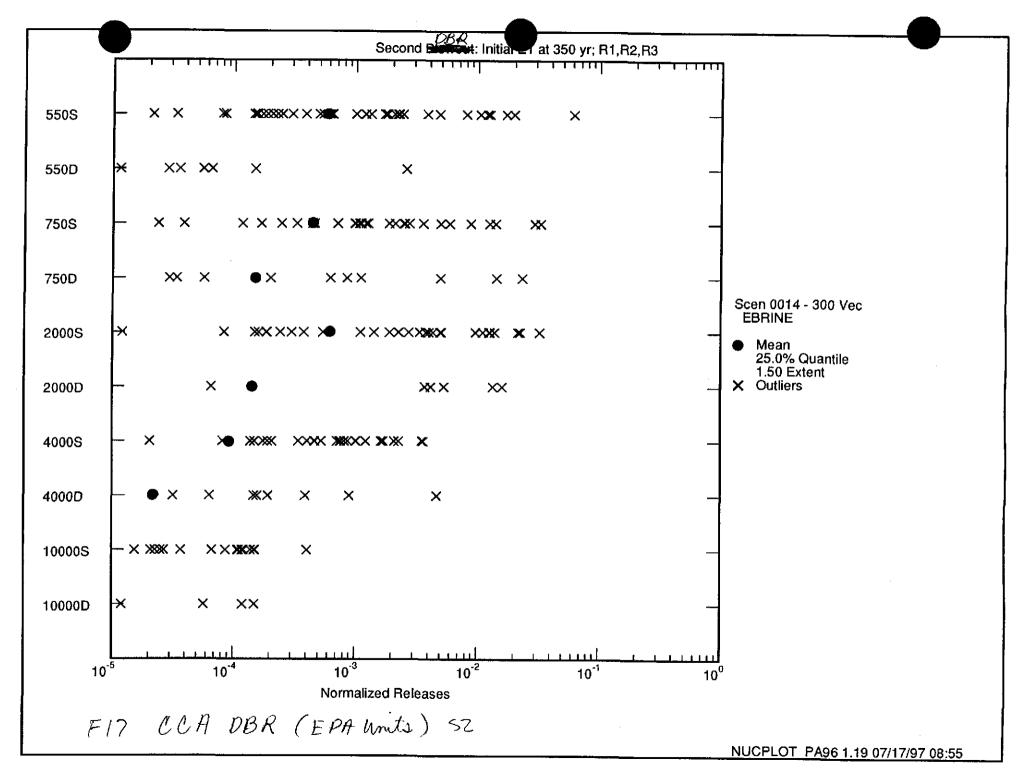
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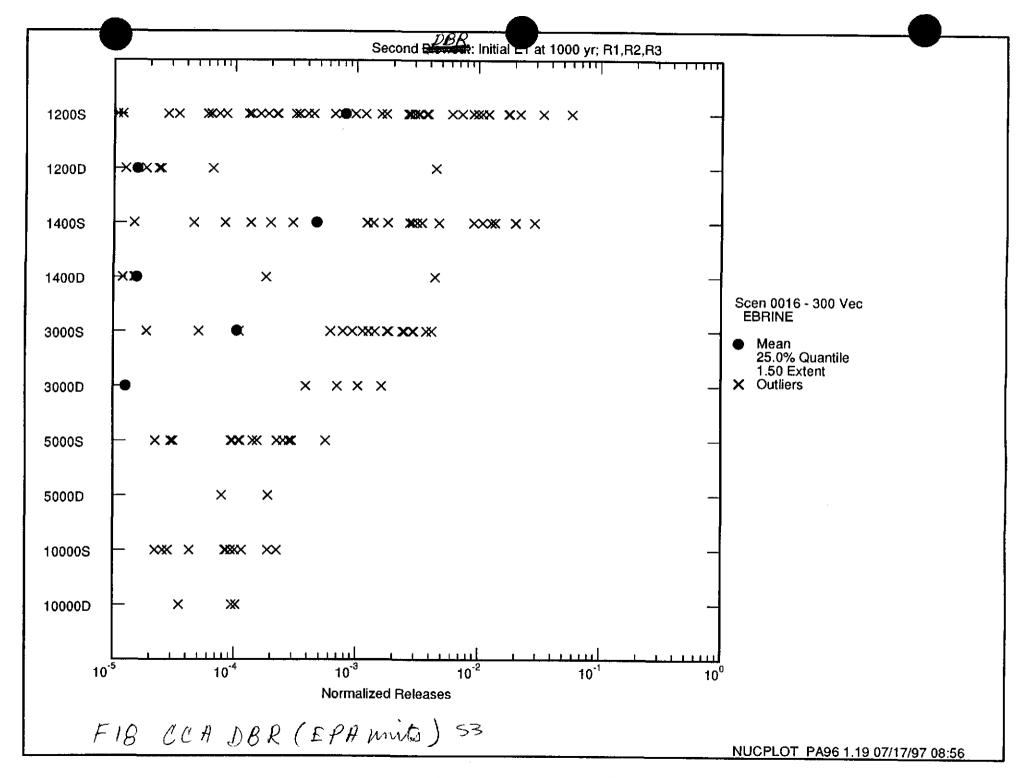
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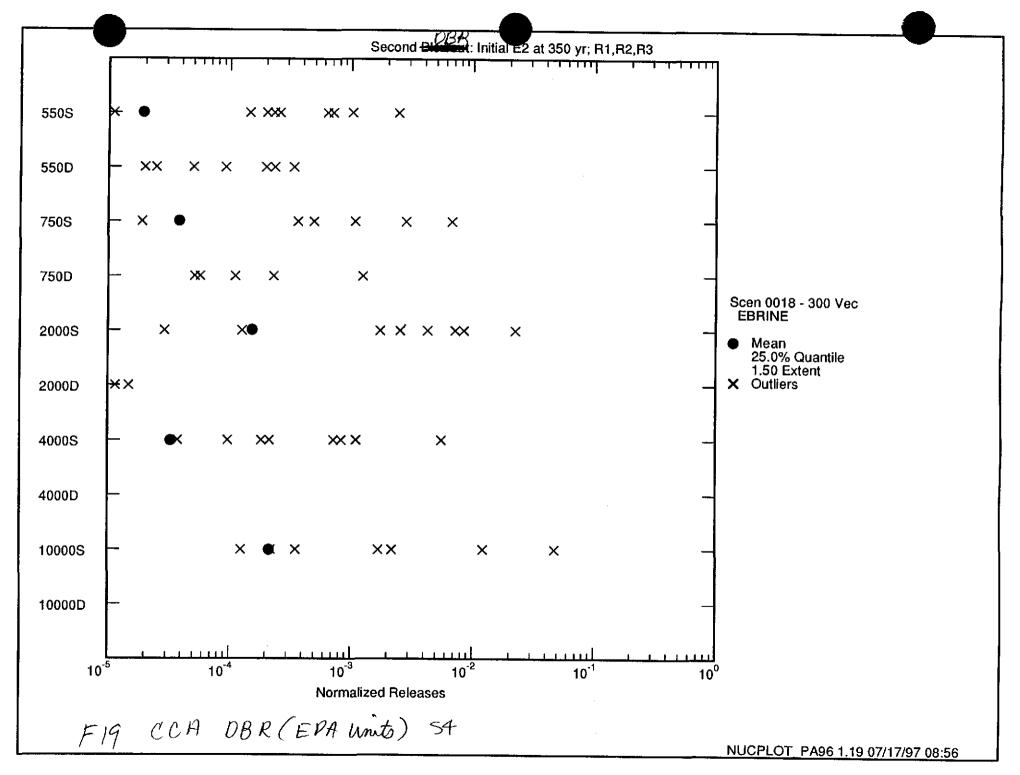
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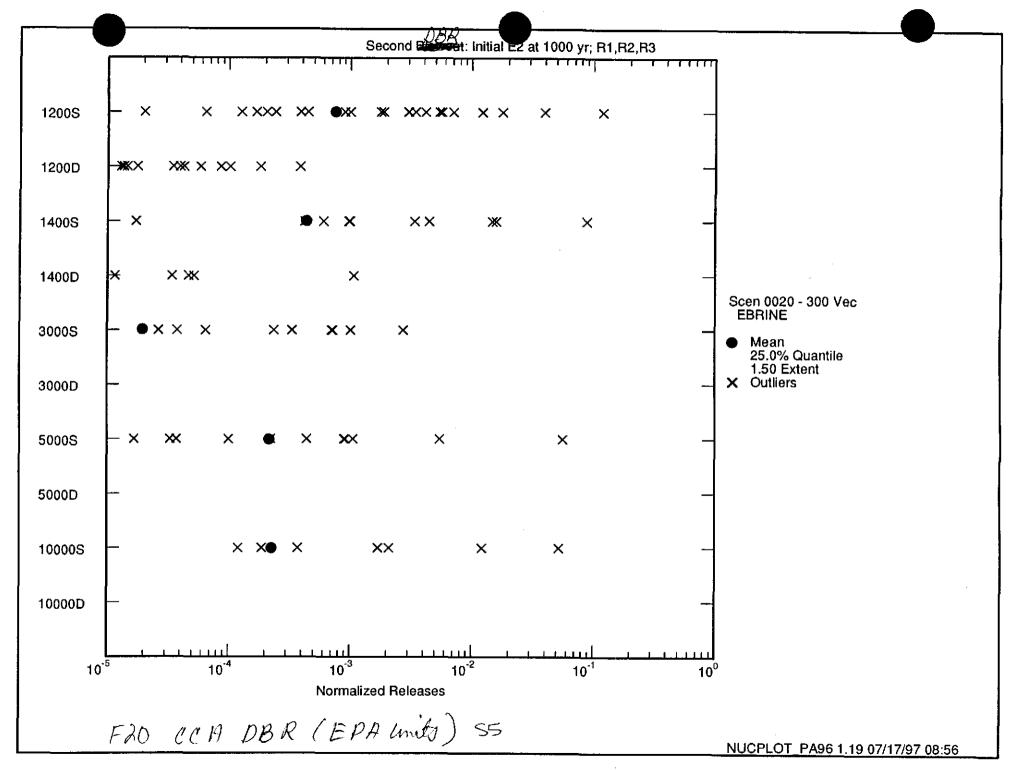
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APPENDIX G CCDF_GF RESULTS

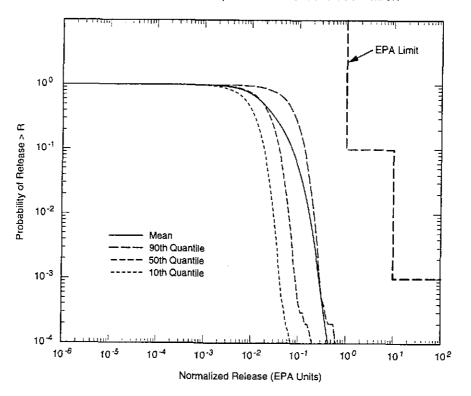
Appendix G includes Figures which contain CCDF results from CCDF_GF.

Figures

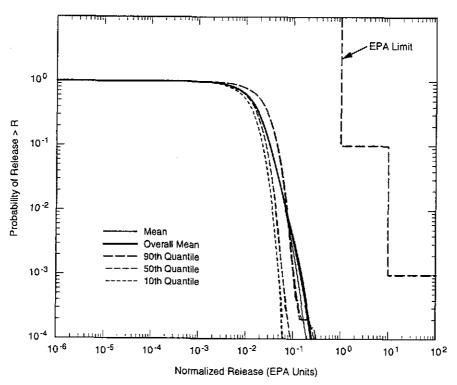
- G.1 G.3 Summary PAVT and CCA CCDFs for cuttings/cavings, spallings, and direct brine release (blowout)
- G.4 G.18 PAVT replicate 1 CCDFs
- G.19 G.77 CCA replicates 1,2, and 3 CCDFs

Note: Some of these figure titles use the term blowout instead of direct brine release. They are equivalent.

Cuttings Normalized Releases: PAVT-R1 100 Observations, 10000 Futures/Observation

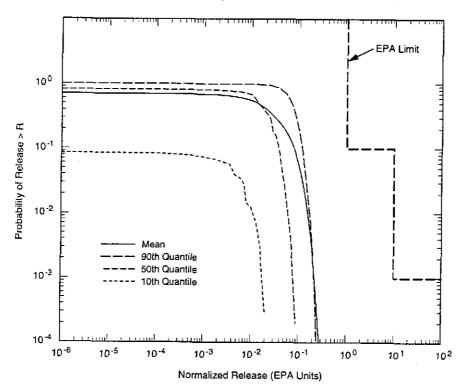


Cuttings Normalized Releases: CCA, R1, R2, R3 300 Observations, 10000 Futures/Observation

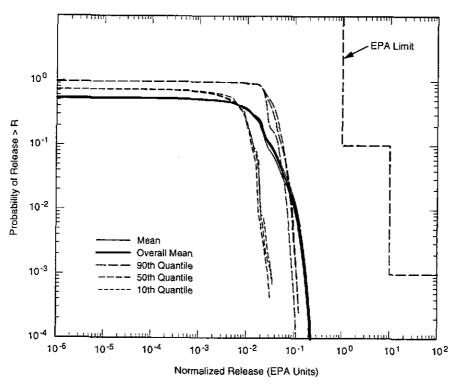


TRI-6342-5531-0

Spallings Normalized Releases: PAVT-R1 100 Observations, 10000 Futures/Observation

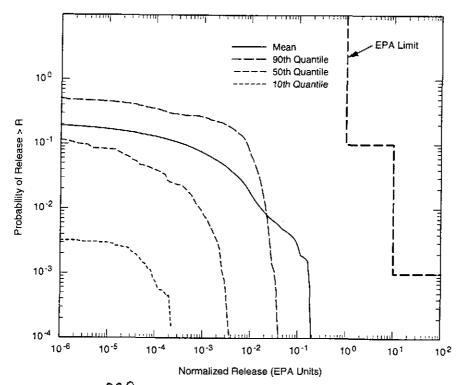


Spallings Normalized Releases: CCA, R1, R2, R3 300 Observations, 10000 Futures/Observation

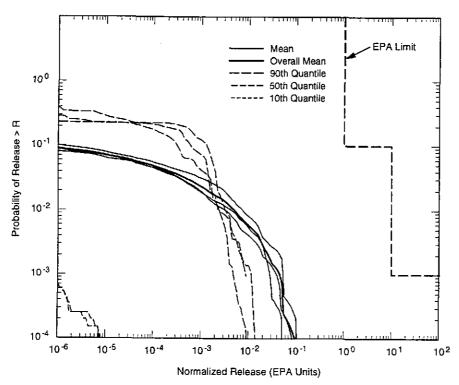


TRI-6342-5532-0

Planeut Normalized Releases: PAVT-R1 100 Observations, 10000 Futures/Observation

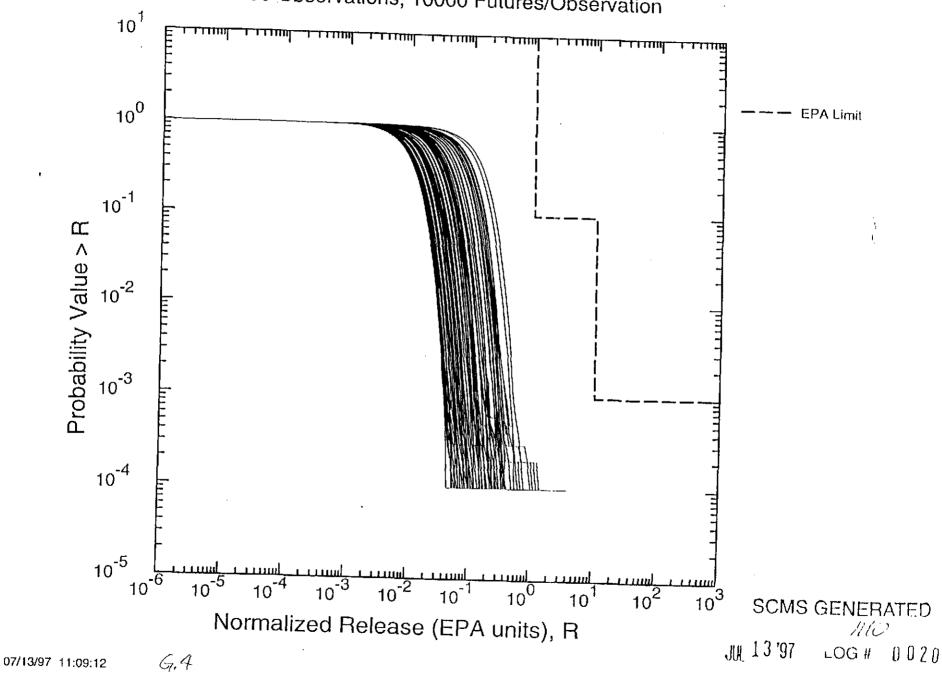


200 Observations, 10000 Futures/Observation

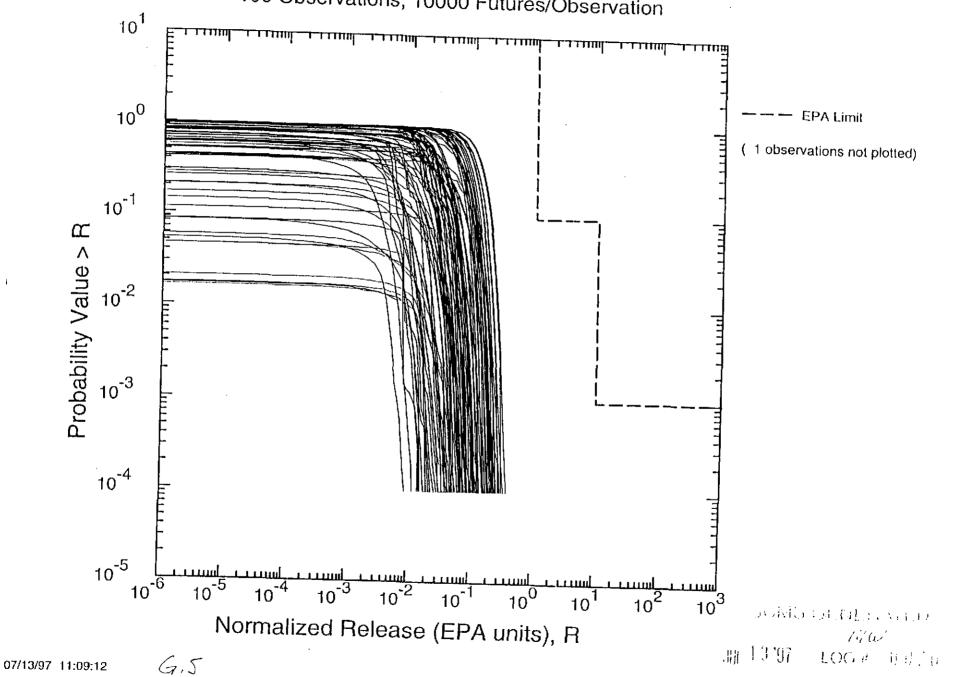


TRI-6342-5533-0

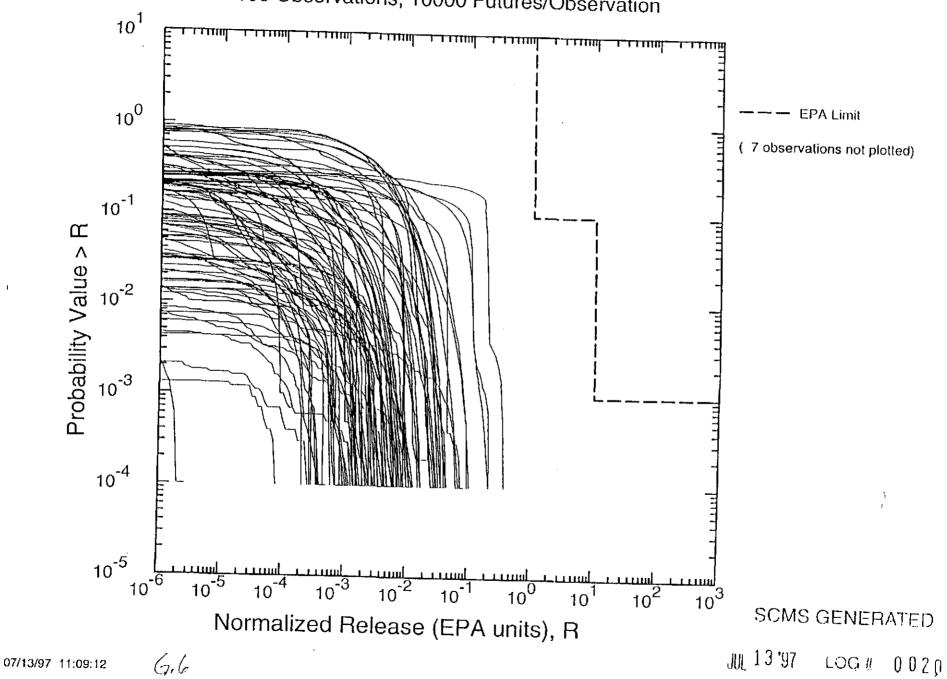
Cuttings Normalized Releases 100 Observations, 10000 Futures/Observation



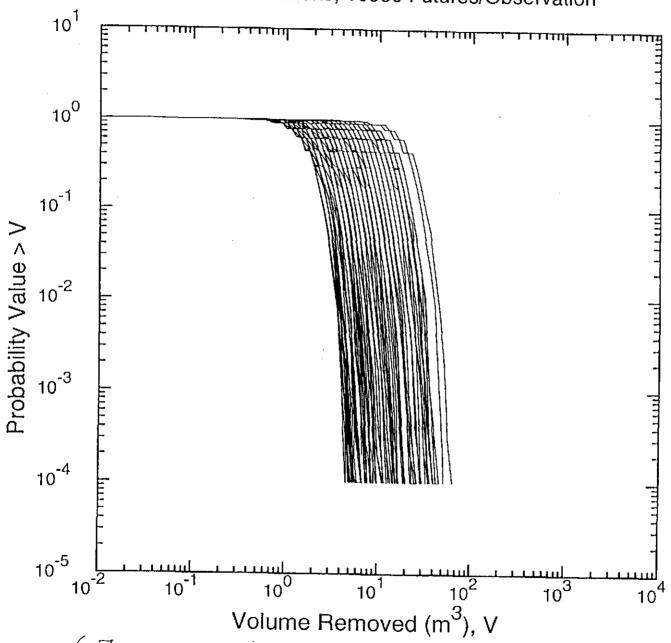
Spallings Normalized Releases 100 Observations, 10000 Futures/Observation



DBR Blowout Normalized Releases 100 Observations, 10000 Futures/Observation



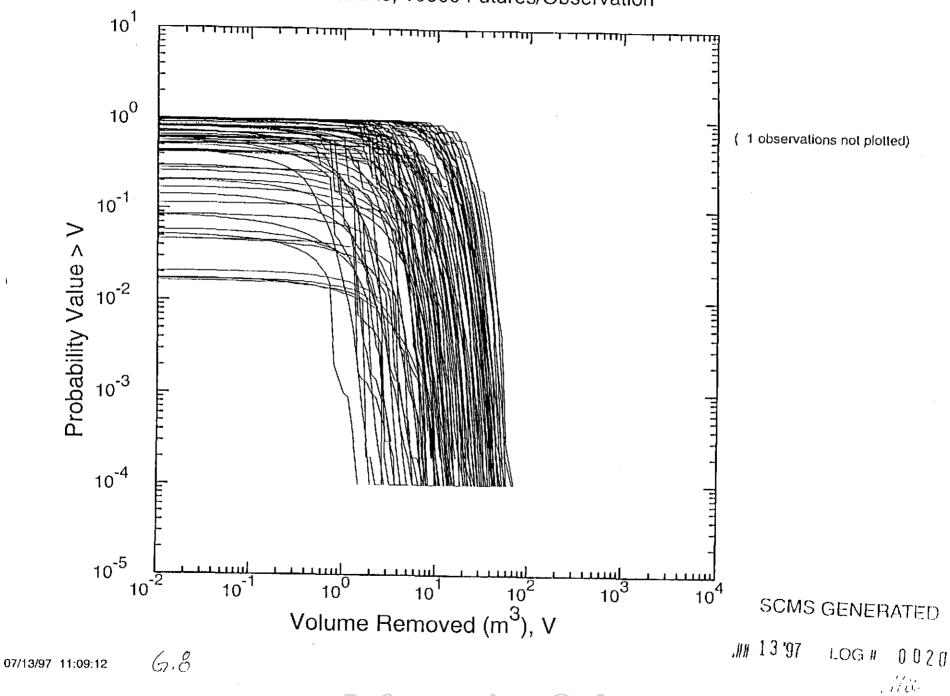
Cuttings Volume Releases
100 Observations, 10000 Futures/Observation



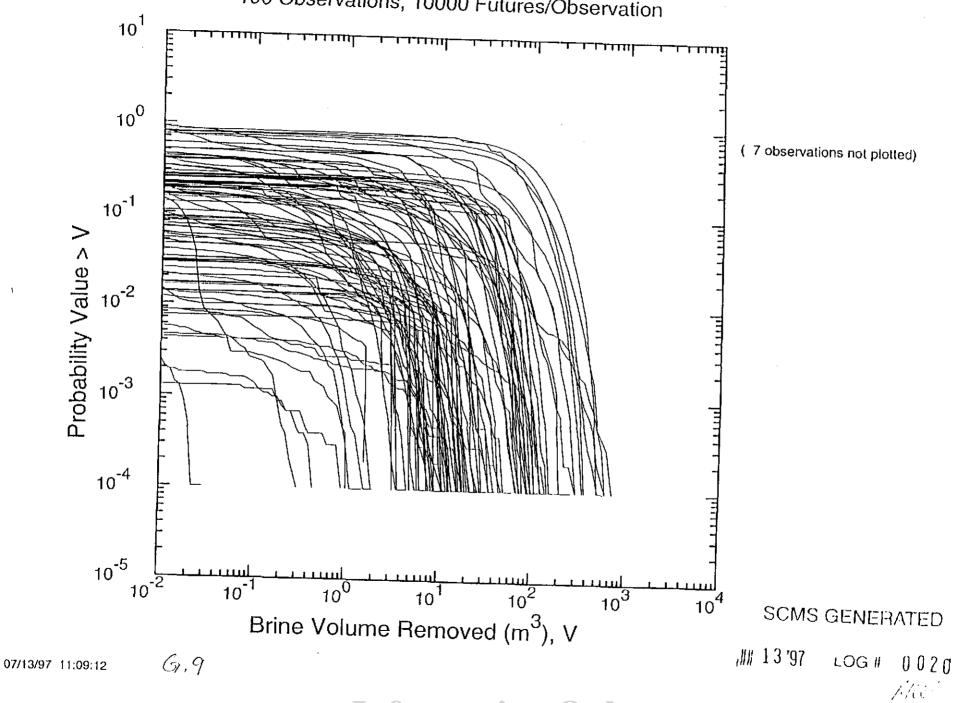
SCMS GENERATED

JIII 13'97 LOG# 0020

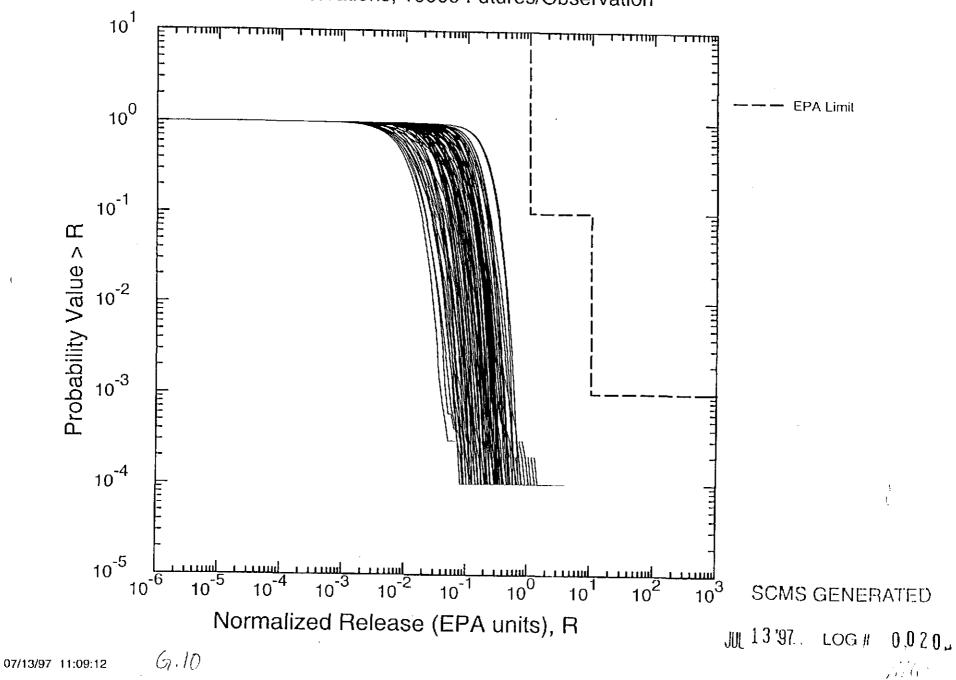
Spallings Volume Releases 100 Observations, 10000 Futures/Observation



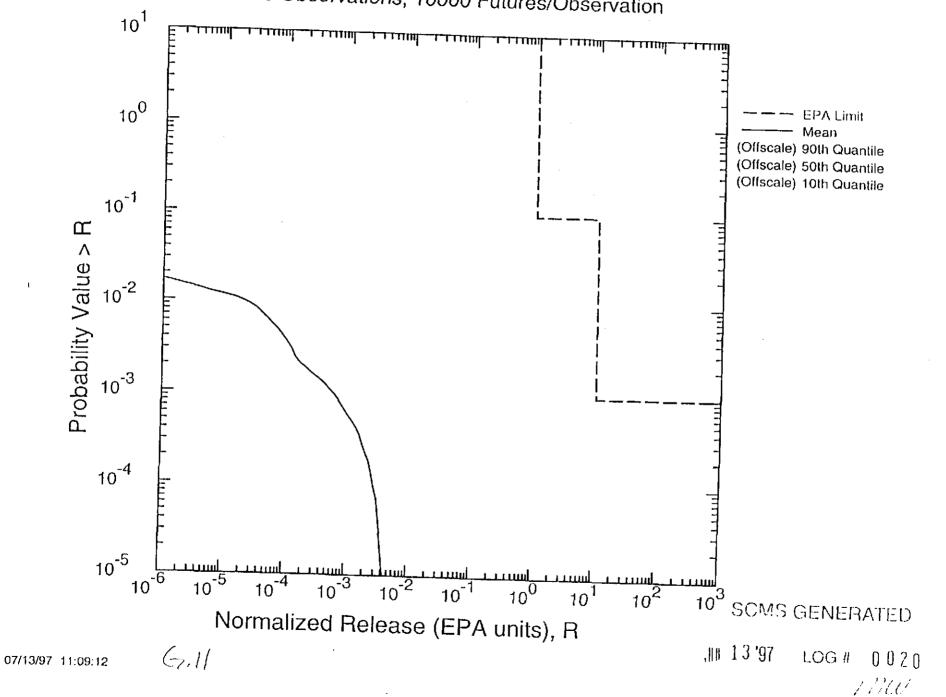
100 Observations, 10000 Futures/Observation



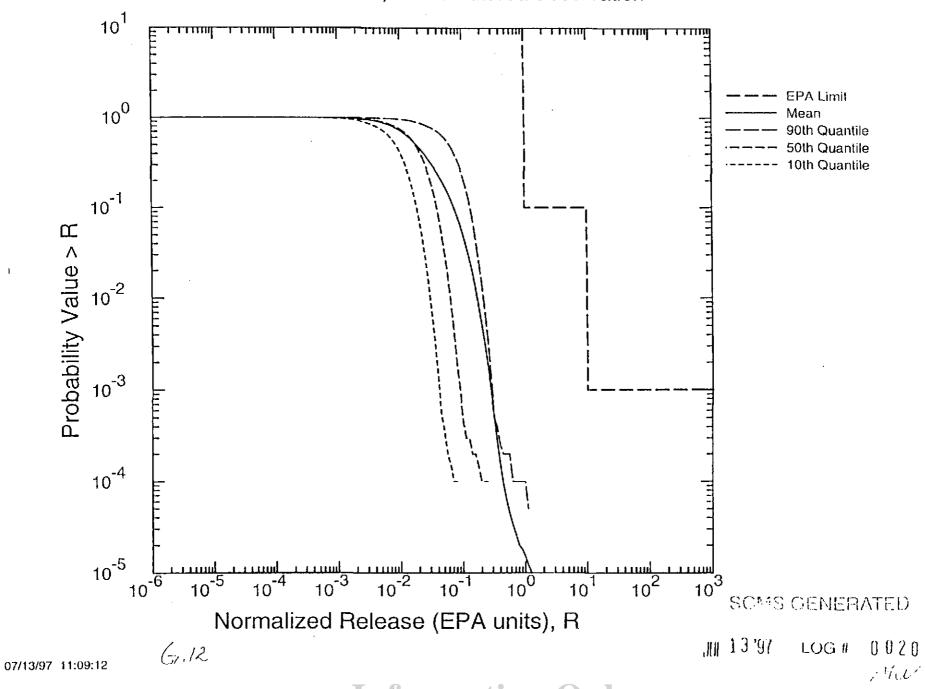
Cutting+Spalling+Blower Normalized Releases 100 Observations, 10000 Futures/Observation



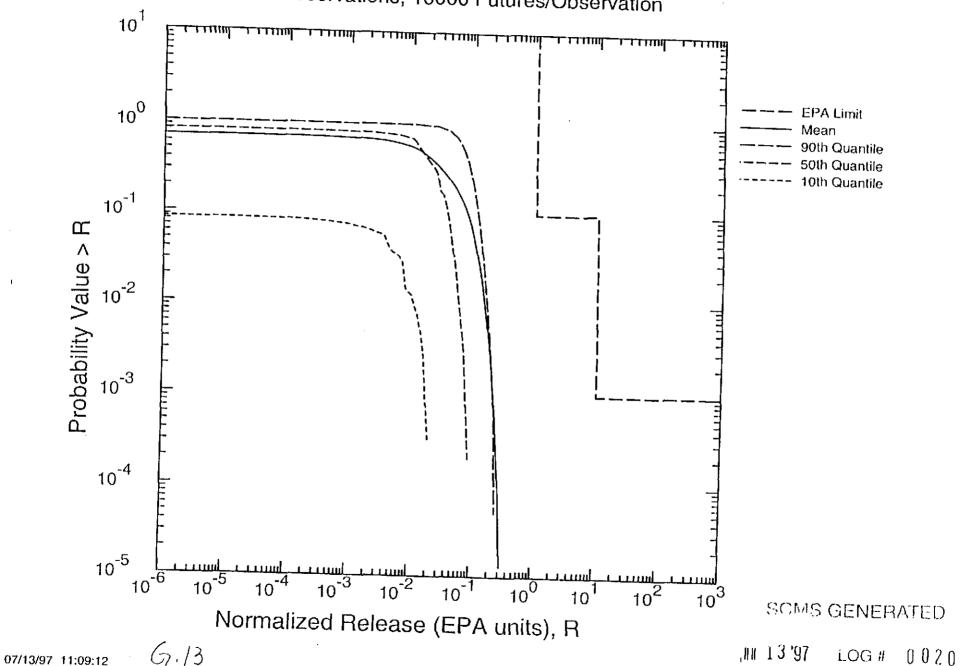
Total From Culebra Normalized Releases 100 Observations, 10000 Futures/Observation



Cuttings Normalized Releases 100 Observations, 10000 Futures/Observation



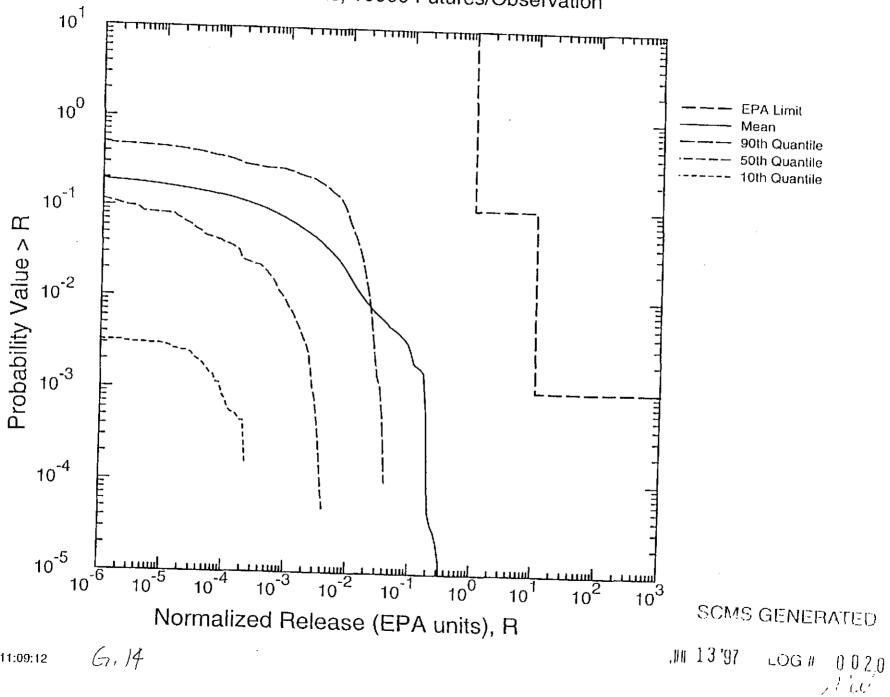
Spallings Normalized Releases 100 Observations, 10000 Futures/Observation



6.13

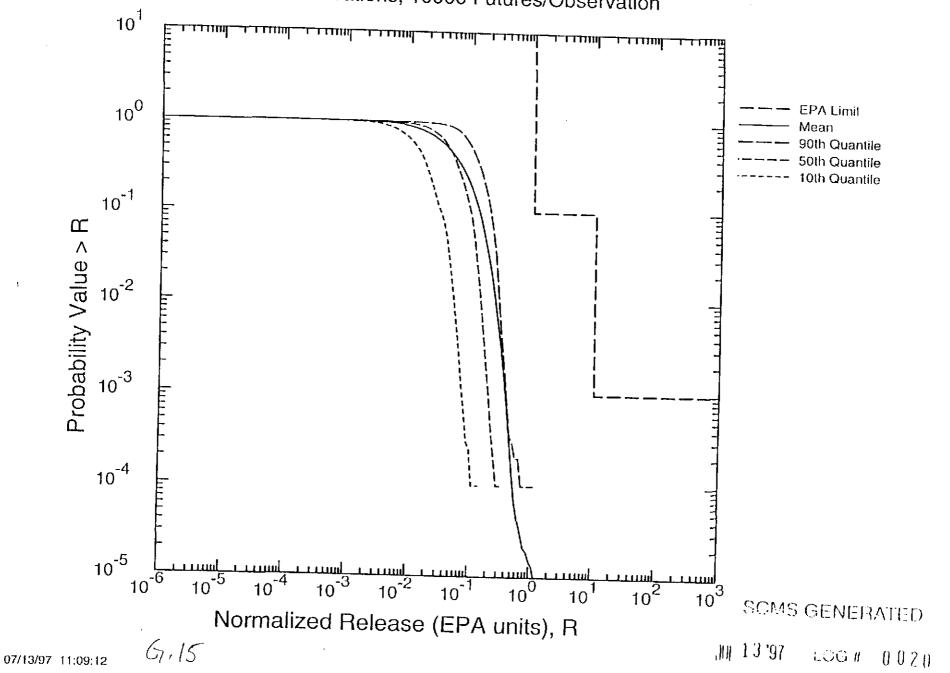
LOG# 0020

DBR t Normalized Releases 100 Observations, 10000 Futures/Observation

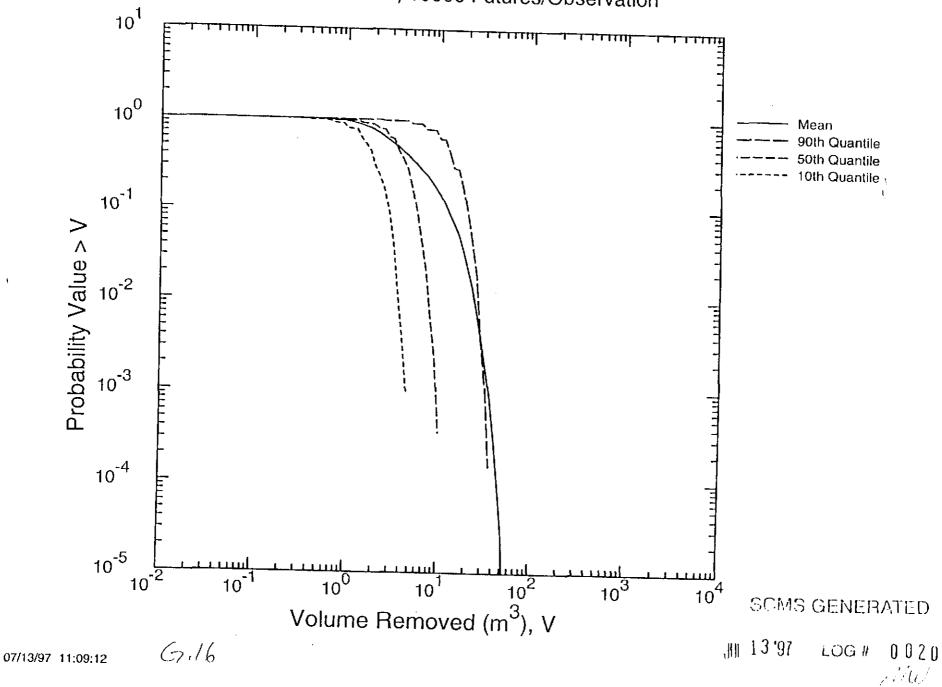


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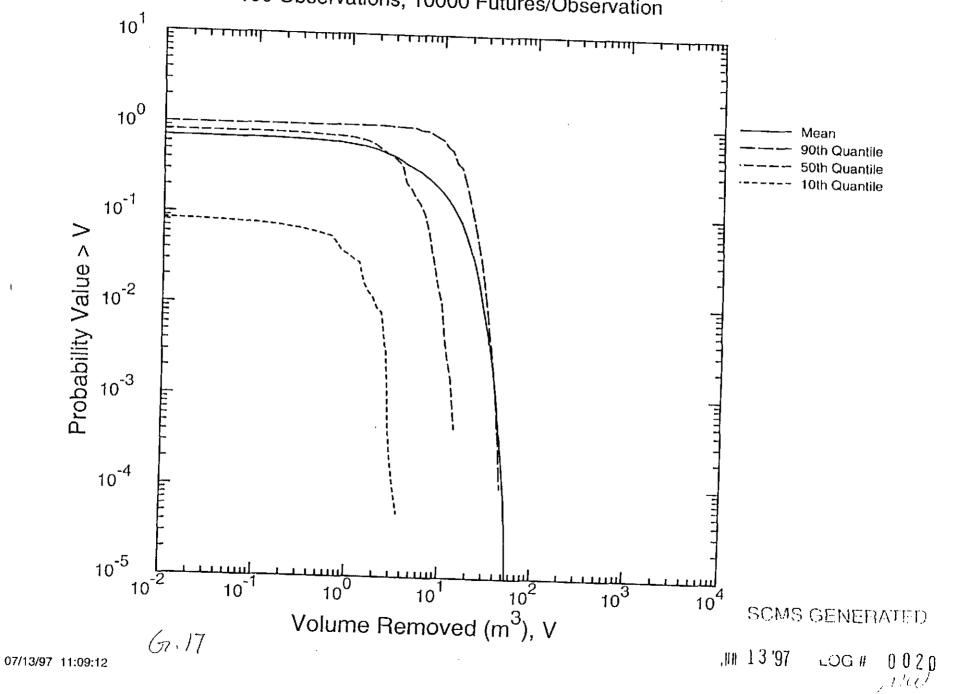
Cutting+Spalling+Blaneut Normalized Releases 100 Observations, 10000 Futures/Observation



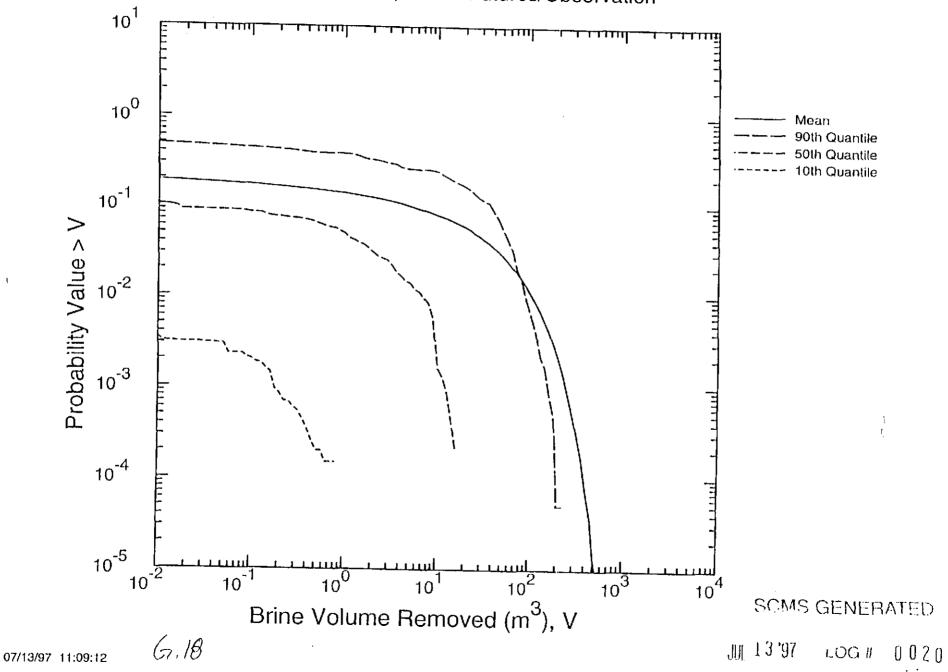
Cuttings Volume Releases
100 Observations, 10000 Futures/Observation



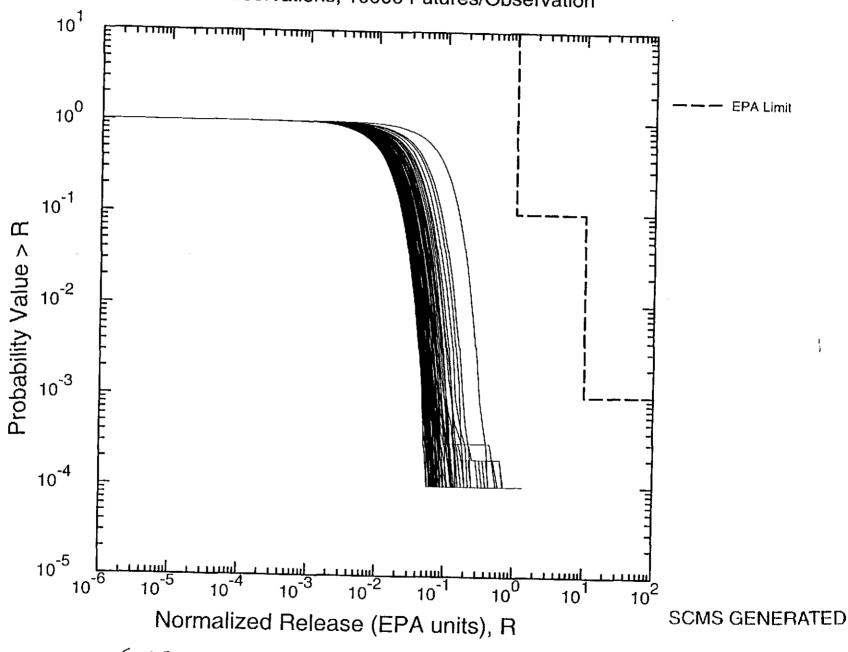
Spallings Volume Releases 100 Observations, 10000 Futures/Observation



100 Observations, 10000 Futures/Observation



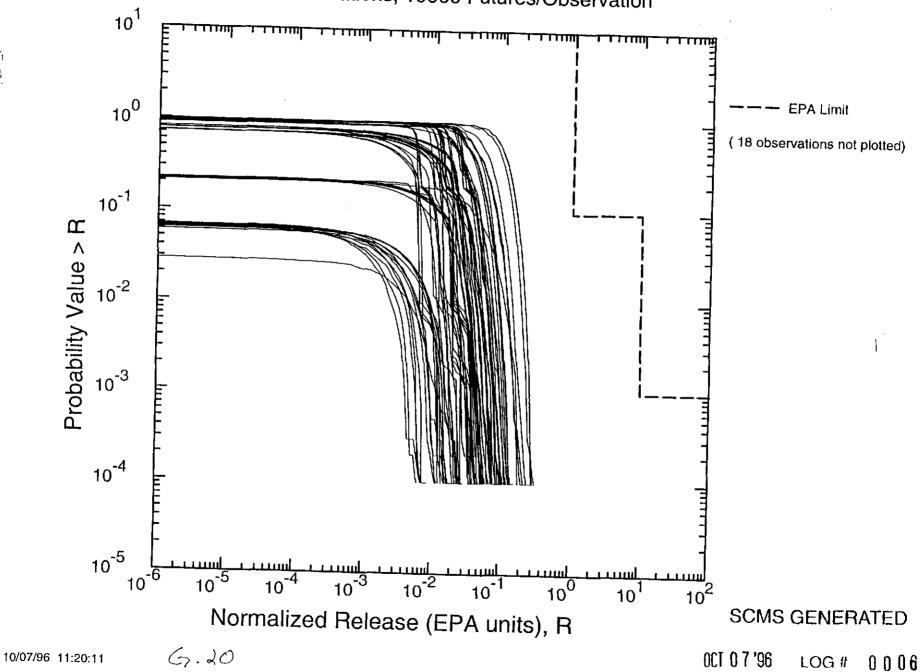
Cuttings Normalized Releases: R1 100 Observations, 10000 Futures/Observation



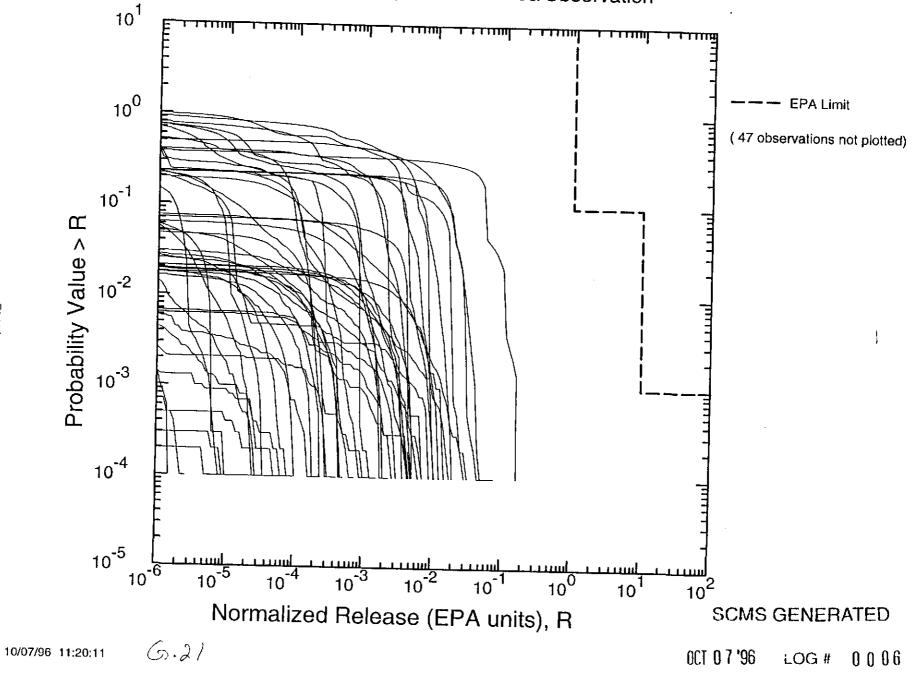
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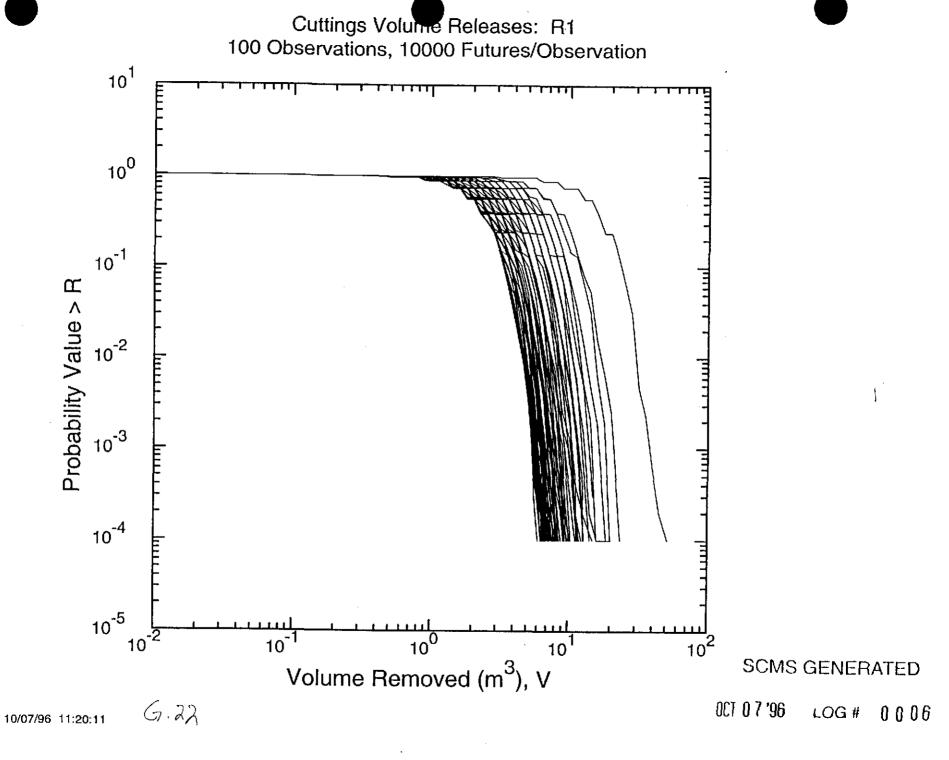
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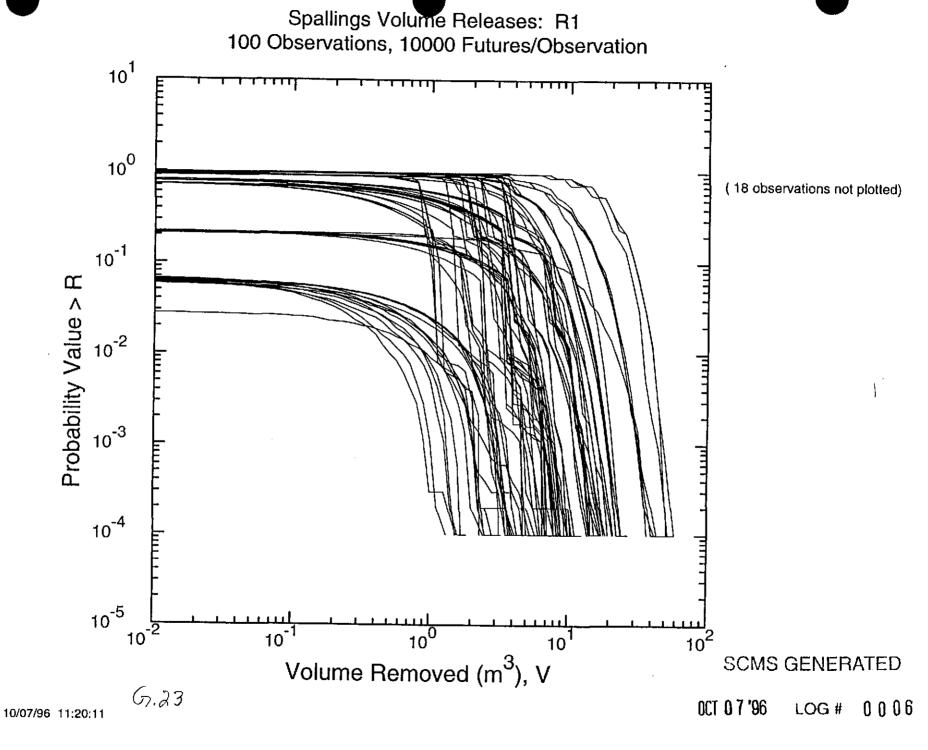
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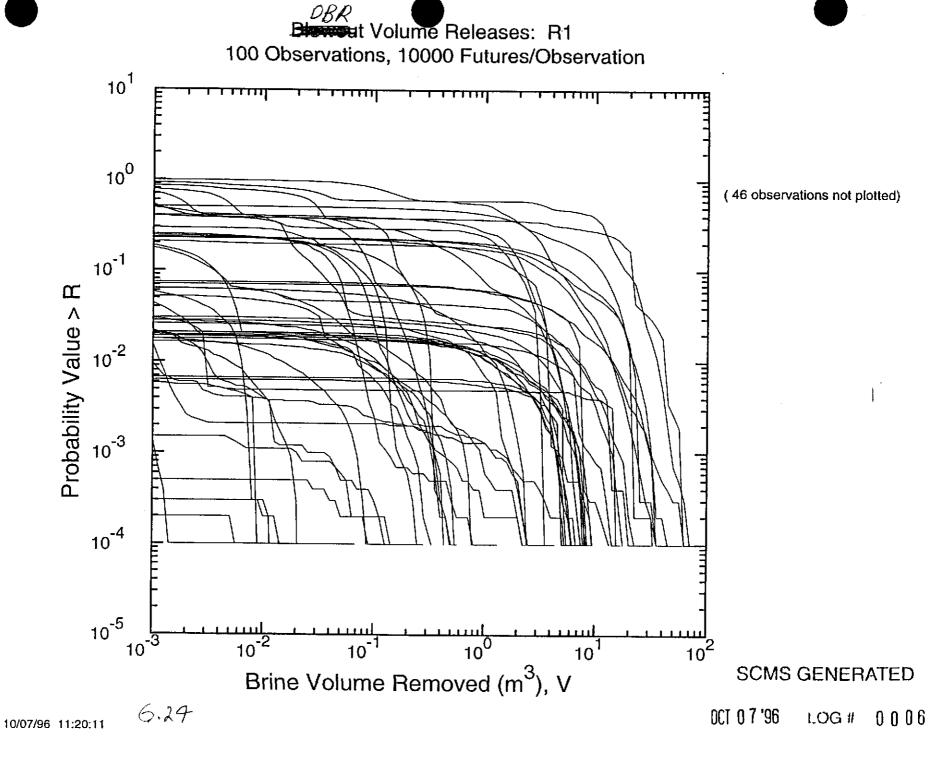


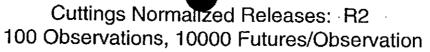
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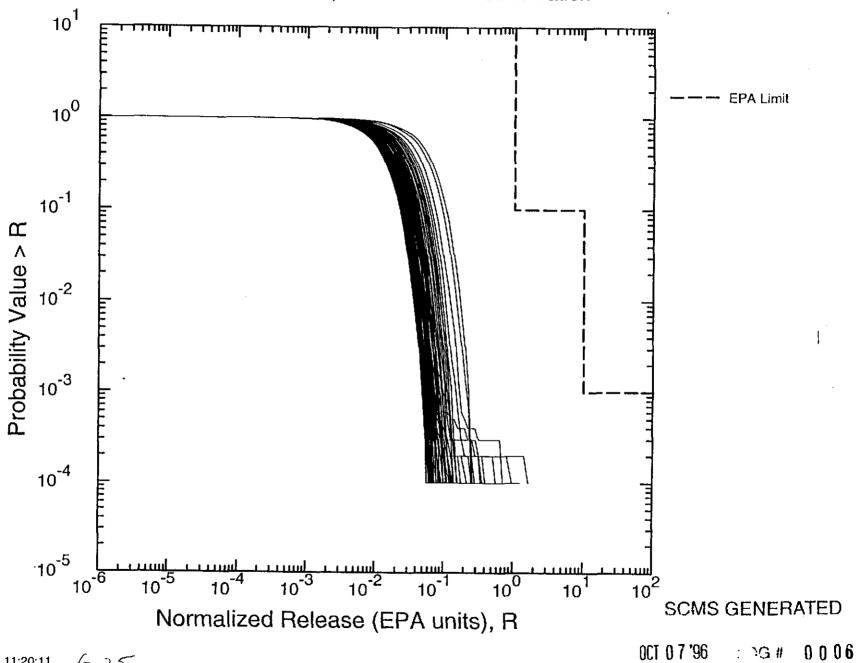




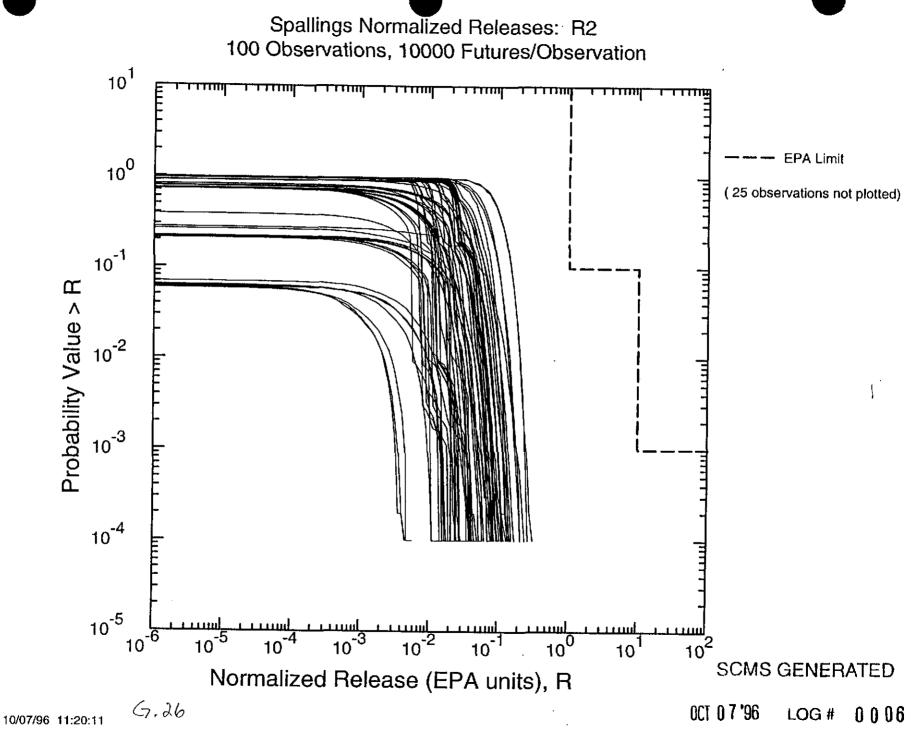






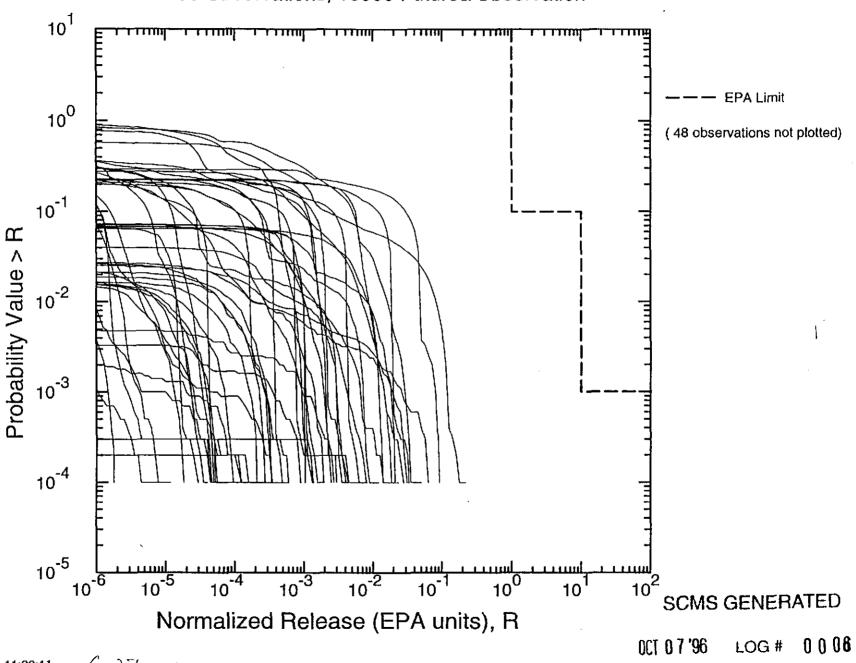


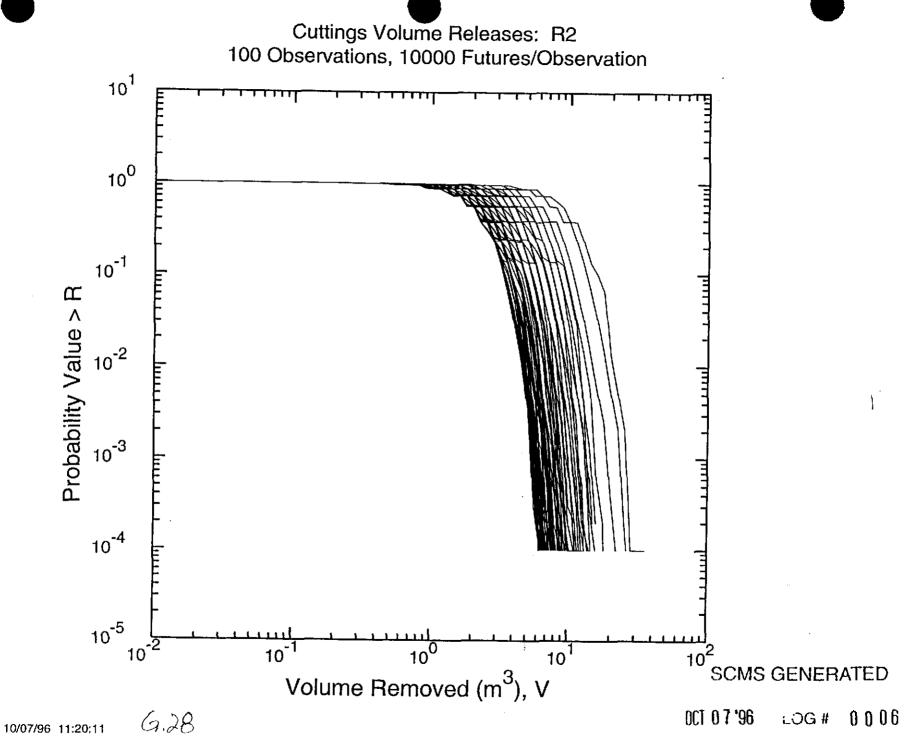
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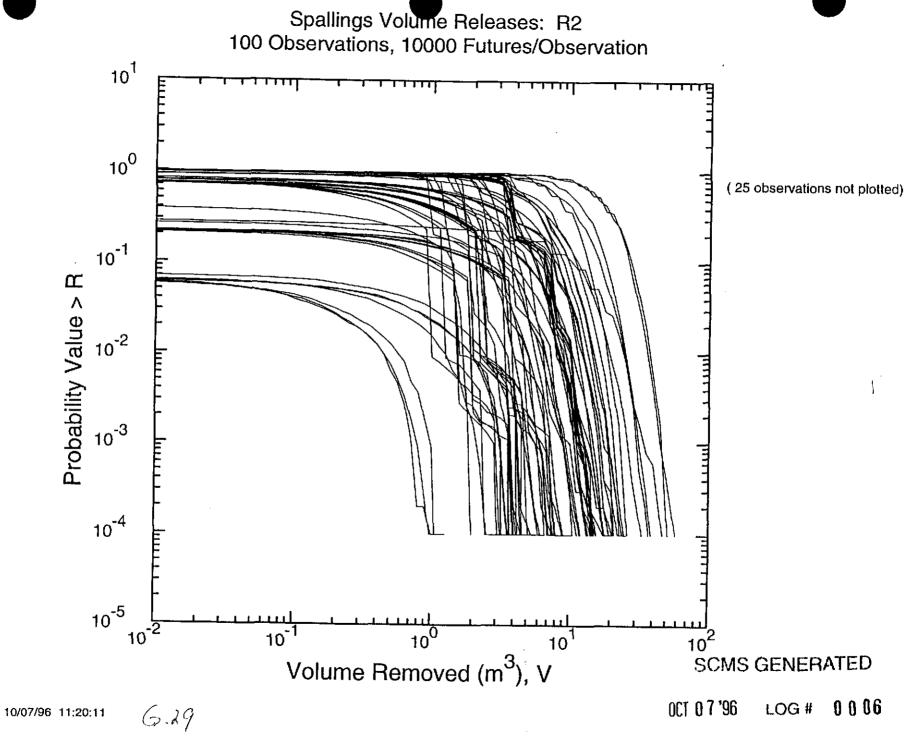
Information Only

DBR
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DBreut Normalized Releases: R2
100 Observations, 10000 Futures/Observation

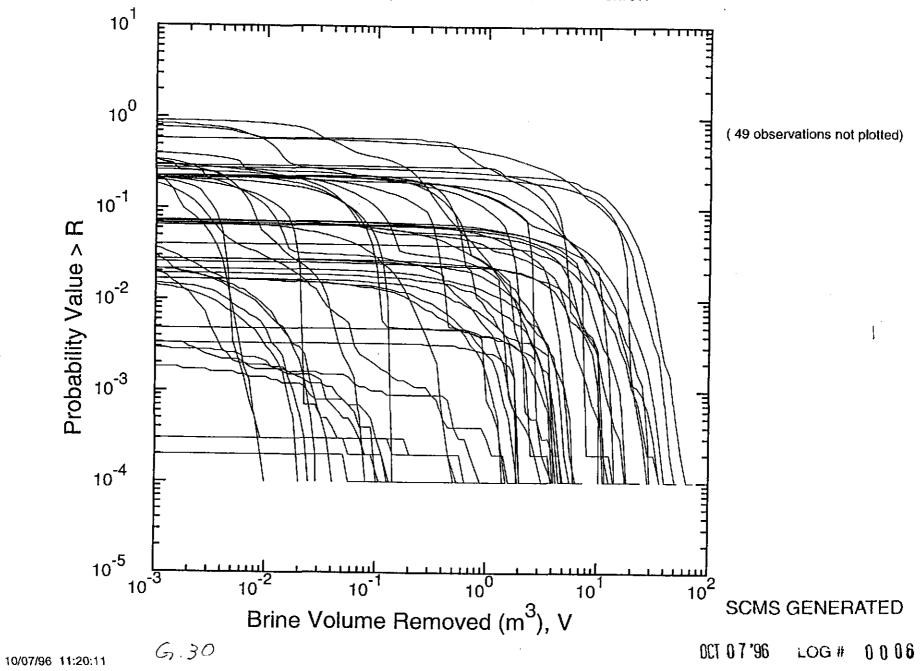


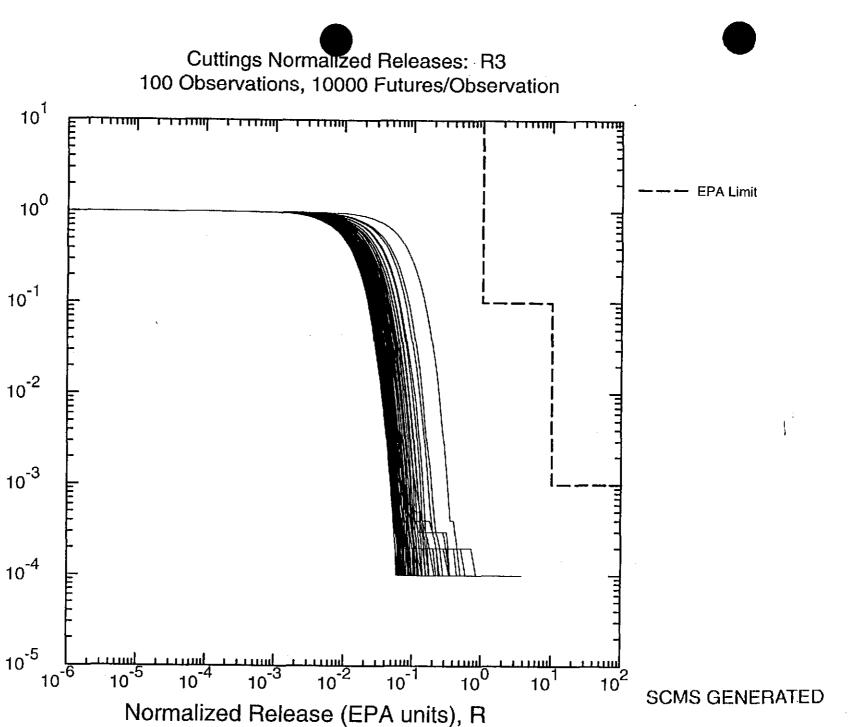


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DBR
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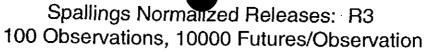


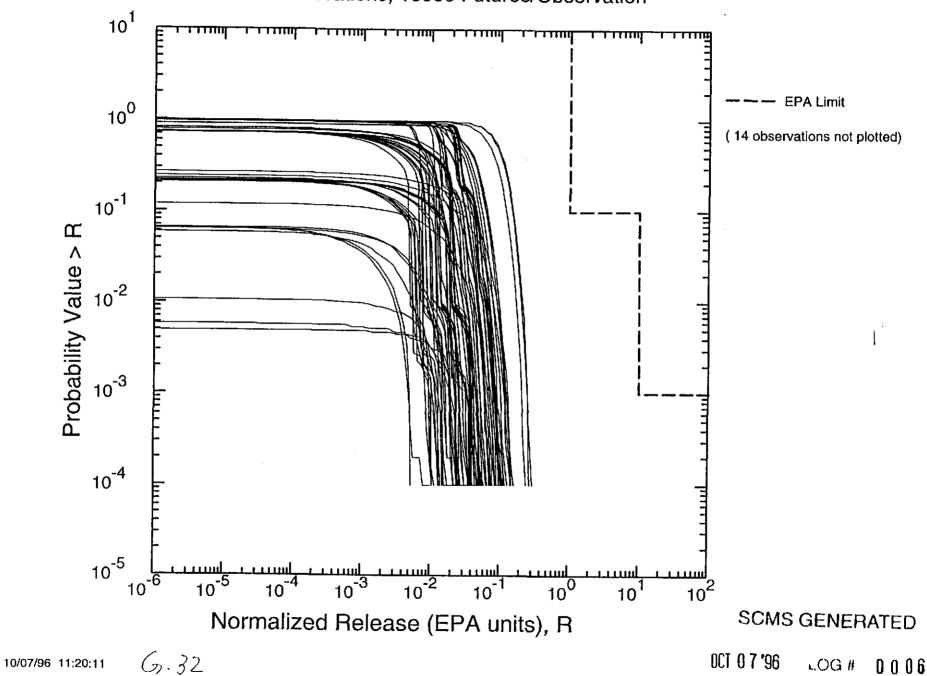


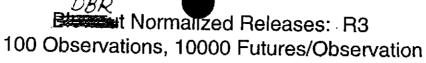
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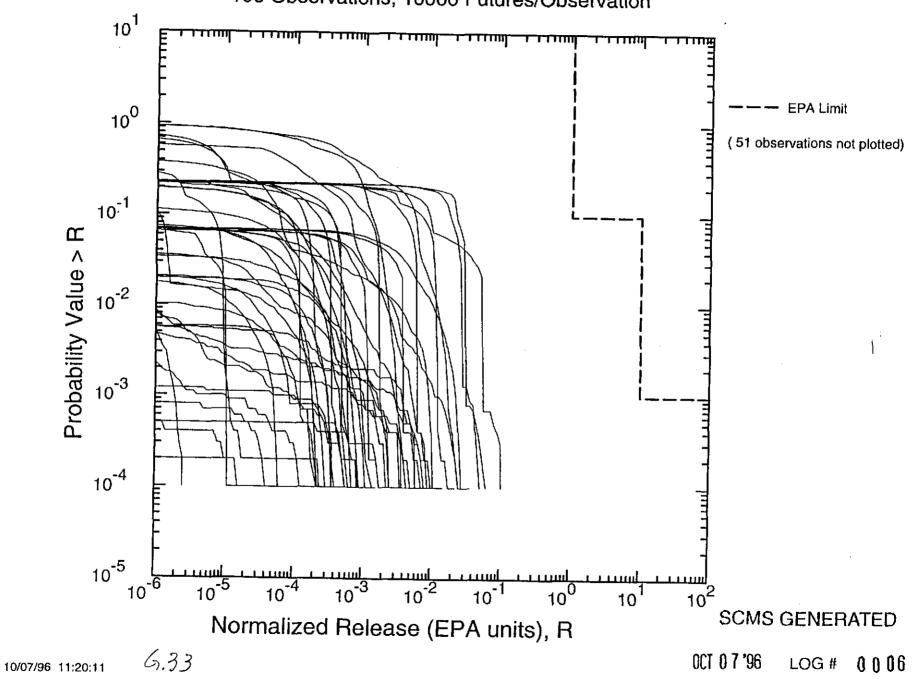
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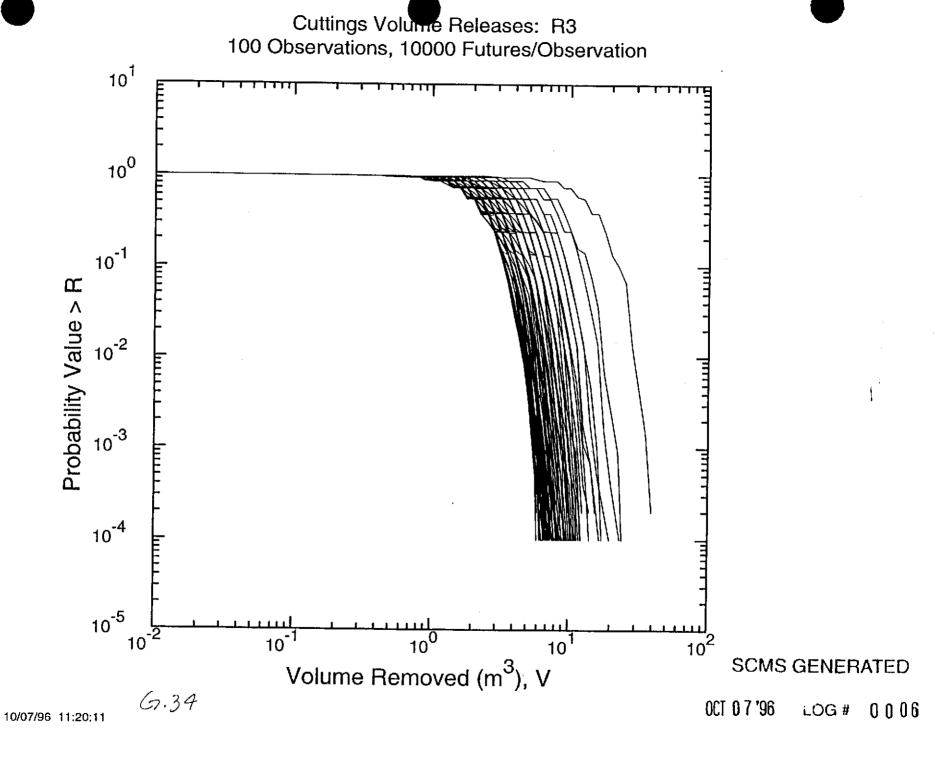
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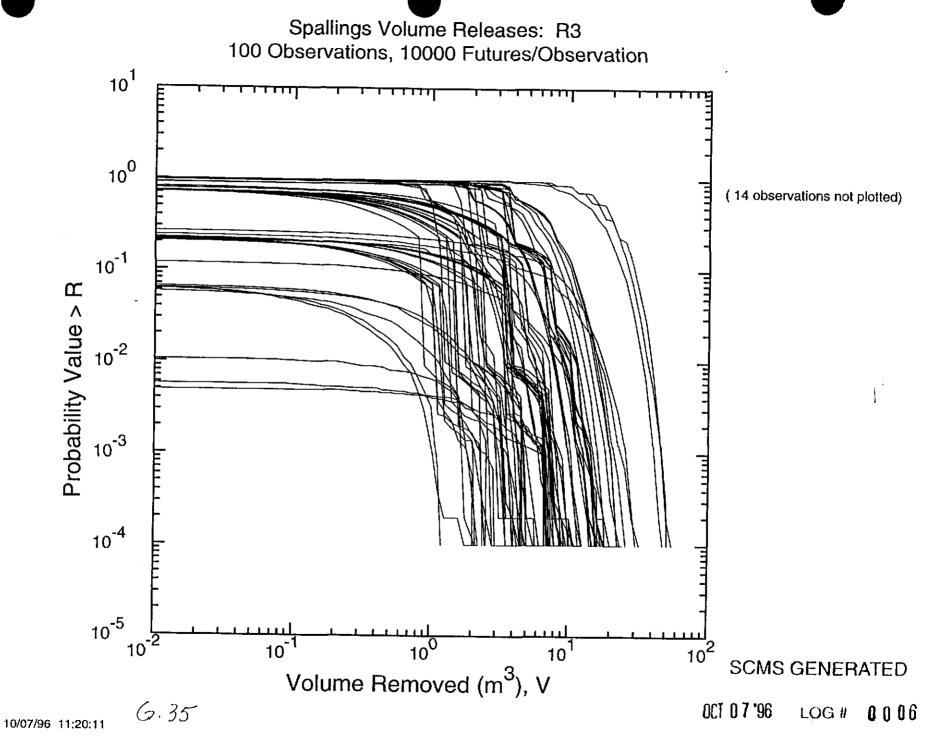






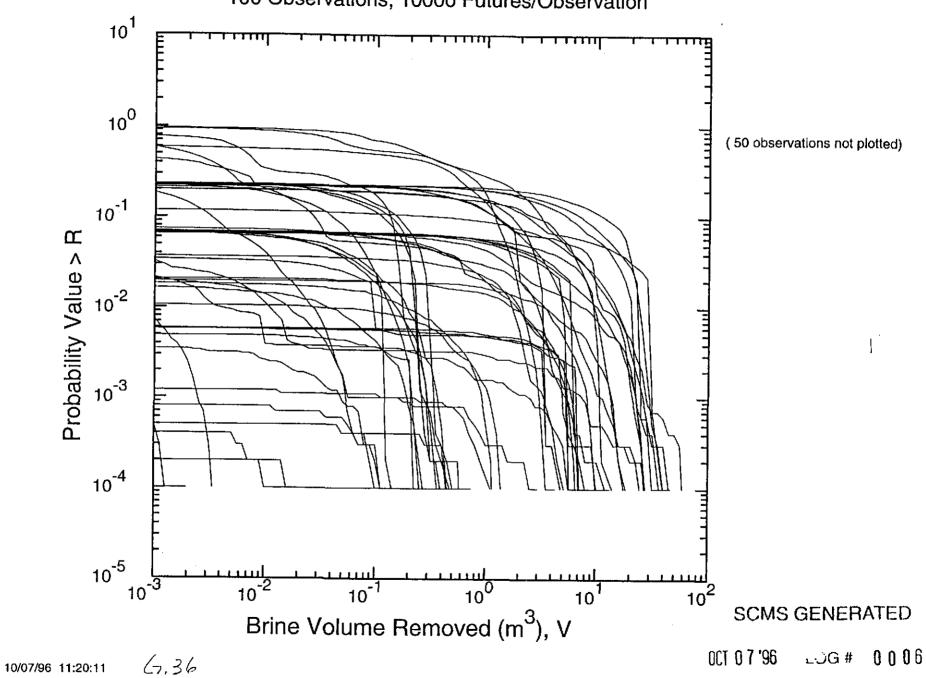


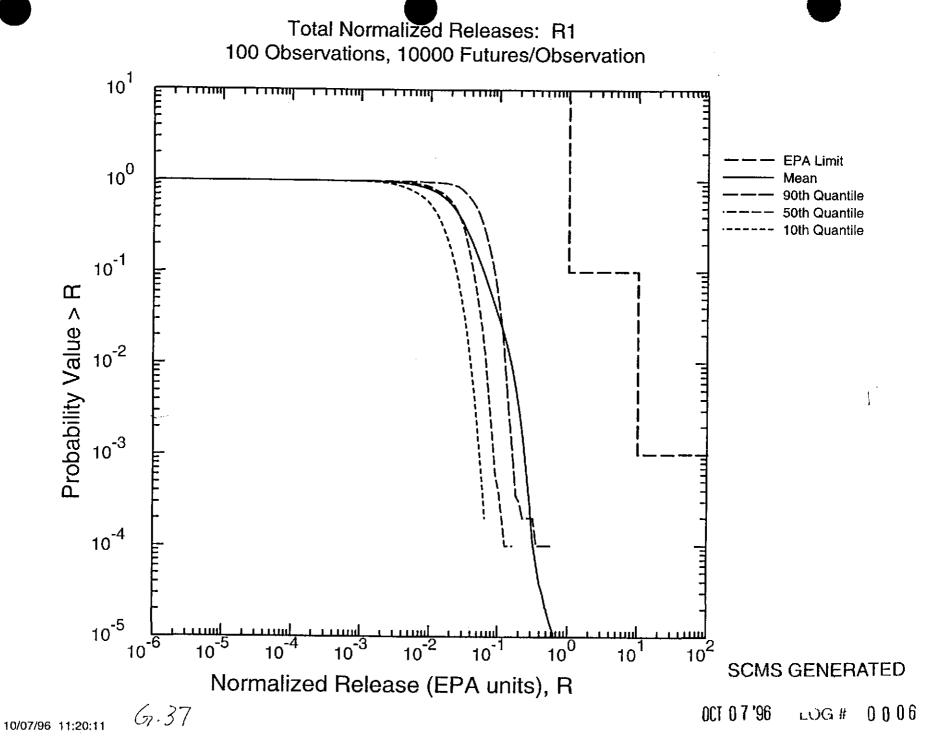
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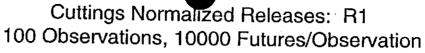


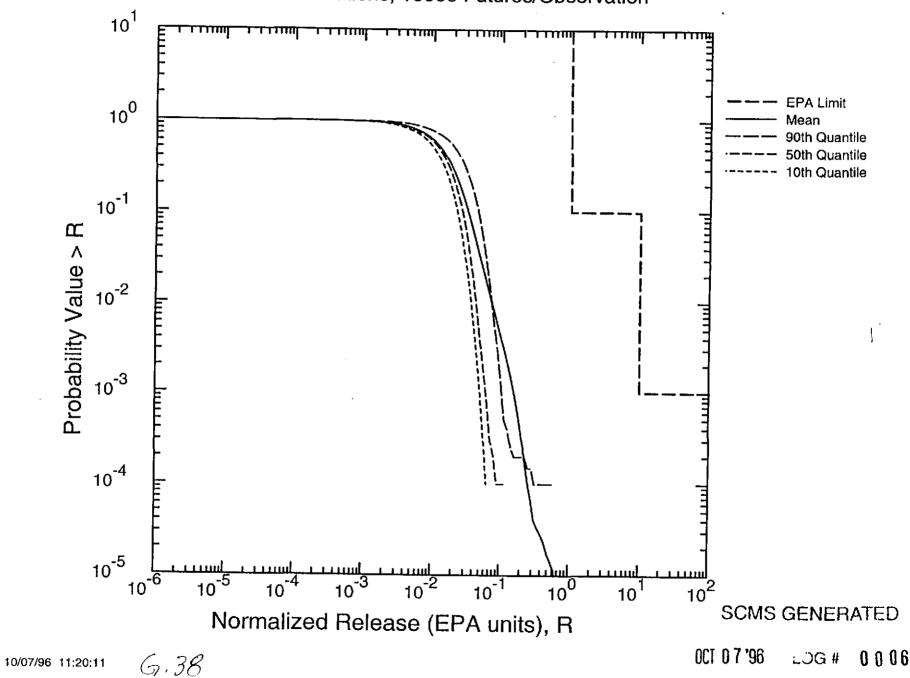
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DBR Planeut Volume Releases: R3 100 Observations, 10000 Futures/Observation

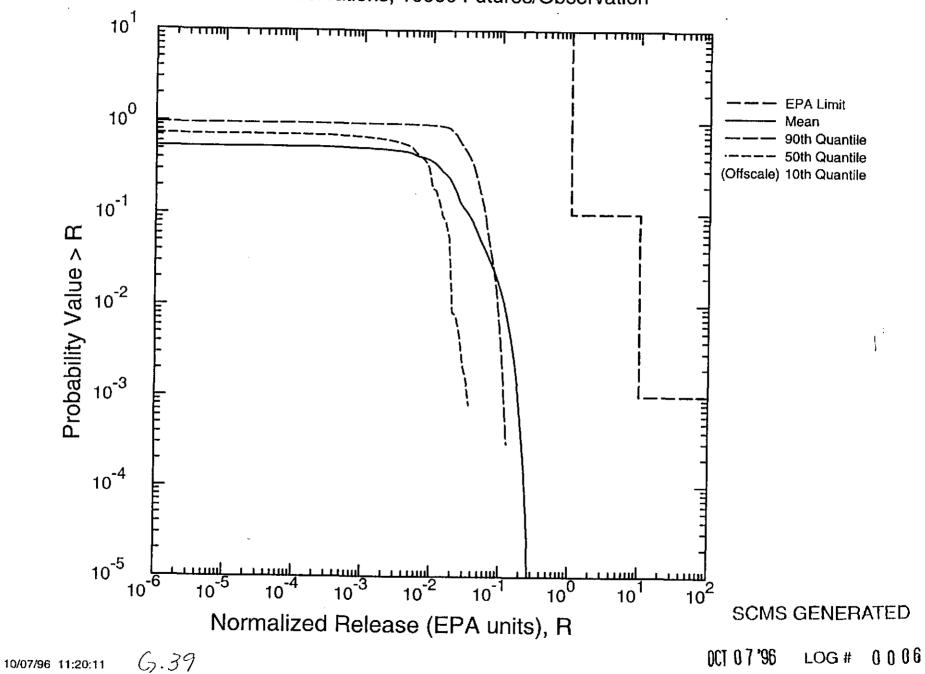




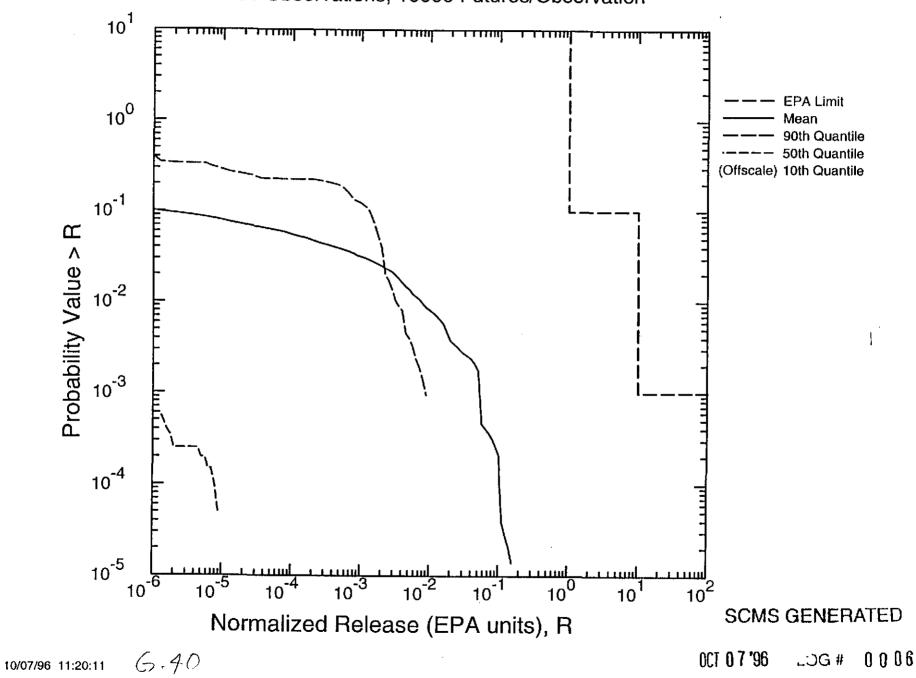


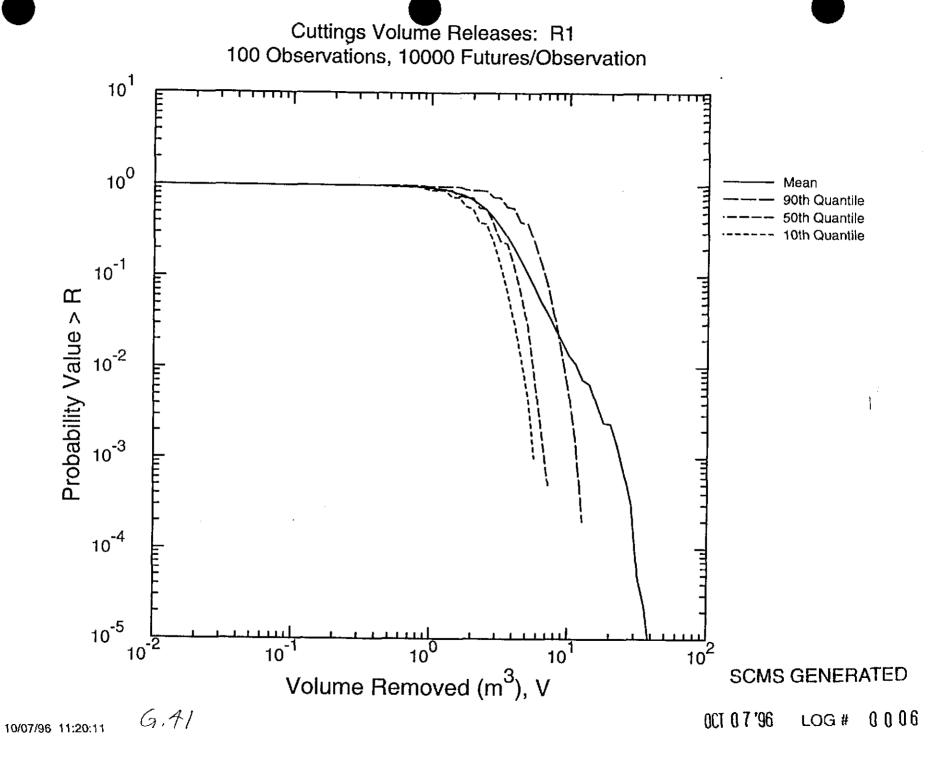


Spallings Normanzed Releases: R1 100 Observations, 10000 Futures/Observation

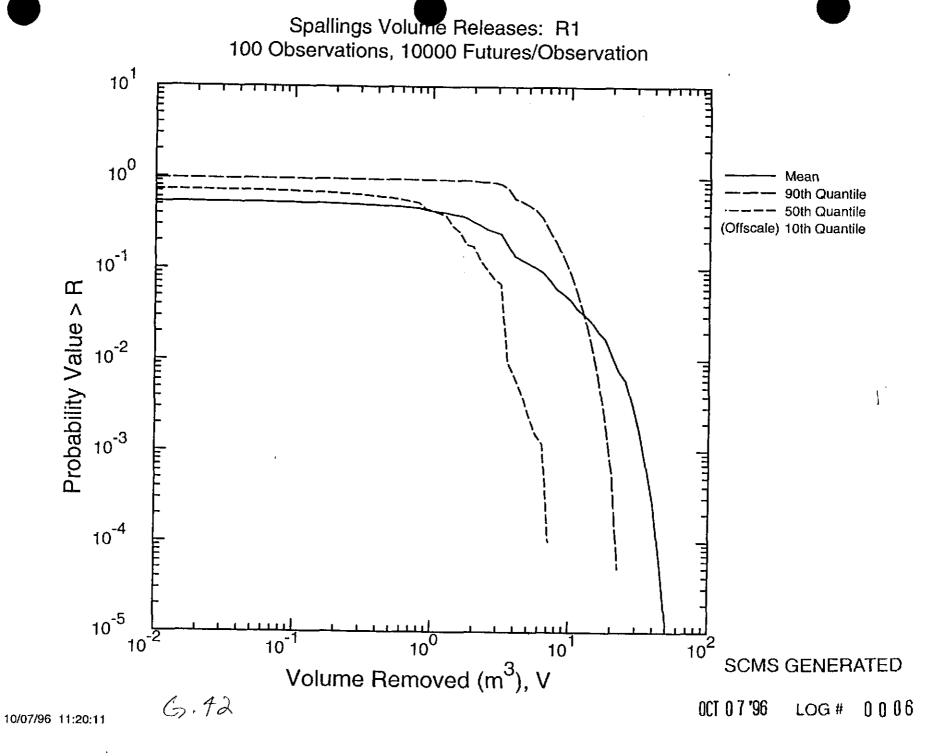


DBR
Biomat Normalized Releases: R1
100 Observations, 10000 Futures/Observation



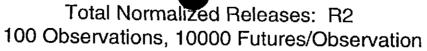


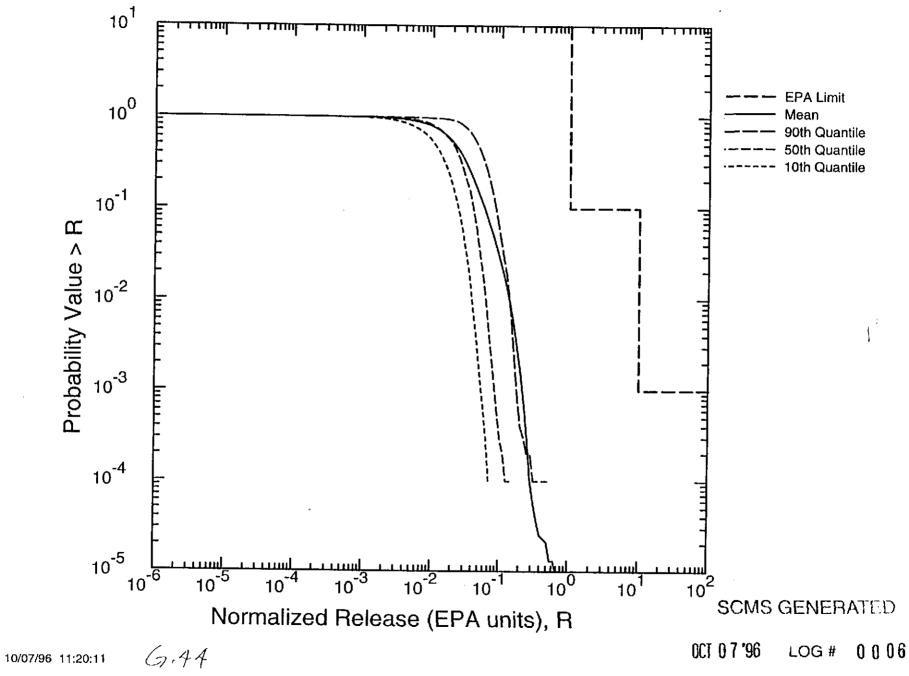
Information Only



DBR Blowsut Volume Releases: R1 100 Observations, 10000 Futures/Observation 10¹ 10⁰ Mean 90th Quantile 50th Quantile (Offscale) 10th Quantile 10⁻¹ Probability Value > R 10⁻² 10⁻³ 10⁻⁴ 10⁻⁵ 10^{-ंडें} 10⁻² 10-1 10² **SCMS GENERATED** Brine Volume Removed (m³), V G.43 LOG# 0006 ' OCT 0 7 '96 10/07/96 11:20:11

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Cuttings Normalized Releases: R2 100 Observations, 10000 Futures/Observation **EPA Limit** Mean 90th Quantile 50th Quantile 10th Quantile 10⁻³ 10⁻²

10⁻⁵ 10⁻⁵ 10⁻⁴ 10⁻³ 10⁻² 10⁻¹ 10⁰ 10¹ 10²

Normalized Release (EPA units), R

5. 45

OCT 07'96 LOG # 0 0 0 6

10¹

10⁰

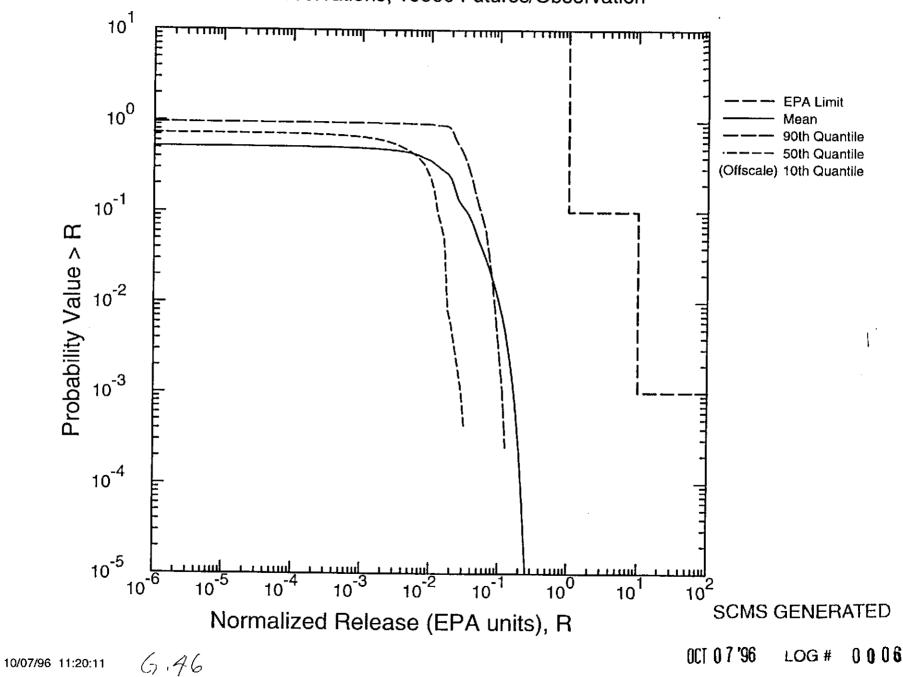
10⁻¹

10⁻⁴

10⁻⁵

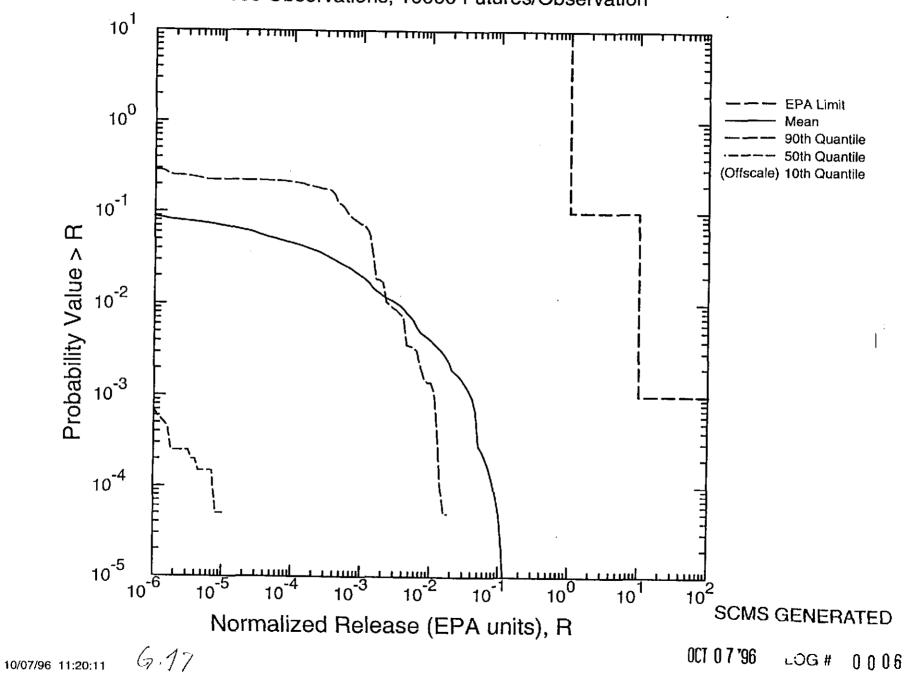
Probability Value > R

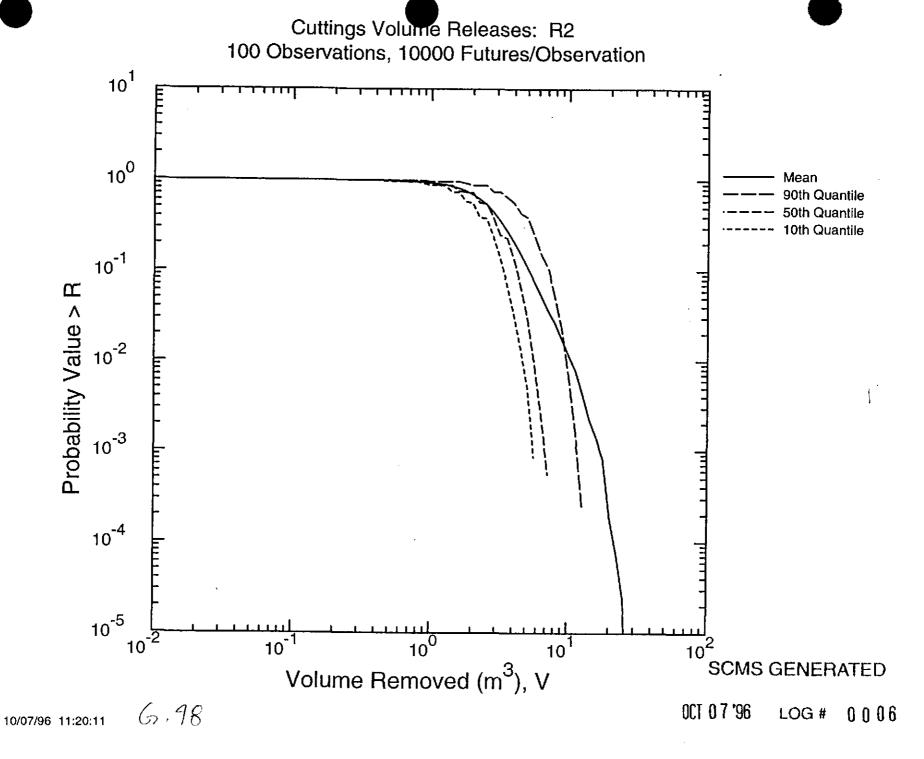
Spallings Normanzed Releases: R2 100 Observations, 10000 Futures/Observation

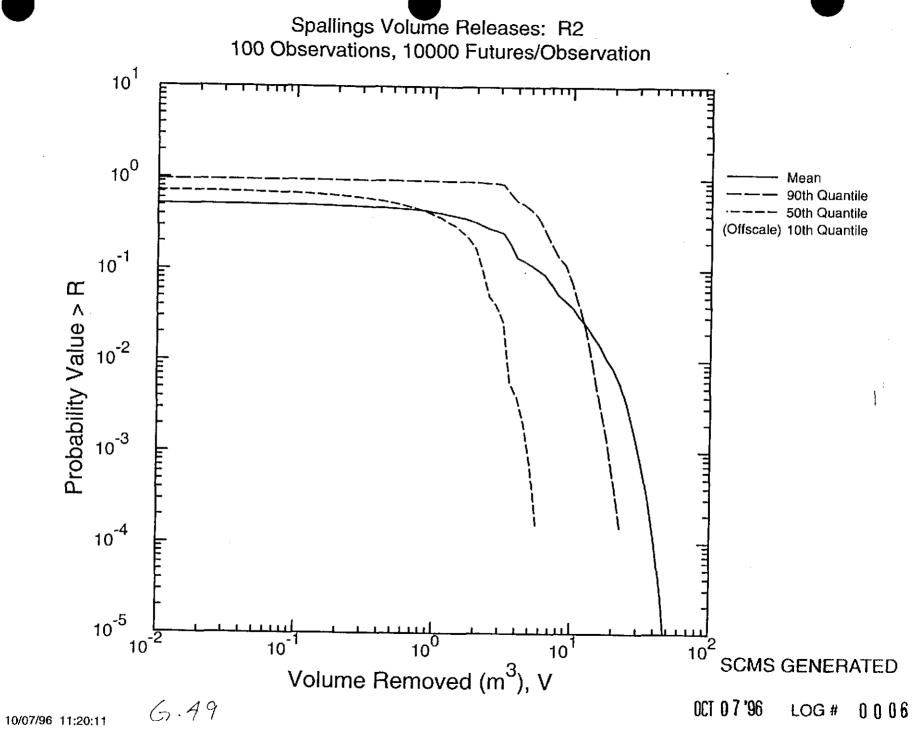


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DBR Blaweut Normalized Releases: R2 100 Observations, 10000 Futures/Observation







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DBR Blament Volume Releases: R2 100 Observations, 10000 Futures/Observation Mean 90th Quantile 50th Quantile (Offscale) 10th Quantile 10⁻² 10⁰ 10⁻¹ 10

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OCT 0 7 '96

Brine Volume Removed (m³), V

101

10⁰

10⁻¹

10⁻²

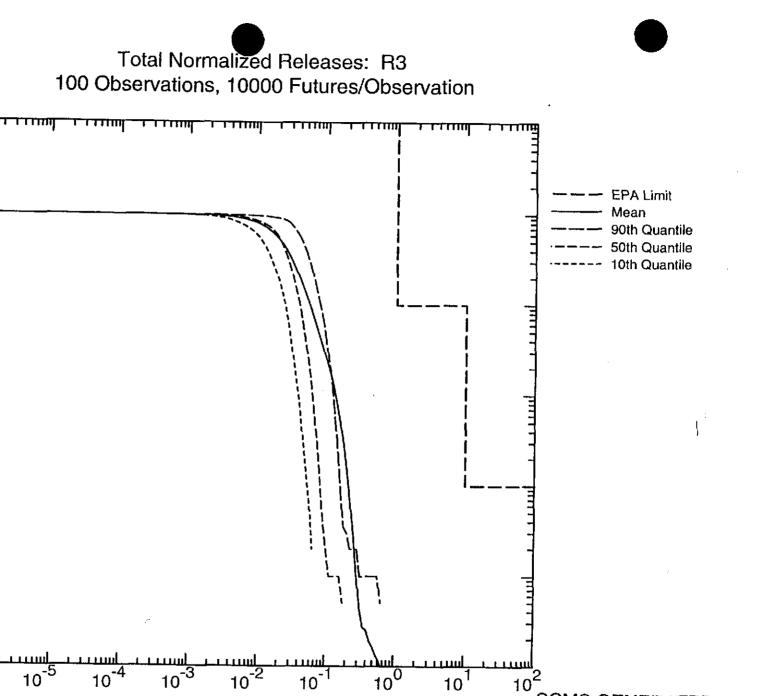
10⁻⁴

10⁻⁵

10/07/96 11:20:11

6.50

Probability Value > R



Normalized Release (EPA units), R

10¹

100

10⁻¹

10⁻⁴

10⁻⁵

10/07/96 11:20:11

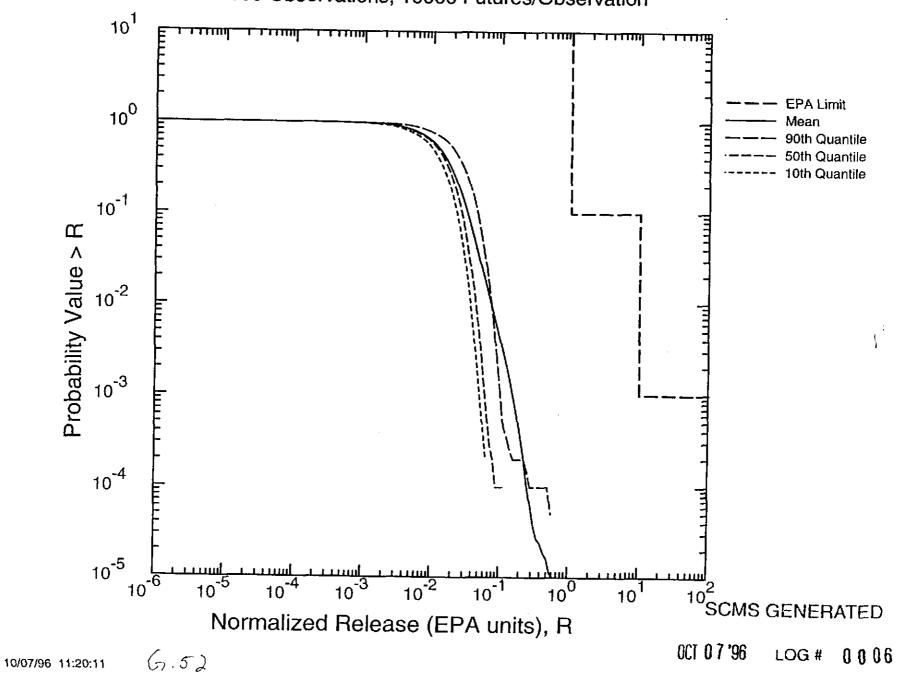
10⁻⁶

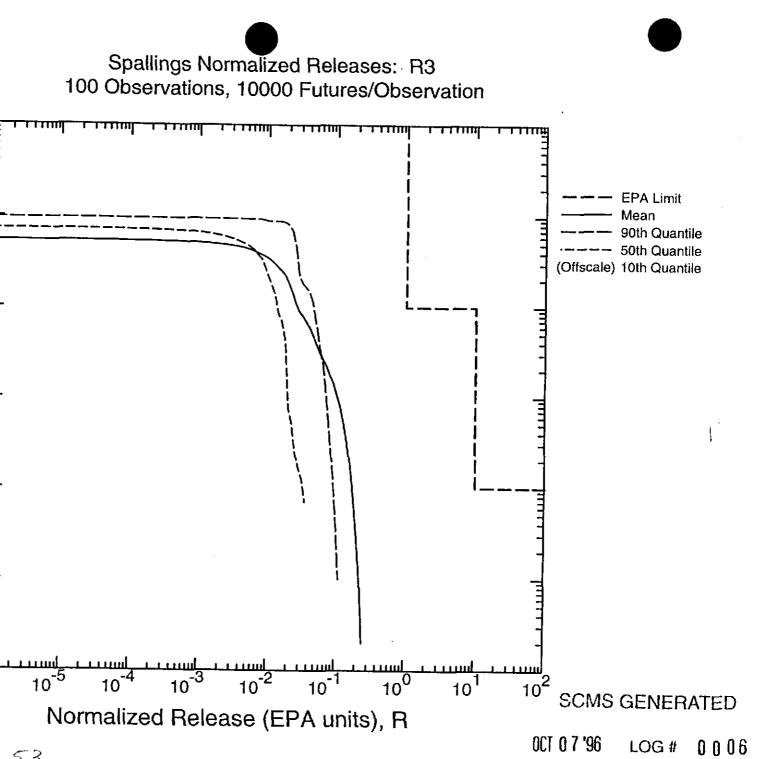
Probability Value > R

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Cuttings Normalized Releases: R3
100 Observations, 10000 Futures/Observation





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10¹

10⁰

10⁻¹

10⁻³

10⁻⁴

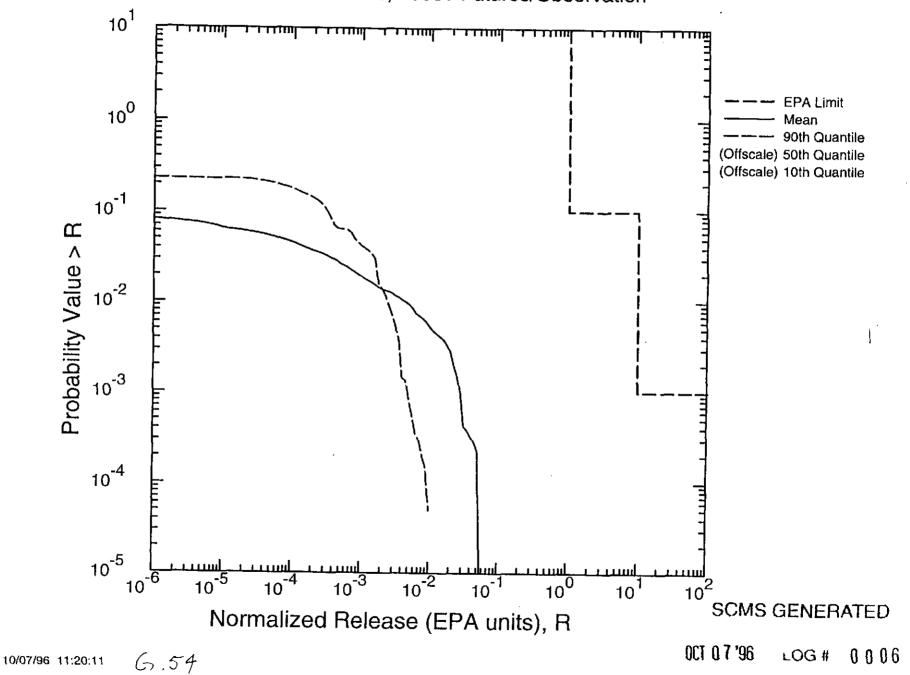
10⁻⁵

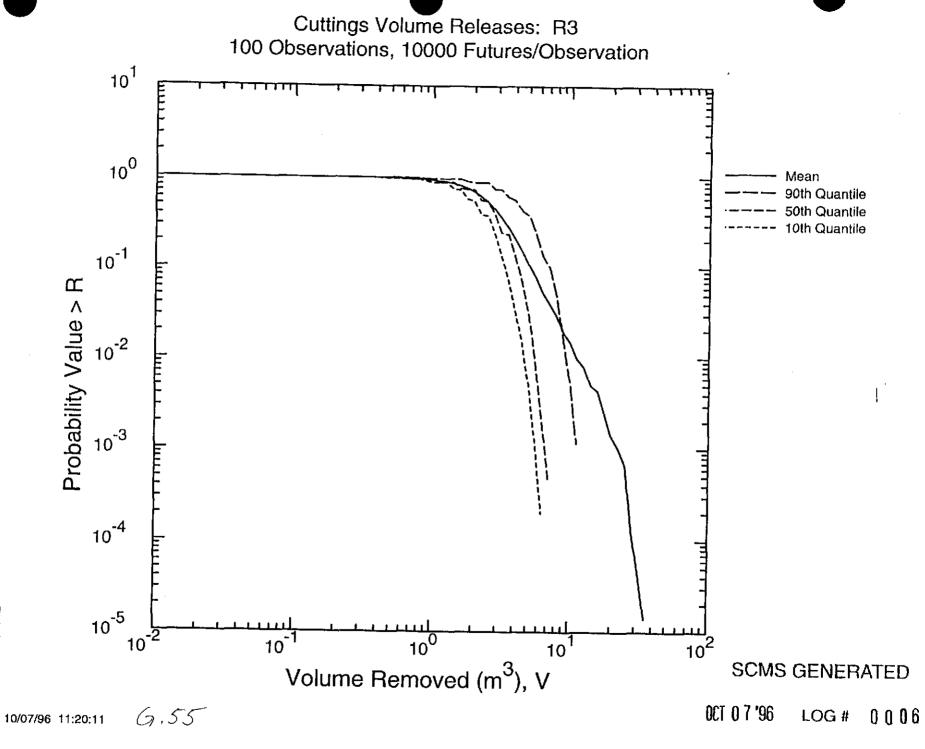
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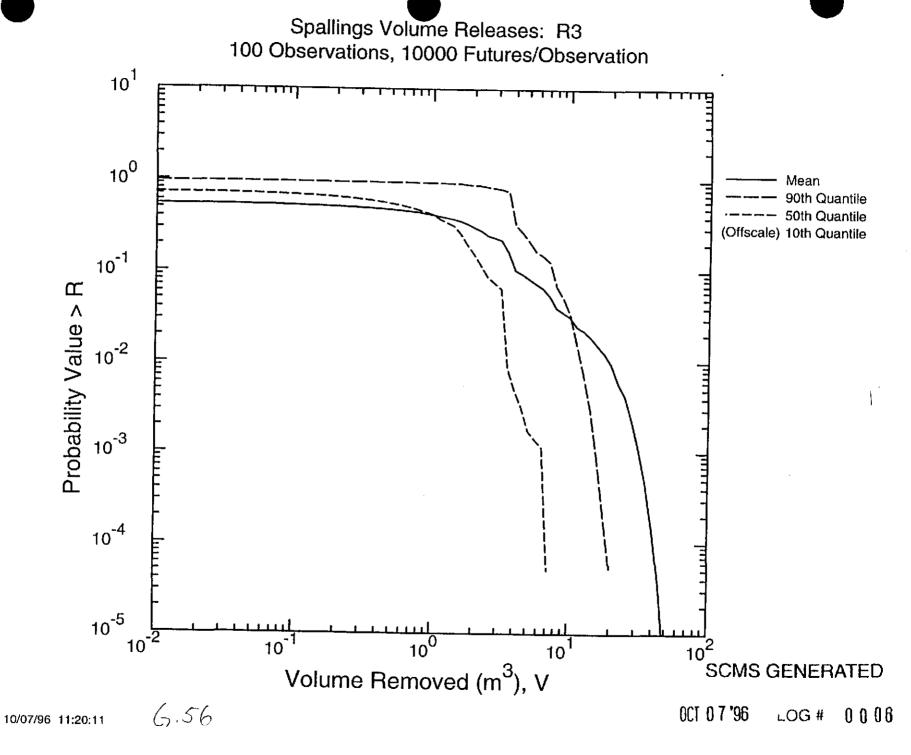
6.53

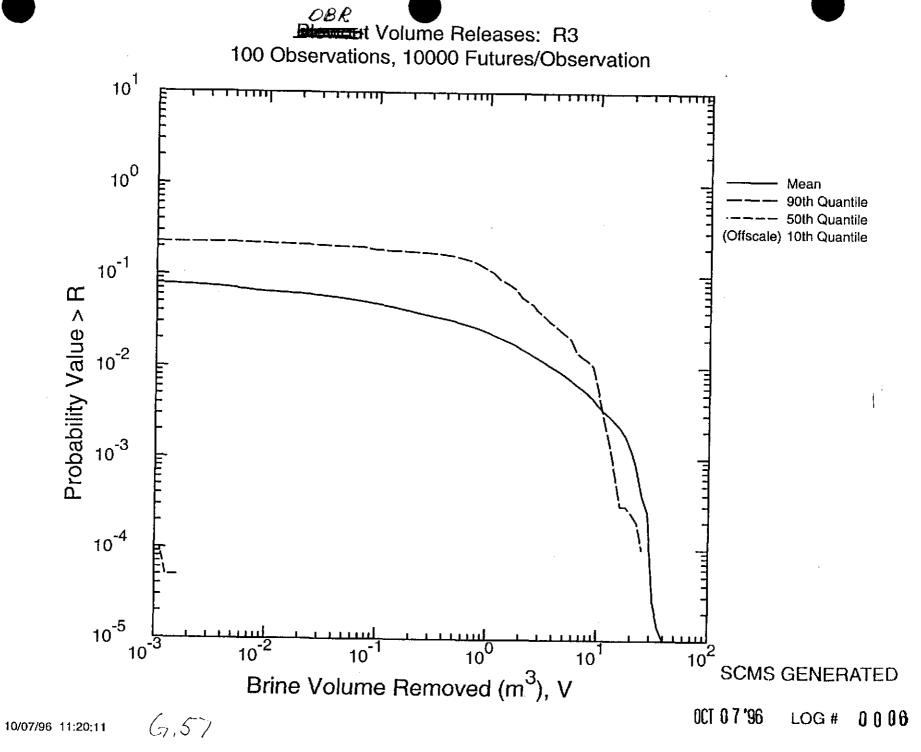
Probability Value > R

DBR
Bleweut Normalized Releases: R3
100 Observations, 10000 Futures/Observation

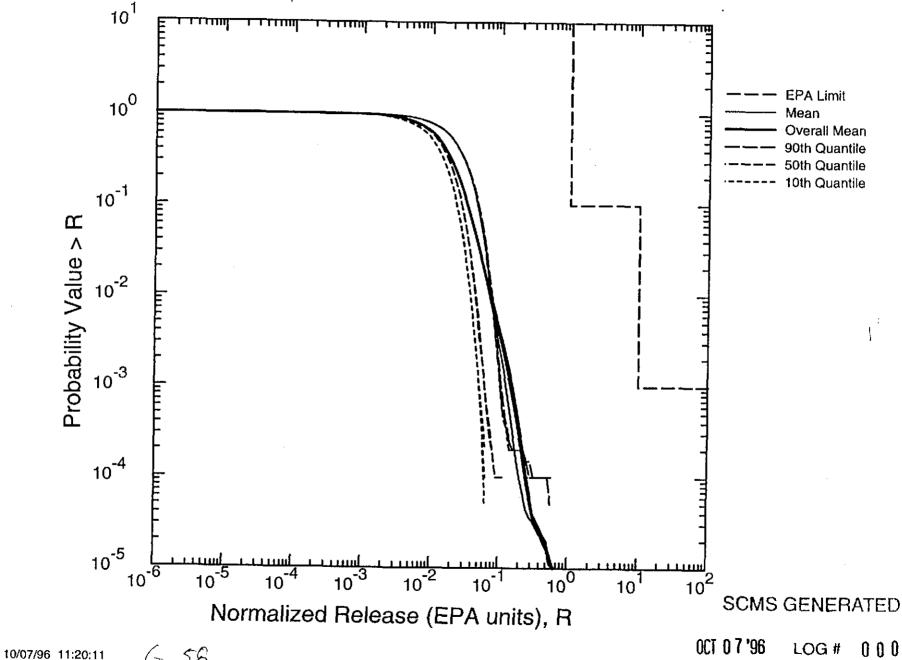






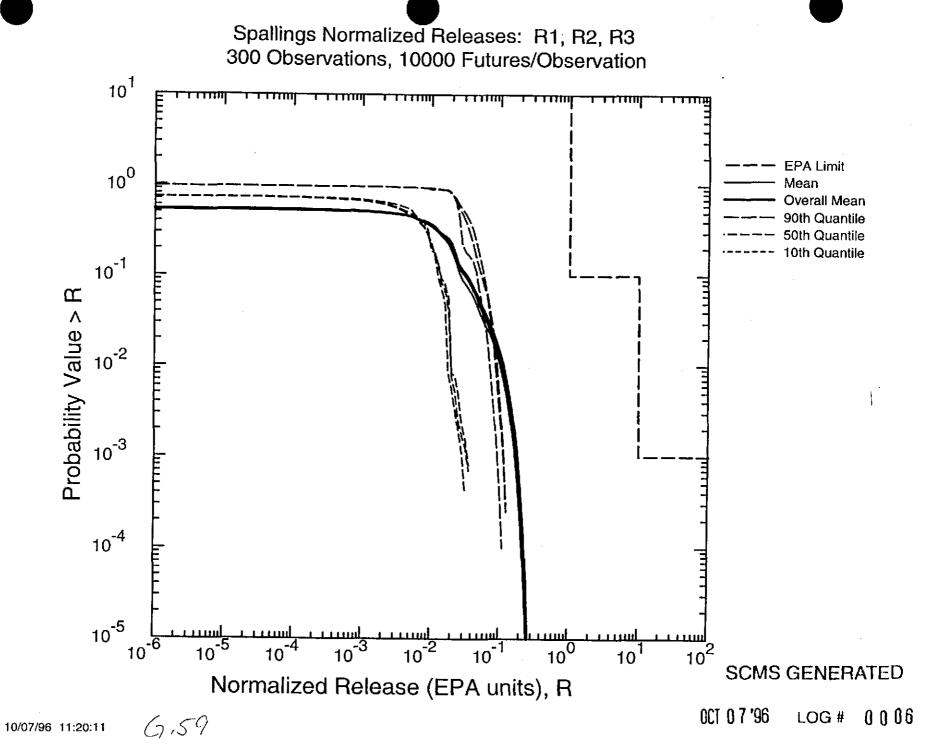


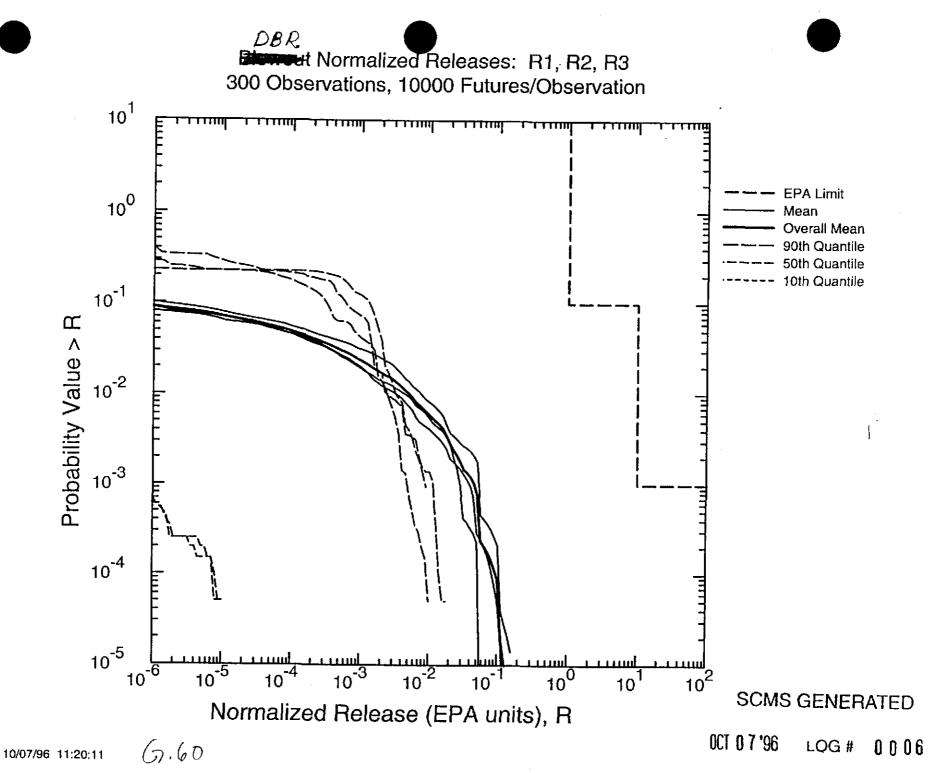
Cuttings Normalized Releases: R1, R2, R3 300 Observations, 10000 Futures/Observation

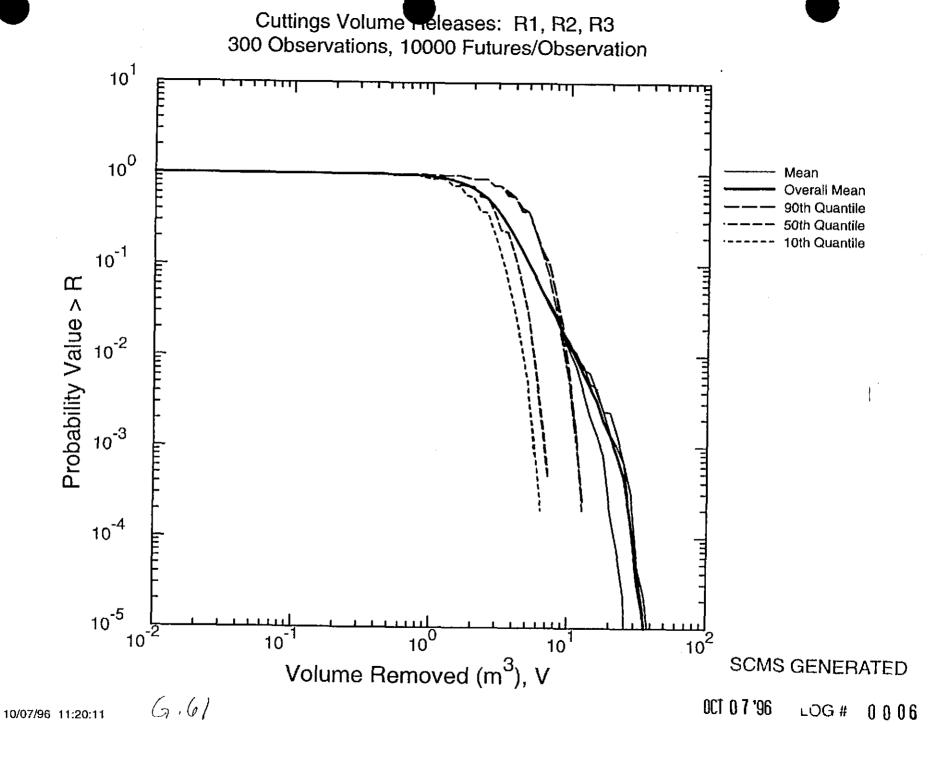


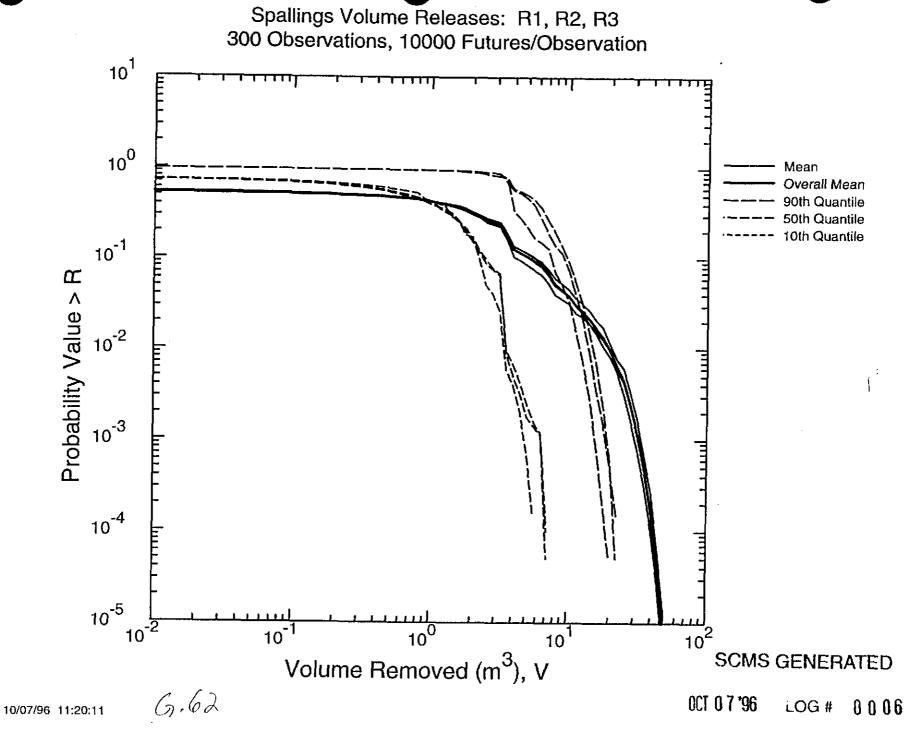
6,58

OCT 07'96 0006LOG#

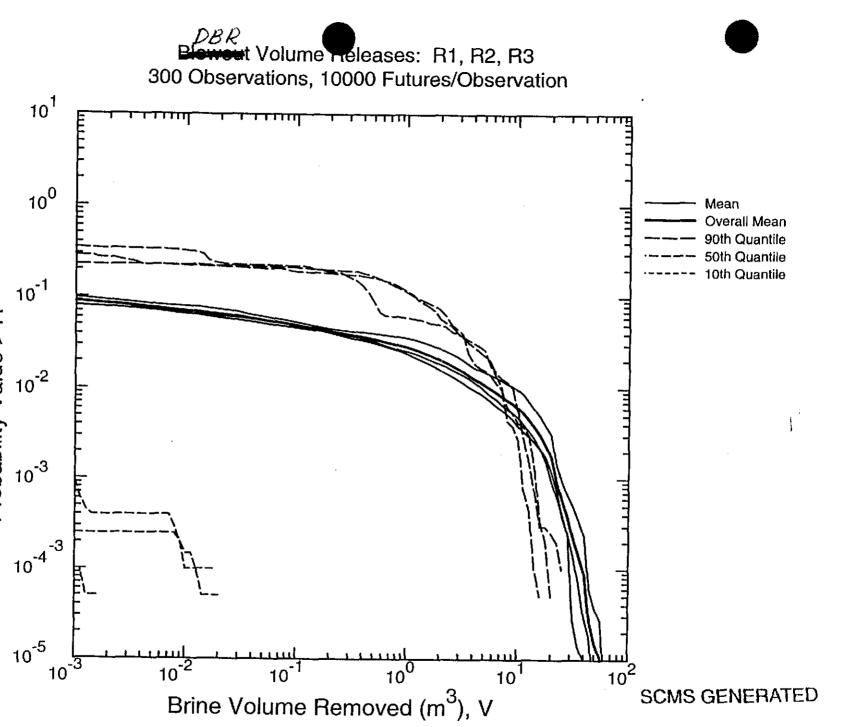








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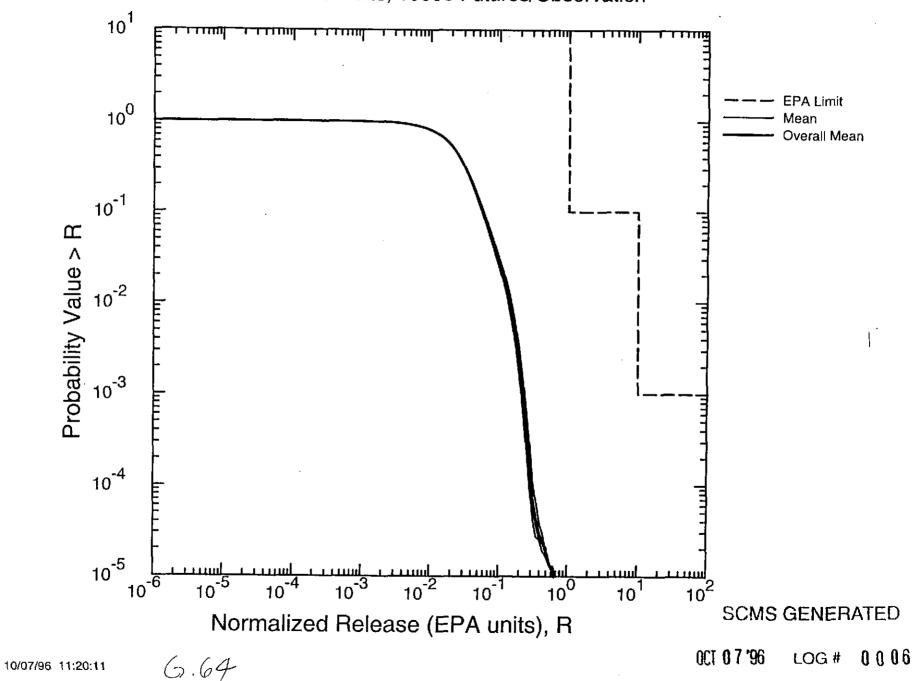


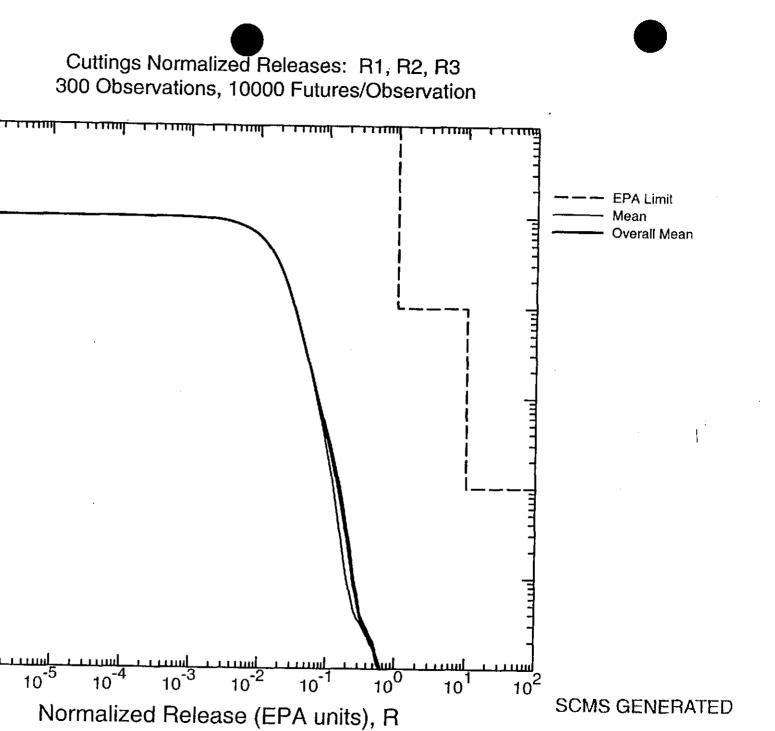
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Probability Value > R

OCT 07'96 LOG# 0006

Total Normalized Heleases: R1, R2, R3 300 Observations, 10000 Futures/Observation





OCT 07'96 LOG # 0006

10¹

10⁰

10⁻¹

10⁻³

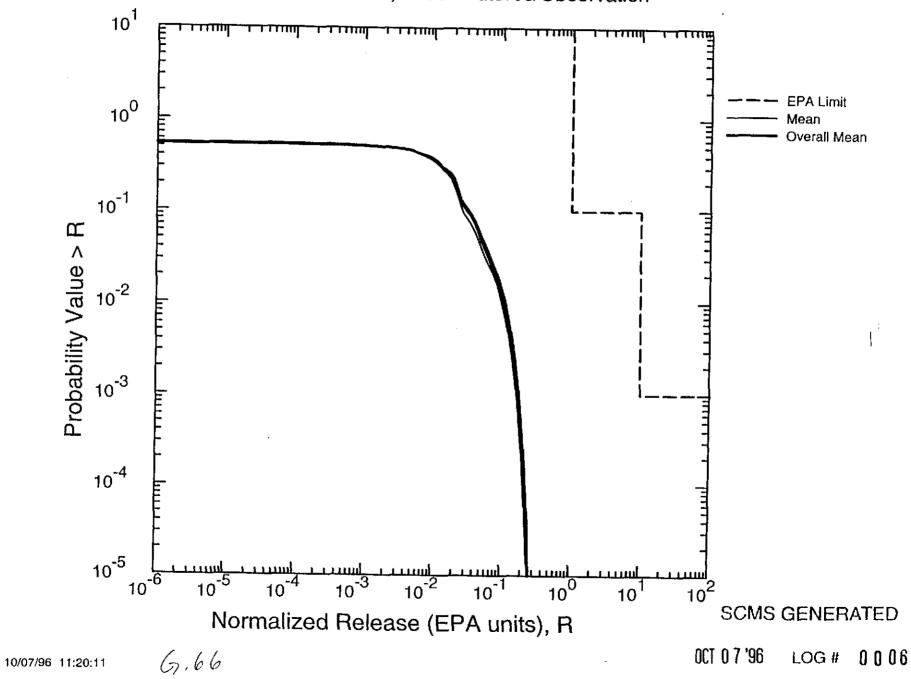
10⁻⁴

10⁻⁵

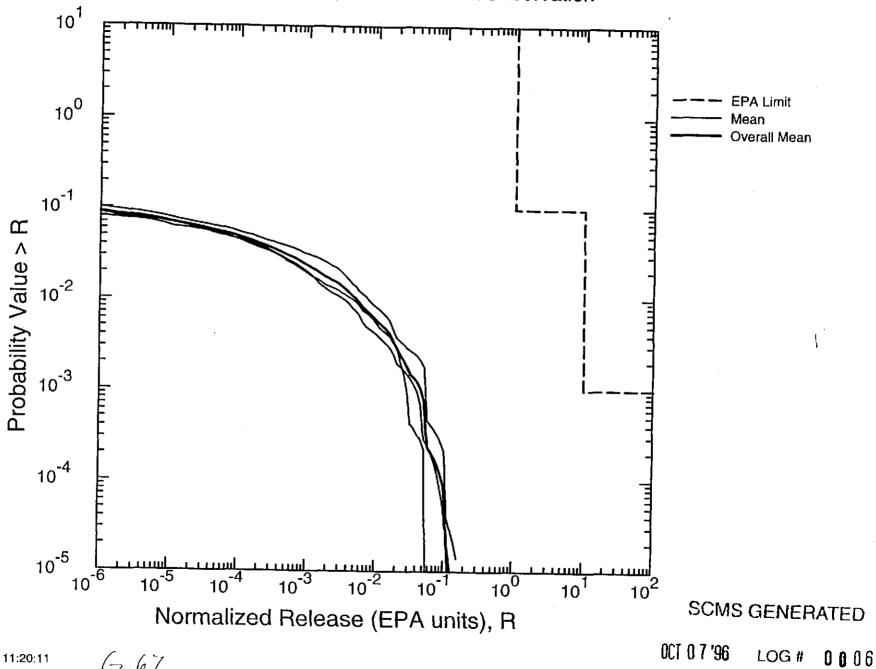
10⁻⁶

Probability Value > R

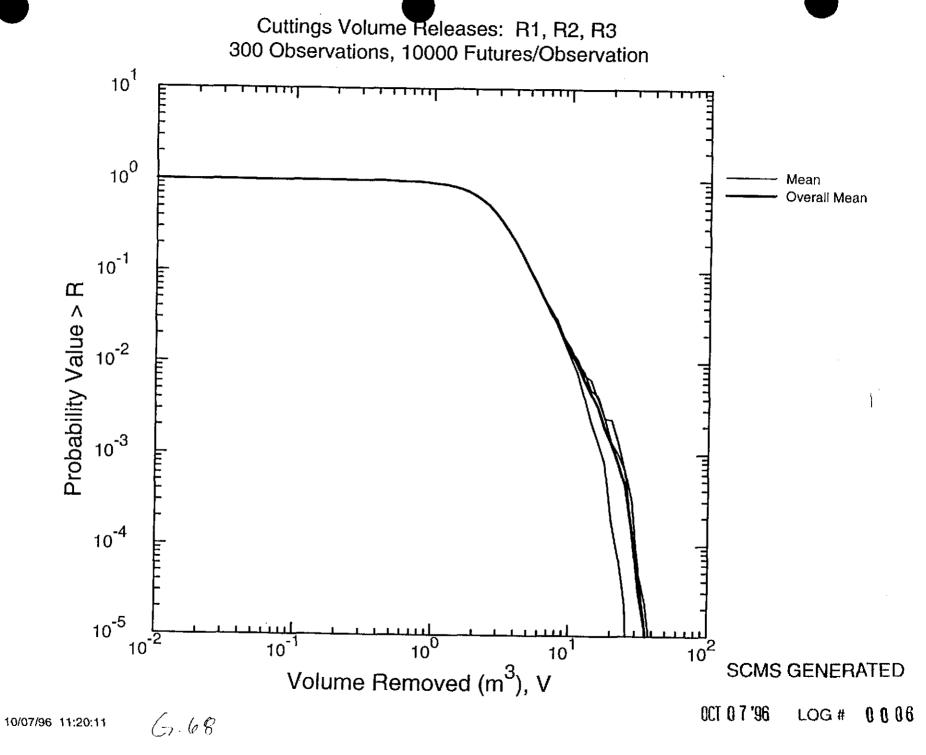
Spallings Normalized Releases: R1, R2, R3 300 Observations, 10000 Futures/Observation



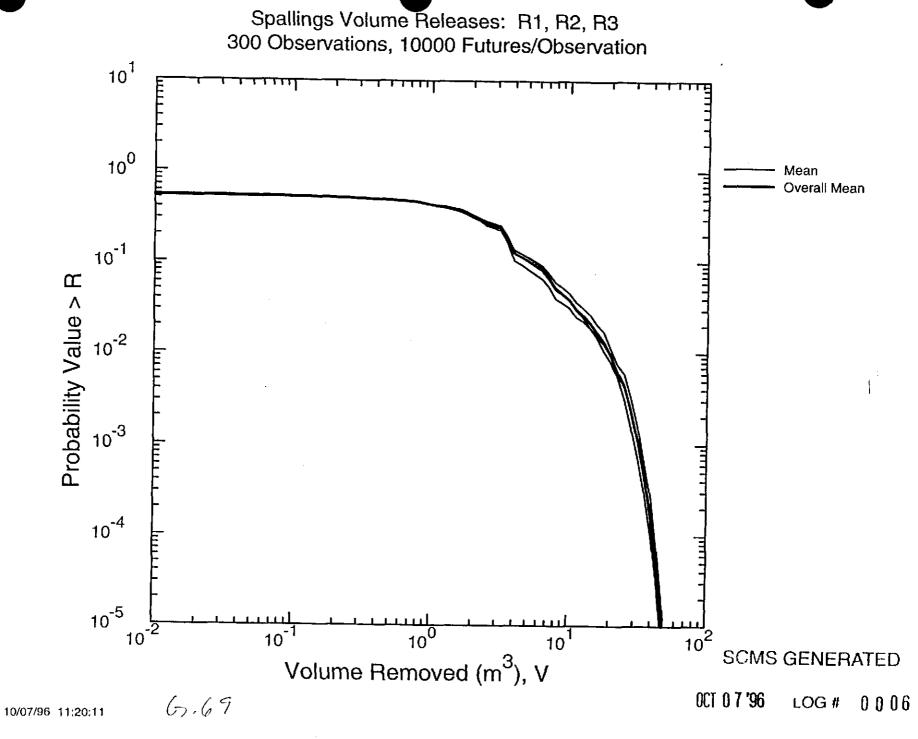
DBR t Normalized Releases: R1, R2, R3 300 Observations, 10000 Futures/Observation



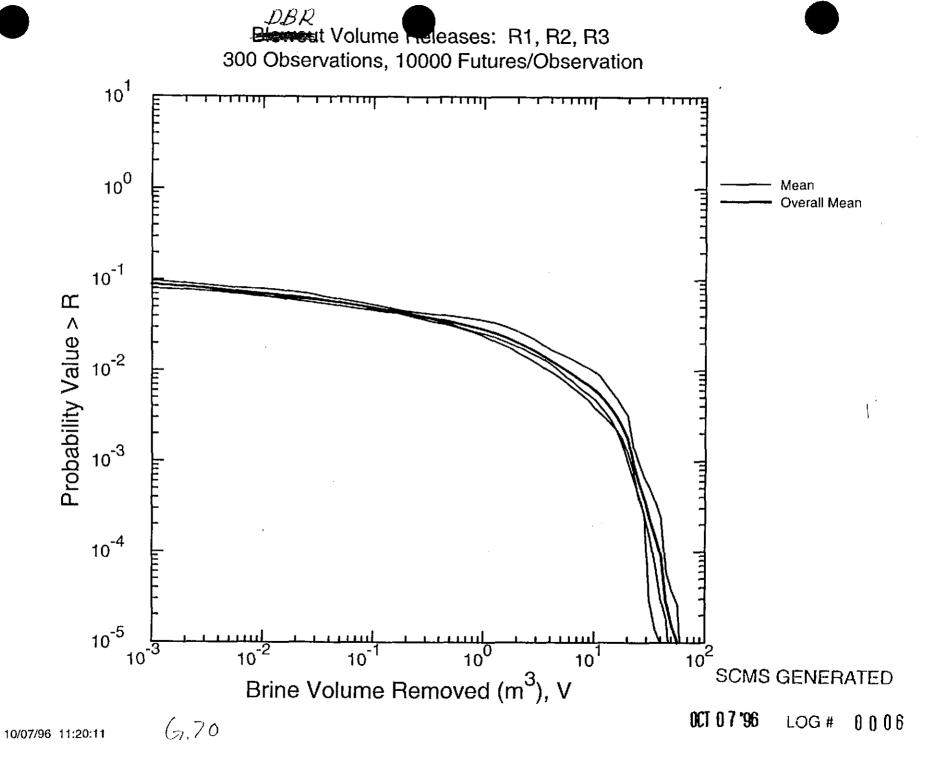
67.67 10/07/96 11:20:11



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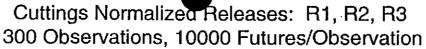


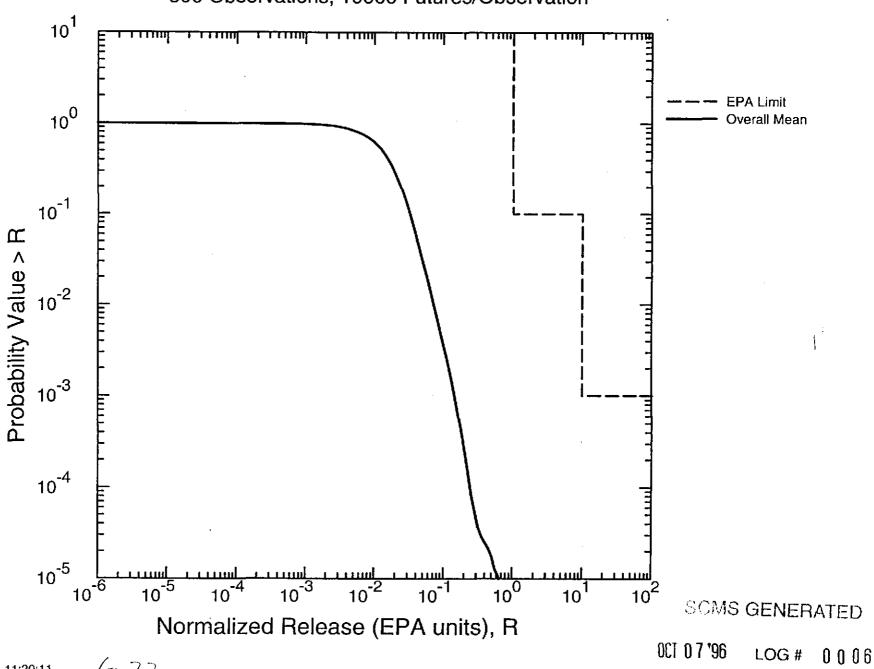
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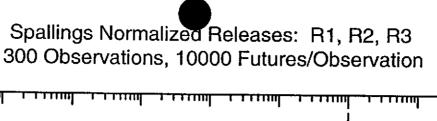


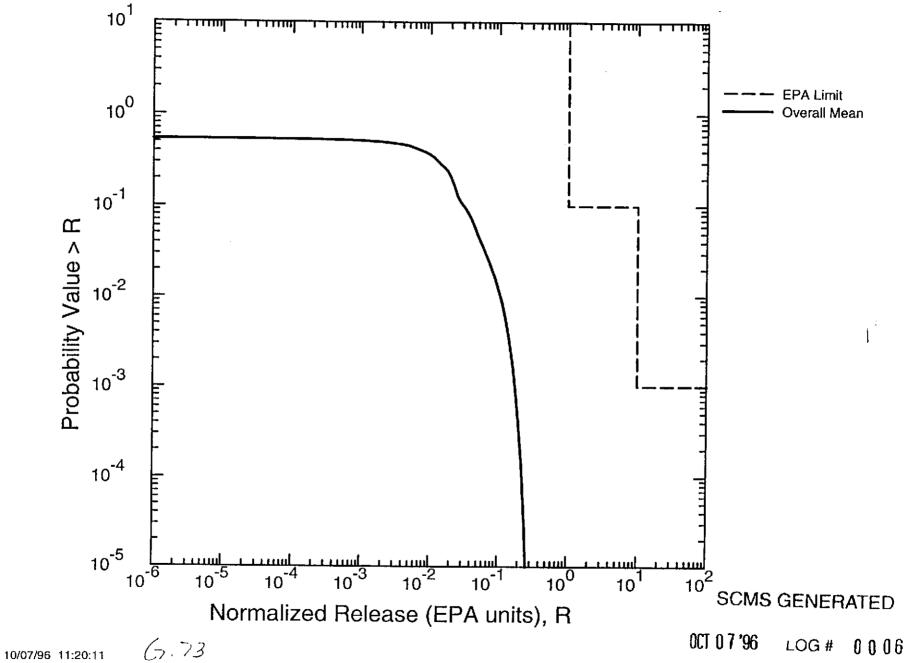
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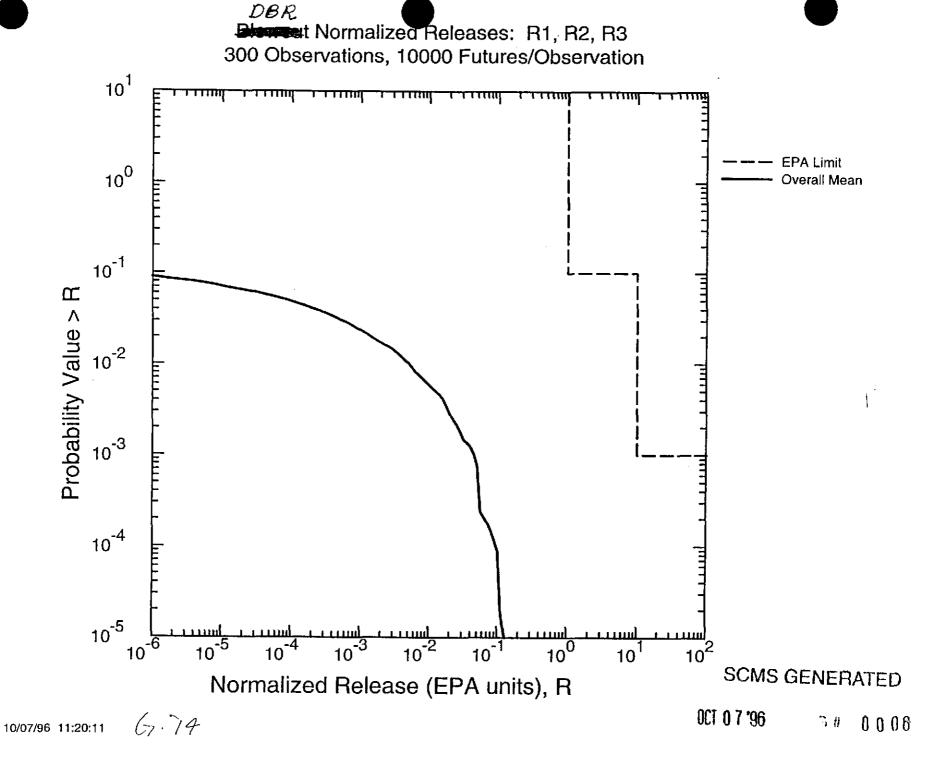
Total Normalized Releases: R1, R2, R3 300 Observations, 10000 Futures/Observation 10¹ **EPA** Limit 10⁰ Overall Mean 10⁻¹ Probability Value > R 10⁻⁴ 10⁻⁵ 10⁻⁶ 10⁻⁵ 10⁻³ 10² 101 SCMS GENERATED Normalized Release (EPA units), R 6.71 LOG# 0006 OCT 0 7 '96 10/07/96 11:20:11



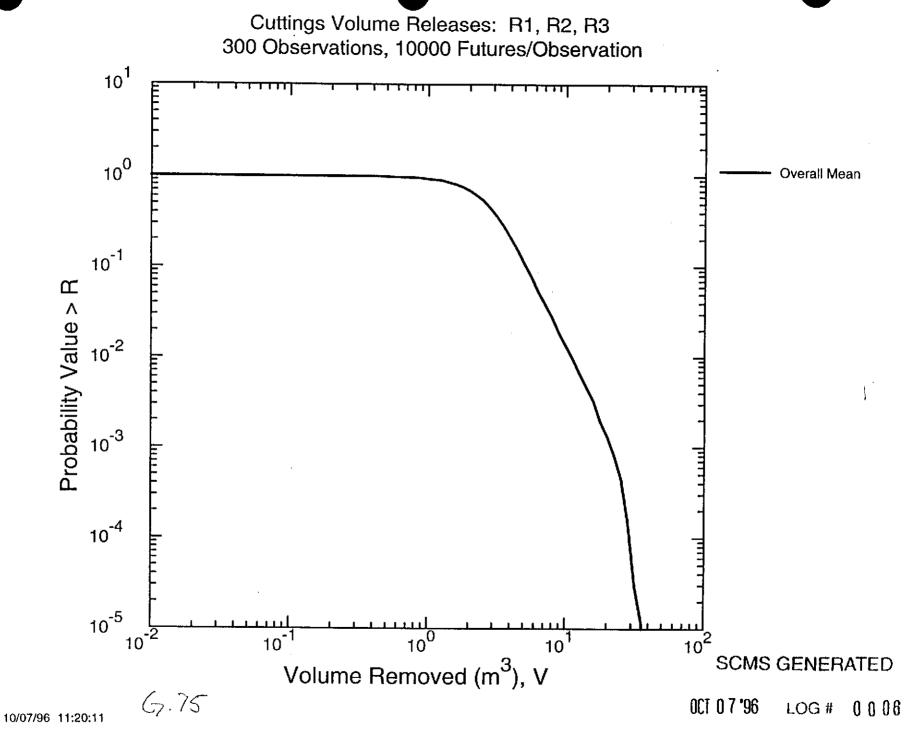




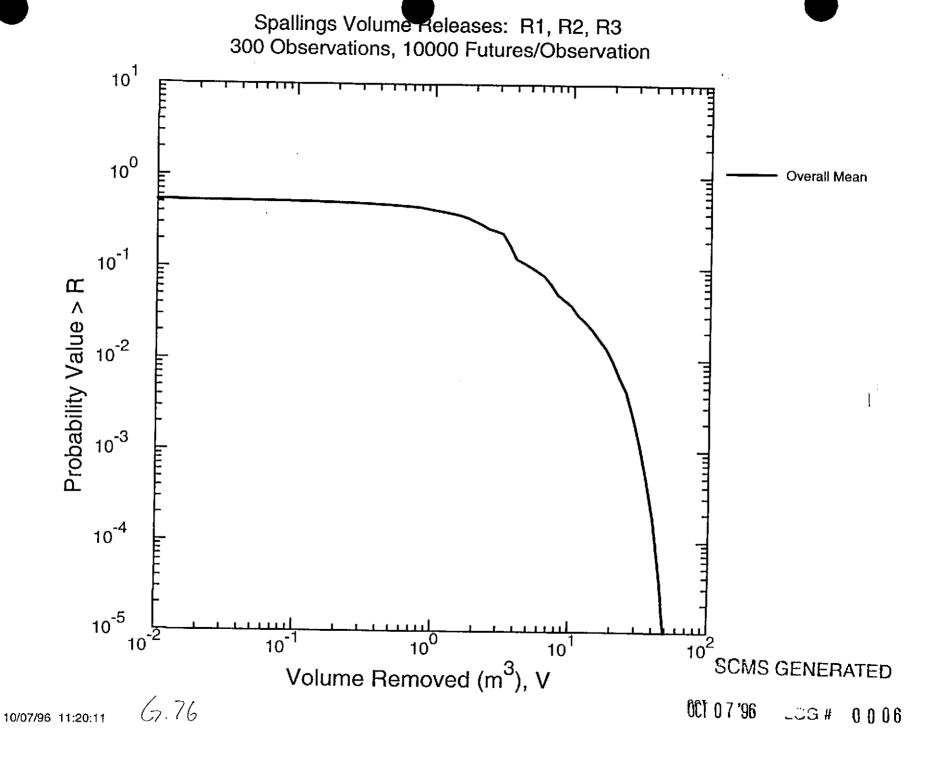




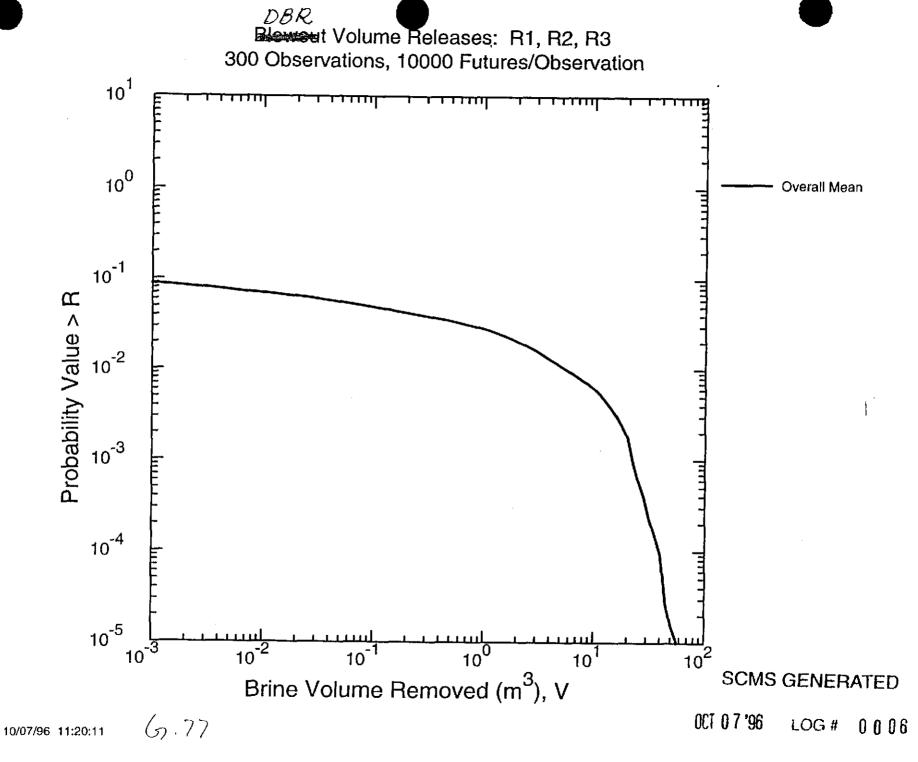
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APPENDIX H

CODE VERSIONS AND SOFTWARE PROBLEM REPORT (SPR) NUMBERS

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PA Verification Runs		Associated SPR's and Change Controls		
Code Name	Version	SPR No.	Code Version	Change Control
BRAGFLO	4.10	97-002	4.00, 4.01	5/12/97
		97-003	4.00, 4.01	(All SPR's
		97-007	4.00, 4.01	addressed by one
		97-008	4.00, 4.01	Change Control Form)
	. :	97-009	4.00, 4.01	
		97-010	4.00, 4.01	
NUTS	2.05	97-004	2.03	3/26/97 (2.03 to 2.04) 6/18/97 (2.04 to 2.05)
PANEL	3.60		 	(2.04 to 2.03)
SECOFL2D	3.03			
SECOTP2D	1.41	97-006	1.30, 1.31	6/9/97
		97-012.	1.30, 1.31	(All SPR's
		97-013	1.30, 1.31	addressed by one Change Control Form)
CUTTINGS_S	5.04			
SUMMARIZE	2.15	96-007	2.10	7/18/96
CCDGGF	3,00	97-005	2.01	5/20/97
CCDGSUM	2.00			

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